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Layered water in crystal interfaces as source for bone viscoelasticity: arguments from a multiscale approach

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Extracellular bone material can be characterised as a nanocomposite where, in a liquid environment, nanometre-sized hydroxyapatite crystals precipitate within as well as between long fibre-like collagen fibrils (with diameters in the 100 nm range), as evidenced from neutron diffraction and transmission electron microscopy. Accordingly, these crystals are referred to as ‘interfibrillar mineral’ and ‘extrafibrillar mineral’, respectively. From a topological viewpoint, it is probable that the mineralisations start on the surfaces of the collagen fibrils (‘mineral-encrusted fibrils’), from where the crystals grow both into the fibril and into the extrafibrillar space. Since the mineral concentration depends on the pore spaces within the fibrils and between the fibrils (there is more space between them), the majority of the crystals (but clearly not all of them) typically lie in the extrafibrillar space. There, larger crystal agglomerations or clusters, spanning tens to hundreds of nanometers, develop in the course of mineralisation, and the micromechanics community has identified the pivotal role, which this extrafibrillar mineral plays for tissue elasticity. In such extrafibrillar crystal agglomerates, single crystals are stuck together, their surfaces being covered with very thin water layers. Recently, the latter have caught our interest regarding strength properties (Fritsch et al. 2009 *J Theor Biol.* 260(2): 230–252) – we have identified these water layers as weak interfaces in the extrafibrillar mineral of bone. Rate-independent gliding effects of crystals along the aforementioned interfaces, once an elastic threshold is surpassed, can be related to overall elastoplastic material behaviour of the hierarchical material ‘bone’. Extending this idea, the present paper is devoted to viscous gliding along these interfaces, expressing itself, at the macroscale, in the well-known experimentally evidenced phenomenon of bone viscoelasticity. In this context, a multiscale homogenisation scheme is extended to viscoelasticity, mineral-cluster-specific creep parameters are identified from three-point bending tests on hydrated bone samples, and the model is validated by statistically and physically independent experiments on partially dried samples. We expect this model to be relevant when it comes to prediction of time-dependent phenomena, e.g. in the context of bone remodelling.

Keywords: viscoelasticity; bone; multiscale; creep; relaxation; gliding event

1. Introduction

‘Bone’ relates to the key load-carrying material in vertebrates: it is produced and resorbed by tens-of-micrometres-sized biological cells (osteocytes, osteoblasts, osteoclasts and their precursors; Buckwalter et al. 1995a, 1995b; Erlebacher et al. 1995; Filvaroff and Derynck 1998; Bonucci 2009), but, as such, does not belong to them – rather, at a scale of tens of micrometres, ‘bone’ appears as extracellular material. This material can be characterised as a nanocomposite where, in a liquid environment, nanometre-sized hydroxyapatite crystals precipitate within as well as between long, fibre-like collagen fibrils (with diameters in the 100 nm range), as evidenced from neutron diffraction (Lees et al. 1984; Bonar et al. 1985; Lees 1987) and transmission electron microscopy (Lees and Probst 1988; Arsenault et al. 1991; Lees et al. 1994; Probst and Lees 1996). Accordingly, these crystals are referred to as ‘intrafibrillar mineral’ and ‘extrafibrillar mineral’, respectively. The latter needs to be dissolved or rinsed off, as to see the collagen fibrils in atomic force microscopy (Lees et al.

1994; Sasaki et al. 2002; Hassenkam et al. 2004; Bozec et al. 2005; Hassenkam et al. 2005). From a topological viewpoint, it is probable that the mineralisation starts on the surfaces of the collagen fibrils (‘mineral-encrusted fibrils’), from where the crystals grow both into the fibril and into the extrafibrillar space (Höhling 1967; Landis et al. 1996; Sasaki et al. 2002; Wiesmann et al. 2005). Since the mineral concentration depends on the pore spaces within the fibrils and between the fibrils (there is more space between them), the majority of the crystals (but clearly not all of them) typically lies in the extrafibrillar space (Lees 1987; Hellmich and Ulm 2001; Sasaki et al. 2002). There, larger crystal agglomerations or clusters (Su et al. 2003), spanning tens to hundreds of nanometres, develop in the course of mineralisation, and the micromechanics community has identified the pivotal role, which this extrafibrillar mineral plays for tissue elasticity (Crolet et al. 1993; Aoubiza et al. 1996; Pidaparti et al. 1996; Hellmich and Ulm 2002a, 2002b, 2005a, 2005b; Hellmich et al. 2004a; Hellmich et al. 2004b; Fritsch and Hellmich 2007; Nikolov and Raabe

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2008; Hamed et al. 2010; Martinez-Reina et al. 2010; Reisinger et al. 2010; Sansalone et al. 2010). In such extrafibrillar crystal agglomerates, single crystals are stuck together, their surfaces being covered with very thin water layers (Zahn and Hochrein 2003; deLeeuw 2004; Bhowmik et al. 2007; Astala and Stott 2008; Bhowmik et al. 2009; Corno et al. 2009). These layers exhibit a mass density, which is higher than that of standard liquid water, they are made of structured ‘ice-like’ water (Pan et al. 2007).

Recently, we have identified these water layers as weak interfaces in the extrafibrillar mineral of bone (Fritsch et al. 2009). In this line, rate-independent gliding effects of crystals along the aforementioned interfaces, once an elastic threshold is surpassed, can be related to overall elastoplastic material behaviour of the hierarchical material ‘bone’. Extending this idea, the present paper is devoted to viscous gliding along these interfaces, expressing itself, at the macroscale, in the well-known experimentally evidenced phenomenon of bone viscoelasticity. Based on both experimental and computational studies, the idea that water layers at water–mineral interfaces are the source of material creep is widely accepted in geophysics (see, e.g. Morrow et al. (2000) for a multitude of gouge minerals, Stipp et al. (2006) for quartzite or Tullis and Yund (1991) for albite rock), as well as in cement and concrete research (Kalinichev et al. 2007; Alizadeh et al. 2010). In cement pastes, the micro- and nanostructures of calcium silicate hydrates exhibit length dimensions similar to those found in the extrafibrillar polycrystals of bone. However, the precise local physicochemistry of water in very crowded biological or chemical environments with a characteristic length of nanometres seems to be still a matter of discussion: the slowdown of the orientational dynamics of the water molecules may be due to confined length scales or interface interactions (Moilanen et al. 2009).

The remainder of the paper is organised as follows: first, we extend the multistep homogenisation scheme of Fritsch et al. (Fritsch and Hellmich 2007; Fritsch et al. 2009) from elasticity to viscoelasticity (Section 2). Then we will first discuss experiments used for viscoelastic parameter identification (Section 3), followed by statistically and physically independent experiments used for model validation (Section 4). Finally, we will discuss composition-dependent creep behaviour of bone (Section 5), before concluding the paper (Section 6).

2. Multiscale homogenisation theory for bone viscoelasticity

2.1 Fundamentals of continuum micromechanics (random homogenisation theory) – separation of scales

Continuum micromechanics (Hill 1963, 1965; Suquet 1997; Zaoui 1997, 2002; Scheiner and Hellmich 2009) is

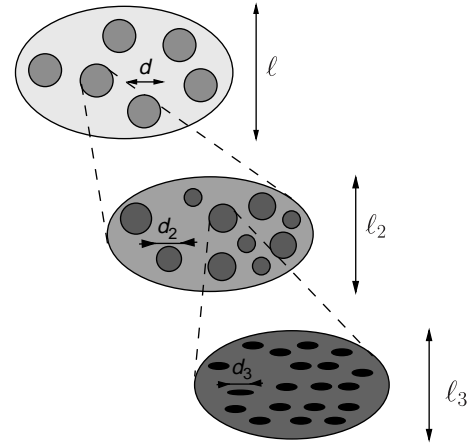


Figure 1. Multistep homogenisation (Fritsch and Hellmich 2007).

based on the idea that a material is a microheterogeneous body filling a macrohomogeneous representative volume element (RVE) with characteristic length ℓ , $\ell \gg d$, where d stands for the characteristic length of the inhomogeneities within the RVE (see Figure 1), and $\ell \ll \mathcal{L}$, where \mathcal{L} is the characteristic lengths of geometry or loading of a structure built up by the material defined on the RVE. Quasi-homogeneous subdomains, the so-called material phases (Suquet 1997; Zaoui 1997, 2002), with known physical properties, e.g. volume fractions or elastic/viscoelastic properties, are reasonably chosen, as to describe the complicated microstructure within an RVE as simply as possible, but not simpler than that. The elastic/viscoelastic behaviour of these inhomogeneities within the RVE (material phases), as well as the volume fractions, their characteristic shapes and their interactions, are used to estimate the correlation between homogeneous deformations acting on the boundary of the RVE and resulting (average) stresses, in other words, to estimate the homogenised mechanical behaviour of the overall material.

If a single phase has a heterogeneous microstructure itself, RVEs can be introduced within this phase in order to estimate its mechanical behaviour. These RVEs have dimensions, which fulfil $\ell_2 \leq d$, and imply again smaller inhomogeneities with characteristic length $d_2 \ll \ell_2$, and so on (see Figure 1). Such an approach is referred to as multistep homogenisation and should, in the end, provide access to ‘universal’ phase properties at sufficiently low observation scales. For bone, we employ here a six-step homogenisation scheme (see Figure 2).

