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# Nanoscale Investigation of Polarization Interaction and Polarization Switching in Ferroelectric P(VDF-TrFE) Copolymer Samples

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NANOSCALE INVESTIGATION OF  
POLARIZATION INTERACTION AND POLARIZATION SWITCHING IN  
FERROELECTRIC P(VDF-TrFE) COPOLYMER SAMPLES

by

Jihee Kim

A DISSERTATION

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NANOSCALE INVESTIGATION OF  
POLARIZATION INTERACTION AND POLARIZATION SWITCHING IN  
FERROELECTRIC P(VDF-TrFE) COPOLYMER SAMPLES

Jihee Kim, Ph. D.

University of Nebraska, 2008

Adviser: Stephen Ducharme

Ferroelectric properties of thin films and self-assembly of copolymers of polyvinylidene fluoride with trifluoroethylene (P(VDF-TrFE)) have been studied. All samples were fabricated with Langmuir-Blodgett (LB) film deposition technique. Two main observations are presented in this dissertation. One is a polarization interaction effect in multi-layered thin films made of two different copolymers, and the other is local polarization switching of the self-assembly, called nanomesas.

The multilayer films were built with two different content ratio of P(VDF-TrFE) copolymers. They were P(VDF-TrFE 80:20) and P(VDF-TrFE 50:50) with phase transition temperatures of  $133 \pm 4$  °C and  $70 \pm 4$  °C respectively. The polarization interaction effect resulted in transition temperature changes of the materials, and the determined interaction length was approximately 11 nm, perpendicular to the film plane.

Nanomesas of P(VDF-TrFE) copolymer were found during annealing study of thinner films with less than 3 deposited layer thin films. Nanomesas are disk shaped isolated islands approximately 9 nm in height and 100 nm in diameter in average.

Ferroelectric switching properties of nanomesas have been shown macroscopically in the previous studies. In this work, the switching properties of individual nanomesas were probed at nanoscale. Nanomesas, switched with  $\pm 7 \text{ V}_{\text{dc}}$  were recorded using piezoresponse force microscopy (PFM). Switching hysteresis loops from a local area of  $12\sim 15 \text{ nm}^2$  within an individual nanomesa were also obtained using switching spectroscopy PFM (SS-PFM). The coercive field determined from the well behaved switching loops is  $\sim 250 \sim 450 \text{ MV/cm}$ .

**This is dedicated to Jesus**

**Through Mary,**

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## Chapter 1 Introduction

Ferroelectric copolymers of vinylidene fluoride (VDF)<sub>x</sub> with trifluoroethylene (TrFE)<sub>100-x</sub> have been a main subject in our research group for the last decade. P(VDF-TrFE) is a very well known ferroelectric copolymer. The development of P(VDF-TrFE) copolymer is originated from discovery of the piezoelectricity and pyroelectricity of PVDF. The piezoelectricity and the pyroelectricity of PVDF were first discovered in 1969 and 1971, respectively.<sup>1,2</sup> Since then, PVDF was widely investigated to understand its basic properties as well as for its technical applications, such as electromechanical transducers, pyroelectric detectors for infrared imaging, etc. Due to the potential inexpensive massive fabrication, which is a merit of flexible polymers, PVDF had drawn much research interests to it. As one way to improve the piezoelectricity and pyroelectricity of PVDF, copolymers of PVDF were also synthesized<sup>3</sup> and investigated. P(VDF-TrFE) is one of those synthesized copolymers for that purpose. Eventually, in the early 1980's ferroelectricity of both PVDF and P(VDF-TrFE) were clearly revealed.<sup>4,5</sup> The more detailed development of PVDF is well introduced in the specialized text by Wang *et al.*<sup>6,7</sup>

Mostly, ferroelectric polymers have been studied in a form of thin films. Thin films can be fabricated in many different ways, for example, solution casting, dipping or spinning.<sup>8</sup> In our lab, we have prepared thin films of P(VDF-TrFE) copolymer by using Langmuir-Blodgett technique.<sup>9</sup> Thin films of P(VDF-TrFE) made by Langmuir-Blodgett

technique show very good ordering, which results in strong X-ray diffraction peak, which are discussed in later chapters (see section 2.2, and chapter 3). The representative copolymers of 70% VDF with 30% of TrFE, P(VDF-TrFE 70:30), have been intensively studied in our group.<sup>10</sup> In addition to the fundamental characterization studies (crystal structure, dielectric properties, switching properties of thin films of P(VDF-TrFE)), many application studies (developing memory devices, pyroelectric scanning microscope, nanofabrication) also have been done.

There are two main projects presented in this dissertation. One is the polarization interaction between P(VDF-TrFE 80:20) and P(VDF-TrFE 50:50) copolymers presented in Chapter 3, and the other one is the polarization switching in a self-assembly films of P(VDF-TrFE 70:30) copolymer, namely nanomesas, presented in Chapter 4. Nanomesas are disk-shaped islands with dimensions of approximately 9 nm in thickness and 100 nm in diameter, and they will be introduced in the next chapter 2. There are two appendices at the end of the dissertation. In appendix A, an initial testing work for setting a Near Field Pyroelectric Scanning Microscopy (NFPSM) system is summarized. In appendix B, Nan imprints attempts are summarized.

In this chapter, before presenting all the works mentioned above, basic concepts of ferroelectricity, and introduction of P(VDF-TrFE) copolymers, and Langmuir-Blodgett thin film fabrication technique will be briefly introduced. The basic diagnostic sample characterization measurements taken routinely in our lab will be introduced in chapter 2.

## 1.1 Ferroelectricity

A ferroelectric material exhibits a stable macroscopic polarization that can be repeatedly switched by an external electric field between equal-energy states of opposite polarization.<sup>10</sup> Dielectric materials can be categorized as nonferroelectric (normal dielectric or paraelectric) and ferroelectric<sup>11</sup>. In paraelectric (normal dielectric) materials, electric polarization occurs when an electric field is applied to the materials. There are three different types of electric polarization according to the mechanisms of electric polarization; Electronic polarization, atomic or ionic polarization, and orientational polarization. Electronic polarization occurs due to the displacement of the outer electron clouds with respect to the inner positive atomic cores under an applied field. In the case of atomic or ionic polarization, the electric field displaces atoms or ions of a polyatomic molecule relative to each other. Orientational polarization occurs among the materials consisting of molecules or particles with a permanent dipole moment. To have permanent dipole moments, the material should be composed of molecules with an asymmetrical structure in which the centroid of the negative charge and that of the positive charge are not coincident.<sup>11</sup> The permanent dipole moments are randomly oriented in their equilibrium states of in paraelectric material; however, under the influence of an electric field they become aligned to the direction of the field, and then show macroscopic electric polarization. When the field is removed, the electric polarizations of paraelectric materials return to their non-polarized equilibrium state.

Ferroelectric materials have the electric polarization in their equilibrium states without help of an external electric field. This type of polarization is called the spontaneous polarization. Spontaneous polarization can be described as ordered orientational polarization in the absence of applied field, also spontaneous polarization is reversible. To have ordered polarization, the ferroelectric material should be crystalline. This implies that the crystal structure and dielectric properties of ferroelectric materials are interrelated. This state of spontaneous polarization is also temperature dependant. Roughly speaking, above the critical temperature, called the phase transition temperature,  $T_c$ , the spontaneous polarization disappears. In other word, at this  $T_c$  ferroelectric materials undergo phase transition from the ordered phase, ferroelectric, to disordered phase, paraelectric as temperature increases, and vice versa when temperature decreases. In the remainder of this chapter, we will look at the dielectric phase transition of ferroelectric materials described by Landau-Ginzburg-Devonshire (LGD) thermodynamic free energy model developed from the Landau theory of continuous phase transitions, and also look at the reversibility of the spontaneous polarization with respect to the applied field in a typical ferroelectric hysteresis loop.<sup>12,13,14</sup>

### Phase Transition<sup>10,11</sup>

The Landau theory of continuous phase transitions is based on a thermodynamic free energy, which can be expressed as a power series in a small quantity called the order parameter. Ginzburg developed Mean-field models of the continuous ferroelectric phase transition,<sup>15,16,17</sup> which treat the polarization as an order parameter in the Landau theory.

A similar treatment was developed by Devonshire shortly thereafter.<sup>18,19,20</sup> For this dissertation LGD formalism for the uniaxial case, where the electric polarization and an applied field are parallel to the unique crystalline axis, shall only be discussed.

The LGD form of the Gibbs free-energy density can be written<sup>15,16</sup>

$$G = G_0 + \frac{\alpha}{2}P^2 + \frac{\beta}{4}P^4 + \frac{\gamma}{6}P^6 - PE \quad (1)$$

where  $E$  is the electric field,  $G_0$  is the free-energy density of the paraelectric phase at zero field, and the expansion coefficients  $\alpha$ ,  $\beta$ , and  $\gamma$  are in general dependent on temperature and pressure. The equilibrium condition corresponds to the absolute minimum of the free-energy density. The Landau theory requires that the first coefficient  $\alpha$  vanish at the so-called Curie temperature  $T_0$ , so that the simplest form for the first coefficient is

$$\alpha = \frac{1}{\epsilon_0 C} (T - T_0)$$

(2)

where  $T$  is the temperature,  $C > 0$  is the Curie-Weiss constant, and  $\epsilon_0$  is the permittivity of free space. The coefficients  $C$ ,  $\beta$ , and  $\gamma$  are generally assumed independent of temperature, but it is often best to confine the LGD analysis to temperatures near the Curie temperature to ensure this. The sign of the second coefficient  $\beta$  determines whether the transition is first-order ( $\beta < 0$ ) or second-order ( $\beta > 0$ ).

The constitutive relation between polarization  $P$  and electric field  $E$  is obtained from the minimum of the free energy Eq.1, yielding the expression.

$$E = \alpha P + \beta P^3 + \gamma P^5 \quad (3)$$

If the electric field is not high, we can use first-order approximation for paraelectric phase where  $P$  is small, then we have

$$E = \alpha P = \frac{1}{\epsilon_0 C} (T - T_0) P$$

(4)

combined with the definition of  $\alpha$ , Eq.2.  $P$  for  $T > T_c$  can be expressed as

$$P = \chi \epsilon_0 E \quad (5)$$

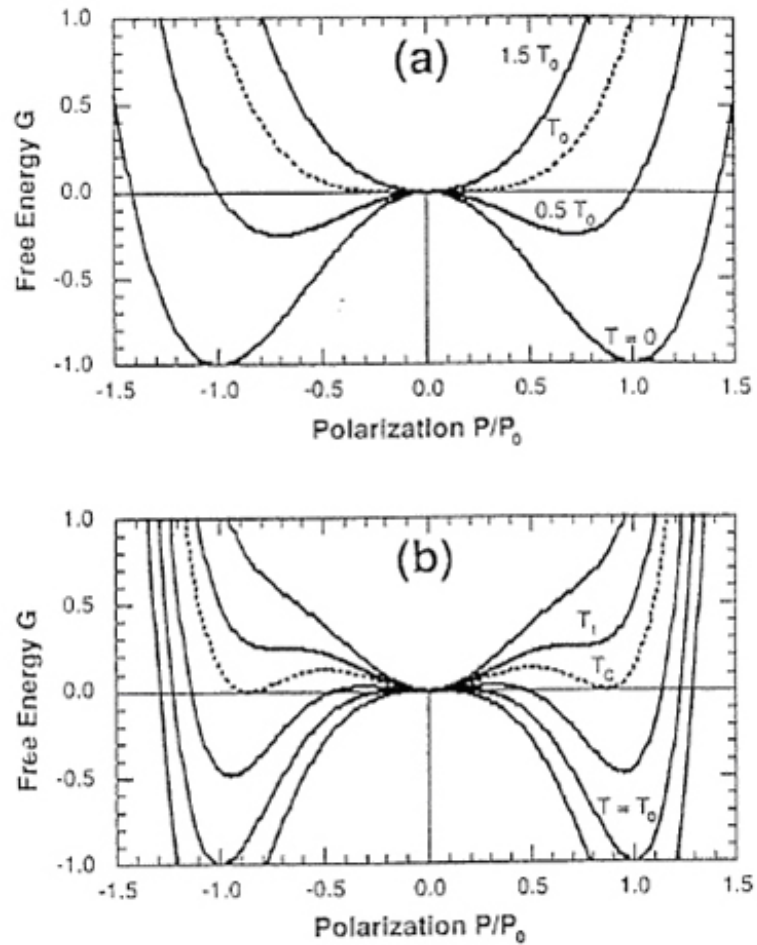
Thus, from Eq. 4 and Eq. 5 the inverse polarizability in the paraelectric phase.

$$\frac{1}{\chi} = \epsilon_0 \frac{\partial E}{\partial P} = \frac{(T - T_0)}{C} \quad (T > T_c) \quad (6)$$

This is the so-called Curie-Weiss law, which is built into the definition of  $\alpha$ . The total dielectric constant of the medium  $\epsilon = \epsilon_\infty + \chi$  contains contributions  $\epsilon_\infty$  from the background electronic polarizability.

The second-order LGD ferroelectric is described by the free energy density in Eq.1 with expansion coefficient values  $C > 0$ ,  $\beta > 0$ , and  $\gamma = 0$ . The second-order LGD ferroelectric has two distinct phases, a nonpolar paraelectric phase and a polar ferroelectric phase. The free-energy plots in Figure 1a illustrate the distinction between these phases. At temperatures above the equilibrium phase transition temperature  $T_C = T_0$ , the free energy has a single minimum free energy at  $P = 0$ . This is the paraelectric phase, which has no spontaneous polarization at zero applied electric field.





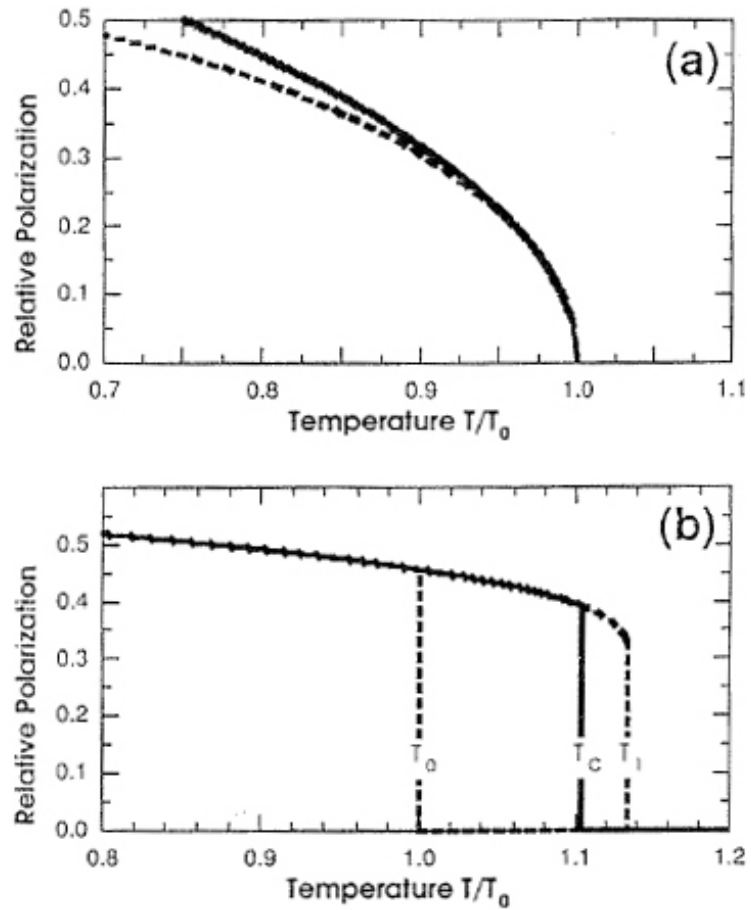
**Figure 1.1** shows Free-energy density (Eq.1) from the LGD phenomenology at various temperatures and zero electric field. The temperature increases from bottom to top. (a) Second-order transition: (b) first-order transition; this figure was published in *Ferroelectric and dielectric thin films*, S. Ducharme *et al.*, p547, Copyright Academic Press (2002).

At temperatures below  $T_C$  in zero field, there are two equivalent minimum free energy, where the magnitude of the equilibrium polarization in zero electric field, the spontaneous polarization is

$$P_s = \pm \sqrt{\frac{|\alpha|}{\beta}} = \sqrt{\frac{(T_0 - T)}{\epsilon_0 C \beta}} \quad (T < T_C) \quad (7)$$

which is obtained by solving Eq. 3 when  $E = 0$ , and by ignore the 5<sup>th</sup> power term (remember  $\beta > 0$  here). The zero-field equilibrium polarization  $P(E = 0) = \pm P_s$  can point in either direction along the symmetry axis, corresponding to the two energetically equivalent states of the ferroelectric crystal at zero electric field. The spontaneous polarization in the ferroelectric phase decreases steadily with increased temperature and vanishes at the transition temperature, as shown in Figure 2a. At a second-order phase transition, the order parameter (spontaneous polarization) decreases smoothly to zero.

The first-order LGD ferroelectric is described by the free energy density in Eq.1 with expansion coefficient values  $\beta < 0$  and  $\gamma > 0$ . The first-order transition is more complicated than the second-order transition. The representative characteristics of the first-order transition are firstly the discontinuous transition at the Curie temperature  $T_0$ , and secondly the actual phase transition  $T_C$  is not the same as  $T_0$ , and thirdly there is a region of metastable phase coexistence. We can calculate  $T_1$  the temperature above which there is no more ferroelectric phase. These characteristic temperatures  $T_0$ ,  $T_C$ , and  $T_1$  are manifest in thermal hysteresis of first-order transition materials.



**Figure 1.2** shows spontaneous polarization from the mean-field ferroelectric models: (a) the second-order LGD ferroelectric from Eq. 7 (solid Line) and the second order mean-field Ising model (dashed line); (b) the first-order LGD ferroelectric, where the solid lines denote equilibrium solutions and the dashed lines denote metastable solutions; this figure was published in *Ferroelectric and dielectric thin films*, S. Ducharme *et al.*, p548, Copyright Academic Press (2002).

The free-energy plots of the first-order LGD ferroelectric is shown in Figure 1b. For the minimum values of G for this is

$$\frac{dG}{dP} = \alpha P - |\beta| P^3 + \gamma P^5 = 0 \quad (8)$$

and the solution of Eq.8 yields  $P_s = 0$  and

$$P_s = \pm \left\{ \frac{1}{2\gamma} \left[ |\beta| \pm (|\beta|^2 - 4\gamma\alpha)^{1/2} \right] \right\}^{1/2} \quad (9)$$

Eq.9 shows that when  $\alpha = 0$  ( $T = T_0$ ),  $P = \pm (|\beta| / \gamma)^{1/2}$ , and this implies that  $P_s$  changes discontinuously from  $P_s = +(|\beta| / \gamma)^{1/2}$  or  $P_s = -(|\beta| / \gamma)^{1/2}$  to  $P = 0$  abruptly at  $T = T_0$ , this is the nonequilibrium case, and this is the distinctive characteristic of the first order phase transition. Now let us look at the actual transition temperature  $T_C$ , this is the equilibrium case, which is higher than the Curie temperature  $T_0$ . The  $T_C$  can be calculated by imposing the condition that the free energy of the polar and the nonpolar phases are equal at  $T_C$ . This leads Eq.1 to

$$\frac{1}{2} \frac{(T_C - T_0)}{\epsilon_0 C} P^2 - \frac{1}{4} |\beta| P^4 + \frac{1}{6} \gamma P^6 = 0 \quad (10)$$

And, the applied field is set equal to zero. This gives

$$E = \frac{dG}{dP} = \frac{(T_C - T_0)}{\epsilon_0 C} P - |\beta| P^3 + \gamma P^5 = 0 \quad (11)$$

From Eq. 10 and 11, we obtain

$$P_s = \pm \left[ \frac{3}{4} \left( \frac{|\beta|}{\gamma} \right) \right]^{1/2} \quad (12)$$

$$T_C - T_0 = \frac{3}{16} \varepsilon_0 C \frac{|\beta|^2}{\gamma} \quad (13)$$

This results show that the discrepancy between the actual phase transition temperature and the Curie temperature is  $(3/16)\varepsilon_0 C \beta^2 / \gamma$ , and the magnitude of the discontinuous change in spontaneous polarization is  $\sqrt{3|\beta|/4\gamma}$ . Lastly,  $T_1$  can be calculated by applying the minimum free-energy condition that only one value of P above  $T_1$ , corresponding to the condition

$$|\beta|^2 - 4\gamma \frac{T_1 - T_0}{\varepsilon_0 C} = 0 \quad (14)$$

thus

$$T_1 = T_0 + \frac{1}{4} \frac{\varepsilon_0 C \beta^2}{\gamma} \quad (15)$$

Figure 2.b summarizes the thermal hysteresis. It shows that if a crystal is not in equilibrium, the paraelectric phase can persist on cooling through  $T_C$  as far as  $T_0$  due to the local minimum at  $P=0$ , and the ferroelectric phase can persist on heating through  $T_C$  as far as  $T_1$  due to the local minima at  $\pm P_s$ .

