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# Polarization and coherence in the Hanbury Brown–Twiss effect

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## ABSTRACT

We study the correlation of intensity fluctuations in random electromagnetic beams, the so-called Hanbury Brown–Twiss effect (HBT). We show that not just the state of coherence of the source, but also its state of polarization has a strong influence on the far-zone correlations. Different types of sources are found to have different upper bounds for the normalized HBT coefficient.

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## 1. Introduction

In their landmark experiment, Hanbury Brown and Twiss studied the correlation of intensity fluctuations at two detectors with a variable separation distance, to determine the angular diameter of radio stars (1–3). Since then the eponymous Hanbury Brown–Twiss effect (HBT) has been applied in many other fields, such as nuclear physics (4) and atomic physics (5–7). In optics, it has been used to study certain inverse problems (8, 9), and to determine the mode index of vortex beams (10). It is also explored in classical versions of ghost imaging (11).

In the original astronomical studies that were carried out by Hanbury Brown and Twiss, polarization issues could be ignored, and therefore a scalar description sufficed (12, Ch. 7). A generalization to random electromagnetic beams, as generated for example, by multi-mode lasers, can be found in (13, Ch. 8). In recent years, several studies were dedicated to the correlation of intensity fluctuations in such beams, among them (14, 15), in which the degree of cross-polarization was introduced. The usefulness of this concept has been questioned in (16). The evolution of the HBT effect during propagation was studied in (17, 18).

In the present study, we examine the far-zone HBT effect that occurs in a wide class of partially coherent beams, the so-called Electromagnetic Gaussian Schell-Model (EGSM) beams (12). As we will demonstrate, not just the state of coherence of the source, but also its state

of polarization plays a major role. Also, different types of sources are found to have different upper bounds for the normalized HBT coefficient.

## 2. The HBT effect in random electromagnetic beams

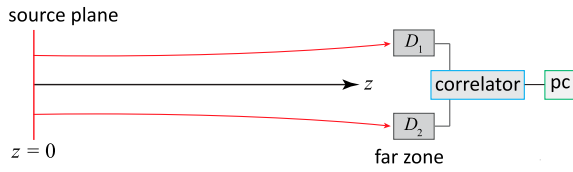
We consider a stochastic, wide-sense stationary, electromagnetic beam propagating close to the  $z$  axis into the half-space  $z > 0$  (see Figure 1). The vector  $\rho = (x, y)$  denotes a transverse position. To simplify the notation, we will from here on suppress the  $\omega$  dependence of the various quantities. In the space–frequency formulation of coherence theory, the coherence and polarization properties of a beam at two points  $\rho_1$  and  $\rho_2$  in the same transverse plane  $z$  can be described by its cross-spectral density (CSD) matrix (12)

$$\mathbf{W}(\rho_1, \rho_2, z) = \begin{pmatrix} W_{xx}(\rho_1, \rho_2, z) & W_{xy}(\rho_1, \rho_2, z) \\ W_{yx}(\rho_1, \rho_2, z) & W_{yy}(\rho_1, \rho_2, z) \end{pmatrix}, \quad (1)$$

with

$$W_{ij}(\rho_1, \rho_2, z) = \langle E_i^*(\rho_1, z) E_j(\rho_2, z) \rangle, \quad (i, j = x, y), \quad (2)$$

where the angled brackets denote an ensemble average. The intensity of a single realization of the beam is defined as



**Figure 1.** Illustrating the Hanbury Brown–Twiss experiment.  $D_1$  and  $D_2$  are intensity detectors, located in the far zone at  $(\rho_1, z)$  and  $(\rho_2, z)$ , whose output is sent to a correlator that is connected to a pc.

$$I(\rho, z) = |E_x(\rho, z)|^2 + |E_y(\rho, z)|^2, \quad (3)$$

whereas its expectation value

$$\begin{aligned} \langle I(\rho, z) \rangle &= \langle |E_x(\rho, z)|^2 \rangle + \langle |E_y(\rho, z)|^2 \rangle \\ &= \text{Tr } \mathbf{W}(\rho, \rho, z), \end{aligned} \quad (4)$$

where Tr denotes the trace. The intensity variation is given by the expression

$$\Delta I(\rho, z) = I(\rho, z) - \langle I(\rho, z) \rangle. \quad (6)$$

We can introduce a measure of the correlation of intensity fluctuations at two points by defining the HBT coefficient as

$$C(\rho_1, \rho_2, z) = \langle \Delta I(\rho_1, z) \Delta I(\rho_2, z) \rangle. \quad (7)$$