2.2 Viscoelastic homogenisation of extrafibrillar space (porous hydroxyapatite polycrystal)

2.2.1 Micromechanical representation

An RVE \hat{V}_{ef} of hydroxyapatite foam (see Figure 2(c)) has a characteristic length between 100 and 500 nm. It is built up by

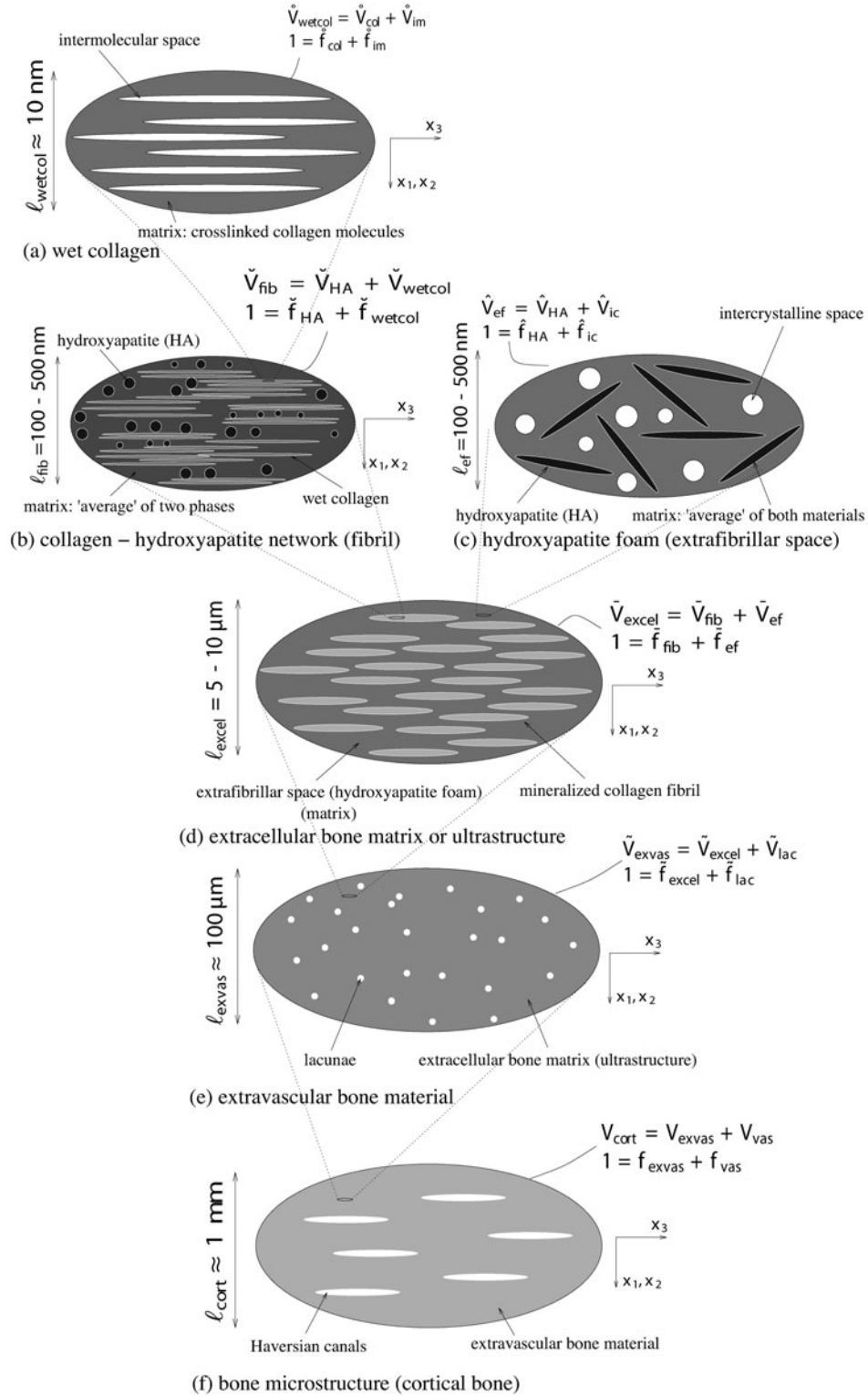


Figure 2. Micromechanical representation of bone material by means of a six-step homogenization scheme (Fritsch et al. 2009).

hydroxyapatite needles,¹ being oriented in all directions (labelled by suffix 'HA'), and spherical, water-filled pores, called intercrystalline space (labelled by suffix 'ic'). Homogeneous ('macroscopic') time-dependent strains

$\mathbf{E}_{\text{ef}}(t)$ are imposed, in terms of displacements $\xi(\mathbf{x}, t)$, at the boundary of the RVE_{ef}, $\partial \hat{V}_{\text{ef}}$, through

$$\forall \mathbf{x} \in \partial \hat{V}_{\text{ef}} : \xi(\mathbf{x}, t) = \mathbf{E}_{\text{ef}}(t) \cdot \mathbf{x}, \quad (1)$$

where \mathbf{x} is the position vector inside and at the boundary of the RVE_{ef}, and t is the time variable. These macroscopic strains are identical to the spatial average of the resulting kinematically compatible ('microscopic') strain field $\boldsymbol{\varepsilon}(\mathbf{x}, t)$ across the volume of the RVE (Zaoui 2002). In our case, this reads as

$$\mathbf{E}_{\text{ef}}(t) = \frac{1}{\hat{V}_{\text{ef}}} \int_{\hat{V}_{\text{ef}}} \boldsymbol{\varepsilon}(\mathbf{x}, t) dV = \phi \boldsymbol{\varepsilon}_{\text{ic}}(t) + (1 - \phi) \int_{\varphi=0}^{2\pi} \int_{\vartheta=0}^{\pi} \boldsymbol{\varepsilon}_{\text{HA}}(\varphi, \vartheta; t) \frac{\sin \vartheta d\varphi d\vartheta}{4\pi}, \quad (2)$$

where $r \in [\text{HA}, \text{ic}]$ and \hat{V}_{ef} are the volume of the RVE_{ef}, porosity ϕ is the volume fraction of the intercrystalline space, $\boldsymbol{\varepsilon}_{\text{ic}}$ refers to the spatial average of microstrains over this porosity, and $\boldsymbol{\varepsilon}_{\text{HA}}(\varphi, \vartheta; t)$ are the average strains in the needle-shaped hydroxyapatite phase oriented in (φ, ϑ) -direction, see Figure 3.

Analogously, homogeneous macroscopic stresses $\boldsymbol{\Sigma}_{\text{ef}}(t)$ are identical to the spatial average of equilibrated microstresses $\boldsymbol{\sigma}(\mathbf{x}, t)$ across the RVE,

$$\begin{aligned} \boldsymbol{\Sigma}_{\text{ef}}(t) &= \frac{1}{\hat{V}_{\text{ef}}} \int_{\hat{V}_{\text{ef}}} \boldsymbol{\sigma}(t) dV \\ &= \phi \boldsymbol{\sigma}_{\text{ic}}(t) + (1 - \phi) \int_{\varphi=0}^{2\pi} \int_{\vartheta=0}^{\pi} \boldsymbol{\sigma}_{\text{HA}}(\varphi, \vartheta; t) \\ &\quad \times \frac{\sin \vartheta d\varphi d\vartheta}{4\pi}, \end{aligned} \quad (3)$$

where $\boldsymbol{\sigma}_{\text{HA}}(\varphi, \vartheta; t)$ is the average stresses in the needle-shaped hydroxyapatite phase oriented in (φ, ϑ) -direction, see Figure 3.

2.2.2 Viscoelasticity of material phases

Considering viscous interfaces of layered water² within the extrafibrillar clusters of hydroxyapatite, as stated in the Introduction section, we assign linear viscoelastic

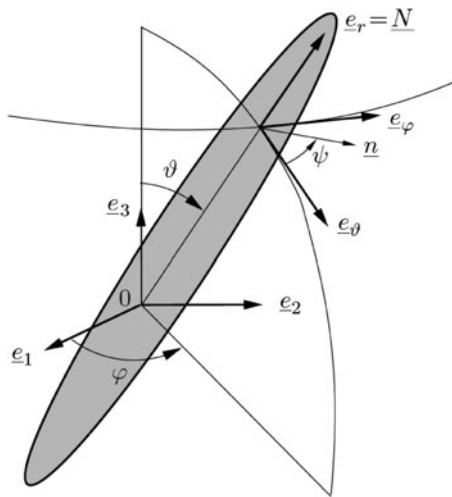


Figure 3. Cylindrical HA-inclusion (Fritsch et al. 2009).

behaviour to all needle-shaped phases in RVE_{ef}, according to

$$\boldsymbol{\sigma}_{\text{HA}}(t) = \int_{-\infty}^t \mathbf{r}_{\text{HA}}(t - \tau) : \dot{\boldsymbol{\varepsilon}}_{\text{HA}}(\tau) d\tau = [\mathbf{r}_{\text{HA}} * \boldsymbol{\varepsilon}_{\text{HA}}](t), \quad (4)$$

where $\dot{\boldsymbol{\varepsilon}}_{\text{HA}}$ denotes the temporal derivative of the strain tensor of the hydroxyapatite needles, $\mathbf{r}_{\text{HA}}(t - \tau)$ is the fourth-order tensorial relaxation function, τ is the integration variable related to the time instant when $\dot{\boldsymbol{\varepsilon}}_{\text{HA}}$ was imposed onto the needles, and $*$ represents the Stieltjes convolution operator. Thereby, $\mathbf{r}_{\text{HA}}(t = \tau)$ refers to instantaneous elasticity, while $\mathbf{r}_{\text{HA}}(t > \tau)$ refers to viscoelastic deformations. The special case of $\mathbf{r}_{\text{HA}} = \text{constant}$ ($\partial \mathbf{r}_{\text{HA}} / \partial t = 0$) refers to pure elasticity, i.e. $\mathbf{r}_{\text{HA}} = \mathbf{c}_{\text{HA}}$, where \mathbf{c}_{HA} is the fourth-order elastic stiffness tensor of hydroxyapatite. For the subsequent developments, it is convenient to represent Equation (4) in the Laplace–Carson (LC) domain defined through ‘frequency’ variable p , with the LC transformation given as (Donolato 2002)

$$f^*(p) = \mathcal{C}\{f(t)\} = p\hat{f}(p) = p \int_0^{\infty} f(t) e^{-pt} dt, \quad (5)$$

where $f^*(p)$ is the LC transform of the time-dependent function $f(t)$, and $\hat{f}(p)$ is the Laplace transform of $f(t)$. Namely, the insertion of Equation (4) into (5) yields an algebraic equation in the LC domain, given as

$$\boldsymbol{\sigma}_{\text{HA}}^*(p) = \mathbf{r}_{\text{HA}}^*(p) : \boldsymbol{\varepsilon}_{\text{HA}}^*(p). \quad (6)$$