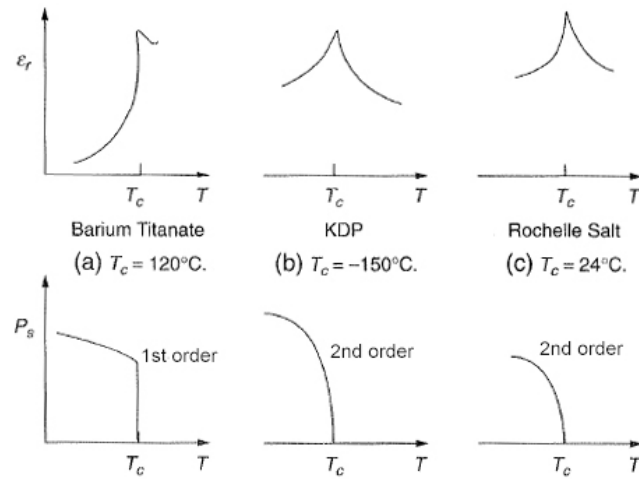
### Dielectric Anomaly<sup>11</sup>

The Curie-Weiss law,  $\varepsilon = C/(T - T_0)$  in paraelectric phase from Eq.6 with ignoring the background electronic polarizability predicts anomalous behavior of the

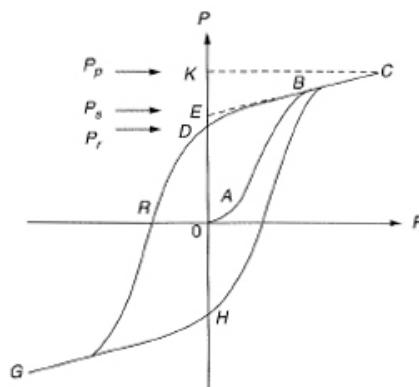
dielectric constant near the Curie temperature. In fact, the dielectric constants of ferroelectric materials show very rapid increases around the phase transition and result in a high peak. Therefore, the high peak of the dielectric constants is used to determine the phase transition temperatures of the materials (see Figure 3)

### Ferroelectric Hysteresis loop<sup>11</sup>

The most prominent features of ferroelectric properties are hysteresis and nonlinearity in the relation between the polarization  $P$  and the applied electric field  $E$ . A typical hysteresis loop is shown schematically in Figure 4. When the field is small, the polarization increases linearly with the field. This is due mainly to field-induced polarization because the field is not large enough to cause orientation of the domains (portion OA). At fields higher than the low-field range, polarization increases nonlinearly with increasing field because all domains start to orient toward the direction of the field (portion AB). At high fields, polarization will reach a state of saturation corresponding to portion BC, in which most domains are aligned toward the direction of the poling field. Now, if the field is gradually decreased to zero, the polarization will decrease, following the path CBD. By extrapolating the linear portion CB to the polarization axis (or zero-field axis) at E, OE represents the spontaneous polarization  $P_S$  and OD represents the remanent polarization  $P_r$ . The linear increase in polarization from  $P_S$  to  $P_p$  is due mainly to the normal field-induced dielectric polarization.  $P_r$  is smaller than  $P_S$  because when the field is reduced to zero, some domains may return to their original position.



**Figure 1.3** shows schematic illustration of the variation of the dielectric constant  $\epsilon_r$  and the spontaneous polarization of  $P_s$  with temperature for three typical ferroelectric crystals; (a) Barium titanate ( $\text{BaTiO}_3$ ) with  $T_c = 120^\circ\text{C}$ , (b) Potassium dihydrogen phosphate (KDP,  $\text{KH}_2\text{PO}_4$ ) with  $T_c = -150^\circ\text{C}$ , and (c) Potassium Sodium tartrate-tetrahydrate (Rochelle Salt,  $\text{KNaC}_2\text{H}_4\text{O}_4 \cdot 4\text{H}_2\text{O}$ ) with  $T_c = 24^\circ\text{C}$ ; this figure was published in Dielectric phenomena in Solids, Kwan Chi Kao, p216, Copyright Elsevier, Inc (2004).



**Figure 1.4** shows a schematic diagram of a typical ferroelectric hysteresis loop; this figure was published in Dielectric phenomena in Solids, Kwan Chi Kao, p217, Copyright Elsevier, Inc (2004).

For most ferroelectric materials, the component due to the normal field-induced dielectric polarization is very small compared to the spontaneous polarization; therefore, for most application, this component can be ignored and the saturation region is nearly flat in practice. The magnitude of the difference between  $P_p$  and  $P_s$  in Figure 4 is exaggerated for the purpose of clear illustration. The field required to bring the polarization to zero is called the coercive field  $E_C$  (portion OR on zero polarization axis). The hysteresis arises from the energy needed to reverse the metastable dipoles during each cycle of the applied field. The area of the loop represents the energy dissipated inside the specimen as heat during each cycle.

## 1.2 Ferroelectric Polymer: PVDF and P(VDF-TrFE)

Now, let us look at origin of the ferroelectricity of PVDF polymer, and its crystal structure and difference between PVDF and its copolymer with trifluoroethylene (TrFE), P(VDF-TrFE).

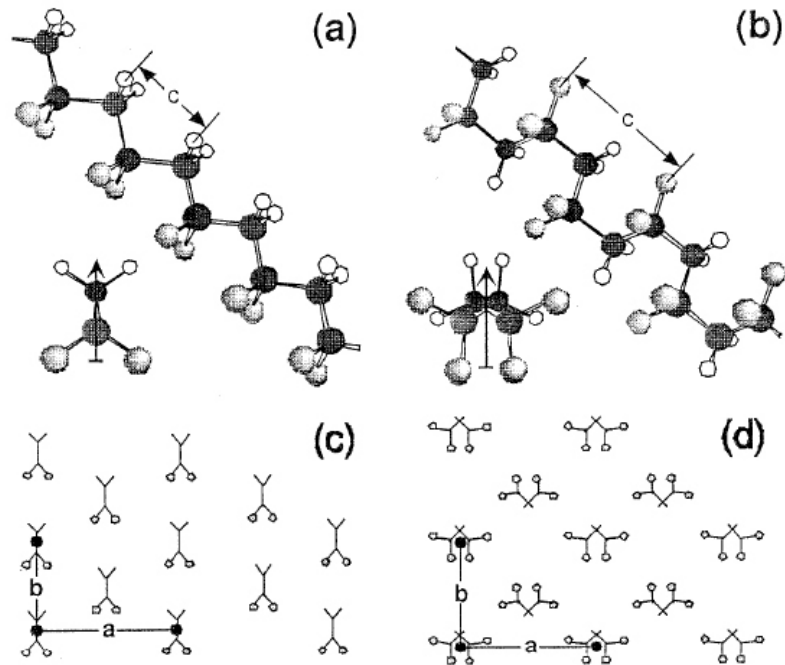
### Molecular and Crystal Structure of PVDF

The vinylidene fluoride  $C_2H_2F_2$  monomers form a linear carbon-carbon chain with structure  $-(CH_2-CF_2)-$ . The monomer has a dipole moment pointing roughly from the fluorines to the hydrogens. In the polymer chains  $(CH_2-CF_2)_n$ , the monomers arrange in a fashion to minimize the potential energy of the chains. There are two most common stable conformations. One is the all-trans  $TTTT$  conformation (see Figure 5.a), and the other is the alternating trans-gauche  $TGT\bar{G}$  conformation (see Figure 5.b). The trans



bond ( $T$ ) has a dihedral angle of approximately  $\sim 180^\circ$  and the left and right gauche bonds ( $G$  and  $\bar{G}$ ) have dihedral angles of approximately  $\pm 60^\circ$ . The all-trans  $TTTT$  conformation has a net dipole moment of about  $7.0 \times 10^{-30}$  C-m essentially perpendicular to the chain axis<sup>21</sup> and the alternating trans-gauche  $TGT\bar{G}$  conformation has  $4.0 \times 10^{-30}$  C-m and  $3.4 \times 10^{-30}$  C-m in perpendicular and in parallel to the chain respectively due to the inclination of dipoles to the molecular axis<sup>22</sup>.

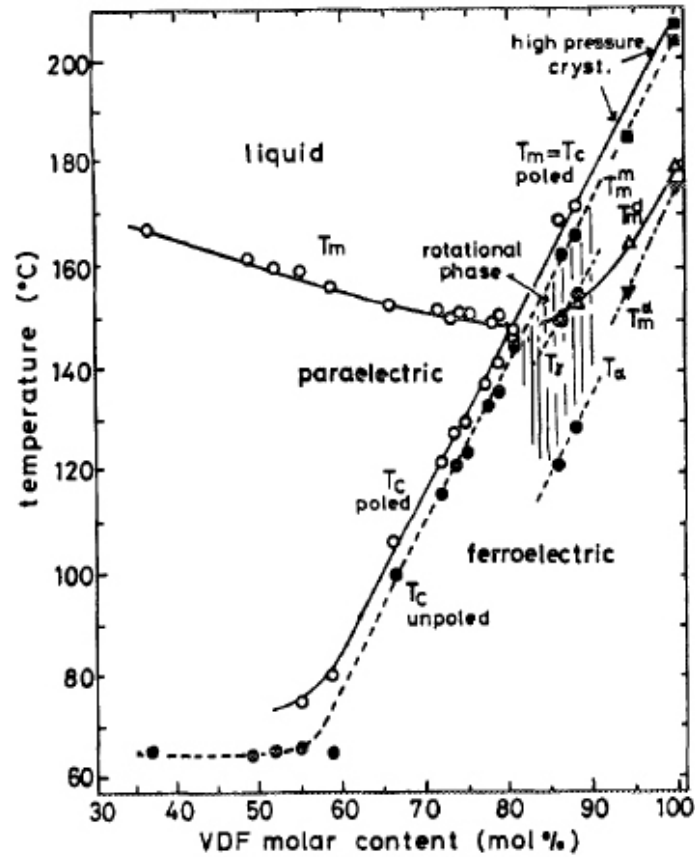
Crystal structure of the all-trans ( $TTTT$ ) conformation is called  $\beta$  phase, and it is ferroelectric phase.  $\beta$  phase is orthorhombic  $m2m$  structure with the chains along the crystal  $c$ -axis and the dipoles aligned approximately along the crystal  $b$ -axis as shown in Figure 5c.<sup>3,23,24,25</sup> This  $\beta$  phase is a uniaxial ferroelectric, as the polarization can be repeatably switched between opposite but energetically equivalent directions along the 2-fold  $b$ -axis. The  $\beta$  phase unit cell consists of two  $-(\text{CH}_2-\text{CF}_2)-$  formula units, one along the  $c$ -axis parallel to the chains (see Figure 5a) times two in the plane perpendicular to the  $c$ -axis (see Figure 5c). The unit cell dimensions are approximately  $c = 0.256$  nm along the chain axis,  $b = 0.491$  nm along the polarization direction, the 2-fold axis, and  $a = 0.858$  nm perpendicular to the chain axis and to the polarization.<sup>24</sup> Crystal structure of the alternating trans-gauche  $TGT\bar{G}$  conformation, called  $\alpha$  phase is paraelectric. The real paraphrase is closer to a random  $(TG)_{1/2}(T\bar{G})_{1/2}$  structure with no net dipole to the chain. The unit cell dimensions for  $\alpha$  phase are  $c = 0.462$  nm,  $b = 0.496$  nm, and  $a = 0.964$  nm.



**Figure 1.5** shows conformations and crystalline forms of PVDF: (a) in the all-trans conformation (inset, end view of a chain); (b) in the alternating trans-gauche conformation (inset, end view of a chain); (c) end-on view of the crystal structure of the ferroelectric  $\beta$  phase, composed of close-packed all-trans chains; (d) end-on view of the crystal structure of the paraelectric  $\alpha$  phase, composed of close-packed trans-gauche chains. Reprinted with permission from L. M. Blinov *et al.*, *Physics Uspekhi* **43**, 243 (2000) © “Uspekhi Fizicheskikh Nauk” 2000.

*P(VDF-TrFE) copolymer*

The degree of crystallinity for both  $\alpha$  phase and  $\beta$  phase of PVDF is approximately 50 %.<sup>26</sup> However, the crystallinity of copolymers of PVDF with trifluoroethylene (TrFE) can be improved over 90% by mechanical stretching or electrical polarization, which was not applicable to PVDF. The methods are only applicable to the films made by melting method, however PVDF can be made by solution method. Also, PVDF does not show the ferroelectric-to-paraelectric transition because the Curie temperature is about 20 °C higher than the melting temperature 205 °C.<sup>3,22</sup> Thus, there is no Curie temperature for PVDF. However, copolymers of PVDF with trifluoroethylene (TrFE, C<sub>2</sub>HF<sub>3</sub>) have the ferroelectric-to-paraelectric transition.<sup>27,28</sup> (see Figure 6) Addition of larger and less polar TrFE units suppresses the transition temperature by reducing the average dipole moment of the chains, expanding the lattice, and introducing defects.<sup>29,30</sup> The reduced average dipole moment of the copolymer chains can be compensated by improving its crystallinity comparing to PVDF. In case of the copolymer with 70% PDF and 30% TrFE, P(VDF-TrFE 70:30), it has the highest spontaneous polarization of about 0.1 C/m<sup>2</sup>, a first-order ferroelectric-paraelectric phase transition at approximately 100 °C.<sup>10</sup> A review of the first-order ferroelectric transition properties of P(VDF-TrFE) copolymers can be found in Furukawa's work.<sup>7,31</sup>



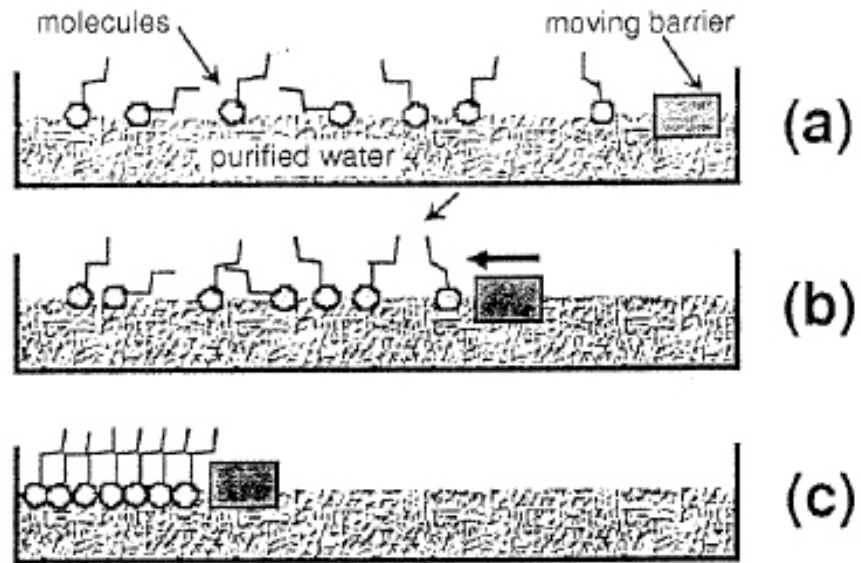
**Figure 1.6** shows phase diagram of P(VDF-TrFE): Curie temperature  $T_c$  and melting temperature  $T_m$  determined from DSC peaks in heating process are plotted. Solid squares are obtained for high-pressure crystallized films.  $T_m$  of mixed phase film and for drawn film are expressed by  $T_m^m$  and  $T_m^d$ , respectively.  $T_m^\alpha$  is melting temperatures of  $\alpha$ -phase spherulitic crystals.  $T_\alpha$  and  $T_\gamma$  are DSC peak temperatures of mixed phase appearing below melting point. The rotational phase is in the hatched region. Reused with permission from Keiko Koga, Journal of Applied Physics, 67, 965 (1990). Copyright 1990, American Institute of Physics.

### 1.3 Langmuir-Blodgett thin films of P(VDF-TrFE) copolymers

P(VDF-TrFE) films made by melting method showed possible improvement of the crystallinity by mechanical stretching and electrical poling. P(VDF-TrFE) copolymer films we have studied are not made by melting method. They are fabricated with Langmuir-Blodgett (LB) method and their x-ray results have shown good crystal structure<sup>32,33</sup>, even though the crystallinity of the films has not been quantitatively determined. The reliable layering properties have been observed.<sup>34</sup> LB technique is very simple, and it is easy to control the thickness of films, and good quality of samples can be reproducible with consistency.

#### Langmuir-Blodgett Films

Basic principle of Langmuir-Blodgett technique is amphiphilic property of molecules, such as fatty acids. Irving Langmuir performed systematic investigations of the behavior of fatty acid molecules on water surface, confirming the monomolecular nature of the films.<sup>10,35</sup> The molecular monolayers on the water surface are called “Langmuir” films. The dispersed Langmuir films on the water can be compressed using a barrier. (see Figure 7) The densely formed Langmuir film on the water surface now can be transferred to a solid substrate, and they are called “Langmuir-Blodgett”(LB) films. Langmuir film transfer can be done by both vertical and horizontal dipping. The horizontal dipping is also called the horizontal Langmuir-Schaefer method.



**Figure 1.7** shows formation of a dense monolayer confined to a water (or other liquid) surface by; (a) dispersal of molecules at low area density; (b) two-dimensional compression by sweeping a movable barrier across the liquid surface; (c) holding the monolayer at constant pressure with the barrier; this figure was published in *Ferroelectric and dielectric thin films*, S. Ducharme *et al.*, p556, Copyright Academic Press (2002).

*Langmuir-Blodgett Fabrication of P(VDF-TrFE) Films*

P(VDF-TrFE) copolymers are not amphiphilic, however, they consist of macromolecules with low solubility in water, and readily form metastable monolayers on a water subphase.<sup>10,36</sup> P(VDF-TrFE) copolymer films used for the research presented in this dissertation were fabricated with a NIMA model 622C automated LB trough. The routine sample fabrication procedures were as follows. The cleaned trough was filled with de-ionized pure water with a resistivity of 18 M $\Omega$ . Then, prepared copolymer solutions in DMSO with 0.01 ~0.06 % weight concentrations were dispersed on the water surface. The dispersed copolymer solutions became a thin film on the water, and then the film was to be compressed at a rate of 20~60 cm<sup>2</sup>/min by two barriers from the outside towards the center of the trough where the pressure sensor was placed. The film compression was performed under the pressure control. The target pressure for the films was 5 mN/m, which is well below the collapse pressure. Once the target pressured was reached, the copolymer films on the water were transferred to a desired substrate. The transferring method we used was the horizontal Schafer method.

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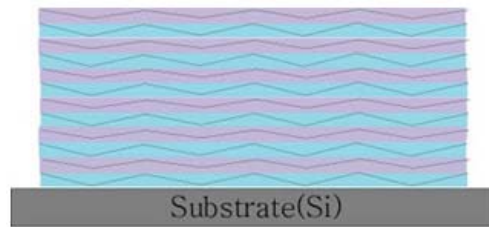


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## Chapter 2 Sample Characterization

The ferroelectric properties of LB thin films of P(VDF-TrFE 70:30) copolymers with a range of 50~200 nm thick, corresponding to 30~100 LB layers had been thoroughly studied and reported earlier.<sup>1,2</sup> After this establishment, some of the characterization experiments have become our routine diagnostic measurements, such as x-ray diffraction (XRD), capacitance vs. temperature (CT), capacitance vs. DC voltage (CV, butterfly curve), and etc. The results of the diagnostic measurements are used to determine the qualities of newly made samples in the lab.