If the source fluctuations are governed by Gaussian statistics, one can use the Gaussian moment theorem to derive that (14, Equation (8))

$$C(\rho_1, \rho_2, z) = \sum_{ij} |W_{ij}(\rho_1, \rho_2, z)|^2. \quad (8)$$

It is convenient to use a normalized correlation coefficient, indicated by the subscript  $N$ , namely

$$C_N(\rho_1, \rho_2, z) = \frac{C_0(\rho_1, \rho_2, z)}{\langle I(\rho_1, z) \rangle \langle I(\rho_2, z) \rangle} \quad (9)$$

$$= \frac{\sum_{ij} |W_{ij}(\rho_1, \rho_2, z)|^2}{\text{Tr } \mathbf{W}(\rho_1, \rho_1, z) \text{Tr } \mathbf{W}(\rho_2, \rho_2, z)}. \quad (10)$$

It can be shown (16) that  $0 \leq C_N(\rho_1, \rho_2, z) \leq 1$ .

### 3. Electromagnetic Gaussian Schell-model beams

The cross-spectral density matrix elements of an EGSM beam in the source plane  $z = 0$  read

$$W_{ij}(\rho_1, \rho_2, 0)$$

$$= A_i A_j B_{ij} \exp \left[ -\frac{\rho_1^2}{4\sigma_i^2} - \frac{\rho_2^2}{4\sigma_j^2} - \frac{(\rho_1 - \rho_2)^2}{2\delta_{ij}^2} \right]. \quad (11)$$

The source parameters  $A_i, B_{ij}, \sigma_i$  and  $\delta_{ij}$  are independent of position, but may depend on frequency. For their physical meaning, we refer to (19, 20). We will restrict ourselves to the case where the width of the spectral densities associated with  $E_x$  and  $E_y$  are equal, i.e. we assume that  $\sigma_x = \sigma_y = \sigma$ . The parameters have to satisfy several constraints, i.e. (12, Sec. 9.4.2)

$$B_{xx} = B_{yy} = 1, \quad (12)$$

$$B_{xy} = B_{yx}^*, \quad (13)$$

$$|B_{xy}| \leq 1, \quad (14)$$

$$\delta_{xy} = \delta_{yx}. \quad (15)$$

Furthermore, the two conditions for the source to generate a beam-like field are (21)

$$\frac{1}{4\sigma^2} + \frac{1}{2\delta_{ii}^2} \ll \frac{2\pi^2}{\lambda^2}. \quad (16)$$

And finally, the non-negativeness of the cross-spectral density matrix implies that (22)

$$\sqrt{\frac{\delta_{xx}^2 + \delta_{yy}^2}{2}} \leq \delta_{xy} \leq \sqrt{\frac{\delta_{xx}\delta_{yy}}{|B_{xy}|}}. \quad (17)$$

After propagating a distance  $z$  through free space, the CSD matrix elements evolve into (see (12), where the one but last minus sign in Equation (10) on p. 184 should be a plus sign):

$$\begin{aligned} W_{ij}(\rho_1, \rho_2, z) &= \frac{A_i A_j B_{ij}}{\Delta_{ij}^2(z)} \exp \left[ -\frac{(\rho_1 + \rho_2)^2}{8\sigma^2 \Delta_{ij}^2(z)} \right] \\ &\times \exp \left[ -\frac{(\rho_1 - \rho_2)^2}{2\Omega_{ij}^2 \Delta_{ij}^2(z)} + \frac{ik(\rho_2^2 - \rho_1^2)}{2R_{ij}(z)} \right], \end{aligned} \quad (18)$$

where

$$\frac{1}{\Omega_{ij}^2} = \frac{1}{4\sigma^2} + \frac{1}{\delta_{ij}^2}, \quad (19)$$

$$\Delta_{ij}^2(z) = 1 + (z/\sigma k \Omega_{ij})^2, \quad (20)$$

$$R_{ij}(z) = [1 + (\sigma k \Omega_{ij}/z)^2]z, \quad (21)$$

and  $k = \omega/c$  is the wavenumber,  $c$  being the speed of light. Because we intend to study the HBT effect in the far zone of the source, we note for future use that

$$\lim_{z \rightarrow \infty} \Delta_{ij}^2(z) = \frac{z^2}{(\sigma k \Omega_{ij})^2}, \quad (22)$$

$$\lim_{z \rightarrow \infty} R_{ij}(z) = z. \quad (23)$$

We will apply Equations (18), (22) and (23) to beams that are generated by different types of sources.