Given the disordered arrangement of needle-shaped phases, it is sufficient (Fritsch et al. 2006) to assign isotropic phase properties to them, so that their relaxation tensor reads as

$$\mathbf{r}_{\text{HA}}^*(p) = 3k_{\text{HA}}^*(p) \mathbf{I}_{\text{vol}} + 2\mu_{\text{HA}}^*(p) \mathbf{I}_{\text{dev}}. \quad (7)$$

In Equation (7), \mathbf{I}_{vol} is the volumetric part of the fourth-order unit tensor \mathbf{I} , $I_{\text{vol},ijkl} = 1/3 \delta_{ij} \delta_{kl}$, with Kronecker delta δ_{ij} ($\delta_{ij} = 1$ if $i = j$, and $\delta_{ij} = 0$ if $i \neq j$), while \mathbf{I}_{dev} is the deviatoric part of \mathbf{I} , $\mathbf{I}_{\text{dev}} = \mathbf{I} - \mathbf{I}_{\text{vol}}$; the components of \mathbf{I} are defined as $I_{ijkl} = 1/2(\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk})$. Note that the bulk modulus of hydroxyapatite is independent of p , and hence identical to the elastic bulk modulus of hydroxyapatite (see Table 1), $k_{\text{HA}}^*(p) \equiv k_{\text{HA}}$, since gliding along interfaces does not result in any volume changes [compare also Fritsch et al. (2007) for a micromechanical development related to this statement]. For μ_{HA} , we here adopt, as a first approximation, the well-known Burgers model (TerHaar 1950; Vandamme and Ulm 2006)

$$\mu_{\text{HA}}^*(p) = \left(\frac{1}{\mu_{\text{HA,inst}}} + \frac{1}{\mu_{\text{HA,KV}} + p\eta_{\text{HA,KV}}} + \frac{1}{p\eta_{\text{HA,M}}} \right)^{-1}, \quad (8)$$

where $\mu_{\text{HA,inst}}$ is the elastic shear modulus of hydroxyapatite (see Table 1) and μ_{KV} , η_{KV} and η_{M} are the creep parameters of the Kelvin-Voigt and the Maxwell type, respectively. Identification of tissue-independent creep properties of water layer-penetrated hydroxyapatite clusters is the very focus of

Table 1. Phase stiffness values of the elementary components of bone.

Phase	Bulk modulus k [GPa]	Shear modulus μ [GPa]	Experimental source
Hydroxyapatite Water containing Non-collagenous Organics or osteocytes	$k_{\text{HA}} = 82.6$ $k_{\text{H}_2\text{O}} = 2.3$	$\mu_{\text{HA}} = 44.9$ $\mu_{\text{H}_2\text{O}} = 0$	(Katz and Ukraincik 1971)
	c_{ijkl} [GPa]	c_{ijkl} [GPa]	
(Molecular) collagen	$c_{\text{col},3333} = 17.9$ $c_{\text{col},1111} = 11.7$	$c_{\text{col},1133} = 7.1$ $c_{\text{col},1122} = 5.1$ $c_{\text{col},1313} = 3.3$	(Cusack and Miller 1979)

the present paper. However, since direct experimental determination seems to be out of reach for the moment, we will back-analyse them from creep tests on macroscopic bone samples in Section 3. Therefore, we need to proceed with the homogenisation of creep behaviour defined by Equations (7) and (8), up to the macroscopic level, as described below.

2.2.3 Homogenised viscoelastic behaviour of extrafibrillar space

Constitutive Equation (6) is formally identical to linear elasticity, so that the superposition principle is valid in the LC domain, i.e. the LC-transformed macroscopic strain $\mathbf{E}_{\text{HA}}^*(p)$ is proportional to the LC-transformed microscopic strains in the needle-shaped hydroxyapatite phases,

$$\boldsymbol{\varepsilon}_{\text{HA}}^*(\varphi, \vartheta; p) = \mathbf{A}_{\text{HA}}^*(\varphi, \vartheta; p) : \mathbf{E}_{\text{ef}}^*(p), \quad (9)$$

and to the (average) microscopic strains in the intercrystalline pores

$$\boldsymbol{\varepsilon}_{\text{ic}}^*(p) = \mathbf{A}_{\text{ic}}^*(p) : \mathbf{E}_{\text{ef}}^*(p), \quad (10)$$

where $\mathbf{A}_{\text{HA}}^*(\varphi, \vartheta; p)$ denotes the LC-transformed fourth-order strain concentration tensor of the (φ, ϑ) -oriented hydroxyapatite phase and $\mathbf{A}_{\text{ic}}^*(p)$ refers to the concentration tensor of the intercrystalline space. Equation (9) expresses the viscoelastic correspondence principle (Read 1950; Sips 1951; Laws and McLaughlin 1978; Beurthey and Zaoui 2000). Insertion of Equation (9) into the LC-transformed constitutive relation Equation (6), and averaging over all phases according to Equation (3) yields

$$\begin{aligned} \boldsymbol{\Sigma}_{\text{ef}}^*(p) = & \left[\phi \mathbf{c}_{\text{H}_2\text{O}} : \mathbf{A}_{\text{ic}}(p) + (1 - \phi) \int_{\varphi=0}^{2\pi} \int_{\vartheta=0}^{\pi} \mathbf{r}_{\text{HA}}(p) : \mathbf{A}_{\text{HA}}(\varphi, \vartheta; p) \right. \\ & \left. \times \frac{\sin \vartheta d\vartheta d\varphi}{4\pi} \right] : \mathbf{E}_{\text{ef}}^*(p) = \mathbf{R}_{\text{ef}}^*(p) : \mathbf{E}_{\text{ef}}^*(p). \end{aligned} \quad (11)$$

Equation (11) defines the LC-transformed homogenised relaxation tensor of the extrafibrillar space, $\mathbf{R}_{\text{ef}}^*(p)$, which is the inverse of the homogenised creep tensor in the LC domain, $\mathbf{J}_{\text{ef}}^*(p)$,

$$\mathbf{J}_{\text{ef}}^*(p) = [\mathbf{R}_{\text{ef}}^*(p)]^{-1}. \quad (12)$$

The concentration tensors $\mathbf{A}_{\text{HA}}^*(\varphi, \vartheta; p)$ and $\mathbf{A}_{\text{ic}}^*(p)$ are determined from formally elastic matrix-inclusion problems of the Eshelby-Laws type (Eshelby 1957; Laws 1977), i.e. the average strains in each material phase are approximated by the homogeneous strains in an ellipsoidal inclusion with the phase properties, surrounded by an infinite matrix with the properties of the overall extrafibrillar polycrystal ('self-consistent' approach), this matrix being subjected, at infinity, to fictitious homogeneous strains \mathbf{E}^0 . Accordingly, the phase strains read as

$$\boldsymbol{\varepsilon}_{\text{HA}}^*(\varphi, \vartheta; p) = \left[\mathbf{I} + \mathbf{P}_{\text{cyl}}^{*,\text{ef}}(\varphi, \vartheta; p) : (\mathbf{r}_{\text{HA}}^*(p) - \mathbf{R}_{\text{ef}}^*(p)) \right]^{-1} : \mathbf{E}^0, \quad (13)$$

$$\boldsymbol{\varepsilon}_{\text{ic}}^*(p) = \left[\mathbf{I} + \mathbf{P}_{\text{sph}}^{*,\text{ef}}(p) : (\mathbf{c}_{\text{ic}} - \mathbf{R}_{\text{ef}}^*(p)) \right]^{-1} : \mathbf{E}^0, \quad (14)$$

where $\mathbf{P}_{\text{cyl}}^{*,\text{ef}}$ is Hill's shape tensor of a cylindrical inclusion in the isotropic extrafibrillar matrix and $\mathbf{P}_{\text{sph}}^{*,\text{ef}}$ is the analogon for a spherical inclusion, see (Fritsch and Hellmich 2007) for details. Also, the intercrystalline space exhibits elasticity of water, $\mathbf{c}_{\text{ic}} = 3k_{\text{H}_2\text{O}}\mathbf{I}_{\text{vol}}$. Insertion of Equations (13) and (14) into Equation (2) yields an expression for \mathbf{E}^0 , and re-insertion of this expression into Equations (13) and (14), respectively, yields, according to Equations (9) and (10), the sought concentration tensors as

$$\begin{aligned} \mathbf{A}_{\text{HA}}^* = & \left[\mathbf{I} + \mathbf{P}_{\text{cyl}}^{*,\text{ef}}(\varphi, \vartheta; p) : (\mathbf{r}_{\text{HA}}^*(p) - \mathbf{R}_{\text{ef}}^*(p)) \right]^{-1} : \left\{ \phi \left[\mathbf{I} + \mathbf{P}_{\text{sph}}^{*,\text{ef}}(p) : (\mathbf{c}_{\text{ic}} - \mathbf{R}_{\text{ef}}^*(p)) \right]^{-1} \right. \\ & \left. + (1 - \phi) \int_{\varphi=0}^{2\pi} \int_{\vartheta=0}^{\pi} \left[\mathbf{I} + \mathbf{P}_{\text{cyl}}^{*,\text{ef}}(\varphi, \vartheta; p) : (\mathbf{r}_{\text{HA}}^*(p) - \mathbf{R}_{\text{ef}}^*(p)) \right]^{-1} \frac{\sin \vartheta d\vartheta d\varphi}{4\pi} \right\}^{-1} \end{aligned} \quad (15)$$

$$\mathbf{A}_{ic}^* = \left[\mathbf{I} + \mathbf{P}_{sph}^{*,ef}(p) : (\mathbf{c}_{ic} - \mathbf{R}_{ef}^*(p)) \right]^{-1} : \left\{ \phi \left[\mathbf{I} + \mathbf{P}_{sph}^{*,ef}(p) : (\mathbf{c}_{ic} - \mathbf{R}_{ef}^*(p)) \right]^{-1} + (1 - \phi) \int_{\varphi=0}^{2\pi} \int_{\vartheta=0}^{\pi} \left[\mathbf{I} + \mathbf{P}_{cyl}^{*,ef}(\varphi, \vartheta; p) : (\mathbf{r}_{HA}^*(p) - \mathbf{R}_{ef}^*(p)) \right]^{-1} \frac{\sin \vartheta d\varphi d\vartheta}{4\pi} \right\}^{-1} \quad (16)$$