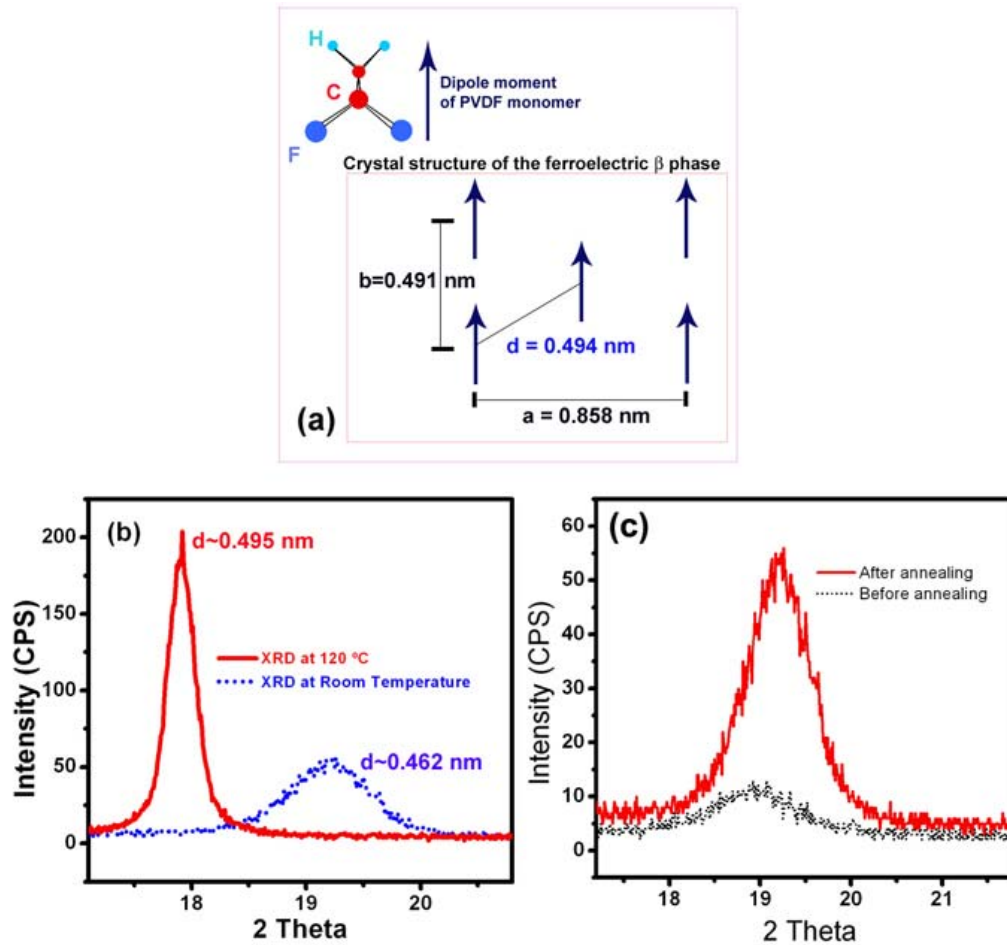
According to the purpose of the diagnostic measurements mentioned above, proper construction of samples is needed. There are three different types of samples based on their configuration: one is thin films, the second is self-assembly structure (Nanomesas), and the third is capacitors of both thin films and nanomesas. In this chapter, the three types of samples are introduced with along their routine characterization measurements. In addition to that, thickness measurements of thin films with x-ray reflectivity and observation of nanomesa formation during annealing with atomic force microscopy (AFM) are discussed in this chapter, and these measurements were done for the first time in this study.



**Figure 2.1** show a sample configuration of simple continuous films deposited on Si substrate.

## 2.1 Thin Films

The configuration of thin films (Fig. 2.1) is the simplest form of samples that we study. Thin films are constructed simply by depositing LB films of P(VDF-TrFE) copolymer on a cleaned smooth substrate, such as Si wafer and highly ordered pyrolytic graphite (HOPG) according to the procedure of Langmuir-Scheafer technique introduced in section 1.3. Si wafer is the most commonly used substrate for structural studies of thin film in our lab. Highly ordered pyrolytic graphite substrates (HOPG) are used for specialized studies such as scanning tunneling microscopy (STM), or piezoelectric force microscopy (PFM)<sup>3</sup> where the electrical grounding of samples during the measurements is crucial. Thin films on Si wafer with the simple configuration (Fig. 2.1) are used to characterize the crystal structure and the thickness of thin films with x-ray diffraction (XRD) and x-ray reflectivity (XRR), respectively. XRD has already been one of our routine diagnostic measurements, however, XRR was first tried during the study for this dissertation. In this section XRD and XRR will be briefly introduced, and the new results of XRR measurements will discussed in detail later in the section 2.4.



**Figure 2.2** (a) shows schematic ferroelectric structure of PVDF copolymer crystal structure based on Legrand's report in *Ferroelectrics* **91**, 303 (1989). The spacing between chains indicated as  $d$  is what we measure with the vertical XRD with our P(VDF-TrFE) copolymer LB thin films: (b) shows two XRD data taken from 20 LB layers of 50:50 at room temperature and at 120 °C as indicated on the figure. At room temperature the film is in ferroelectric,  $\beta$  phase where dipole moments are in order and at 125 °C the films is in paraelectric,  $\alpha$  phase. In  $\alpha$  phase, dipole moments are not in order anymore (see chapter 1), and it results in expanded layer spacing: (c) shows XRD measurements before and after annealing on 20 LB layers of 50:50 copolymer on Si. Annealing condition was 135 °C for 2 hours

*X-ray Diffraction (XRD)*

What we measure with XRD is the out-of-plane layer spacing<sup>4</sup> of LB thin films of P(VDF-TrFE) copolymers. The layer spacing,  $d$  of 70:30 copolymer is approximately 0.45 nm in ferroelectric phase and 0.48 nm in expanded paraelectric phase.<sup>5</sup> The Figure 2.2b shows XRD peaks taken from 20 LB layers of 50:50 copolymer sample measured at room temperature (ferroelectric  $\beta$  phase) and at 125 °C (paraelectric  $\alpha$  phase) with a Rigaku theta-two-theta diffractometer with  $K_{\alpha}$  radiation from a fixed copper anode,  $\lambda=1.54 \text{ \AA}$ . The unit cell dimensions obtained from a bulk sample of PVDF polymer are  $c = 0.256 \text{ nm}$  along the chain axis,  $b = 0.491$  along the polarization direction, the 2-fold axis, and  $a = 0.858 \text{ nm}$  perpendicular to the chain axis.<sup>6</sup> The configuration of this structure viewed from [001] direction is illustrated in Figure 2.2a. The measured spacing  $d$  (110) peak of 50:50 copolymer was  $\sim 0.462 \text{ nm}$  in the ferroelectric  $\beta$  phase, and  $\sim 0.495 \text{ nm}$  in the paraelectric  $\alpha$  phase as shown in Figure 2.2b. Though the dimension of  $d$  is very similar to the spacing  $b$  (010) peak, this peak is forbidden peak to be measured. As Figure 2.2a and b clearly presents, XRD measurements show us the crystal structure of thin films.

The last step of the thin film preparation is annealing. Annealing enhances the crystallinity of films and ferroelectric properties. The annealing effect on P(VDF-TrFE 70:30) LB films has been reported.<sup>7</sup> (The shorter name 70:30 for P(VDF-TrFE 70:30) will be used, and similarly for all the copolymers with different contents.) The example of annealing effect on a thin film sample of 50:50 copolymer is shown in Figure 2.2c

with XRD data before and after annealing as labeled. The increased intensity of XRD after annealing clearly shows the improvement of the crystallinity of the 50:50 copolymer thin film. The improvement is approximately a factor of 4, and the annealing was done at 135 °C for 2 hours.

The absolute percentage of crystallinity of a sample cannot be determined by this XRD measurement. However, a relative crystallinity comparison between different samples or before and after annealing is possible since the area under the XRD peak represents the amount of crystallized films. As a matter of fact, the XRD peak can be a good standard to examine the quality of newly made samples. P(VDF-TrFE) copolymer LB thin films are manually fabricated hence it is reasonable to question the reproducibility of films. The reproducibility of films is in fact excellent. Consistent results of XRD peak and dielectric measurements (which will be discussed later in the section 2.3) over a decade of study are a strong indication of it.

#### *X-ray Reflectivity (XRR)*

What we measure with XRR is the thickness of thin films, and also we can determine the LB layer transfer ratio as nm/layer by measuring thicknesses of thin film samples with various deposited layers. This transfer ratio shows us the layering property of LB thin films. Previously variable-angle spectroscopic ellipsometry (VASE) and capacitance measurement were used to measure sample thicknesses. The results of VASE and capacitance measurements showed sound layering property of copolymer LB films

over a range from 5 to 120 LB layers.<sup>8</sup> The film thickness determined by these measurements is approximately 1.8 nm per 1 LB layer (1.8 nm/layer). However, these measurements are indirect since the calculated refractive index of films were used for VASE data analysis, and then from the result of VASE, the dielectric constant of the films was determined for capacitance measurement analysis.<sup>8,9</sup> In addition to that, while our recent research focus is on thinner films, the statistics on the films less than 10 LB layers have not been sufficiently achieved in those studies since VASE and capacitance measurements are more accurate with thicker samples. Therefore, we chose x-ray reflectivity (XRR) measurement to determine more accurately the thickness of films with less than 20 LB layers.

We performed XRR measurements with a multi-purpose x-ray diffractometer, a Bruker-AXS D8 Discover with  $K_{\alpha}$  radiation from a fixed copper anode,  $\lambda=1.54 \text{ \AA}$ . XRR measurement will be discussed in detail later in the section 2.4. The thickness of 20 LB layers of 70:30 copolymer sample deposited on Si wafer was measured by XRR after annealing to be approximately 37 nm, which shows an excellent agreement to the previous studies. Therefore, a very simple, powerful, and direct thickness measurement, XRR can be routinely used as a diagnostic measurement.

## **2.2 Self-assembly Structure: Nanomesas**

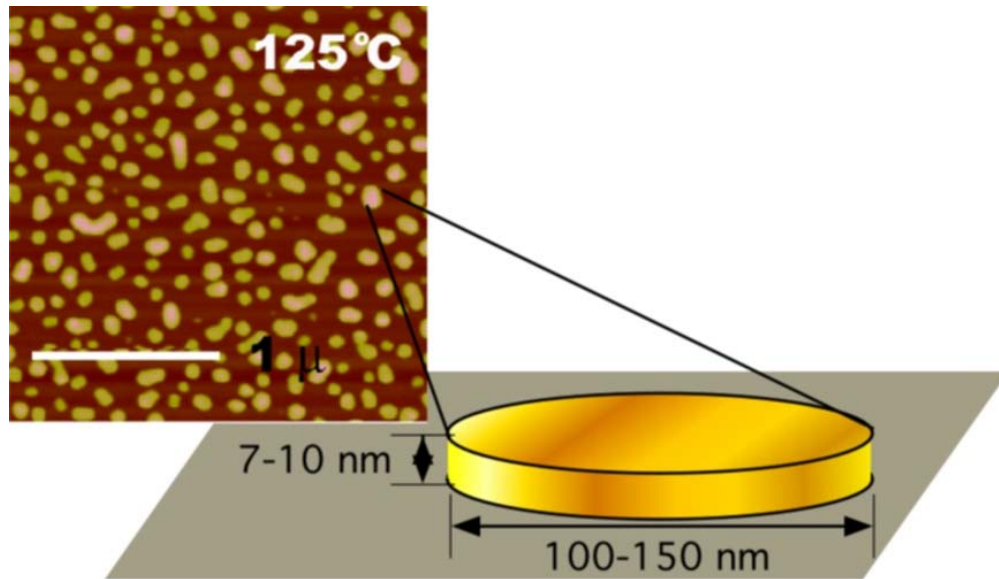
There has been very interesting new structure found by Bai *et al.* during investigation of annealing effect on thinner films with physical thickness less than 10

nm.<sup>10,11</sup> The new structure is ‘nanomesas’, which are self assembled structures formed after annealing of P(VDF-TrFE) copolymer. They are shaped as isolated islands with dimensions of approximately 100 nm in diameter, and 9 nm in thickness. Nanomesas shown in Figure 2.3 were obtained by annealing 1 LB layer of 70:30 copolymer sample deposited on Si wafer at 125 °C for 1 hour.<sup>10,11</sup> According to their study, P(VDF-TrFE) copolymers have plastic flow when they are in paraelectric phase, and nanomesas are manifest of it. Observation of nanomesa formation in real time has been separately performed and shown in the section 2.5 in detail.

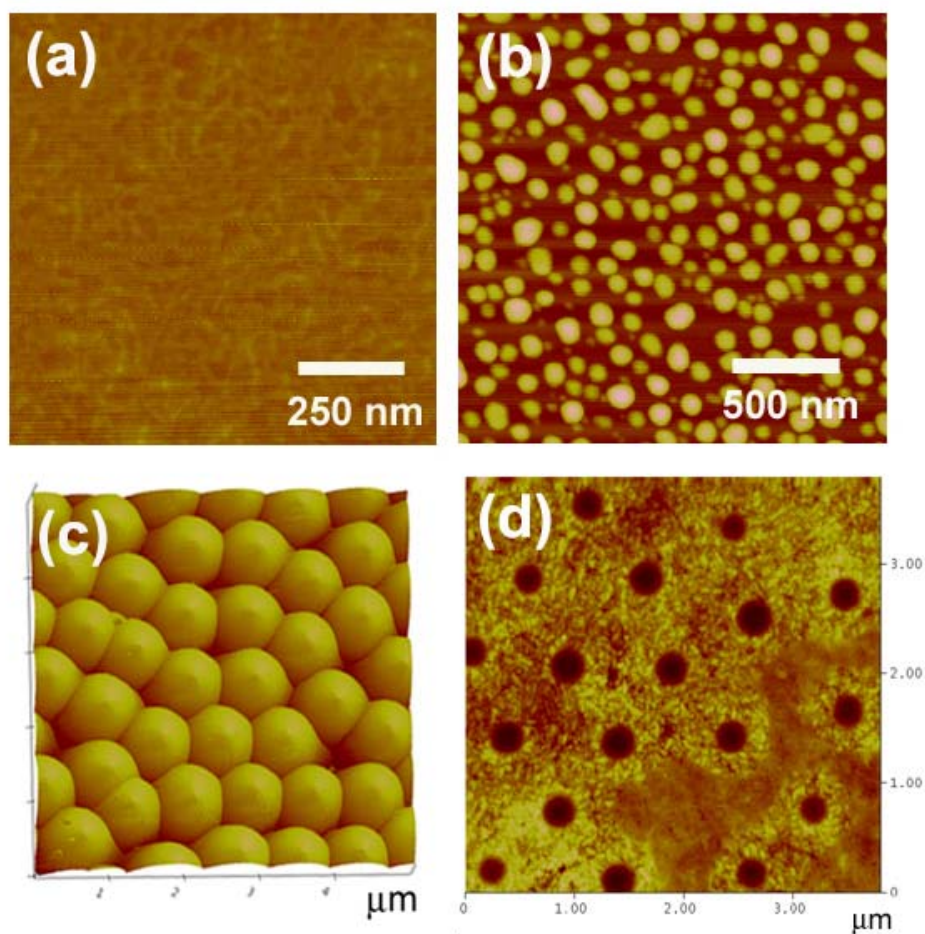
#### *Morphology of Sample: Atomic Force Microscopy*

Atomic force microscopy (AFM) is a very simple, convenient, and non-invasive tool to obtain topographical images of sample by using the attractive Van der Waals force between the AFM tip and the sample.<sup>12,13</sup> A Digital Instrument model Dimension 3100 AFM was used for our measurements. The AFM tip used was a Si tip consisting of a cantilever with nominal values of length, width, thickness, spring constant, and resonant frequency of 125  $\mu\text{m}$ , 35  $\mu\text{m}$ , 4  $\mu\text{m}$ , 40 N/m, 300 kHz, respectively. The scanning was conducted in tapping mode which is a non-contact mode. In this tapping mode the flexible cantilever of the AFM tip is oscillating at its resonance frequency with fixed set-up amplitude, which corresponds to the separation between the tip and the sample surface, and it is kept constant through the entire scanning. The interaction force between the tip and the sample surface depends on the distance between them, and so does the oscillation amplitude.





**Figure 2.3** is an AFM image of nanomesas formed from 1 LB layer of 70:30 copolymer sample on Si after annealing at 125 °C for 1 hour: this Figure 2.3 is reused with permission from Mengjun Bai, Applied Physics Letters, 85, 3528 (2004). Copyright 2004, American Institute of Physics.



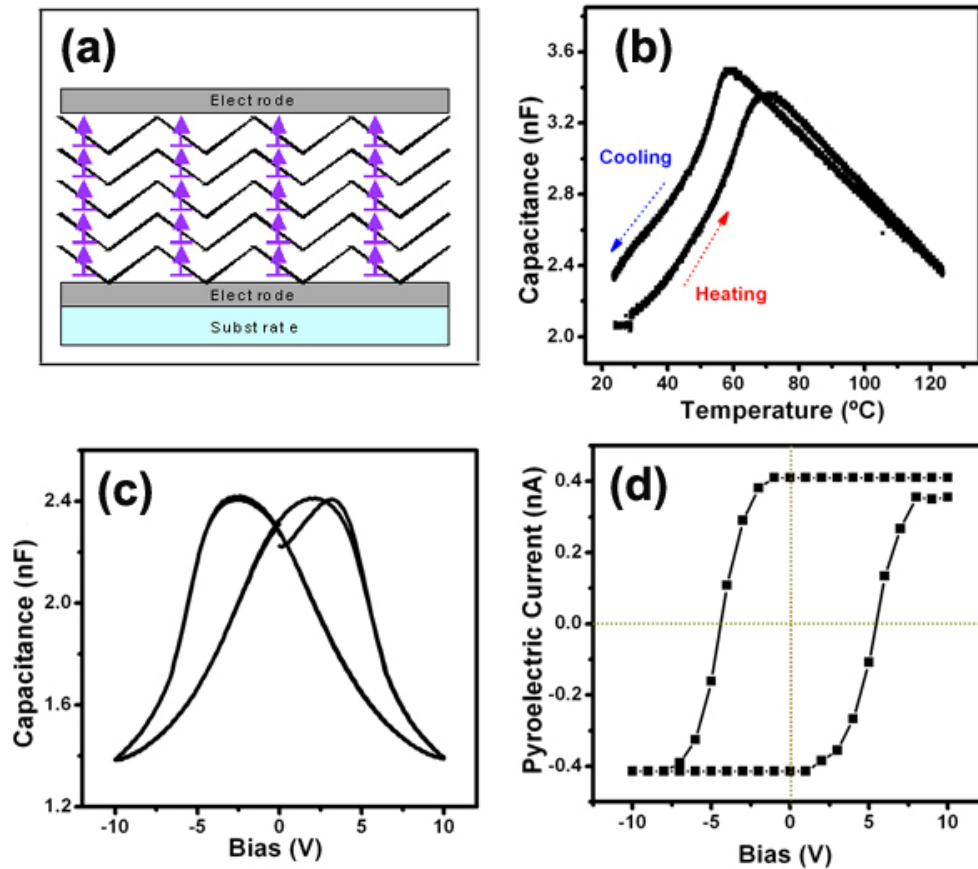
**Figure 2.4** (a) is an image taken from a fresh film of 1 LB layer of 50:50 copolymer on Si wafer: (b) is an image of nanomesas formed from the film shown in (a) after annealing it at 140 °C for 1 hour. First nanomesa observation was made on a 70:30 film shown in Figure 2.2b: (c) is an image of silica particles placed on top of a 70:30 copolymer sample with 22 LB layers: (d) is an image taken after the silica particles (c) were washed away. In between (c) and (d) the silica particles were pressed onto the film (see Appendix B).

The piezoelectric transducer where the AFM tip is connected controls the height of and the oscillation amplitude of the tip according to the topography of the sample surface. This is how an AFM collects the height information of the sample surface. The position of the tip is detected by laser beam which is deflected off the back to the cantilever.

Some AFM images are shown in Figure 2.4. After the first observation of nanomesas (see Figure 2.3 and 2.4b), not only to characterize nanomesas, but also nanofabrication of samples by using the mobility of P(VDF-TrFE) copolymers films in paraelectric phase has been our recent interest. For the nanofabrication study, observing the morphology change in films (see Figure 2.4d) is necessary, and AFM is an ideal tool for probing topography of thin film samples. One example of nanofabrication technique is pressing the films with silica particles (see Figure 2.4c) called nanoimprinting, and in Appendix B the nanoimprint work is discussed.

### **2.3 Capacitors**

To investigate the dielectric properties of films, capacitor samples were made by depositing LB layers of P(VDF-TrFE) copolymers on a glass substrate with the bottom and the top Al electrodes as shown in Figure 2.5a. For glass substrates, 1 mm thick, microscope slides, and 0.1 mm thick cover glasses are typically used. Firstly, on a clean glass substrate, the bottom electrodes, 1 mm width stripes, were evaporated. After that LB films of P(VDF-TrFE) copolymers films were deposited, and then, lastly top electrodes were evaporated.