#### 4. Unpolarized beams

For a rotationally symmetric, unpolarized source that generates an EGSM beam, we have that

$$A_x = A_y = A, \quad (24)$$

$$\delta_{xx} = \delta_{yy} = \delta, \quad (25)$$

$$B_{xy} = B_{yx} = 0, \quad (26)$$

$$\delta_{xy} = \delta_{yx} = 0. \quad (27)$$

The two non-zero matrix elements are equal, i.e.

$$W_{xx}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) = W_{yy}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) = W(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z), \quad (28)$$

with, in the far zone,

$$\begin{aligned} W(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) &= \left( \frac{Ak\sigma\Omega}{z} \right)^2 \exp \left[ -\frac{(\boldsymbol{\rho}_1 + \boldsymbol{\rho}_2)^2 k^2 \Omega^2}{8z^2} \right] \\ &\times \exp \left[ -\frac{(\boldsymbol{\rho}_2 - \boldsymbol{\rho}_1)^2 k^2 \sigma^2}{2z^2} \right] \\ &\times \exp \left( ik \frac{\rho_2^2 - \rho_1^2}{2z} \right), \end{aligned} \quad (29)$$

where

$$\frac{1}{\Omega^2} = \frac{1}{4\sigma^2} + \frac{1}{\delta^2}. \quad (30)$$

If we take the first reference point to be on the  $z$  axis ( $\boldsymbol{\rho}_1 = \mathbf{0}$ ), then it is seen from Equation (29) that  $W(\mathbf{0}, \boldsymbol{\rho}_2, z)$  is rotationally symmetric, i.e. it depends only on  $\rho_2 = |\boldsymbol{\rho}_2|$ . In the far-field, the polar angle  $\theta \approx \tan \theta = \rho_2/z$ . Hence, the matrix elements can be expressed as

$$\begin{aligned} W(\mathbf{0}, \theta, z) &= \left( \frac{Ak\sigma\Omega}{z} \right)^2 \exp \left( -\frac{\theta^2 k^2 \Omega^2}{8} \right) \\ &\times \exp \left( -\frac{\theta^2 k^2 \sigma^2}{2} \right) \exp \left( ik \frac{\theta^2 z}{2} \right). \end{aligned} \quad (31)$$

Using Equation (8), we obtain for the HBT coefficient the formula

$$\begin{aligned} C(\mathbf{0}, \theta, z) &= 2 \left( \frac{Ak\sigma\Omega}{z} \right)^4 \exp \left( -\frac{\theta^2 k^2 \Omega^2}{4} \right) \\ &\times \exp \left( -\theta^2 k^2 \sigma^2 \right). \end{aligned} \quad (32)$$

From Equations (32) and (10), one readily finds that the normalized HBT coefficient is given by the expression

$$C_N(\mathbf{0}, \theta) = \frac{1}{2} \exp \left( -\frac{\theta^2 k^2 \Omega^2}{4} \right) \exp \left( -\theta^2 k^2 \sigma^2 \right) \quad (33)$$

$$= \frac{1}{2} \exp \left( -\frac{4\theta^2 k^2 \sigma^4}{\delta^2 + 4\sigma^2} \right), \quad (34)$$

where the  $z$  dependence has dropped out. It is evident from Equation (34) that the far-zone HBT coefficient of an unpolarized, rotationally symmetric beam depends on both the effective source size  $\sigma$  and the correlation length  $\delta$ . Also, it is seen that this coefficient has an upper bound of  $1/2$ .

#### 5. Linearly polarized beams

Let us next consider a source that is linearly polarized along the  $x$  direction. We then have

$$A_x = A, \quad (35)$$

$$\delta_{xx} = \delta. \quad (36)$$

The only non-zero matrix element,  $W_{xx}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z)$ , takes on the far-zone form

$$\begin{aligned} W_{xx}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) &= \left( \frac{Ak\sigma\Omega}{z} \right)^2 \exp \left[ -\frac{(\boldsymbol{\rho}_1 + \boldsymbol{\rho}_2)^2 k^2 \Omega^2}{8z^2} \right] \\ &\times \exp \left[ -\frac{(\boldsymbol{\rho}_2 - \boldsymbol{\rho}_1)^2 k^2 \sigma^2}{2z^2} \right] \\ &\times \exp \left( ik \frac{\rho_2^2 - \rho_1^2}{2z} \right). \end{aligned} \quad (37)$$