Insertion of [Equations \(15\) and \(16\)](#) into [Equation \(11\)](#) yields an implicit expression for the determination of \mathbf{R}_{ef}^* . The integrals in [Equations \(15\) and \(16\)](#) can be solved very efficiently with the help of Stroud's integration formula (Stroud [1971](#); Pichler et al. [2009](#))

$$\int_{\varphi=0}^{2\pi} \int_{\vartheta=0}^{\pi} \left[\mathbf{I} + \mathbf{P}_{cyl}^{*,ef}(p)(\vartheta, \varphi) : (\mathbf{r}_{HA}^* - \mathbf{R}_{ef}^{*,SCS}(p)) \right]^{-1} \frac{\sin \vartheta d\varphi d\vartheta}{4\pi} = \sum_{j=0}^n \omega(\vartheta_j, \varphi_j) \left[\mathbf{I} + \mathbf{P}_{cyl}^{*,ef}(p)(\vartheta_j, \varphi_j) : (\mathbf{r}_{HA}^* - \mathbf{R}_{ef}^{*,SCS}(p)) \right]^{-1}. \quad (17)$$

The scalar weight $\omega(\vartheta_j, \varphi_j)$ and the orientations ϑ_j and φ_j are defined in [Table 2](#).

When summing up the tensors $\mathbf{P}_{cyl}^{*,ef}$ in [Equation \(17\)](#), they all have to be given in the same base frame. However, analytical expressions for $\mathbf{P}_{cyl}^{*,ef}$ are standardly available in a (local) base frame coinciding with the principal axis of the ellipsoid, see the Appendix. When

using the $[6 \times 6]$ 'Kelvin-Mandel' matrix notation, given as (Nadeau and Ferrari [1998](#); Helnwein [2001](#); Cowin [2003](#))

$$\mathbf{P} = \begin{bmatrix} P_{1111} & P_{1122} & P_{1133} & \sqrt{2}P_{1123} & \sqrt{2}P_{1131} & \sqrt{2}P_{1112} \\ P_{2211} & P_{2222} & P_{2233} & \sqrt{2}P_{2223} & \sqrt{2}P_{2231} & \sqrt{2}P_{2212} \\ P_{3311} & P_{3322} & P_{3333} & \sqrt{2}P_{3323} & \sqrt{2}P_{3331} & \sqrt{2}P_{3312} \\ \sqrt{2}P_{2311} & \sqrt{2}P_{2322} & \sqrt{2}P_{2333} & 2P_{2323} & 2P_{2331} & 2P_{2312} \\ \sqrt{2}P_{3111} & \sqrt{2}P_{3122} & \sqrt{2}P_{3133} & 2P_{3123} & 2P_{3131} & 2P_{3112} \\ \sqrt{2}P_{1211} & \sqrt{2}P_{1222} & \sqrt{2}P_{1233} & 2P_{1223} & 2P_{1231} & 2P_{1212} \end{bmatrix} \quad (18)$$

the corresponding component transformation from the local frames into one global frame can be done very efficiently through (Nadeau and Ferrari [1998](#))

$$\mathbf{P}_{cyl,global}^{ef}(\varphi, \vartheta; p) = \mathbf{Q}(\varphi, \vartheta) \mathbf{P}_{cyl,local}^{ef}(p) \mathbf{Q}^t(\varphi, \vartheta), \quad (19)$$

whereby $\mathbf{Q}^t(\varphi, \vartheta)$ is the transpose of $\mathbf{Q}(\varphi, \vartheta)$,

$$\mathbf{Q}(\varphi, \vartheta) = \begin{bmatrix} q_{11}^2 & q_{12}^2 & q_{13}^2 & \frac{2}{\sqrt{2}}q_{12}q_{13} & \frac{2}{\sqrt{2}}q_{13}q_{11} & \frac{2}{\sqrt{2}}q_{11}q_{12} \\ q_{21}^2 & q_{22}^2 & q_{23}^2 & \frac{2}{\sqrt{2}}q_{22}q_{23} & \frac{2}{\sqrt{2}}q_{23}q_{21} & \frac{2}{\sqrt{2}}q_{21}q_{22} \\ q_{31}^2 & q_{32}^2 & q_{33}^2 & \frac{2}{\sqrt{2}}q_{32}q_{33} & \frac{2}{\sqrt{2}}q_{33}q_{31} & \frac{2}{\sqrt{2}}q_{31}q_{32} \\ \sqrt{2}q_{21}q_{31} & \sqrt{2}q_{22}q_{32} & \sqrt{2}q_{23}q_{33} & q_{23}q_{32} + q_{33}q_{22} & q_{21}q_{33} + q_{31}q_{23} & q_{22}q_{31} + q_{32}q_{21} \\ \sqrt{2}q_{31}q_{11} & \sqrt{2}q_{32}q_{12} & \sqrt{2}q_{33}q_{13} & q_{33}q_{12} + q_{13}q_{32} & q_{31}q_{13} + q_{11}q_{33} & q_{32}q_{11} + q_{12}q_{31} \\ \sqrt{2}q_{11}q_{21} & \sqrt{2}q_{12}q_{22} & \sqrt{2}q_{13}q_{23} & q_{13}q_{22} + q_{23}q_{12} & q_{11}q_{23} + q_{21}q_{13} & q_{12}q_{21} + q_{22}q_{11} \end{bmatrix} \quad (20)$$

Table 2. Scalar weights $\omega(\vartheta_j, \varphi_j)$ and orientations ϑ_j and φ_j for Stroud's integration (Pichler et al. [2009](#)).

J	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
$\sin(\vartheta_j)\cos(\varphi_j)$	$+r$	$+r$	$-r$	$-r$	$+t$	$+t$	$-t$	$-t$	$+s$	$+s$	$-s$	$-s$	1	0	0
$\sin(\vartheta_j)\sin(\varphi_j)$	$+s$	$-s$	$+s$	$-s$	$+r$	$-r$	$+r$	$-r$	$+t$	$-t$	$+t$	$-t$	0	1	0
$\cos(\vartheta_j)$	$+t$	$+t$	$+t$	$+t$	$+s$	$+s$	$+s$	$+s$	$+r$	$+r$	$+r$	$+r$	0	0	1
$\omega(\vartheta_j, \varphi_j)$	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15	1/15

$$r = 1/2, s = (\sqrt{5} + 1)/4 \text{ and } t = (\sqrt{5} - 1)/4.$$

and q_{ij} and $i = 1, \dots, 3$, $j = 1, \dots, 3$ are the elements of matrix \mathbf{q} ,

$$\mathbf{q} = [\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3], \quad (21)$$

$$\mathbf{e}_1 = \begin{bmatrix} \cos\varphi \cos\vartheta \\ \sin\varphi \cos\vartheta \\ -\sin\varphi \end{bmatrix}, \quad \mathbf{e}_2 = \begin{bmatrix} -\sin\varphi \\ \cos\varphi \\ 0 \end{bmatrix}, \quad (22)$$

$$\mathbf{e}_3 = \begin{bmatrix} \cos\varphi \sin\vartheta \\ \sin\varphi \sin\vartheta \\ \cos\varphi \end{bmatrix}.$$

2.3 Homogenisation up to the macrolevel

The viscoelastic behaviour of the remaining five homogenisation steps up to the macrolevel follows from an expression analogous to Equations (11), (15) and (16), but for a finite number of phases (Laws and McLaughlin 1978; Benveniste 1987; Zaoui 2002)

$$\mathbf{R}^{*,\text{est}}(p) = \sum_r f_r \mathbf{r}_r^*(p) : [\mathbf{I} + \mathbf{P}_r^{*,0}(p) : (\mathbf{r}_r^*(p) - \mathbf{R}^{*,0}(p))]^{-1} : \left\{ \sum_s f_s [\mathbf{I} + \mathbf{P}_s^{*,0}(p) : (\mathbf{r}_s^*(p) - \mathbf{R}^{*,0}(p))]^{-1} \right\}^{-1}, \quad (23)$$

where \mathbf{r}_r^* is the LC-transformed relaxation tensor of phase r , f_r is the volume fraction of phase r and $\mathbf{P}_r^{*,0}$ is the LC-transformed Hill's morphology tensor of an ellipsoidal inclusion representing the characteristic shape of phase r , being embedded in a fictitious matrix with LC-transformed relaxation tensor $\mathbf{R}^{*,0}$: choice of the latter defines the morphological nature of the material: if $\mathbf{R}^{*,0}$ coincides with one of the phase relaxation tensors, the latter phase is a matrix, in which all other phases are embedded (Mori-Tanaka scheme (Mori and Tanaka 1973)); if $\mathbf{R}^{*,0}$ is identical to $\mathbf{R}^{*,\text{est}}$, then all phases are in mutual contact, as in a polycrystal (self-consistent scheme (Hershey 1954; Laws and McLaughlin 1978)). In this sense, an RVE $\check{V}_{\text{wetcol}}$ of wet collagen (Figure 2(a)) consists of a contiguous matrix of cross-linked molecular collagen, in which cylindrical intermolecular pores are embedded; an RVE \check{V}_{fib} of mineralised fibrillar material (Figure 2(b)) consists of mutually interpenetrating hydroxyapatite crystal agglomerations (of, on average, spherical shape) and cylindrical microfibrils made up of wet collagen, modelled through a self-consistent scheme; an RVE \check{V}_{excel} of extracellular bone matrix (Figure 2(d)) consists of an extrafibrillar matrix with fibrillar inclusions; an RVE \check{V}_{exvas} of extravascular material (Figure 2(e)) consists of a matrix of extracellular matrix

with embedded lacunar pores (inhabited by one osteocyte each; and being drained, i.e. exhibiting zero elastic stiffness) and an RVE V_{cort} of cortical bone (Figure 2(f)) consists of a matrix of extravascular material with embedded vascular pores (i.e. Haversian canals populated, among others, by osteoblasts, osteoclasts and blood vessels; being drained, i.e. exhibiting zero elastic stiffness). Explicitly, cortical bone obeys the following material behaviour

$$\mathbf{R}_{\text{cort}}^*(p) = [f_{\text{exvas}} \mathbf{R}_{\text{exvas}}^*(p) : \left\{ f_{\text{exvas}} \mathbf{I} + f_{\text{vas}} [\mathbf{I} + \mathbf{P}_{\text{cyl}}^{*,\text{exvas}}(p) : (-\mathbf{R}_{\text{exvas}}^*(p))]^{-1} \right\}^{-1}]^{-1}. \quad (24)$$