**Figure 2.5** (a) show a sample configuration of capacitor films: (b) shows capacitance vs. Temperature taken from a same 20 LB layers of 50:50 copolymer capacitor sample, and it clearly presents the thermal hysteresis and dielectric anomaly peaks at phase transition temperatures upon heating and cooling: (c) is a butterfly curve which is capacitance measured with respect to DC voltage bias from a 15 LB layers of 70:30 copolymer capacitor sample. It clearly shows switching properties of the sample: (d) is pyroelectric current switching hysteresis loop taken also from a 15 LB layers of 70:30 copolymer capacitor sample. It shows both pyroelectricity and ferroelectric switching property of the sample. (Samples of data (b) and (c) are prepared under same conditions)

The annealing of capacitor samples has not shown clear effect, and it can be interpreted as the performance of capacitor films is not highly dependent on the crystallinity of films.

*Phase Transition: Capacitance vs. Temperature (CT)*

The presence of the ferroelectric-to-paraelectric phase transition of LB thin films of 70:30 copolymer has been confirmed by capacitance vs. temperature (CT) measurement.<sup>14,15,16,17</sup> The CT measurements showed the dielectric anomalies at the phase transition temperature according to the Curie-Weis law,  $\epsilon(T) = C/(T - T_c)$  where  $\epsilon$  is a dielectric constant,  $C$  is Curie-Weis constant,  $T$  is a measurement temperature, and  $T_c$  is the transition temperature. Also the CT showed thermal hysteresis upon heating and cooling. This thermal hysteresis is an indication of the first-order phase transition. Figure 2.5b is a CT measurement from a 50:50 copolymer capacitor film with 20 LB layers deposited on Si wafer. It clearly shows that thermal hysteresis, and the phase transition temperatures are approximately 70 °C upon heating and 60 °C upon cooling. The measurement was performed with an impedance analyzer, the model Hewlett-Packard 4192A. The AC signal used for the capacitance measurement was 0.1 V at 1 kHz. The sample was ramped with a rate of 1 °C/min up to 125 °C, and then cooled down to room temperature with the same ramping rate. This simple CT measurement is a very solid and reliable tool to determine the quality of samples by comparing the consistency of the measured phase transition temperatures and the peak heights of a newly made sample to the prototype sample.

Switching: Capacitance vs. Voltage Bias (CV) and Pyroelectric current hysteresis loop ( $I_p$ )

The CT measurement alone is not sufficient to prove the films are ferroelectric because, in principle, dielectric anomaly can be seen at most phase transitions, not necessarily ferroelectric phase transition, even though the thermal hysteresis phenomena can be a supporting proof of ferroelectricity. Therefore, any measurements show switching property of the films can be good complementary measurements to prove ferroelectricity of the films. The CV curves and pyroelectric current hysteresis loop ( $I_p$ ) measurements are the routine switching measurements for ferroelectric polymers and the results of those measurements on 70:30 copolymer films are have been reported.<sup>15,18</sup>

Figure 2.5c and d show respectively CV and  $I_p$  measurements recorded from two 70:30 copolymer capacitor samples prepared under the same conditions. The capacitors consisted of an area of 1 mm<sup>2</sup> with 15 LB layers of 70:30 copolymer films sandwiched between Al electrodes each about 100 nm thick on a cover glass substrate. CV was recorded with the impedance analyzer, 4192A with an AC signal of 0.1 V at 1 kHz. CV curves basically show the change of capacitance with respect to DC voltage. The DC voltage sweep was done at 1.5 V/min between +/-10V for two cycles. Polarization switching from one direction to the opposite direction occurs at voltages where the two peaks of capacitance are placed. The two peaks indicate the increased energy in the capacitor due to the switching, and the voltages where the switching occurs are called coercive voltages, and they are approximately  $2.6 \pm 0.2$  V. The direction of the

macroscopic polarization is relative to the direction of the applied DC voltage to the sample.

The pyroelectric current measurements reveal pyroelectric property of copolymer samples as well as switching property. As it was shortly mentioned in chapter 1, the ferroelectric materials also have pyroelectric and piezoelectric properties, which all originate from the noncentrosymmetric crystal structure.<sup>19</sup> The temperature increase or decrease causes a change in the spontaneous electric polarization in ferroelectric (or pyroelectric) materials. If the ferroelectric materials are in contact with metal electrodes, then the change in electric polarization will give rise to a change in compensating charges on the electrodes. Therefore, this change will produce a current in an external circuit. The switching of the polarization direction will be manifested as switching of the direction of the current in the circuit. For the pyroelectric current measurement shown in Figure 2.5d, He-Ne laser with 8 mW of the maximum power was used to change the sample temperature by illuminating the sample with the laser beam, chopped at a frequency of 2 kHz.<sup>20</sup> This modulated laser beam provides an oscillating temperature in the sample. Therefore, the pyroelectric current,  $I_p = d\vec{P}/dt = p(dT/dt)$  was produced, where  $p = d\vec{P}/dT$ , called the pyroelectric coefficient. The current was collected with a lock-in amplifier referenced to the chopping frequency. The lock-in amplifier is a model SR850 DSP from Stanford Research Systems. Before the current measurement the sample was poled with DC voltage shown in x axis of the plot. While the current was collecting, the DC voltage was removed namely field-off process, so the switching is from the steady

state polarization. The pyroelectric current hysteresis loop in Figure 2.5d clearly shows switching property of the copolymer films and the coercive voltage is  $5.0 \pm 0.5$  V, corresponding to the coercive field of  $185 \pm 15$  MV/m (taking into account the thickness of 1 LB layer is approximately 1.8 nm)<sup>21</sup>. It shows good agreement with previous reports.<sup>1,18,22</sup> The coercive voltage,  $V_C$  determined by CV curve is 50 % smaller than the value determined by  $I_P$  hysteresis loop. This could be due to slow switching nature of the P(VDF-TrFE) copolymer films. The complete switching of a whole sample may require 100s or more<sup>11</sup>, therefore CV measurement of 1.5 V/min rate likely show partial switching of the sample while  $I_P$  loop was taken for 15 minutes per 1 V step. This is also a general trend that the peak of CV occurs at lower voltages than  $V_C$  of  $I_P$  loop.

## 2.4 Thickness of P(VDF-TrFE) Thin Films

In this section thicknesses of P(VDF-TrFE) thin films consisting less than 20 LB layers measured with XRR will be discussed in detail as mentioned in the section 2.1.

### 2.4.1 Introduction

#### Motivation

A distinguishing property of Langmuir-Blodgett (LB) thin films of P(VDF-TrFE) copolymers is the easy thickness control in nanometer scale. As it has been introduced in Chapter1, LB films of P(VDF-TrFE) are deposited layer by layer by transferring the Langmuir copolymer film dispersed on the top of the water subphase. The multi-sample analysis of 70:30 copolymer films from 5 to 125 LB layers were investigated with



variable-angle spectroscopic ellipsometry (VASE) and capacitance measurements by Bai *et al.*<sup>21</sup> His work has shown a very nice linear relation between the measured thicknesses of the films vs. the number of layers deposited. This linear relation indicates the excellent layering property of copolymer thin films made by LB technique.

The layering transfer ratio of 70:30 copolymer films determined from ellipsometry was 1.8 nm/layer. The study, however, was heavily weighed with thicker films, more than 20 LB layers<sup>21</sup>, because spectroscopic measurements are less accurate with thinner samples. The study of thinner ferroelectric films requires more accurate measurements of their thicknesses. Therefore, we looked for new tool to measure the thickness of thinner films, and X-ray reflectivity (XRR) was chosen. XRR is an optimal tool to measure the thinner films because XRR is known for its atomic scale sensitivity, and the range of the measurable film thickness is from 0.1 to 500 nm.<sup>23</sup> XRR studies on other polymer thin films, and other LB films can be found in books written by M. Tolan<sup>24</sup>, and J. Daillant.<sup>25</sup>

#### Study Plan and Sample Preparation

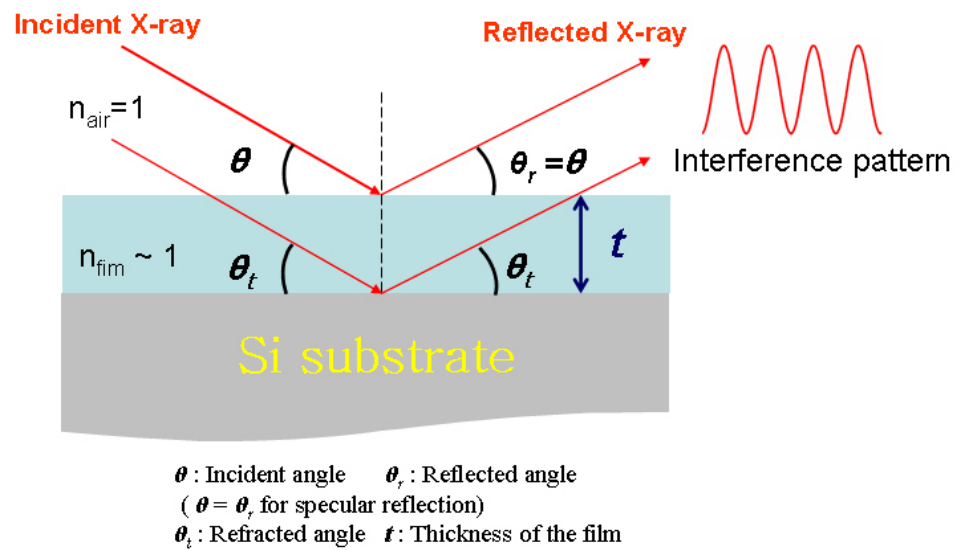
We designed the thickness study with two types of samples. The first type of samples had thicknesses typical of most commonly used copolymer samples in our lab, which are 15 to 30 LB layers, and to compare the results to the value, 1.8 nm per layer obtained by ellipsometry study. We expected that the results of the first type could give us a good comparison with ellipsometry results demonstrating on the usefulness of XRR

measurements on our LB copolymer thin film system. The second type consisted of thinner samples, from 1 to 11 LB layers, and then obtain the transfer ratio (or average thickness of films per layer) of the thinner films. XRR is not suitable for thin films with more than 5 nm of the roughness and XRR measurements on those rough films will result in null data. Therefore, obtaining useful XRR data themselves will manifest the quality of thinner LB copolymer films, such as the smoothness and the uniformity.

Three copolymers, 70:30, 50:50, and 80:20 were used to make films. Thin films of 20 LB layers as a prototype samples used in our lab, and a series of films with 1 to 11 LB layers of each copolymer were prepared. All samples were deposited on Si wafers, approximately 500 micron thick under the same deposition conditions on the LB trough, and those conditions are described in Chapter1. The size of the samples were approximately 1 ~ 4 cm<sup>2</sup>.

#### **2.4.2. Measurements**

XRR measurements were performed on a multi-purpose x-ray diffractometer, a Bruker-AXS D8 Discover with K<sub>α</sub> radiation from a fixed copper anode,  $\lambda=1.54 \text{ \AA}$ . The width of the slit used for all measurements was 0.2 mm. Scan conditions were set at the scan interval as 0.005 ° in  $2\theta$ , and the scanning rate as 1~5 sec/step. This scan condition is relatively slow scan compared to the typical scan condition 0.01° of scan interval and 1 sec/step of scanning time. For a series of thinner samples, XRR measurements were performed only on the fresh samples as deposited without annealing.



**Figure 2.6** illustrates the x-ray beam path in x-ray reflectivity measurement.

Since the thinner films undergo drastic morphology change after annealing,<sup>10,11</sup> comparing the thickness of the films before and after annealing are not meaningful. The films with 20 LB layers were measured both before and after annealing. The annealing was done at 135 °C for 2 hours in a closed thermal stage with heating and cooling rate of 1 °C/min.

#### *Relation of X-ray interference pattern and the Film thickness*

Similar to visible light, x-ray radiation is also refracted and reflected at the interface between two media and follows Snell's law as shown in Figure 2.6. The thin film shown in Figure 2.6 is a single material layer.<sup>a</sup> In this work all copolymer thin film samples were a single material layer system so they have only two interfaces; air-film, and film-substrate as schematically shown in Figure 2.6. Also, here we only treated the specular reflection, and did not account for diffuse reflection.

During the x-ray reflection measurement, the x-ray reflected from the air-film interface will interfere with the x-ray reflected from the film-substrate interface, and collected XRR data will show the interference pattern. Then, we can determine the thickness of the film by analyzing the interference pattern with the thin film interference equation for either the constructive interference or the destructive interference. However,

---

<sup>a</sup> This material layer is a different concept from the LB layer. A stack of a number of LB copolymer layers is one material layer which we consider homogeneous for the present study. This material layer we talk about in XRR study depends on the refractive index of the material similarly the mass density of the material.

the distinguishing property of x-rays from the visible optical light is the refractive index of films,  $n$  for x-ray radiation is very close to unity, and it is

$$n = 1 - \delta - i\beta \quad (2.1)$$

where  $\delta$  is the dispersion factor, and  $\beta$  is the absorption factor. The dispersion factor,  $\delta$  for soft materials is an order of  $10^{-5}$  and the absorption factor is approximately 3 orders less than the dispersion factor<sup>26</sup>, therefore we assume negligible x-ray absorption for this study. The effect of the refractive index being close to unity results in a rapid decrease in Fresnel reflectivity<sup>27</sup> (the reflectivity with respect to the angle of incidence) with angle  $\theta$  right after the critical angle  $\theta_c$ , below which the total reflection occurs. Therefore, the region of interest for XRR measurements is the small incident angle region where reflectivity is high in intensity. Note that the critical angle can be expressed in terms of the dispersion factor,  $\theta_c = \sqrt{2\delta}$ <sup>24,25</sup> and the Fresnel reflectivity of x-ray decays proportion to  $1/\theta^4$ , for  $\theta > 3\theta_c$ , where  $\theta$  is incident angle. Based on our measurements, XRR data became noisy above  $8^\circ$  in  $2\theta$  for films thinner than 10 nm, and above  $2^\circ$  in  $2\theta$  for films thicker than 10 nm. Since we are only working in the small angle region, the small angle approximation was applied for the analysis of XRR data.

The thickness,  $t$  of the thin films can be determined by using the thin film interference equation in general. Following equation is for the destructive interference

$$2t \sin \theta_i = \left(m - \frac{1}{2}\right)\lambda, \quad m = 1, 2, 3, \dots \quad (2.2)$$

where  $\lambda$  is the wavelength of x-ray, 1.54Å for our measurement, and  $\theta_i$  is the refracted angle of x-ray in the film (Fig. 2.6). Eq. 2.2 can be modified for XRR by applying the small angle approximation and Snell's law ( $\cos \theta = n \cos \theta_i$ ) into the equation. The modified thin film equation for destructive interference is as following

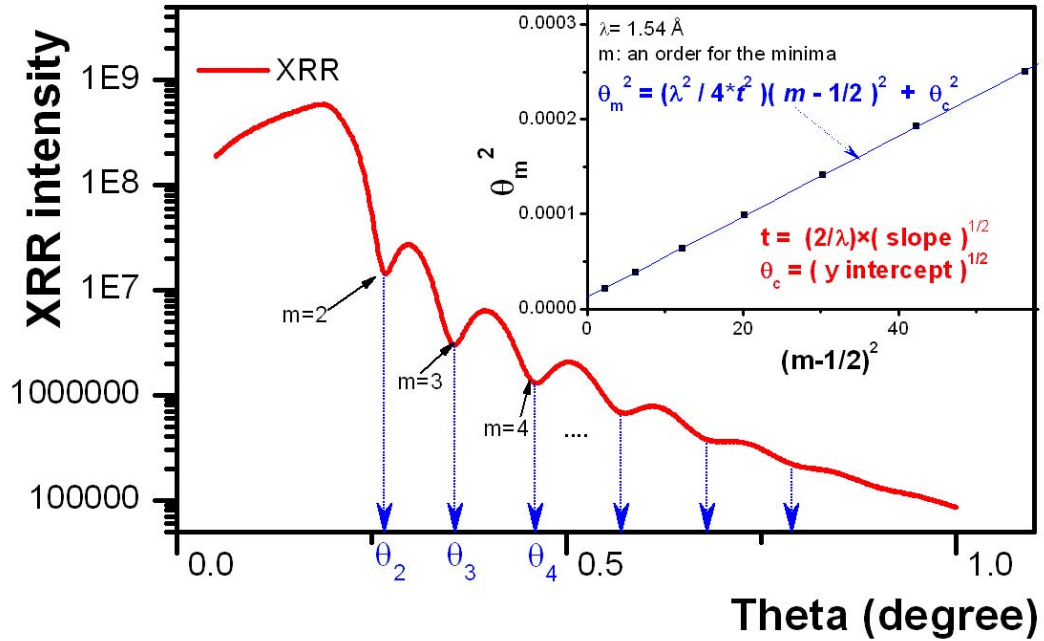
$$\theta_m^2 = \frac{\lambda^2}{4t^2} \left(m - \frac{1}{2}\right)^2 + \theta_c^2 \quad (2.3)$$

where  $\theta_m$  is the incident angle  $\theta$  indexed with the destructive interference fringe number  $m$ . Kiessig developed this method of analysis so it bears his name, the interference fringes in XRR are called Kiessig fringes, and the thickness determination method using the modified thin film interference equation (Eq. 2.3) is called the Kiessig fringe method.

In the rest of this section the Kiessig fringe method will be reviewed (see Fig. 2.7), and this method was our main tool for the study of film thickness by x-ray reflectivity.

### Kiessig Fringe Method

Firstly, XRR measurements were recorded, and then the minimum positions of the interference fringes,  $\theta_m$  in the  $\theta$  axis were read from XRR data. After finishing assigning  $\theta_m$ , the graph of  $\theta_m^2$  vs.  $(m - 1/2)^2$  was plotted and fit to the linear regression model, and then the parameters  $t$  and  $\theta_c$  were extracted from the slope and the y intercept of the fit, respectively. The film thickness  $t$  was calculated using Eq. 2.3, where slope =  $\lambda^2 / 4t^2$ .



**Figure 2.7** illustrates the Kiessig fringe method, the thickness method that we used for this study. XRR data from a 20 LB layer film of 70:30 copolymer is shown in the main plot. Positions of the minima of Kiessig fringes are indicated as  $\theta_m$ , and then they were plotted according to the modified Bragg equation and shown in the sub-plot.

As described above, the Kiessig fringe method is really simple. However, assigning the correct order  $m$  to the first apparent fringe in the data is very important, therefore it needs to be done carefully. That is because not always the first apparent fringe namely  $\theta_0$  in the data is the real first fringe  $m=1$ . The first few fringes can be placed below  $\theta_c$ , therefore hidden in the data. This depends on the thickness and the density of the sample. For example, for the XRR data shown in Figure 2.7,  $\theta_0$  is  $\theta_2$ , in other words the first apparent minimum is in reality the second destructive interference, or  $m=2$ . When  $\theta_0$  is correctly assigned, data points in  $\theta_m^2$  vs.  $(m-1/2)^2$  plot should make a straight line, especially at small angles, and when it is incorrectly assigned, it will result in a distortion of the straight line, and an incorrect thickness of the film. To choose correct order for  $\theta_0$  we plotted  $\theta_m^2$  vs.  $(m-1/2)^2$  with different  $\theta_0$ , and tested the straightness of  $\theta_m^2$  vs.  $(m-1/2)^2$  plot with the goodness of the line fit.