As before, we take the first reference point,  $\boldsymbol{\rho}_1$ , to be on the  $z$  axis. Again expressing the relevant quantities in terms of the polar angle  $\theta$ , we obtain for the HBT coefficient the expression

$$\begin{aligned} C(\mathbf{0}, \theta, z) &= \left( \frac{Ak\sigma\Omega}{z} \right)^4 \exp \left( -\frac{\theta^2 k^2 \Omega^2}{4} \right) \\ &\times \exp \left( -\theta^2 k^2 \sigma^2 \right). \end{aligned} \quad (38)$$

Hence, its normalized version

$$C_N(\mathbf{0}, \theta) = \exp \left( -\frac{4\theta^2 k^2 \sigma^4}{\delta^2 + 4\sigma^2} \right). \quad (39)$$

It is seen that the far-zone HBT coefficient for a linearly polarized EGSM beam does not depend on the direction of polarization. Furthermore, it is twice as large as the coefficient for unpolarized light, as given by Equation (34), the upper bound now being unity.

## 6. Partially polarized beams

As a third example, we study a partially polarized, rotationally symmetric source. In that case,

$$A_x = A_y = A, \quad (40)$$

$$\delta_{xx} = \delta_{yy} = \delta. \quad (41)$$

It immediately follows that

$$\Omega_{xx} = \Omega_{yy} = \Omega \neq \Omega_{xy}, \quad (42)$$

$$\Delta_{xx} = \Delta_{yy} = \Delta \neq \Delta_{xy}. \quad (43)$$

The two inequalities follow from the fact that, in general,  $\delta_{xy} \neq \delta$ . For the four matrix elements, we now have the far-zone formulas

$$W_{xx}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) = W_{yy}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) \quad (44)$$

$$\begin{aligned} &= \left(\frac{Ak\sigma\Omega}{z}\right)^2 \exp\left[-\frac{(\boldsymbol{\rho}_1 + \boldsymbol{\rho}_2)^2 k^2 \Omega^2}{8z^2}\right] \\ &\quad \times \exp\left[-\frac{(\boldsymbol{\rho}_2 - \boldsymbol{\rho}_1)^2 k^2 \sigma^2}{2z^2}\right] \\ &\quad \times \exp\left(ik\frac{\rho_2^2 - \rho_1^2}{2z}\right), \end{aligned} \quad (45)$$

$$\begin{aligned} W_{xy}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) &= B_{xy} \left(\frac{Ak\sigma\Omega_{xy}}{z}\right)^2 \\ &\quad \times \exp\left[-\frac{(\boldsymbol{\rho}_1 + \boldsymbol{\rho}_2)^2 k^2 \Omega_{xy}^2}{8z^2}\right] \\ &\quad \times \exp\left[-\frac{(\boldsymbol{\rho}_2 - \boldsymbol{\rho}_1)^2 k^2 \sigma^2}{2z^2}\right] \\ &\quad \times \exp\left(ik\frac{\rho_2^2 - \rho_1^2}{2z}\right), \end{aligned} \quad (46)$$

$$\begin{aligned} W_{yx}(\boldsymbol{\rho}_1, \boldsymbol{\rho}_2, z) &= B_{xy}^* \left(\frac{Ak\sigma\Omega_{xy}}{z}\right)^2 \\ &\quad \times \exp\left[-\frac{(\boldsymbol{\rho}_1 + \boldsymbol{\rho}_2)^2 k^2 \Omega_{xy}^2}{8z^2}\right] \\ &\quad \times \exp\left[-\frac{(\boldsymbol{\rho}_2 - \boldsymbol{\rho}_1)^2 k^2 \sigma^2}{2z^2}\right] \\ &\quad \times \exp\left(ik\frac{\rho_2^2 - \rho_1^2}{2z}\right), \end{aligned} \quad (47)$$

where in the last expression we made use of the fact that  $B_{yx} = B_{xy}^*$  and  $\Omega_{yx} = \Omega_{xy}$ . Taking the first reference point  $\boldsymbol{\rho}_1$  on axis and expressing the relevant quantities in terms of the angle  $\theta$ , we thus find for the HBT coefficient the formula

$$\begin{aligned} C(\mathbf{0}, \theta, z) &= 2 \left(\frac{Ak\sigma}{z}\right)^4 \exp(-\theta^2 k^2 \sigma^2) \\ &\quad \times \left[ \Omega^4 \exp\left(-\frac{\theta^2 k^2 \Omega^2}{4}\right) \right. \\ &\quad \left. + |B_{xy}|^2 \Omega_{xy}^4 \exp\left(-\frac{\theta^2 k^2 \Omega_{xy}^2}{4}\right) \right]. \end{aligned} \quad (48)$$