In Equation (24), f_{exvas} denotes the volume fraction and $\mathbf{R}_{\text{exvas}}^*$ is the relaxation tensor of extravascular material, f_{vas} denotes the volume fraction of the vascular pores and $\mathbf{P}_{\text{cyl}}^{*,\text{exvas}}$ denotes the Hill's tensor, accounting for cylindrical inclusions in a transversely isotropic matrix of extravascular material, for mathematical details of the used Hill's tensors, we refer to (Hellmich et al. 2004b; Fritsch and Hellmich 2007).

To be able to give the predicted relaxation functions of cortical bone from Equation (24) in a physically relevant format, we have to back-transform the LC-transformed material function $\mathbf{R}_{\text{cort}}^*(p)$ into the time domain. Therefore, we employ the Gaver-Wynn-Rho algorithm (Abate and Valkó 2004; Valkó and Abate 2004), as detailed in Scheiner and Hellmich (2009). This results in a constitutive law of the format

$$\begin{aligned} \check{\Sigma}_{\text{cort}}(t) &= \int_{-\infty}^t \mathbf{R}_{\text{cort}}(t - \tau) : \dot{\mathbf{E}}_{\text{cort}}(\tau) d\tau \\ &= [\mathbf{R}_{\text{cort}}^* \mathbf{E}_{\text{HA}}](t). \end{aligned} \quad (25)$$

3. Creep parameter identification from three-point bending test on fully hydrated specimens

We identify the creep characteristics of water interface-penetrated hydroxyapatite clusters from three-point bending test of Iyo et al. (2004): these researchers deflected, by $w = 0.39$ mm, the centre of a beam on two supports, the beam's geometrical dimensions being $l = 32$ mm length, $h = 1$ mm height and $b = 5$ mm width. They recorded the relaxing force $F^{\text{exp}}(t)$ necessary for maintaining a constant deflection of the beam. However, these force measurements are not explicitly reported in the aforementioned paper. Instead, the authors *a priori* assumed a fully linear viscoelastic behaviour of the beam system, and reported a corresponding (assumed) relaxation modulus $R^{\text{lyo}}(t)$, in the format

$$R^{\text{lyo}}(t) = E_0 \left\{ A_1 \exp \left[-\left(\frac{t}{\tau_1} \right)^\beta \right] + (1 - A_1) \exp \left[-\left(\frac{t}{\tau_2} \right)^\gamma \right] \right\}, \quad (26)$$

Table 3. Parameters defining relaxation modulus assumed by Iyo et al. (2004), denoted as $R^{\text{Iyo}}(t)$ in Equation (26).

Direction	E_0 [GPa]	A_1 [-]	τ_1 [s]	τ_2 [$\times 10^6$ s]	β [-]	γ [-]
Longitudinal	14.2	0.08	49	9.3	0.28	0.35
Transverse	11.6	0.11	50	6.4	0.26	0.37

see Table 3 for parameters $E_0, A_1, \tau_1, \tau_2, \beta$ and γ . From this assumed relaxation modulus, the experimentally determined relaxation force $F^{\text{exp}}(t)$ can be re-constructed, according to Bernoulli's beam theory

$$F^{\text{exp}}(t) = \frac{4R^{\text{Iyo}}(t)E_{\text{Iyo}}I}{l \times (h/2)}. \quad (27)$$

Equation (27) relates to the statically determinate structure of a simply supported beam of length l , width b and height h , exhibiting a moment of inertia I

$$I = \frac{bh^3}{12} = 0.4167 \text{ mm}^4, \quad (28)$$

and with E_{Iyo} as the (assumed) maximum longitudinal strain at the beam centre, $E_{\text{Iyo}} = 0.23\%$ (Iyo et al. 2004). The experimentally determined force relaxation is depicted in Figure 4 – the initially applied force amounts to 3.4 N. We reiterate that this force would result in hypothetical elastic strain of $E_{\text{Iyo}} = 0.23\%$ at the bottom of the beam, below the load.

However, these strains clearly exceed those related to purely elastic behaviour, amounting to about 0.045%, after which elastoplastic deformations are expected in the extrafibrillar foam (Fritsch et al. 2009). Hence, plastic events are involved in the three-point bending test. They can be quantified from a well-validated hierarchical micromechanics representation of bone (Fritsch and Hellmich 2007; Fritsch et al. 2009). When specified for bovine tibial bone (out of which Iyo et al. (2004) produced

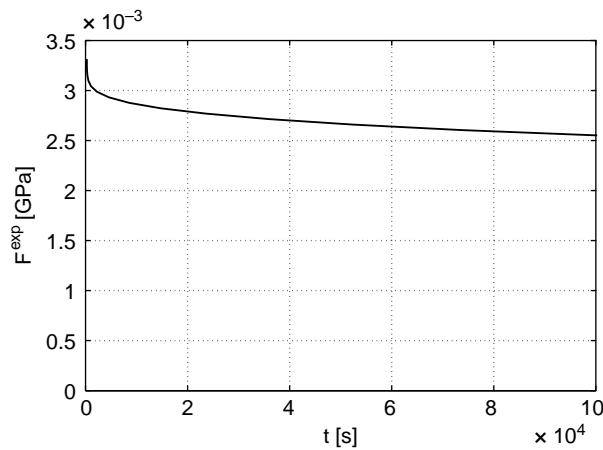

 Figure 4. Time-dependent relaxation force $F^{\text{exp}}(t)$ acting on three-point beam bending system, re-constructed from data and protocol given in Iyo et al. (2004).

Table 4. Volume fractions for bovine tibia (Lees et al. 1979); (Fritsch and Hellmich 2007).

ρ_{wet}	\bar{f}_{col}	\bar{f}_{HA}	\bar{f}_{fib}	\hat{f}_{HA}	\check{f}_{HA}	\check{f}_{col}	f_{vas}	f_{lac}
1.99	0.29	0.46	0.51	0.65	0.28	9.41	0.05	0.02

their beam samples, see Table 4 for corresponding volume fractions), this model predicts a (uniaxial) stress – (triaxial) strain behaviour as depicted in Figure 5, where $\Sigma_{\text{cort},33}$ refers to the uniaxial normal stress component (acting in the beam direction, see Figure 6) and $E_{\text{cort},33}$ denotes the strain component measuring length changes in the same direction.

In tension, the material exhibits a purely elastic behaviour below 11 MPa. Upon further increase of the load, the crystals in the extrafibrillar space start to glide along water layers, which results in an elastoplastic quasi-linear stress–strain relationship. The latter relates to a softer response than the one the material shows initially. Given such a stress–strain relationship, the initial load at the centre of the beam leads, according to Bernoulli's beam theory, to a linear total strain distribution $E_{\text{cort},33}(x_1)$, and to a bilinear stress distribution $\Sigma_{\text{cort},33}(x_1) = \Sigma_{\text{cort},33}(x_1)\mathbf{e}_3 \otimes \mathbf{e}_3$, with \otimes standing for the dyadic product (Salençon 2001), across the beam cross section at the beam centre ($x_3 = 0$), as depicted in Figure 7. The stress distribution can be transformed into a distribution of elastic strains $\mathbf{E}_{\text{cort}}^{\text{el}}(x_1, x_3 = 0)$, through

$$\mathbf{E}_{\text{cort}}^{\text{el}}(x_1) = \mathbf{R}_{\text{cort}}^{-1}(t = \tau) : \Sigma_{\text{cort},33}(x_1), \quad (29)$$

with $\mathbf{E}_{\text{cort}}^{\text{el}}(x_1) = E_{\text{cort},11}^{\text{el}}(x_1)\mathbf{e}_1 \otimes \mathbf{e}_1 + E_{\text{cort},22}^{\text{el}}(x_1)\mathbf{e}_2 \otimes \mathbf{e}_2 + E_{\text{cort},33}^{\text{el}}(x_1)\mathbf{e}_3 \otimes \mathbf{e}_3$. During the relaxation experiment, the axial normal component of the total strain, $E_{\text{cort},33}$, remains constant, i.e. it is time invariant [the normal strain components in one- and two-directions, though, do change (i.e. decrease) in the course of the relaxation of the beam]. Due to the stress decrease in the beam sample during relaxation, the plastic strains $E_{\text{cort}}^{\text{pl}}$ remain unchanged, they are also time invariant. Conclusively, also the initially elastic axial normal strain component, $E_{\text{cort},33}^{\text{el}}$, is time

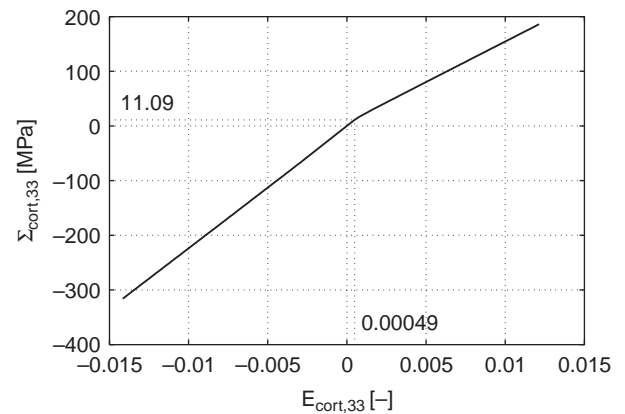


Figure 5. Macroscopic stress–strain diagram for bovine tibia.