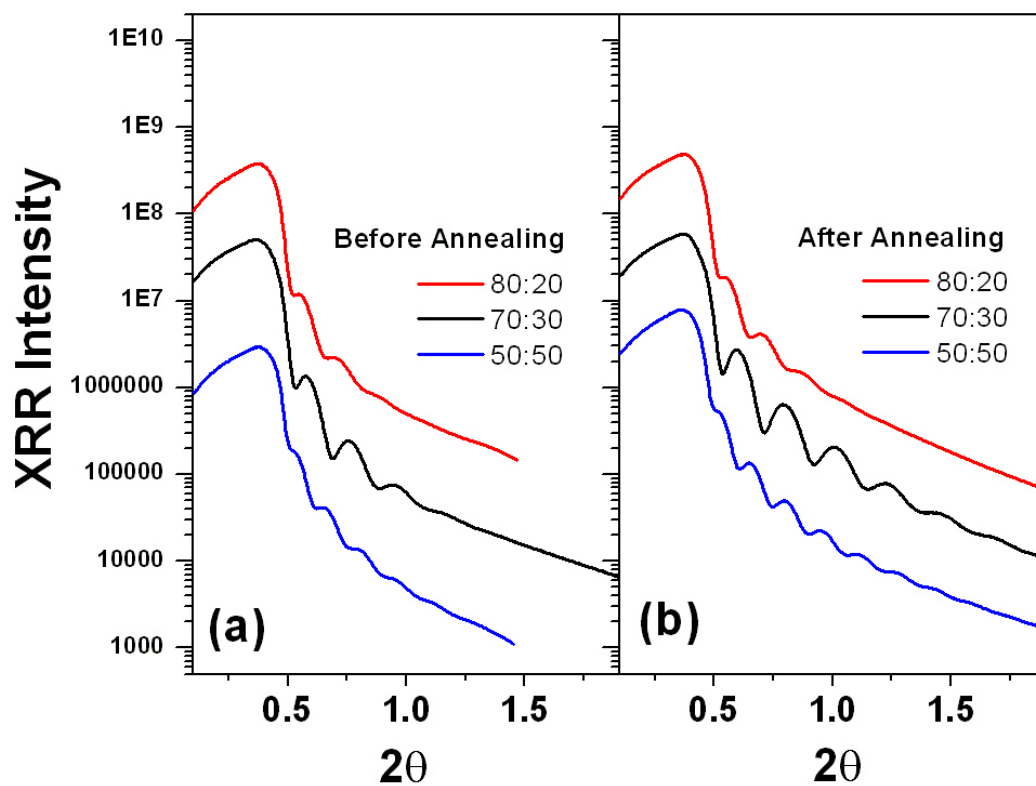
### 2.4.3 Results

All XRR data recorded for this study is shown in Figures 2.8 and 2.10. The thicknesses of all samples were determined by Kiessig fringe method introduced in the previous section, and the results are tabulated in Table 2.1. In case of the thinner samples, the transfer ratio (nm/layer) of each copolymer is shown rather than presenting thickness of all individual samples. The transfer ratio was determined by fitting a plot of ‘the thickness of film vs. the number of layers of the film’ for each copolymer films, as shown in Figure 2.11.

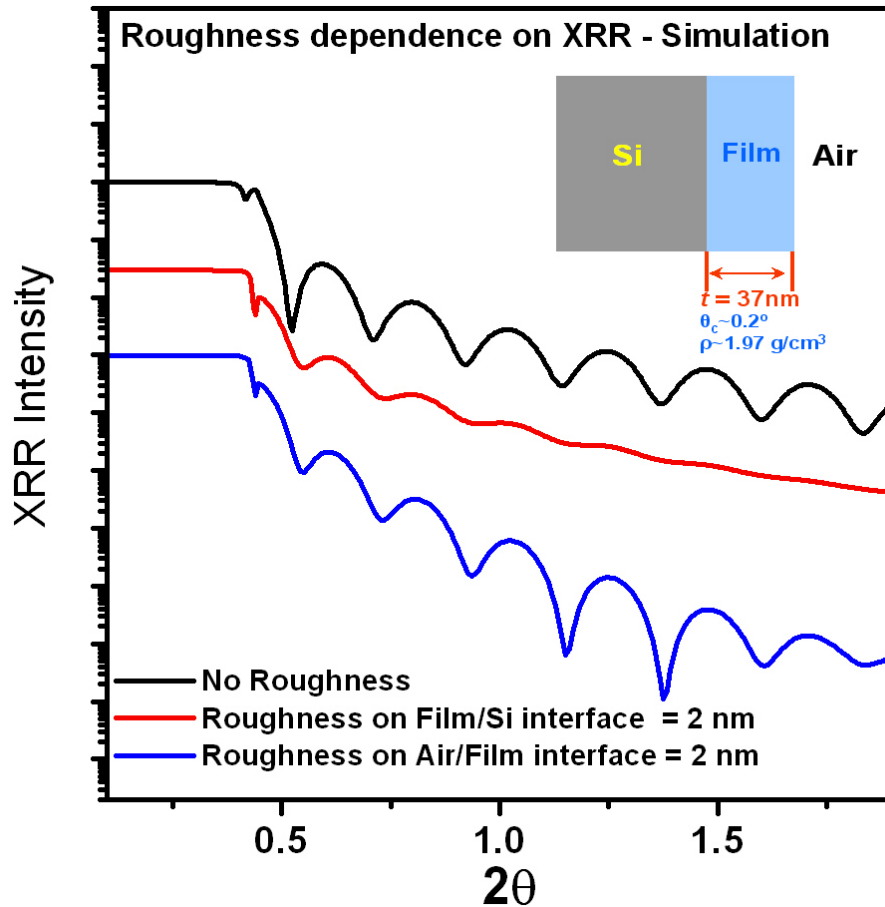


Table 2.1 Thickness and the critical angle of all samples were determined from XRR curves by using Kiessig Fringe method. For 20 LB layer samples, the determined values of individual samples are shown, and for a series of thinner films average transfer ratio, thickness per layer is shown. The series of thinner samples ranged from 1 ~ 11 LB layers,

Copolymers	Kiessig Fringe Method				
	20 LB films Before Annealing		20 LB films After Annealing		Thinner films as deposited
	$t$ [nm]	$\theta_c$ [degree]	$t$ [nm]	$\theta_c$ [degree]	$t$ [nm/layer]
50:50	$50.8 \pm 0.1$	$0.21 \pm$	$51 \pm 0.2$	$0.22 \pm$	$2.5 \pm 0.2$
70:30	$37.2 \pm 0.1$	$0.2 \pm$	$37.3 \pm 0.05$	$0.2 \pm$	$2.6 \pm 0.2$
80:20	$45.6 \pm 0.3$	$0.22 \pm$	$45.7 \pm 0.1$	$0.21 \pm$	$2.7 \pm 0.2$



**Figure 2.8** shows XRR data from 20 LB layers of each copolymer are shown here (a) before and (b) after annealing. The annealing was done at 135 °C for 2 hours.

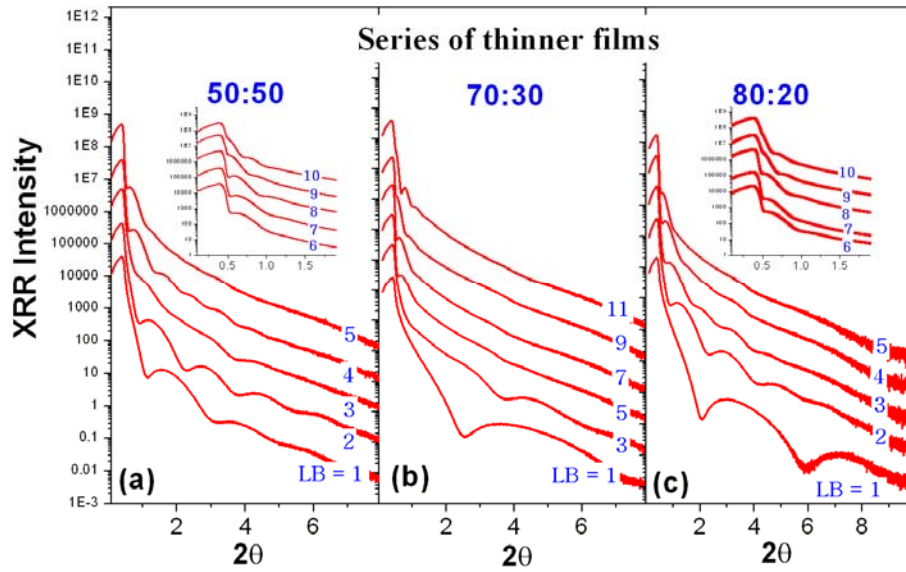


**Figure 2.9** shows three simulated XRR curves of a single layer thin film model. The thin film model has the thickness 37 nm, and the density  $1.97\text{ g/cm}^3$  corresponding to the critical angle approximately  $0.2^\circ$  when considering the film is 70:30 copolymer. As it is indicated on the plot, XRR in black is when there is no roughness in the sample, XRR in red is when there is about 2 nm of the roughness on the film-Si interface, and XRR in Blue is when there is about 2 nm of the roughness on the Air-film interface. This simulation convinced us that the smeared fringes in our data should be dominantly from the film-Si interface roughness.

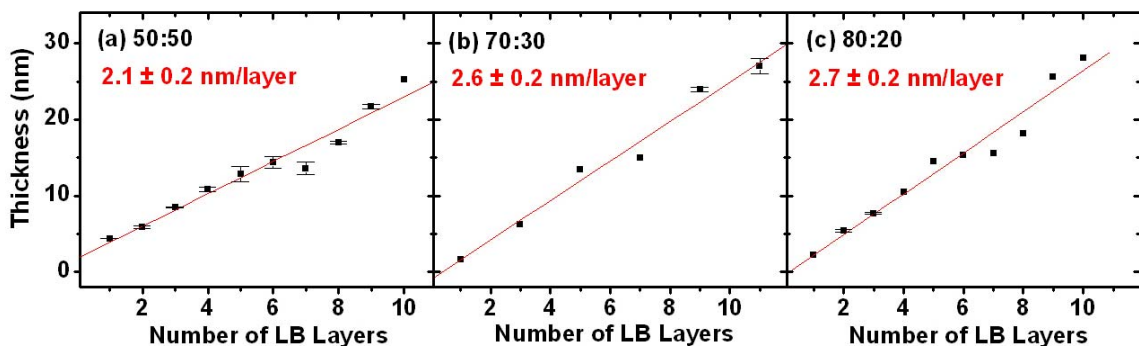
Most of all, the XRR result of 20 LB layers of 70:30 after annealing approximately 1.85 nm/layer showed an excellent agreement with the value 1.8 nm/layer obtained from the previous study. In the previous study all samples were annealed, but this time, measurements were done both before and after annealing for 20 LB layer samples. The 20 LB layer films of all copolymers showed little change in their thicknesses and critical angles before and after annealing (Table 2.1), however, from the annealed films more pronounced fringes were obtained (see Figure 2.8).

To find out the cause for the pronounced fringe shape, a simple simulation was done with the simulation software LEPTOS, supplied with Bruker-AXS. With having seen the little change in film thickness before and after annealing, we made a simple thin film model with fixed parameters of  $t = 37$  nm and the mass density approximately  $1.97$  g/cm<sup>3</sup> corresponding to about  $0.2^\circ$  for the critical angle  $\theta_c$  (also  $\theta_c$  of the films before and after annealing was unchanged), then we simulated the reflectivity by varying the roughness of the film interfaces, as shown in Figure 2.9. The simulation result suggests that the roughness of the film-substrate interface is the main parameter to degrade the shapes of the fringes. The roughness of 2 nm used for the simulation is somewhat high, but it was done purposely to exaggerate the effect for clear presentation.

The thickness of an another set of 20 LB layers of 50:50 and 80:20 samples, reported in Chapter 3 was determined a little differently as described there.



**Figure 2.10** shows XRR data of all thinner films of each copolymer samples as indicated in the plots are shown here. The blue numbers on the data lines is the number of LB layers of the sample the data were taken from. The XRR data from 1~2 LB layer samples of all copolymers show clear oscillations implying the films are uniform. All data were taken from un-annealed samples.



**Figure 2.11** shows the plots of the transfer ratio determination for each copolymer as indicated. Each data point in these plots is the thickness of corresponding XRR shown in Figure 2.9. (Some data points without error bars are from XRR curves that have only 2 measurable minima. The uncertainty shown in the ratio values is obtained from the uncertainty in the slope of the fit lines.)

The previous analysis was done with an assumed dispersion factor  $\delta=6.31 \times 10^{-6}$  without distinction between copolymers and PVDF polymer. This value was obtained, based on the relation  $\delta=(\lambda^2/2\pi)r_e\rho_e$ , introduced in Tolan and Daillant books,<sup>24,25</sup> where  $r_e$  is the classical electron radius, and  $\rho_e$  the electron density. For the estimation  $\rho_e$  of PVDF polymer was used.

In the case of thinner samples, they showed thicker layering for all three copolymers, on average compared to the 20 LB layer films: 2.7 nm/layer, 2.6 nm/layer, and 2.5 nm/layer for 50:50, 70:30, and 80:20 copolymers, respectively (see Fig. 2.11). The thicker layering below 20 LB layer samples was also apparent in the previous study of Bai *et al.* (see Fig. 6a of ref. 21). A possible stronger interaction between the film and the substrate for thinner samples could result in the thicker transfer ratio. Unlike the 20

LB layer sample results, thinner films of 50:50 copolymers did not particularly show a thicker layering than 70:30 and 80:20.

### Discussion

In this study, the thickness of the silicon oxide layer was not carefully considered; therefore to improve the accuracy of the thickness determination the thickness of oxide layer should be looked into in the future study. Also some of the samples among thinner samples did not show good quality of XRR. These samples with poor quality XRR showed rocking curves with split peaks during XRR measurement set-up. Similar split rocking curves were observed from bare Si substrates. We suspected, thus, this problem was originated from the quality of the Si wafer, however, we did not look into the problem in depth.

The roughness of the interfaces cannot be determined with the Kiessig fringe method. We tried to look at the roughness of our sample by fitting XRR with LEPTOS.<sup>24,25,28</sup> We fit the thickness and the mass density of the film, and the roughness of both the air-film and film-substrate interfaces by giving a reasonable initial values for thickness and density by using the results from Kiessig method. However, we have not obtained any good results. Fitting XRR data is another area to look into in the future.

### Conclusion

We have acquired XRR data from even 1 LB layer samples (Fig. 2.10). This strongly supports that one layer of LB copolymer film is sufficiently uniform enough to

obtain valuable XRR data over a large area on order of  $\text{mm}^2$ . Also, the thickness of the 80:20 and 50:50 copolymer LB films were measured for the first time in this study. The thickness measured from 20 LB layer films of 70:30 copolymer sample using XRR showed an excellent agreement with the results obtained from the ellipsometry measurement. The quality of Si substrate such as miscut and the thickness of the silicon oxide layer need to be carefully considered to obtain improved XRR data in the future especially for thinner films where strong influence from the substrate is suspected.

## **2.5 Real-Time Observation of Nanomesa Formation**

In this section observation of nanomesa formation in real-time is presented. Previously nanomesas were observed only after annealing<sup>10</sup>; however, here we directly observed how the film as deposited formed into nanomesas during annealing with atomic force microscopy (AFM).

### **2.5.1 Measurement**

We have observed nanomesa formation during annealing on the stage of an atomic force microscopy (AFM) by taking images at about every 10 °C steps. The AFM system used for the observation is Veeco MultiMode NS-III A. This system provides three different temperature ranges of heating/cooling elements namely temperature controllable scanners. The three temperature ranges are for air and inert gasses; -35 °C to 100 °C, ambient to 250 °C, and -35 ° to 250 °C.<sup>29</sup> The heating element, used for this observation was the second range from ambient to 250 °C. The sample was mounted on



the top of the scanner with thermal conducting tape, and the temperature of the system was controlled by the current controller provided with the heating scanner. The temperature from one temperature to the next temperature (5~10 °C steps) was increased approximately at a rate of 1 °C/min, and then the increase of the temperature was interrupted by a 5 min of soaking time. After the soaking, the temperature was stabilized and ready for scanning, and then 2~6 images were recorded at each temperature. The reason why we recorded a few number of images at one temperature is to the time dependence of the film separation at a fixed temperature. One image took approximately 9 min. Over all the experiment, the temperature was increased from room temperature (25 °C) to 135 ° at an average rate of approximately 10 °C/hr. All images were recorded in non-contact tapping mode. The spring constant of the AFM tip used for this study was  $k = 42 \text{ N/m}$ , and the resonant frequency of the cantilever of the tip was approximately 320 kHz.

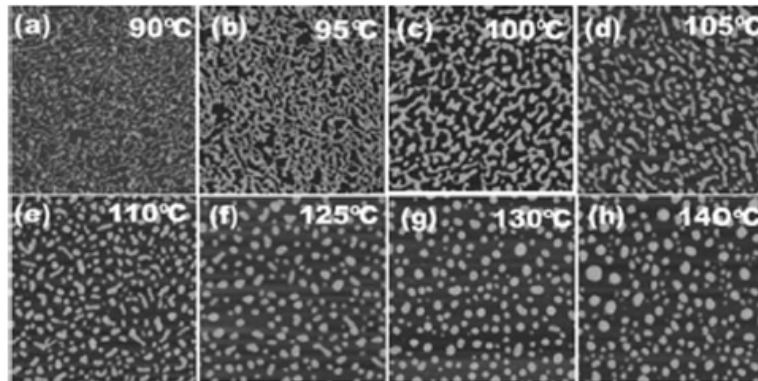
### 2.5.2 Results

We were able to reach a sample temperature 135 °C with no difficulties. However, at 135 °C the tip-surface contact was lost a couple of times. We attributes the lost contact to the fact that the films were in the high energy state of paraelectric phase with plastic flow.<sup>10,11</sup> It is also assumed that the flow of the material became very active at 135 °C getting close to its melting temperature, 150 °C.<sup>30</sup> The results of this real-time observation on nanomesa formation showed an excellent agreement to the previous studies done by Bai *et al.*<sup>10,11</sup> He showed the morphology change of 1 LB layer of 75:25 copolymer with

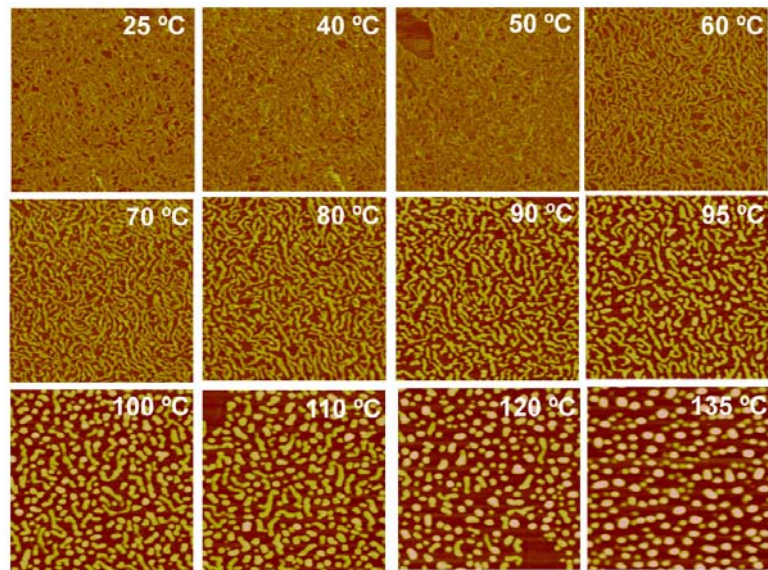
respect to the annealing temperature (Fig. 2.12). The images shown in Figure 2.12 were taken at room temperature after annealing by Bia. The indicated temperatures on the images are annealing temperatures. The set of images shown in Figure 2.13 are from this work, the real-time observation of nanomesa formation. In Figure 2.13 the temperatures indicated on the images are scanning temperatures at which the images were recorded.

What these images reveal is that the film separation is not reversible process because the amount of separation occurred during annealing seems to be preserved after the annealing. It is clear if we compare images between Figure 2.12 and Figure 2.13 indicated with the same temperatures of annealing (for 2.12) and scanning (for 2.13). The morphology of the film did not show much difference from the fresh sample as deposited (Fig. 2.13). The separation of film started from 60 °C and started to form isolated films from 90 °C (Fig. 2.13). This isolated films formed at 90 ° are the early form of nanomesas.

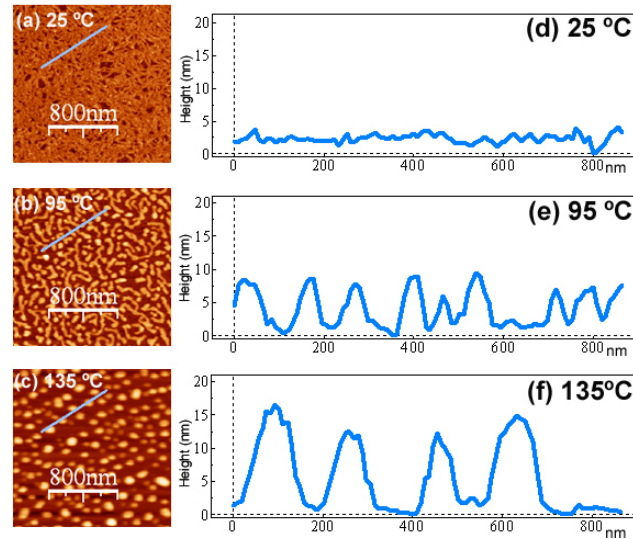
The development of the height,  $h$  with respect to the temperatures is shown in Figure 2.14 with some examples. The example images (Fig. 2.14a, b, and c) were selectively chosen among the images shown in Figure 2.13. The line profiles presented in Figure 2.14e, f, and g are from the parts, highlighted with blue lines in Figure 2.14a, b, and c, respectively. This clearly shows that the increase of  $h$  was followed by film separation. This increase of the  $h$  is plotted in Figure 2.15a.