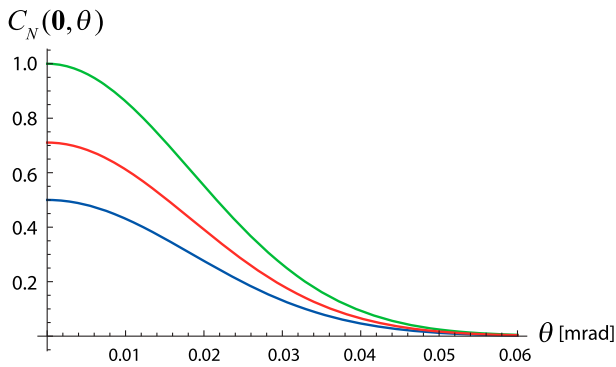
A straightforward calculation then yields the equations

$$\begin{aligned} C_N(\mathbf{0}, \theta) &= \frac{1}{2} \exp\left[-\theta^2 k^2 \left(\sigma^2 - \frac{\Omega^2}{2}\right)\right] \\ &\quad \times \left\{ \exp\left[-\left(\frac{\theta k \Omega}{2}\right)^2\right] \right. \\ &\quad \left. + \left(\frac{\Omega_{xy}}{\Omega}\right)^4 |B_{xy}|^2 \exp\left[-\left(\frac{\theta k \Omega_{xy}}{2}\right)^2\right] \right\} \end{aligned} \quad (49)$$

$$\begin{aligned} &= \frac{1}{2} \exp\left(-\frac{4\theta^2 k^2 \sigma^4}{\delta^2 + 4\sigma^2}\right) \\ &\quad \times \left\{ 1 + |B_{xy}|^2 \left(\frac{\Omega_{xy}}{\Omega}\right)^4 \right. \\ &\quad \left. \times \exp\left[-\frac{\theta^2 k^2 (\Omega_{xy}^2 - \Omega^2)}{4}\right] \right\}. \end{aligned} \quad (50)$$

Equation (50) shows that the normalized far-zone HBT coefficient of a rotationally symmetric, partially polarized source depends on its effective size  $\sigma$ , the two coherence lengths  $\delta$  and  $\delta_{xy}$ , and the parameter  $B_{xy}$ . Compared to the unpolarized case, given by Equation (34), the coefficient is now larger, due to the presence of the factor between curly brackets that is always greater than unity. The upper bound now exceeds 1/2 due to the fact that  $|B_{xy}| > 0$  for partially polarized sources. Clearly, a non-zero correlation between the two Cartesian components of the electric field in the source plane increases the correlation of the intensity fluctuations in the far zone. It is worth pointing out that the constraint expressed by (17) defines an upper limit for the value of  $|B_{xy}|$ .

We illustrate our results in Figure 2 in which the far-zone normalized HBT coefficient is plotted for three different kinds of EGSM sources, i.e. an unpolarized source, a linearly polarized source and a partially polarized source. The coefficient for the linearly polarized case is the only one with a unit upper bound, and its value always exceeds that of the other cases. The partially coherent source produces an HBT coefficient that, at all observation angles, is larger than that of its unpolarized counterpart.



**Figure 2.** The normalized far-zone Hanbury Brown–Twiss coefficient for three EGSM sources with different states of polarization: linearly polarized (green curve), partially polarized (red curve) and unpolarized (blue curve). In these examples, the parameters are:  $\lambda = 632.8$  nm,  $\sigma = 4$  mm,  $\delta = 2$  mm,  $\delta_{xy} = 2.3$  mm and  $B_{xy} = 0.5$ .

## 7. Conclusions

We have examined the Hanbury Brown–Twiss effect that occurs in random beams generated by electromagnetic Gaussian Schell-model sources. Expressions for the normalized far-zone HBT coefficient were derived in terms of the source parameters. This coefficient was shown to have an upper limit that depends on the state of coherence and polarization in the source plane. Our results show that the far-zone HBT effect coefficient can be used to obtain properties of the source.

## Disclosure statement

No potential conflict of interest was reported by the authors.

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