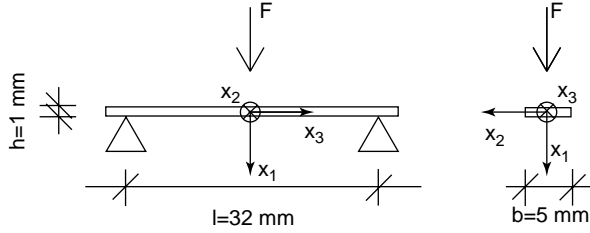


Figure 6. Specimen tested by Iyo et al. (2004).

invariant, it plays the role of prescribed strain in a purely viscoelastic experiment. In order to preserve the mathematical format of small-strain Bernoulli beam theory, it is useful to formulate the axial stress relaxation in the LC domain

$$\Sigma_{\text{cort},33}^*(p, x_1) = \frac{1}{J_{\text{cort},3333}^*(p)} \times E_{\text{cort},33}^{\text{el}}(x_1), \quad (30)$$

where $J_{\text{cort},3333}^*$ is the axial normal component of the LC-transformed creep tensor $\mathbf{J}_{\text{cort}}^*(p) = \mathbf{R}_{\text{cort}}^{*-1}(p)$; in Equation (30), we account for the fact that all time-invariant quantities do not depend on the frequency variable p either. Axial stresses $\Sigma_{\text{cort},33}^*$ result in a bending moment around axis x_2

$$M_2^*(p) = \int_A \Sigma_{\text{cort},33}^*(p, x_1) x_1 dA, \quad (31)$$

and the latter is related to the relaxing force acting in the beam centre, according to the equilibrium conditions

$$F^{\text{mod}}(p) = \frac{4M_2^*(p)}{l}. \quad (32)$$

Upon back-transformation from the LC domain to the time domain, we obtain the model-predicted force relaxation evolution $F^{\text{mod}}(t)$, as a function of the (so far unknown) Burgers creep parameters of crystal clusters with wet interfaces. We can now determine the creep parameters of the Burgers model, μ_{KV} , η_{KV} and η_{M} .

such that the difference between the experimental relaxation force $F^{\text{exp}}(t)$ and the model-predicted relaxation force $F^{\text{mod}}(t)$ is minimised. More specifically, we minimise, through a two-membered evolution strategy (Schwefel 1977; Hellmich and Ulm 2002), the standardised relative difference D , defined as

$$D = \frac{1}{N+1} \sum \sqrt{\left(\frac{F^{\text{mod}}(t) - F^{\text{exp}}(t)}{F^{\text{exp}}(t)} \right)^2}, \quad D \rightarrow 0. \quad (33)$$

The resulting Burgers parameters are listed in Table 5.

4. Model validation by means of partially dried specimens

In order to check the relevance of the Burgers creep parameters of Table 5 (which were back-analysed from a three-point bending test on a bovine tibial sample, as described in Section 3), we use the viscoelastic multiscale model of Figure 2 (with the stiffness characteristics of Table 4 and the creep parameters in Table 5) in order to predict the viscoelastic behaviour of additional bone samples tested under conditions different from the aforementioned bending test, and we then compare the latter model predictions with corresponding experimental results. In this context, we consider the cantilever bending tests of (Sasaki et al. 1993; see Figure 8), where the beam samples are cut out of the femur of a 36-month-old cow, such that the beam axis coincides with the longitudinal material direction of the bone tissue. For such an experimental set up, Sasaki et al. (1993) examined two different cases: (i) a specimen soaked in water (with a water content of $\phi = 0.22$ g water/g bone) and (ii) a partially de-hydrated specimen (with a water content of $\phi = 0.14$ g water/g bone). Given the lack of more specific information and the similarity of bone tissue from bovine

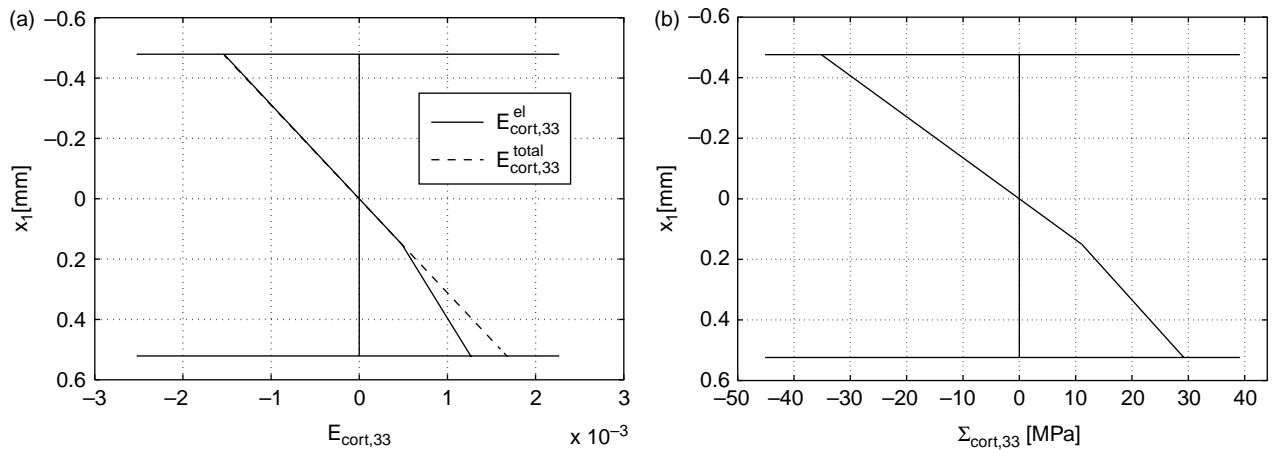


Figure 7. Initial stress and strain distribution over the beam height under the applied load: (a) axial normal strains (elastic and total) and (b) axial normal stresses.

Table 5. Burgers parameters.

$\mu_{HA,KV}$	179.5262 GPa
$\eta_{HA,KV}$	1.3430×10^5 GPa s
$\eta_{HA,M}$	1.2842×10^7 GPa s

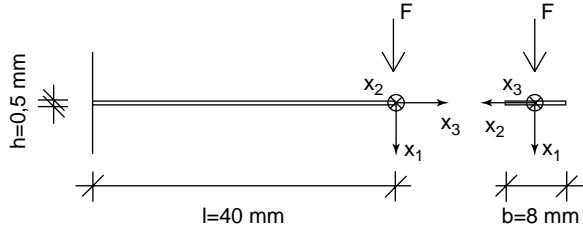


Figure 8. Specimen tested by (Sasaki et al. 1993).

femur and tibia, we again employ the volume fractions given in Table 4.

At first, the cantilever bending tests with $\phi = 0.22$ g water/g bone were examined. The experimental relaxation force and the initial distribution of the elastic strains in the cross section under the load were determined for the experimental data given in Sasaki et al. (1993) with the help of viscoelastic beam theory. The divergence between predictions and experiments is $+2.52 \pm 0.09\%$ (see Figure 9).

Upon drying, water is removed from the pore spaces in bone material, starting with the largest pores, the vascular pores in cortical bone (see Figure 2(f)), followed by the lacunar pores (see Figure 2(e)), before the much smaller intercrystalline pores (see Figure 2(c)) are affected. Only after excessively long drying (such as under vacuum conditions; Cusack and Miller 1979), the smallest intermolecular pores are deprived of the water bound tightly herein. The apparent mass density of water in the intercrystalline pores, per volume of extrafibrillar material, amounts to $\rho_{H_2O} \times (1 - \hat{f}_{HA}) = 0.35 \text{ g/cm}^3$, and

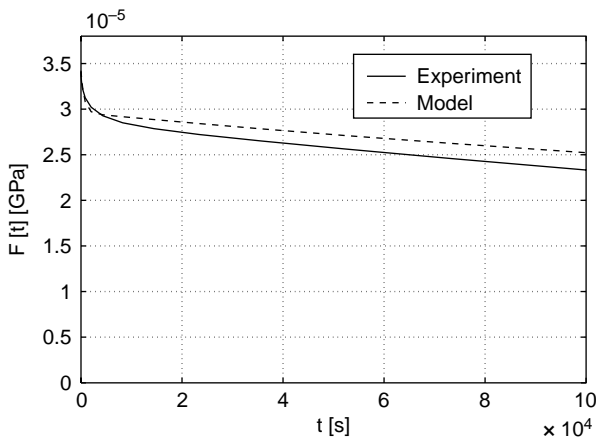


Figure 9. Force relaxation in water-soaked cantilever made of bovine femoral tissue: comparison of model predictions with experimental data of (Sasaki et al. 1993).