**Figure 2.12** shows AFM images of 1 LB layer films of the 75:25 copolymer deposited on Si wafers. All images were recorded after annealing at the indicated temperatures on each image. The size of all images,  $2\ \mu\text{m}\times\mu\text{m}$ : this figure is reused with permission from Bai *et al. J. Phys. Condens. Matter* **18**, 7383 (2006). © Institute of Physics and IOP Publishing Limited 2006

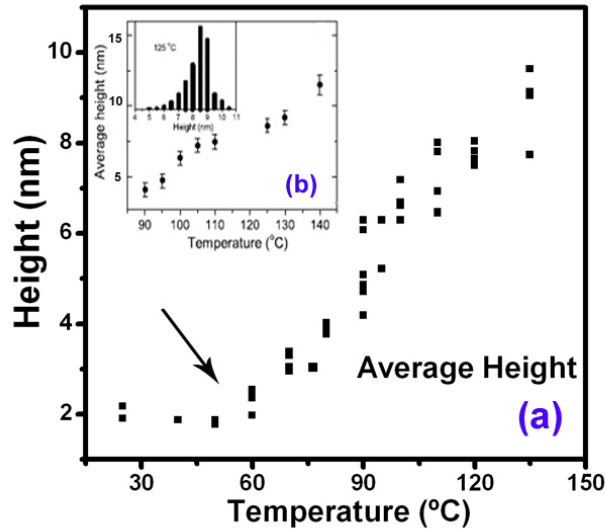


**Figure 2.13** shows AFM images of 1 LB layer of 70:30 copolymer taken during annealing. The temperature indicated on the images is the scanning temperatures. All images represent film areas of  $2\ \mu\text{m}\times\mu\text{m}$ .

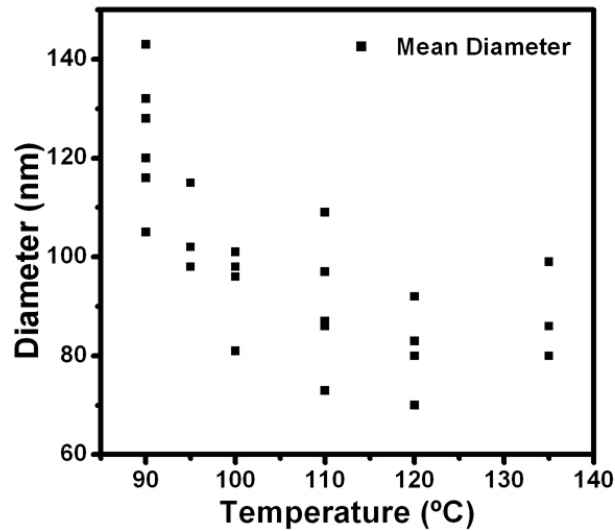


**Figure 2.14** shows the height development of the film with respect to the scanning temperatures. As the film starts the separation, it developed its height due to conservation of the material.

The  $h$  of films was measured by using the roughness analysis option in NanoScope software (a scanning microscope image analysis tool), equipped with the Veeco AFM system. The height analysis shown in Figure 2.15a makes excellent agreements with our two different previous studies. One is the onset temperature of paraelectric phase upon heating. This plot clearly shows the drastic change that occurred at 60 °C as marked with an arrow and one of our previous x-ray diffraction studies on 70:30 copolymer films showed a drastic increase of paraelectric phase material at 60 °C.<sup>7</sup> The other is the linear trend of the height increase. Both the real time observation and Bai's annealing study<sup>11</sup> shown in Figure 2.15b show the height increase approximately at a rate of 1nm per 10°C.



**Figure 2.15** (a) shows the increase of the average height of 1 LB layer of 70:30 copolymer film deposited on Si wafer as it was heated and (b) is the average heights of 1 LB layers of 75:25 copolymer deposited on Si wafer after they were annealed at different temperatures as it is indicated.<sup>3</sup> Figure 2,15b is reused with permission from Bai *et al. J. Phys. Condens. Matter* **18**, 7383 (2006). © Institute of Physics and IOP Publishing Limited 2006



**Figure 2.16** (a) shows the decrease of the mean diameter of 1 LB layer of 70:30 copolymer film deposited on Si wafer as it was heated.

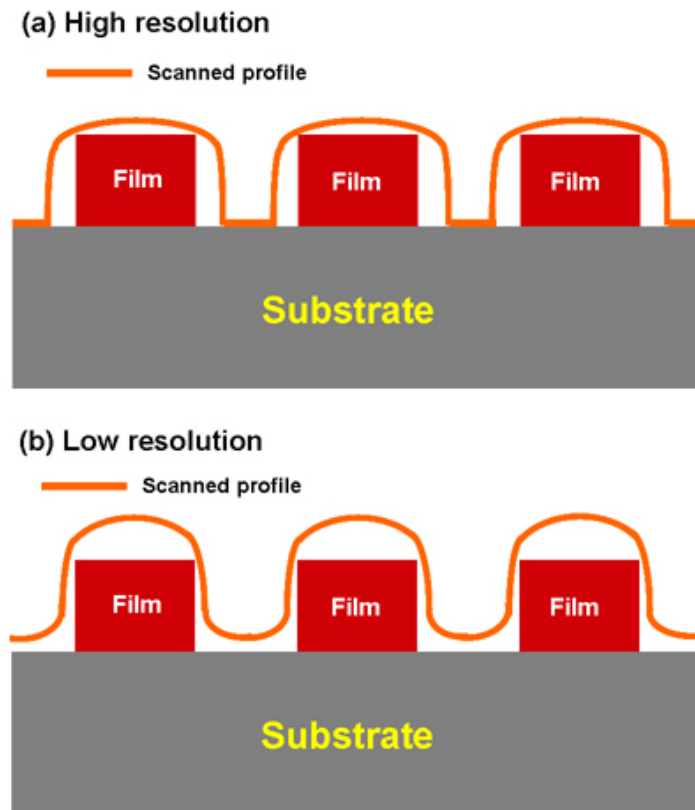
Also the mean lateral size of the nanomesa was analyzed and plotted in Figure 2.16. The determination of the lateral size (diameter) of nanomesas was done with the same image analysis software, NanoScope software. This analysis is only applicable to the images of particle-like films, in other words, only films with completely isolated areas. This complete isolation in the film (an early form of nanomesas) happened above 90 °C. The diameter,  $D$  shows linear decrease up to 110 °C, and the decrease became unclear beyond that point. This phenomenon seems less obvious in  $h$  change.

All data points in Figure 2.15 and 16 were obtained from different images taken at the assigned temperatures in the plot. The size of the images is ranged from 1 to 4  $\mu\text{m}^2$ . In general 1  $\mu\text{m}^2$  images have better resolution than 4  $\mu\text{m}^2$ . This could result in obtaining a smaller  $h$  and  $d$  of nanomesa dimensions from the images recorded over a larger area due to the lower resolution as it is schematically illustrated in Figure 2.17. Therefore, this artifact could have contributed the large uncertainty of  $h$  and  $D$  values among the images recorded at the same temperature. If all the images were taken at one size, then the following two equations (2.4) and (2.5) can be used to test if the distribution of  $h$  and  $D$  is originated from the kinetic change of the film. The equations are obtained from the volume conservation, which assumes, reasonably, that the nanomesas do not exchange mass once separated, or split or recombine.

$$\left( \frac{h_{final}}{h_{initial}} \right)_{at\ fixed\ temp} = \left( \frac{h_{min}}{h_{max}} \right)_{at\ fixed\ temperature} \equiv \frac{1}{r} \quad (2.4)$$

$$\left( \frac{D_{final}}{D_{initial}} \right)_{at\ fixed\ temp} = \left( \frac{D_{max}}{D_{min}} \right)_{at\ fixed\ temperature} \equiv \sqrt{r} \quad (2.5)$$

If the data provides the same  $r$  from both  $h$  data and  $D$  data, then it can be concluded that the distributions in the data is originated from a kinetic morphology change. However, in this study this analysis was not applicable.



**Figure 2.17** is a schematic cartoon to show expected artifact in AFM images analysis due to image resolution related to the size of images. With low resolution image we could be obtained smaller values of the heights and the diameters of isolated films.



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## Chapter 3 Polarization Interaction

### in Multilayered Thin Films of P(VDF-TrFE)

In this chapter the investigation on the effect of polarization interaction occurred in multilayered films of 80:20 and 50:50 copolymers are presented.<sup>a</sup>

#### 3.1 Introduction

The role of finite-size effects in ferroelectric materials is less clear, though of critical importance in the rapidly growing ferroelectric memory industry, where the bistability of polarization of thin ferroelectric films is paramount. Analyses using mean field theory generally conclude that the depolarization field energies and surface energies will suppress ferroelectricity.<sup>1,2</sup> There were several early observations of finite-size effects in ferroelectric oxide thin films<sup>3,4,5</sup> as thin as 100 nm, and of nanoparticles as small as 25 nm,<sup>6,7</sup> although these results were probably dominated by variations in sample composition or microstructure.<sup>8</sup> Improvements in the fabrication of thin perovskite films pushed the limit below 15 nm,<sup>9,10,11,12,13</sup> in accordance with the predictions of first-principles calculations.<sup>14,15</sup> Ferroelectricity has been reported in films as thin as 1 nm in both polymers<sup>16</sup> and oxides.<sup>17</sup> The most remarkable results of the thin film studies were that reduced thickness does not necessarily decrease the Curie temperature or spontaneous polarization. Though polarization measurements of the

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<sup>a</sup> This chapter has been published in *Journal of Condensed Matter*, **19** 086206 (2007). Minor changes from the original Journal has been made for this dissertation.

thinnest ferroelectric polymers are inconclusive,<sup>16</sup> a recent study of BaTiO<sub>3</sub> thin films with SrRuO<sub>3</sub> electrodes showed significant polarization decline only below 15 nm,<sup>18</sup> and studies of unit cell tetragonality in PbTiO<sub>3</sub> films,<sup>19</sup> also indicates a significant decrease in polarization below 10 nm in thickness.

Studies of ferroelectric multilayers and superlattices, composed of ferroelectric oxides with different bulk transition temperatures ( $T_C$ s) or of ferroelectric and paraelectric materials, shed additional light on the thin-film stability puzzle and on the range of polarization correlation. There have been numerous experimental studies of superlattices involving ferroelectric materials, mostly in the past five years. Theoretical modeling has been effective in guiding research in ferroelectric superlattices, predicting interlayer polarization interactions,<sup>20</sup>  $T_C$  enhancement,<sup>21</sup> and enhanced dielectric response.<sup>1,2,22</sup> Experimental results do reveal  $T_C$  enhancement with a critical thickness of order 10 nm or less in ferroelectric superlattices of KTaO<sub>3</sub>/KNbO<sub>3</sub>,<sup>23</sup> in BaTiO<sub>3</sub>/SrTiO<sub>3</sub>,<sup>24,25</sup> and PbTiO<sub>3</sub>/SrTiO<sub>3</sub>.<sup>26</sup> In addition, superlattices of two different paraelectric materials show evidence of both antiferroelectric and ferroelectric ordering,<sup>27</sup> while superlattices consisting of ferroelectric and antiferroelectric layers show interesting intermediate behavior.<sup>28</sup>

Strain can play a major role in epitaxial superlattices when the transition is substantially displacive, as for the oxide studies just mentioned, and other studies of epitaxial films.<sup>29,30,31</sup> There is also evidence for correlations between the critical

superlattice period and the domain size.<sup>23</sup> The influence of strain is likely much smaller in the much softer ferroelectric polymers. For example, an all-organic composite of copper–phthalocyanine (a high dielectric constant material) with ferroelectric P(VDF-TrFE) shows greatly enhanced dielectric properties,<sup>32</sup> which are better explained by short-range exchange interactions at the interface between the two materials, and not by long-range strain effects.<sup>33</sup> The size and length scales are not precisely defined in the composites, and hence interaction information is averaged over a wide range of length scales. Precision deposition of ferroelectric and dielectric multilayers can better control interactions and possibly produce significant enhancement of key functional properties critical to applications such as nonvolatile memory, infrared imaging, and electromechanical transducers.

The ability to tune the ferroelectric properties of nanostructured materials provides some appealing technological opportunities. Ferroelectric superlattices have exhibited enhanced dielectric constants attributed to polarization correlations<sup>26,34,35</sup> or to purely dielectric effects,<sup>36</sup> and enhanced nonlinear optical response,<sup>18,24,35</sup> demonstrating the potential technological benefits of ferroelectric crystal engineering. Other nanoscale structures studied to date, including arrays of pillars<sup>37</sup> and nanotubes,<sup>38,39,40,41</sup> demonstrate additional means of controlling bulk properties through nanostructure.

Our motivation for this work was to investigate the interaction between ferroelectric polymer layers with different  $T_C$ s in a well-defined structure that is relatively

free of strain. Varying the composition and layer thickness should probe several key features of ferroelectric interactions, namely, whether or not ferroelectric layers couple across a paraelectric layer, whether it is possible to induce ferroelectricity in a paraelectric layer without first inducing strain, and what length scales are important for this interaction to occur. In order to accomplish this we chose a multilayered structure consisting of alternating layers of two P(VDF-TrFE) copolymers with different  $T_C$ s. The P(VDF-TrFE) copolymers have nearly the same spontaneous polarization, of order  $0.1 \text{ C/m}^2$ , and a composition-dependent  $T_C$  ranging from  $65 \text{ }^\circ\text{C}$  to  $208 \text{ }^\circ\text{C}$ , for compositions containing 40% VDF to 100% VDF, respectively.<sup>42</sup> The compositions P(VDF-TrFE 50:50) and P(VDF-TrFE 80:20) were chosen for the present study as the two constituents of the multilayer, since they have well-separated bulk  $T_C$ s (measured on heating) of approximately  $65 \text{ }^\circ\text{C}$  and  $142 \text{ }^\circ\text{C}$ ,<sup>42</sup> respectively, and therefore are good candidates for exploring interlayer interaction effects. We chose these values because compositions with more than 80% VDF do not crystallize well and have  $T_C$ s inconveniently located above their melting points. Copolymers with less than 50% VDF have so far proven too variable in their ferroelectric properties to provide reliable samples.

Here we report a study of the structure and ferroelectric properties of multilayers of two ferroelectric copolymers, P(VDF-TrFE 80:20) and P(VDF-TrFE 50:50), with repeat periods of 2, 10 and 20 LB layers, and a constant total thickness of 20 LB layers. The results from these samples were also compared with pure films composed of only each composition and films made from a 1:1 mixture of the two compositions. The two-

dimensional nature of the ferroelectric transition<sup>16, 43</sup> presumably rules out direct ferroelectric interaction between the various layers; however, interactions via the polarization of the intervening layer may still occur. For each sample, we measured the lattice spacing and the dielectric constant as a function of temperature on both heating and cooling. The films with the repeat period 2, which consisted of one LB layer of each composition, exhibit intermediate behavior similar to that of the mixture. Films with repeat period 20, which consisted of contiguous 10 LB layers of each composition, behave like two independent films. The cross-over appears to be with the sample with repeat period 10, which alternates 5 layers of the 50:50 copolymer with 5 layers of the 80:20 copolymer.

### 3.2 Sample Preparation

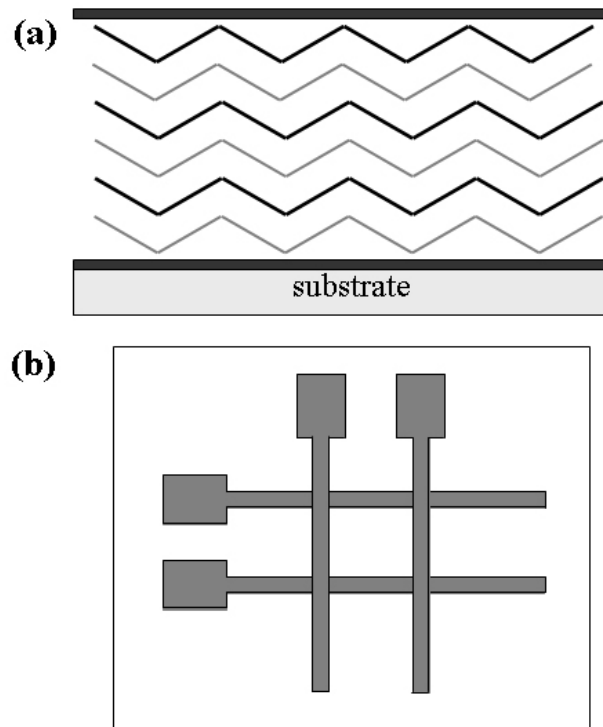
The ultra thin ferroelectric polymer films were deposited by LB deposition using procedures described in detail elsewhere.<sup>43,44,45,46</sup> Langmuir-Blodgett (LB) deposition affords ultra thin films with good crystallinity<sup>47</sup> and stable ferroelectric properties, such as spontaneous polarization and Curie temperature, that are only weakly dependent on thickness.<sup>16,43</sup> Briefly, deposition proceeded as follows. We spread a solution of the polymer (0.05% weight concentration in dimethyl sulfoxide) onto the surface of an ultra pure water (18 M $\Omega$ -cm resistivity) subphase maintained at 25 °C. The polymer surface film was compressed slowly to a surface pressure of 5 mN/m, and then transferred to the substrate by horizontal dipping at a slight angle to control the line of contact. The film thickness was controlled by repeating the LB layer transfer, and multilayered samples

were made by alternating between two isolated trough sections containing the two polymer compositions, each held at the same temperature and surface pressure. Completed samples were annealed for 2 hours at 135 °C to optimize their crystal structure and stabilize the ferroelectric properties.<sup>43,48</sup>

The samples for the present work consisted of homogeneous and multilayer LB films of two P(VDF-TrFE) copolymers, one with 80% VDF, designated 80:20, and the other with 50% VDF, designated 50:50. The LB films were deposited on two different substrates, depending on the intended measurement. Samples for x-ray diffraction measurements consisted of LB films deposited directly on (100) silicon wafers. Capacitors for dielectric measurements were fabricated by evaporating bottom aluminum strip electrodes on a glass microscope slide, then depositing the LB film or multilayer, and evaporating aluminum strip top electrodes oriented orthogonal to the bottom electrodes. The completed capacitor, shown schematically in Figure 3.1, consists of four individually addressable spots.

Measurements were made on six pairs of samples, each pair consisting of one sample for XRD measurements and another for dielectric measurements, made as described above. The LB films on all the samples consisted of 20 LB layers (20 individual transfers) but differ in the composition and sequence of the LB layers. One pair of homogeneous reference samples was made with each of the two copolymers.





**Figure 3.1** shows schematic diagram of sample structure. (a) Layering of the LB films shown between the top and the bottom electrode. The darker line indicates layers of 50:50 copolymer, the lighter lines indicate layers of 80:20 copolymer. (b) Layout of a capacitor sample view from the top showing the orthogonal arrangement of the bottom and top electrode strips.

**Table 3.1** Sample composition and basic properties measured as described in the text. The sample thicknesses were obtained from the x-ray reflectivity data shown in Figure 3.3. The thermal expansion coefficients were obtained from the slopes of the lines in Figure 3.7 for both ferroelectric and paraelectric phases.

Sample	Composition	Repeat Period (LB layers)	Sample Thickness (nm) <sup>b</sup>	Thermal Expansion Coefficient (dL/dT)/L <sub>0</sub> (°C) <sup>-1</sup>	
				Ferroelectric Phase	Paraelectric Phase
<b>50:50</b>	50:50 copolymer	—	50	$3.7 \times 10^{-3}$	$1.3 \times 10^{-3}$
<b>80:20</b>	80:20 copolymer	—	51	$1.3 \times 10^{-3}$	$1.1 \times 10^{-3}$
<b>Period20</b>	alternating 10 LB layers	20	48	$2.8 \times 10^{-3}$ <sup>c</sup> $0.8 \times 10^{-3}$ <sup>c</sup>	$1.4 \times 10^{-3}$
<b>Period10</b>	alternating 5 LB layers	10	42	$1.6 \times 10^{-3}$	$1.3 \times 10^{-3}$
<b>Period2</b>	alternating 1 LB layers	2	46	$0.7 \times 10^{-3}$	$1.0 \times 10^{-3}$
<b>Mixture</b>	equal weights 50:50 & 80:20	—	51	$1.2 \times 10^{-3}$	$1.1 \times 10^{-3}$

<sup>b</sup> The sample thickness was determined from a linear least-squares fit of the positions of the minima in Figure 3. 3, with a root-mean-square statistical uncertainty of 5% or less for all fits.

<sup>c</sup> The sample two thermal expansion coefficients for the period 20 sample are due to the separate behavior of 80:20 and 50:50 layers in the sample; the values  $2.8 \times 10^{-3}$  and  $0.8 \times 10^{-3}$  are from 50:50 layers and 80:20 layers, respectively

Three pairs of multilayer samples consisted of equal-thickness alternating layers of the two copolymers with repeat periods of 2, 10, and 20 LB layers. An additional pair of samples was made from a solution containing equal amounts by weight of the two copolymers. The complete list of samples and their compositions is listed in Table 3.1.

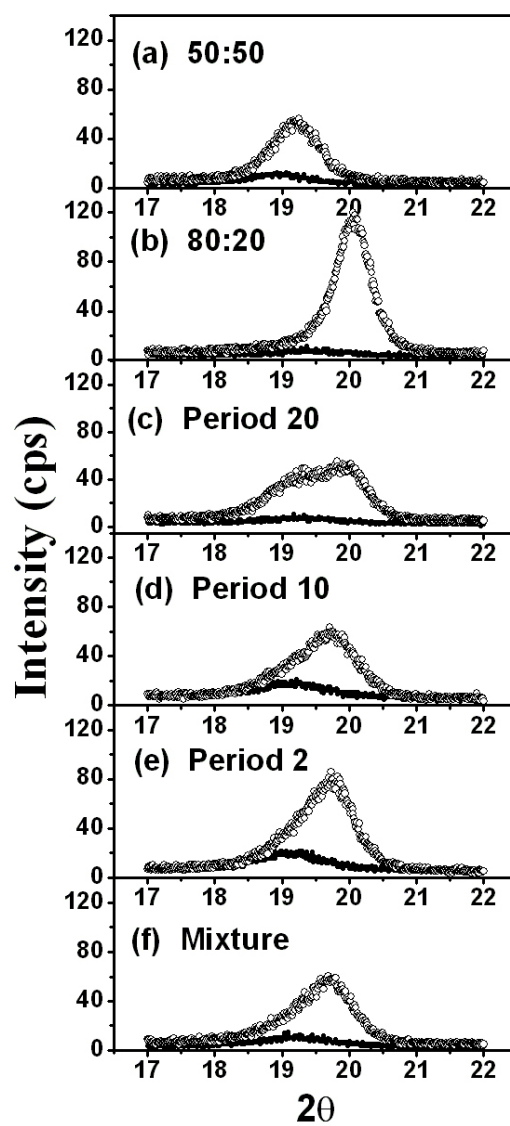
### 3.3 Experimental methods

The breadth of the ferroelectric-paraelectric phase transition and inherent thermal hysteresis due to phase coexistence make it difficult to determine the true phase transition temperature. Therefore, we use both dielectric measurements and x-ray diffraction to investigate the behavior. The advantage of x-ray diffraction is that it provides a *quantitative* measure of the amount of material in the ferroelectric and paraelectric states in the phase coexistence region.<sup>47,49,50</sup> As we shall see, this enables us to clearly define an effective phase transition temperature and also chart the evolution of phase conversion with temperature and history. Since the x-ray scattering lengths of the two compositions are almost identical, we were not able to directly probe the multilayer period. However, as we shall see subsequently, the behavior of the differently structured samples is quite distinct, implying that the structure of the superlattice is preserved to a large extent.

Sample crystallinity was measured by x-ray diffraction (XRD) in the theta-2theta geometry, which measures the crystal spacing normal to the substrate. Previous studies have shown that the LB films have predominately (110) orientation, meaning that the

chains, which are along the (001) direction, are in the film plane and the spontaneous polarization in the ferroelectric phase, which is along the (010) direction is tilted  $30^\circ$  away from the normal.<sup>47,50</sup> The XRD peaks near  $18^\circ$  and  $19^\circ$  at an x-ray wavelength  $\lambda = 1.54 \text{ \AA}$  are the (110) diffraction peaks in the paraelectric and ferroelectric phases, respectively.<sup>51</sup> These peaks have the same structure factor, so the integrated intensities give the relative fraction of material in each phase.<sup>50</sup>

Initial x-ray diffraction measurements were performed on a set of preliminary samples to determine the sample crystallinity and follow the progress of the phase transition as they were heated. These measurements were made on a Rigaku theta-2theta diffractometer with a fixed  $\text{Cu-K}_\alpha$  cathode. This initial XRD measurement showed relatively low crystallinity of the samples before annealing and considerable improvement after annealing, as shown in Figure 3.2. For the 50:50 and 80:20 samples the crystallinity improved by a factor of 5 and 12 respectively as measured by the area under the diffraction peaks. The samples were annealed by heating them from room temperature to  $135^\circ\text{C}$  at a rate of  $1^\circ\text{C}/\text{min}$ , hold it at  $135^\circ\text{C}$  for 2 hours and cool down to room temperature at the same rate. Both prior studies<sup>47,48</sup> and present results indicate that this annealing procedure optimizes the degree of crystallinity. Each sample was then enclosed in a temperature-controlled copper chamber, which was mounted on a goniometer. The chamber operated at atmospheric pressure and had a 9-mm-thick polyimide window for x-ray access. The sample temperature was accurate within  $2^\circ\text{C}$ .



**Figure 3.2** shows x-ray diffraction data from the XRD samples recorded at room temperature with the Rigaku  $\theta$ - $2\theta$  instrument both before (solid circles) and after (open circles) annealing.

The sample temperature was increased at the rate of 1 °C/min. Measurements were made at intervals of 20° C after holding for 20 min at each set temperature. An identical set of samples was then made for the detailed XRD studies performed at the synchrotron.

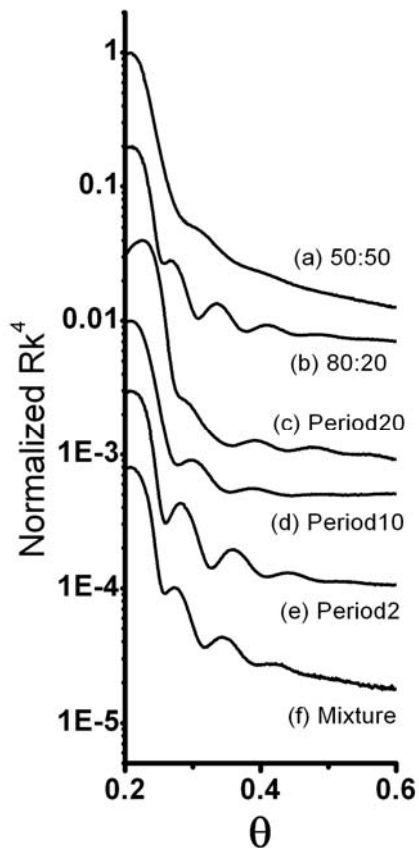
The total thickness of each film was measured after completion of the synchrotron studies by grazing-incidence theta-2theta x-ray reflectivity on a Bruker AXS diffractometer. This data was analyzed as follows. The x-ray diffraction intensity was multiplied by  $k^4$ , where

$$k = \frac{2\pi}{\lambda} \sin \theta \quad (1)$$

is the scattering vector, in order to account for the effects of the Fresnel reflectivity. The modified reflectivity data for all 6 samples are shown in Figure 3.3. The presence of multiple oscillations indicates relatively smooth interfaces. The sample thickness was determined by using the modified Bragg equation,

$$(m + \frac{1}{2})\lambda = 2t\sqrt{\sin^2 \theta_m - \theta_c^2} \quad (2)$$

for the positions of the diffraction minima, where  $m$  is an integer index for the diffraction order,  $\lambda$  is the x-ray wavelength (1.54 Å in this case),  $t$  is the film thickness,  $\theta_m$  is the angle corresponding to the diffraction minimum of index  $m$ ,<sup>52</sup> and  $\theta_c = 0.2^\circ$  is the critical angle of the copolymer for x-rays with wavelength 1.54 Å.



**Figure 3.3** shows X-ray reflectivity data recorded with the Bruker  $\theta$ -2 $\theta$  instrument showing thickness oscillations for the indicated samples. The curves have been offset vertically for clarity. All except for the 50:50 sample were the same as those used for the synchrotron x-ray diffraction studies. The original 50:50 sample was unavailable for the x-ray reflectivity studies, so the sample prepared for the primary check-up study before XRD measurement at the synchrotron was used. Due to small number of fringes with this particular sample, an additional sample was also prepared under same condition, and the thicknesses from both samples are the same within experimental uncertainty.

The small difference in scattering length densities between the two copolymers implies that the multilayered samples may be treated as a single uniform layer for the purposes of this thickness measurement. The thicknesses determined by x-ray reflectivity are listed in Table 3.1. The sample thicknesses for the pure 80:20 and 50:50 and the mixture compositions are 50 nm, while the multi-layer samples are slightly thinner, with an average thickness of 45 nm, slightly thinner than the pure compositions.<sup>d</sup> According to these thickness measurements, each transfer of LB film from the water sub-phase consists of approximately 6 molecular layers per LB transfer. The roughness is estimated to be approximately 2 nm, as seen from previous AFM measurements on P(VDF-TrFE 70:30) copolymer films fabricated under the same conditions.<sup>53</sup>

The bulk of the x-ray diffraction measurements were made at the Advanced Photon Source at Argonne National Laboratory, on the 12-BM/BESSRC-CAT beam line, which operated at a wavelength  $\lambda = 1.0 \text{ \AA}$  with an  $2\theta$  angular resolution of  $0.012^\circ$ . The sample was placed in vacuum on the cold finger of a recirculating gas refrigerator that was mounted on the diffractometer goniometer. The sample temperature was accurate to within  $1^\circ\text{C}$ . The diffraction measurements were recorded on both heating and cooling over the range  $-5^\circ\text{C}$  to  $+125^\circ\text{C}$ , at temperature intervals of  $5^\circ\text{C}$  far from the phase

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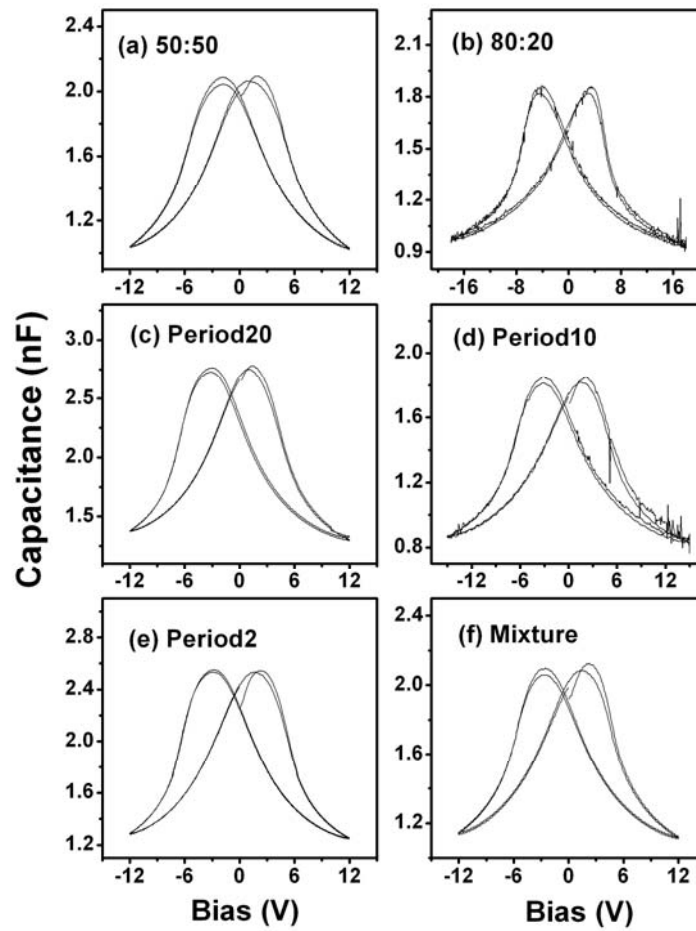
<sup>d</sup> In Appendix C, thickness of different 20 LB layers of 80:20 and 50:50 copolymer samples are presented, and the thickness determination was done with a different form of eq.2 is used. The critical angle does not need for the analysis; rather the critical value was obtained from the analysis. Between two studies the determined thickness shows approximately 1 nm discrepancy for both copolymer films.



transition temperature, and intervals of 3 °C near it. Beginning the measurements well below room temperature ensured that the samples were initially in the ferroelectric phase.

The dielectric constant of a ferroelectric exhibits peaks at the transition between the paraelectric and ferroelectric phases. These peaks are due to the large polarizability near the phase transition. Capacitance measurements were made with a Hewlett-Packard 4192A Impedance Analyzer operating at a frequency of 1 kHz and an amplitude of 0.1 V. The samples were mounted in a temperature-controlled copper chamber at atmospheric pressure. The sample temperature was accurate within 1 °C. The sample capacitance was continuously recorded as the sample was heated at a rate of 1 °C/min from room temperature to 125 °C and while cooling back to room temperature at the same rate. The exception was the pure 80:20 composition sample which was heated to 135 °C.

The switching behavior of the capacitor samples was characterized at room temperature by measuring the capacitance as a bias voltage was slowly varied between opposing polarization saturation levels. The capacitance hysteresis data shown in Figure 3.4 demonstrates that all the samples exhibit the characteristic ‘butterfly’ shape, with capacitance peaks indicating polarization switching. The butterfly curves repeat on continued cycling and are typical of those obtained with the ferroelectric copolymer LB films.<sup>43,54</sup> The magnitude of the coercive voltage varies slightly among the samples, but does not seem to be correlated with the layered structure. This is to be expected, because the coercive field of the copolymers depends only weakly on composition.<sup>55</sup>



**Figure 3.4** shows ‘butterfly’ hysteresis curves of the capacitor samples measured at a frequency of 1 kHz and amplitude 0.1 V while cycling the bias voltage at a rate of 6 V/min.

### 3.4 Results and Discussion

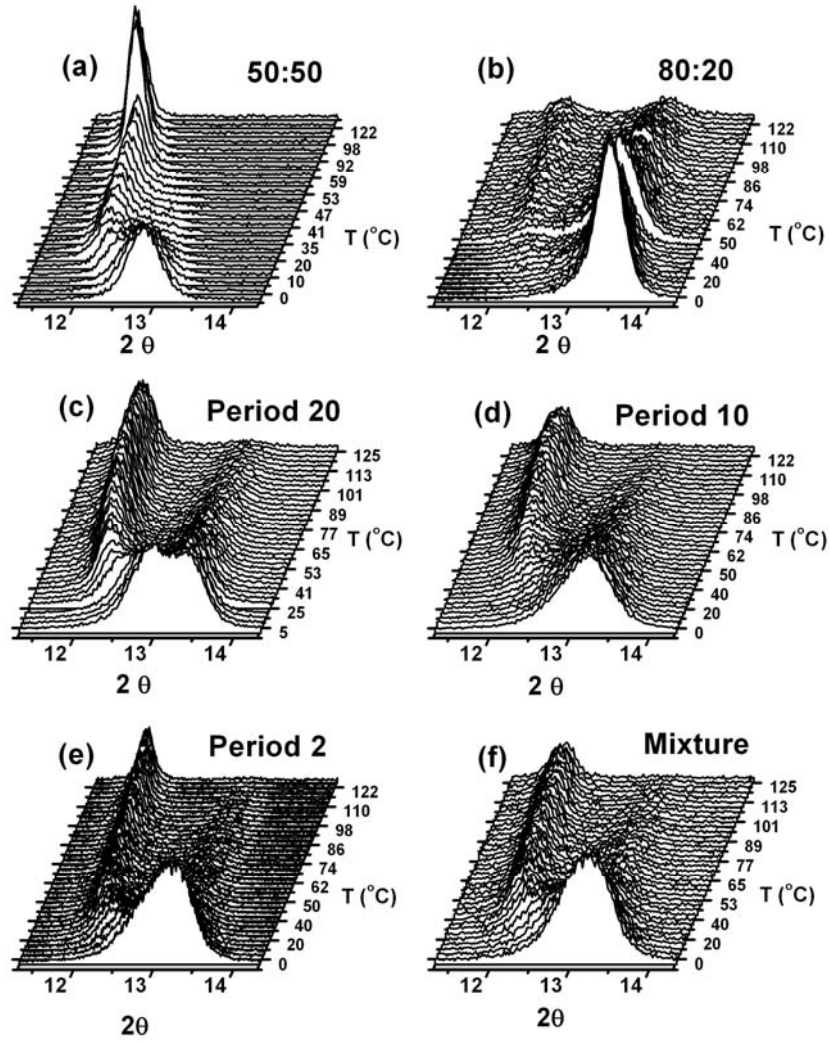
#### Structure

The ferroelectric-to-paraelectric conversion is accompanied by a change in the crystal structure from the all-trans conformation of the ferroelectric phase to the trans-gauche paraelectric phase. Figure 3.2 shows the theta-2theta XRD data from the synchrotron recorded at the lowest ( $-5\text{ }^{\circ}\text{C}$ ) and highest ( $+125\text{ }^{\circ}\text{C}$ ) temperatures for all the samples. The peaks near  $2\theta = 13^{\circ}$  correspond to a (110)  $d$  spacing of  $4.4\text{ \AA}$  for the ferroelectric phase, while the peaks near  $2\theta = 11.9^{\circ}$  correspond to a  $d$  spacing of  $4.8\text{ \AA}$  for the paraelectric phase. The lattice expansion of 10% from the ferroelectric to paraelectric phases is due to the increased size of the chains with trans-gauche conformation.<sup>51</sup> The pure 80:20 sample and the Period 20 sample have noticeable amounts of residual ferroelectric phase at  $125\text{ }^{\circ}\text{C}$ , due to phase coexistence and the relatively high transition temperature of the 80:20 copolymer, a point that will be discussed further below.

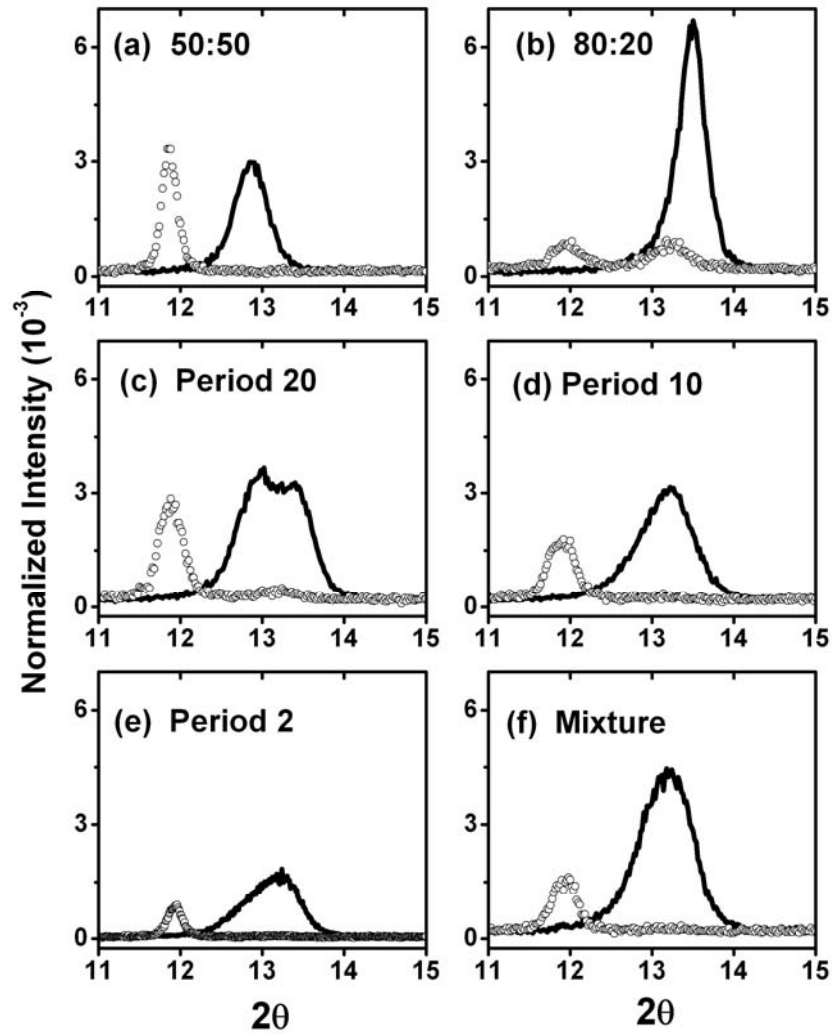
The lattice spacing in the paraelectric phase is only weakly dependent on composition, as the peak positions of the pure 50:50 and pure 80:20 samples at  $125\text{ }^{\circ}\text{C}$  were nearly identical, at  $11.86\pm 0.02^{\circ}$  ( $4.835\pm 0.005\text{ \AA}$ ) and  $11.95\pm 0.02^{\circ}$  ( $4.80\pm 0.01\text{ \AA}$ ), respectively, effectively irresolvable because of the peak width of approximately  $0.4$  degree. The tightly packed ferroelectric phase, on the other hand, is more sensitive to the presence of the extra fluorine atoms on the hydrogen side of the backbone. At  $-5\text{ }^{\circ}\text{C}$ , the peak positions of the pure 50:50 and pure 80:20 samples are readily resolved, at  $12.86\pm 0.02^{\circ}$  ( $4.46\pm 0.01\text{ \AA}$ ) and  $13.48\pm 0.02^{\circ}$  ( $4.26\pm 0.005\text{ \AA}$ ), respectively.