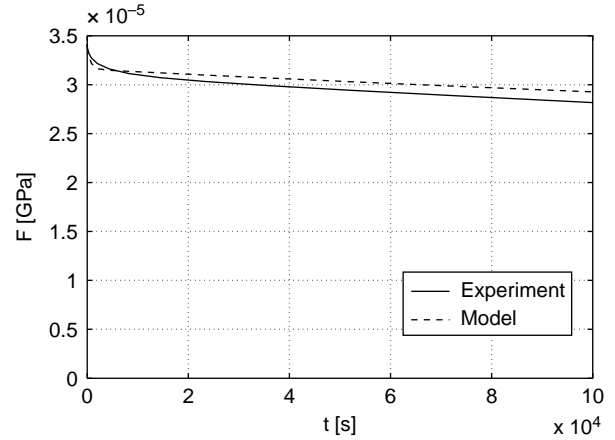


Figure 10. Force relaxation in partially dehydrated cantilever made of bovine femoral tissue: comparison of model predictions with experimental data of (Sasaki et al. 1993).

the intercrystalline water concentration per volume of cortical bone amounts to $0.35 \times (1 - 0.51) \times (1 - 0.02) \times (1 - 0.05) = 0.16 \text{ g/cm}^3$. Consequently, a water loss from 0.22 to 0.14 g/cm^3 , i.e. amounting to a difference of 0.08 g/cm^3 , leads to emptying half of the intercrystalline pore space. Hence, only half of the extrafibrillar crystals are in contact with water, and only these are subject to viscous sliding processes. In terms of our model formulation, only half of the crystals show viscoelastic shear behaviour, the rest behaving in a purely elastic fashion. Accordingly, the partially dried sample creeps less (see Figure 10), and our model predictions are not only qualitatively correct, but also exhibit a satisfactorily small error of $+1.6 \pm 0.04\%$.

5. Composition-dependent creep properties – influence of extracellular mineral content and vascular porosity

Due to biodiversity, there is a great variation in bone microstructure. Because of the significant influence on viscoelastic behaviour of bone materials, especially vascular porosity and mineral content in the extracellular matrix are interesting. Considering mammals, vascular porosity in healthy cortical bone lies between 2% and 8%, and could increase up to 27% in the case of osteoporosis (Bousson et al. 2000; Fritsch et al. 2009). The chemical composition within the extravascular matrix depends only on the organ, the individual and the species, but do not vary in space and time (Boivin and Meunier 2002; Akkus et al. 2003; Roschger et al. 2003; Bossy et al. 2004; Hellmich et al. 2008; Fritsch et al. 2009). The extracellular mineral content \bar{f}_{HA} reaches from 30%, typical for deer antler, up to 70% in equine metacarpus (Fritsch et al. 2009).

Accordingly, we report studies where we vary the vascular porosity between 2% and 30%, and where the ultrastructural mineral volume is chosen between 30% and

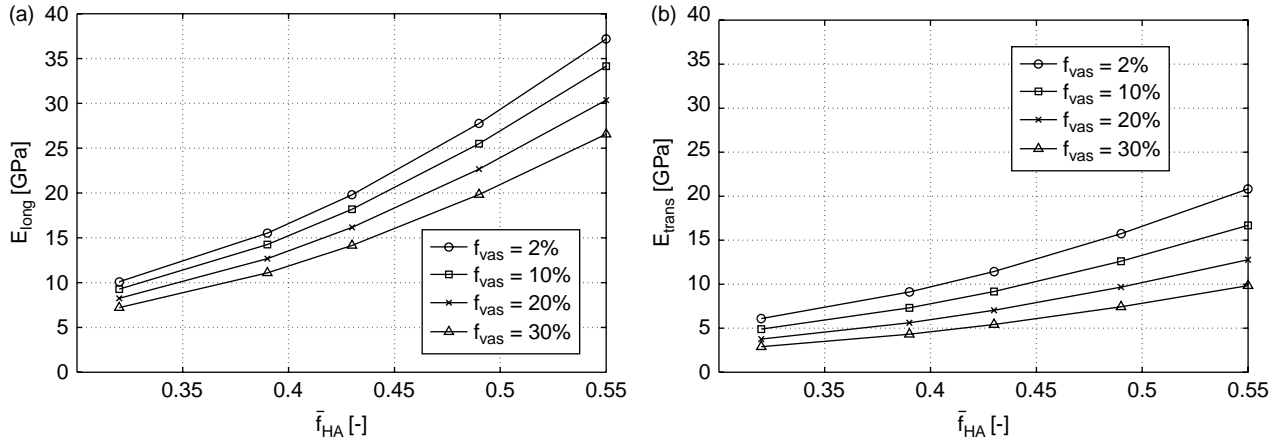


Figure 11. Model-predicted modulus of elasticity in (a) longitudinal direction and (b) transverse direction as function of \bar{f}_{HA} for different f_{vas} .

55%; the lacunar volume fraction is kept at 2% (as in Table 4), and all other volume fractions at all remaining RVEs of Figure 2 follow from Eq. (29) to (49) of Fritsch and Hellmich (2007). In Figure 11, the effect of increasing extracellular mineral content \bar{f}_{HA} , as well as of increasing vascular porosity f_{vas} on modulus of elasticity in longitudinal (Figure 11(a)) and transverse directions (Figure 11(b)), respectively, can be seen. Increasing \bar{f}_{HA} (with f_{vas} kept constant) leads to an increasing Young's modulus, whereas increasing f_{vas} (with \bar{f}_{HA} kept constant) leads to decreasing Young's modulus. These results imply that the mineral is responsible for the stiffness of bone which is consistent with the findings of Currey (2004). The variation of \bar{f}_{HA} and f_{vas} affects the relaxation modulus $1/J_{3333}$ in the same way (see Figure 12(a), (b)).

The plots seen in Figure 13 show the five independent components of the creep tensor \mathbf{J} as functions of time, for different mineral content and different vascular porosities. In addition to the effects discussed before, two further phenomena can be observed: (i) an increase in \bar{f}_{HA} leads to

a decrease in the creep compliances in both directions (J_{1111} and J_{3333}) and (ii) this decrease is more pronounced in the transverse direction than in longitudinal direction. The first effect can be explained by the distribution of load to the hydroxyapatite needles. If the mineral content grows, e.g. if there are more needles, the load applied to one single needle reduces. Hence, the gliding of single hydroxyapatite needles on the thin water layers between them is less distinctive, and therefore the whole material creeps less. This phenomenon is direction-independent. The second effect can be explained by the fact that the minerals in the transverse direction carry much more of an overall macroscopic load than they do in longitudinal direction, where the molecular collagen contributes more. Therefore, higher mineral content expresses itself in a stiffness gain (and creep loss), which is larger in transverse and smaller in longitudinal directions. Higher contribution in load carrying may lead to earlier (and more) plastification.

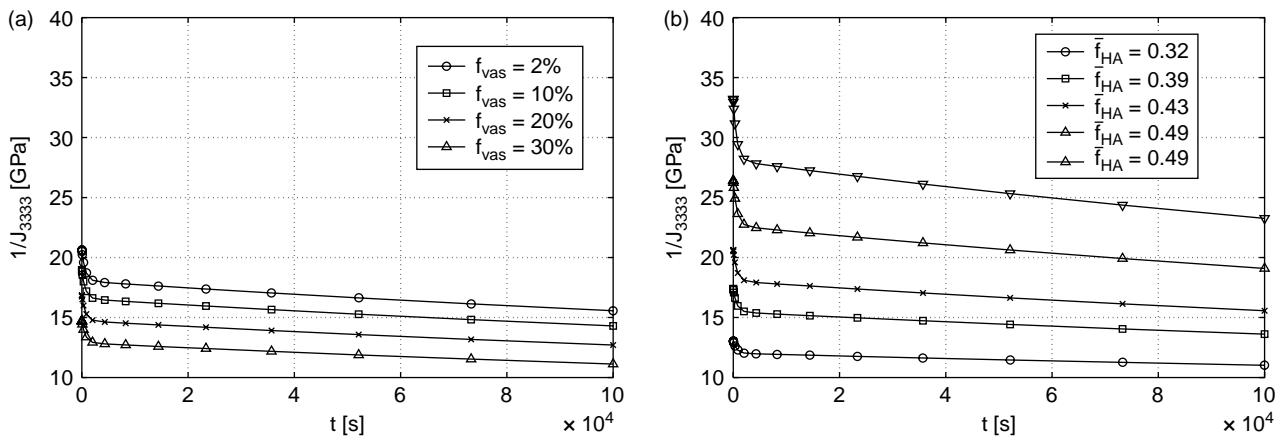


Figure 12. (a) Model-predicted relaxation modulus $1/J_{3333}$ for $\bar{f}_{\text{HA}} = 0.43$ and (b) model-predicted relaxation modulus $1/J_{3333}$ for $f_{\text{vas}} = 2\%$.

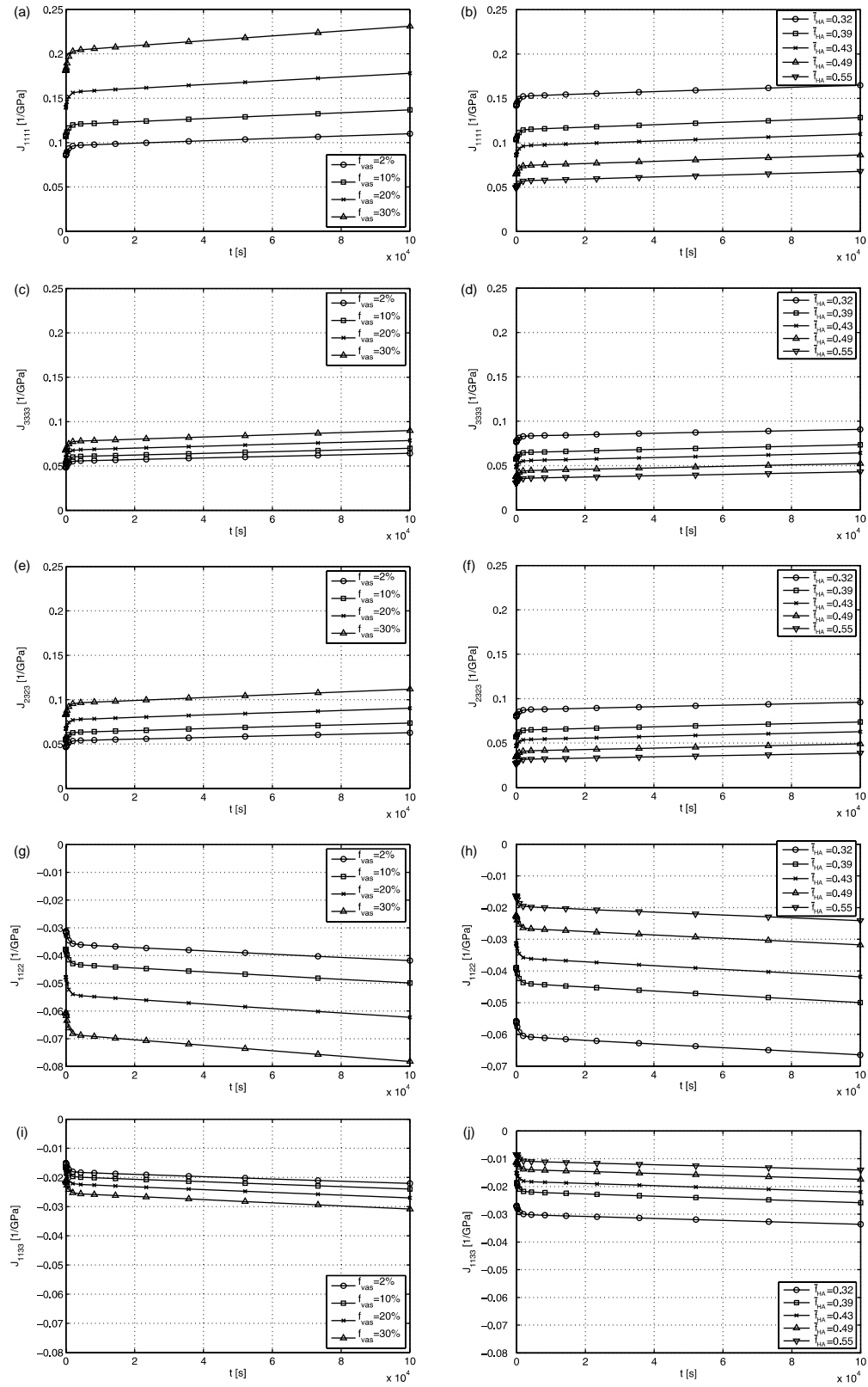


Figure 13. Plots for (a) J_{1111} for $\bar{f}_{HA} = 0.43$, (b) J_{1111} for $f_{vas} = 2\%$, (c) J_{3333} for $\bar{f}_{HA} = 0.43$, (d) J_{3333} for $f_{vas} = 2\%$, (e) J_{2323} for $\bar{f}_{HA} = 0.43$, (f) J_{2323} for $f_{vas} = 2\%$, (g) J_{1122} for $\bar{f}_{HA} = 0.43$, (h) J_{1122} for $f_{vas} = 2\%$, (i) J_{1133} for $\bar{f}_{HA} = 0.43$ and (j) J_{1133} for $f_{vas} = 2\%$.

6. Summary and outlook

A first approach of predicting long-term creep and relaxation functions for bone material considering a multiscale micromechanics model has been proposed in this manuscript. As to the knowledge of the authors, it was the first time that the intercrystalline water layers between hydroxyapatite needles appearing in the extrafibrillar space were regarded as responsible for the viscoelastic behaviour of cortical bone.

The Burgers model turned out to describe the creep behaviour of bone very well. In the first step, the parameters $\mu_{\text{HA,KV}}$, $\eta_{\text{HA,KV}}$ and $\eta_{\text{HA,M}}$ were determined using an evolution strategy. To validate this approach, the predicted values were compared with the results of different experimental tests. The fact that the mean values of the relative error between experimental results and model estimates are less than 3% for several tests, is a clear indicator for the significance of this approach. Because of the correlation between the overall water content and the number of hydroxyapatite needles involved in gliding events, the capability of our new model to predict relaxation forces for varying water contents very well, confirms the relevance of the proposition to assign the viscoelastic properties of bone to intercrystalline water layers between the needles.

Taking a multiscale model into account allowed us to study the effects of varying extracellular mineral contents and vascular porosities on viscoelastic behaviour of bone material. As expected, enlarging the mineral content resulted in an increase of the relaxation modulus, enlarging the vascular porosity resulted in a decrease of the relaxation modulus. The creep compliance reduced as the mineral content increased, which could be explained by the distribution of the applied load on the single hydroxyapatite needles. An unequally fast decrease in the creep compliance in longitudinal and transverse directions could be attributed to the contribution of molecular collagen to load transfer. The question could be raised whether the few experimental results reported here could not have been represented by a simpler model with fewer homogenisations steps. While the answer is potentially ‘yes’, this was not the purpose of the work described herein. We are interested in the general understanding of the mechanical phenomena occurring in bone micro- and nanostructures; and in the present work, we have tackled the question whether the multiscale scheme for bone as given in [Figure 2](#), which has been successfully validated by means of dehydration/demineralisation tests, diffraction tests, microscopic data and ultrasonic tests at different frequencies, as well as by quasi-static tests for elasticity and strength, see (Hellmich and Ulm 2003; Fritsch et al. 2007; Fritsch et al. 2009; Vuong and Hellmich 2011), would also be valid for bone creep, by just introducing tissue independent, ‘universal’ viscous properties related

to sliding along interfaces of layered water. The first results shown here are affirmative.

Our work should also help to better understand, how bone works mechanically in the course of time. Especially, the ability of relaxation behaviour to reduce stress concentrations, which occur at microcracks, bone fractures or fixations of implants, for example, is of interest, in order to optimise, e.g. the treatment after bone fractures or fixation techniques. Another important area is that of mechanobiology where the time dependent, viscoelastic behaviour of bone potentially alters the characteristic times of remodelling events significantly (Lemaire et al. 2004).

Because of lack of long-term experimental data, only bovine tibia was examined in this work. Investigating the viscoelastic behaviour inherent to other bones of other species emerges as interesting task of further research. In this context, enlargement of the very scarce experimental data base should be a central issue, by expanding well-designed experimental protocols both at the macroscale (Brynk et al. 2011) and at the microscale (Han et al. 2011), to creep and relaxation tests.

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Notes

1. Although sometimes referred to as ‘needles’ appearing in electron microscopy (Lees and Probst 1988; Arsenault et al. 1991; Lees et al. 1994; Probst and Lees 1996; Benezra Rosen et al. 2002; Rubin et al. 2003; Hong et al. 2009) there is some consensus that these ‘needles’ could be rather platelets seen ‘on-the-edge’ (Eppell et al. 2001; Su et al. 2003; Tong et al. 2003; Hassenkam et al. 2004); however, these platelets are probable to be much longer than wide (Landis et al. 1991; Moradian-Oldak et al. 1991). From a micromechanical viewpoint, the effect of needle- versus plate-shape on the overall mechanical behaviour of porous polycrystals has been shown to be a minor one (Fritsch et al. 2010).
2. Spreading over considerable crystal surfaces, while being negligible in terms of volume fractions.

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Appendix Fourth-order Hill tensor, $\mathbf{P}_{\text{cyl}}^{\text{ef}}$, for cylindrical inclusions in an isotropic material

The fourth-order Hill tensor, $\mathbf{P}_{\text{cyl}}^{\text{ef}}$, for cylindrical inclusions in an isotropic material can be obtained from

$$\mathbf{P}_{\text{cyl}}^{\text{ef}} = \mathbf{S}_{\text{cyl}}^{\text{Esh,ef}} : \mathbf{C}_{\text{ef}}^{-1}, \quad (\text{A1})$$

where the Eshelby tensor, $\mathbf{S}_{\text{cyl}}^{\text{Esh,ef}}$, is standardly defined in a local coordinate system attached to individual solid needles (as depicted in [Figure 3](#)). The corresponding non-zero components read as follows (Eshelby 1957)

$$S_{\text{cyl},1111}^{\text{esh}} = S_{\text{cyl},2222}^{\text{esh}} = \frac{5 - 4\nu_{\text{ef}}}{8[1 - \nu_{\text{ef}}]},$$

$$S_{\text{cyl},1122}^{\text{esh}} = S_{\text{cyl},2211}^{\text{esh}} = \frac{-1 + 4\nu_{\text{ef}}}{8[1 - \nu_{\text{ef}}]},$$

$$S_{\text{cyl},1133}^{\text{esh}} = S_{\text{cyl},2233}^{\text{esh}} = \frac{\nu_{\text{ef}}}{2[1 - \nu_{\text{ef}}]},$$

$$S_{\text{cyl},2323}^{\text{esh}} = S_{\text{cyl},3232}^{\text{esh}} = S_{\text{cyl},3223}^{\text{esh}} = S_{\text{cyl},2332}^{\text{esh}} =$$

$$S_{\text{cyl},3131}^{\text{esh}} = S_{\text{cyl},1313}^{\text{esh}} = S_{\text{cyl},1331}^{\text{esh}} = S_{\text{cyl},3113}^{\text{esh}} = \frac{1}{4},$$

$$S_{\text{cyl},1212}^{\text{esh}} = S_{\text{cyl},2121}^{\text{esh}} = \frac{3 - 4\nu_{\text{ef}}}{8[1 - \nu_{\text{ef}}]},$$

$$S_{\text{cyl},2112}^{\text{esh}} = S_{\text{cyl},1221}^{\text{esh}} = \frac{3 - 4\nu_{\text{ef}}}{8[1 - \nu_{\text{ef}}]}, \quad (\text{A2})$$

with the Poisson's ratio reading as

$$\nu_{\text{ef}} = \frac{3k_{\text{ef}} - 2\mu_{\text{ef}}}{6k_{\text{ef}} + 2\mu_{\text{ef}}}, \quad (\text{A3})$$

where k_{ef} and μ_{ef} are the bulk and shear moduli of the extrafibrillar material.