*X-ray diffraction results*

Figure 3.5 shows the temperature evolution of the (110) peaks for the six XRD samples from 0°C to 125 °C on heating. The transition between the ferroelectric and paraelectric phases in the VDF copolymers is gradual, owing to the first-order nature of the transition.<sup>56</sup> The breadth of the phase transition is not sensitive to sample defects or inhomogeneity, as is evident by comparing studies of polymorphous lamellar samples<sup>57</sup> with high quality linear-chain crystals of VDF copolymers.<sup>58</sup> Moreover, the phase transition is highly hysteretic, so that the transition temperatures on heating and cooling are different. We will focus on the phase changes observed during heating after stabilization at room temperature or below, because this produces the best repeatability in the initial phase proportions. The proportion of each phase is readily quantified by the intensity of the (110) diffraction peaks, the ferroelectric peak at approximately 13° and the paraelectric peak at approximately 12°. All samples exhibit a large coexistence region, the range of temperatures where both phases persist. The pure 50:50 sample (see Figure 3.5a), having the lower transition temperature, shows essentially full conversion to the paraelectric phase by approximately 80 °C, while the pure 80:20 sample (see Figure 3.5b) is not yet fully converted at 125 °C. These two pure samples provide a useful reference for comparison. For example, the XRD data from the Period 20 sample resembles a superposition of the structures of the two component materials, with two distinct ferroelectric phase XRD peaks recorded at -5 °C and a two-stage transition to the paraelectric phase.



**Figure 3.5** shows the synchrotron x-ray diffraction data as function of temperature, showing the ferroelectric-to-paraelectric phase conversion for the following 20 LB layer films: (a) pure 50:50 copolymer; (b) pure 80:20 copolymer; (c) Period 20; (d) Period10; (e) Period 2; and (f) Mixture.



**Figure 3.6** shows comparison between x-ray diffraction data recorded at the synchrotron at  $-5\text{ }^{\circ}\text{C}$  (solid lines) and at  $125\text{ }^{\circ}\text{C}$  (open circles) for all the samples. The peaks near  $12^{\circ}$  are the (110) peaks from the paraelectric phase, while the peaks between  $13^{\circ}$  and  $14^{\circ}$  are the (110) peaks from the ferroelectric phase.

The mixture sample (see Figure 3.5f), the Period 2 sample (Figure 3.5c), and the Period 10 sample (Figure 3.5d) show nearly full conversion to the paraelectric phase by 125 °C. On the other hand, both the pure 80:20 sample and the Period 20 sample retain some of the paraelectric phase, even at 125 °C, as is evident in Figure 3.6b and Figure 3.6c, indicating that the 80:20 layers in the period 20 sample are relatively unperturbed.

To make a more quantitative comparison, we fit each XRD measurement to a set of peaks with a Gaussian line shape (except for the Period 20 sample, where a Lorentzian line shape resulted in higher quality fits). With such thin films and inherently broad diffraction peaks, the fitting results do not necessarily determine unambiguously which spacings are present. An elementary model calculation of the expected diffraction peak heights, widths and positions for the multilayer samples (assuming planar interfaces and perfect lattice coherence through the thickness of the sample) indicates that the (110) peaks for the ferroelectric structures of the 50:50 and 80:20 copolymers should produce a single irresolvable peak in the Period 2 sample, whereas in the Period 20 sample, the separate peaks should be clearly distinguishable. (The peak widths, which are of the order of  $1^\circ$  in  $2\theta$ , are much greater than the  $0.012^\circ$  resolution of the APS diffractometer.) Note that the model shows that that an apparent merging of the (110) XRD peaks in films with small repeat periods is purely structural – it does not necessarily indicate that the Period 2 sample, for example, behaves as a composite or mixed sample (though this indeed may be the case), only that the two peaks are structurally indistinguishable. In all but the Period 20 sample, the two-peak fits (one peak from the ferroelectric phase and only one

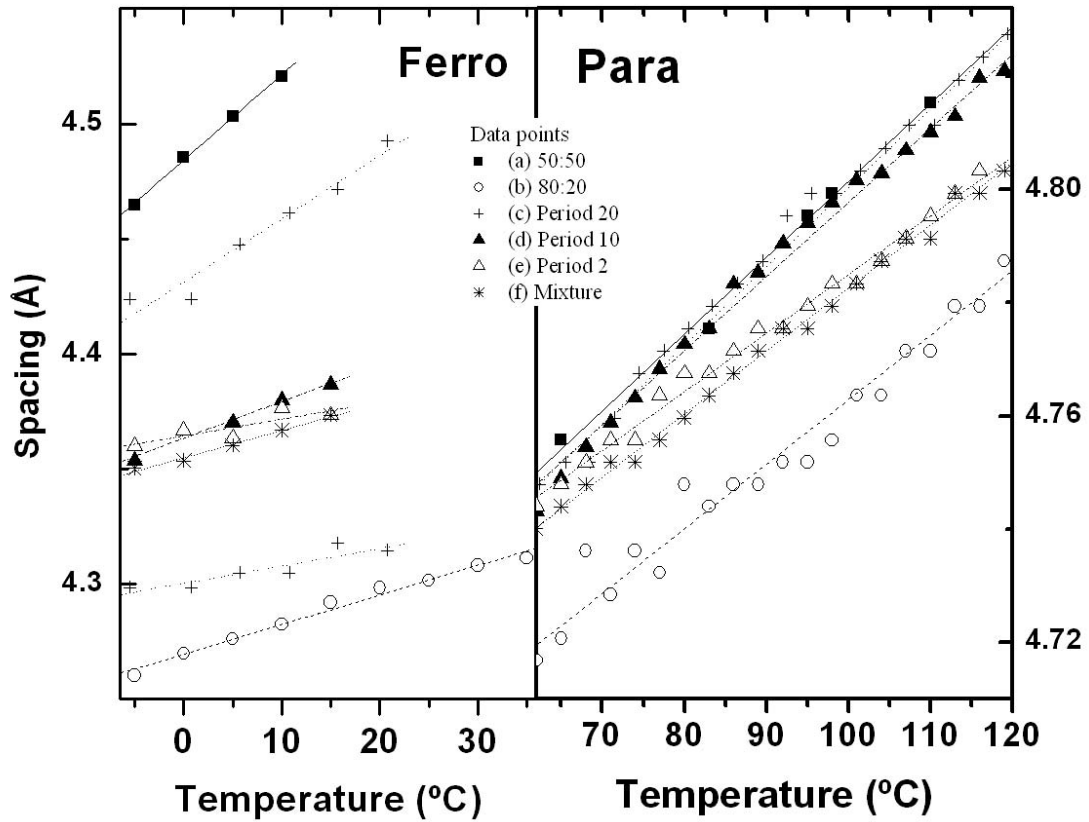
from the paraelectric phase) were much better, meaning that distinct ferroelectric peaks for two independent materials could not be resolved. For the Period 20 sample, we obtained better fits with three-peaks, one for each ferroelectric peak from the two compositions and a single combined paraelectric peak. (The paraelectric peaks are at nearly the same spacing, and so are not resolvable, as we confirmed by attempting to fit two paraelectric peaks.) The peak positions obtained from this analysis are shown in Figure 3. 7. We calculated the integrated intensity of each peak as obtained from the fitting procedure, and normalized the intensity to 1 at each temperature, so that the values represent the fraction of the ferroelectric and paraelectric phases, respectively. The normalized intensities obtained in this fashion are shown in Figure 3.8.

The lattice spacings of all samples obtained from the peak positions of the x-ray diffraction data shown in Figure 3.5 are plotted in Figure 3.7 as a function of temperature. The thermal expansion coefficients for both the ferroelectric and paraelectric phases of all samples were obtained and are listed in Table 3.1. Regardless of the values of the expansion coefficients, the lattice spacing of all the heterogeneous samples is intermediate between that of the pure 50:50 and pure 80:20 copolymers, for both phases. In the paraelectric phase, both the spacing and the thermal expansion coefficients of the samples are within a small range,  $\sim 1\%$  and  $\sim 30\%$ , respectively. In the ferroelectric phase, the lattice spacings and the thermal expansion coefficients of the samples cover a wider range,  $\sim 5\%$  and  $\sim 300\%$ , respectively. The thermal expansion of the ferroelectric and paraelectric peaks in the Period 10 sample are intermediate between the

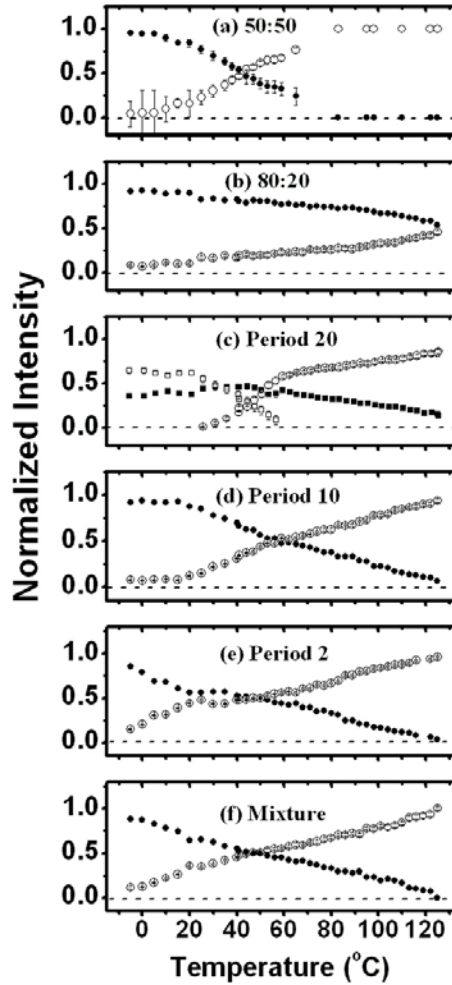


corresponding values for the two pure copolymers, whereas the Period 2 and the mixture samples show a thermal expansion that is close to (but even lower than) the thermal expansion coefficient of the 80:20 sample. If we make the reasonable assumption that the interlayer interaction is proportional to the numbers of interfaces, it follows that the interactions between the 80:20 and 50:50 copolymers tend to reduce the thermal expansion coefficients of both materials. The temperature evolution of each phase is quite different and this leads to a complex temperature dependence of the lattice spacing in the heterogeneous samples. To understand the nature of these interactions better, we next consider the relative proportions of each phase as the samples are heated through the transition temperature.

The relative proportions of each phase, as obtained from the integrated intensities of the x-ray peaks, are shown as a function of temperature in Figure 3.8. For the pure 50:50 copolymer sample (see Figure 3.8a), the data clearly shows the gradual conversion from purely ferroelectric phase (solid circles) at low temperature to purely paraelectric phase (open circles) at high temperatures. The data from the pure 80:20 sample shows a much more gradual conversion that is only half completed at the maximum measurement temperature of 125 °C. The rate of phase conversion differs among the samples. In the pure copolymer samples (see Figure 3.8a and b, we see that below 80 °C the conversion rate of the 50:50 copolymer is greater than the 80:20 copolymer, whereas above 80 °C the 80:20 copolymer has the greater conversion rate.



**Figure 3.7** shows lattice spacings determined from the x-ray diffraction peaks shown in Figure 3.5 as a function of temperature, for the following samples: (a) pure 50:50 (solid squares); (b) pure 80:20 (open circles); (c) Period 20 (crosses); (d) Period 10 (solid triangles); (e) Period 2 (open triangles); and (f) Mixture (asterisks). The lines represent linear regression fits to the peak positions yielding the thermal expansion coefficients, which are listed in Table 3.1.



**Figure 3.8** shows the normalized peak intensity as a function of temperature obtained from analysis of the x-ray diffraction data shown in Figure 3.5. The graphs shown are for the six samples as follows: (a) pure 50:50; (b) pure 80:20; (c) Period 20; (d) Period 10; (e) Period 2; and (f) Mixture. Open circles indicate the paraelectric phase, and solid circles indicate the ferroelectric phase. In the graph (c), the open squares and solid squares indicate the peaks associated with ferroelectric phase of the 50:50 copolymer and the 80:20 copolymer, respectively, as described in the text.

The intensity data from the Period 20 sample in Figure 3.8c show independent phase conversion of the two compositions – the ferroelectric peak corresponding to the 50:50 copolymer spacing tracks the phase conversion rate of the pure 50:50 copolymer films, and similarly for the peak corresponding to the 80:20 composition. In contrast, the transition rates of the Period 10, Period 2, and the mixture samples in Figure 3.5c-e are almost constant over the phase conversion range. This behavior is consistent with an interaction between the different materials, but it is not definitive evidence, because averaging the rates of phase conversion can lead to similar behavior. The endpoints of the phase conversion provide a more useful indicator of the effect of sample structure on the stability of the ferroelectric state.

With the complex phase conversion and thermal hysteresis phenomena, it is often not sufficient to identify a single transition temperature. Therefore, we define several useful critical temperatures as follows. The lower critical temperature  $T_0$  is the temperature at which the paraelectric phase first appears as the sample is heated. The upper critical temperature  $T_1$  is the maximum temperature of the ferroelectric phase. These critical temperatures were determined by extrapolating the XRD peak intensity data in Figure 3.8 –  $T_0$  by extrapolating the paraelectric peak intensity to zero, and  $T_1$  by extrapolating the ferroelectric peak intensity to zero. The phase crossover temperature  $T_{1/2}$  is the temperature at which the integrated intensities of the ferroelectric and paraelectric peaks are equal. The value of  $T_{1/2}$  indicates the effective midpoint of the phase coexistence region, whether or not the layers are interacting. The critical

temperatures of all samples are listed in Table 3.2. The critical temperatures of the pure 50:50 sample determined by this method are  $T_0 = 9 \pm 1$  °C and  $T_1 = 85 \pm 8$  °C. These limits are clear and unambiguous because the phase coexistence region is relatively narrow and the phase transition temperature is low. However, the more gradual transition of the 80:20 sample, together with the high value of the phase transition temperature, lead to more uncertainty in the values of  $T_0$  and  $T_1$ . Even at 125 °C, the sample consists of approximately 50% ferroelectric phase and 50% paraelectric phase, so that we are not able to even define a  $T_1$  for the 80:20 sample. At the lowest temperature of  $-5$  °C, the paraelectric peak is already evident (see Figure 3.5b), and the  $T_0$  of the 80:20 copolymer determined by this extrapolation method ranges between  $-40$  °C and  $-30$  °C.

The transition temperatures listed in Table 3.2 indicate that for the Period 10 sample, the value of the lower critical temperature  $T_0$  is close to that of the pure 50:50 sample, whereas for the Period 2 and mixture samples,  $T_0$  is lower, and in-between that of the 50:50 and 80:20 copolymers. The value of the upper critical temperature  $T_1$  for all three samples is approximately the same, and well above that for the pure 50:50 sample. The phase transition region in the multilayer and mixture samples is much wider than for the pure 50:50 sample, but much narrower than that of the 80:20 sample. The effect of sample structure on the transition temperature is strong evidence for interlayer interaction; the ferroelectric-to-paraelectric phase transition in these films is strongly influenced by the proximity of the 80:20 and 50:50 copolymers, leading to a behavior intermediate to that of the pure samples.

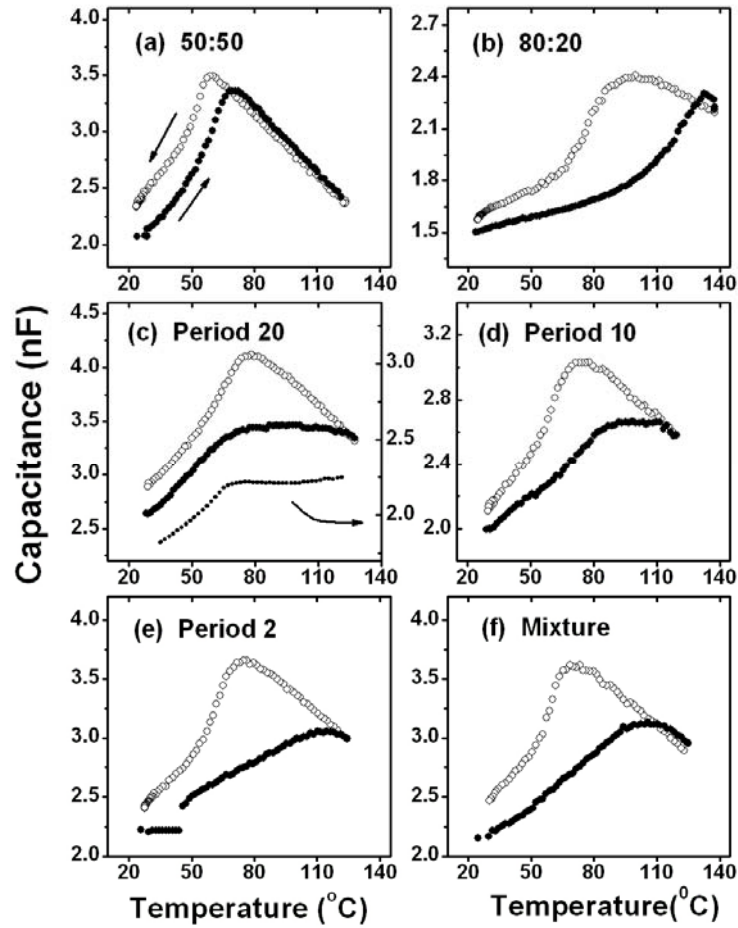
**Table 3.2** Critical temperatures obtained from both XRD intensity and capacitance measurements as described in the text. The values of  $T_0$ ,  $T_1$ , and  $T_{1/2}$  were obtained from the XRD intensity data shown in Figure 3.8. The values of  $T_{c+}$  and  $T_{c-}$  were obtained from the capacitance peaks shown in Figure 3.9.

	Transition Temperature				
	XRD Intensity			Capacitance	
	$T_0$ (°C)	$T_1$ (°C)	$T_{1/2}$ (°C)	$T_{c+}$ (°C)	$T_{c-}$ (°C)
<b>50:50</b>	9±1	85±8	43±2	70±4	59±3
<b>80:20</b>	-35±5	—	138±12	133±4	100±8
<b>Period 20</b>	30±5	170±8	57±6	97±20	78±5
<b>Period 10</b>	9±4	134±8	60±6	101±11	75±6
<b>Period 2</b>	-18±1	128±10	35±15	114±5	76±4
<b>Mixture</b>	-14±1	131±1	49±3	105±6	71±5

Although we do not have enough quantitative information to extract an exact interaction length, we see that as the number of interfaces increase in going from the Period 10 to Period 2 sample,  $T_0$  drops quite dramatically.

### Capacitance results

Another indicator of the ferroelectric-paraelectric phase transition is the dielectric anomaly, a peak that occurs at or near the phase transition temperature. Figure 3.9 shows the dependence of the capacitance on temperature for all samples as they were heated from room temperature to 125 °C and then cooled back to room temperature, both directions at a rate of 1 °C/min. Decreasing the heating or cooling rates by a factor of 5 does not significantly affect the results, so we consider these measurements to be made under quasi-equilibrium conditions.<sup>16</sup> The capacitance data for the pure 50:50 sample (see Figure 3.9a) shows the typical behavior of a ferroelectric polymer, with a peak on heating indicating the ferroelectric-paraelectric phase transition, and another one on cooling indicating the paraelectric-ferroelectric phase transition. The heating and cooling curves show thermal hysteresis, a consequence of the first-order nature of the phase transition. The temperatures of the heating and cooling peaks in the capacitance, designated as  $T_{C+}$  and  $T_{C-}$ , respectively, are listed in Table 3.2. Since the pure 80:20 sample was not fully converted to the paraelectric phase, its cooling peak (see Figure 3.9b) was broadened. The cooling peaks are all very similar, with  $T_{C-}$  values between those for the pure samples. Note that the values of  $T_{1/2}$  obtained from XRD are all lower than  $T_{C-}$ .



**Figure 3.9** shows the dependence of capacitance on temperature during heating (solid circles) and cooling (open circles) for six capacitor samples with the following construction: (a) pure 50:50; (b) pure 80:20; (c) Period 20; (d) Period 10; (e) Period 2; and (f) Mixture.



The breadth of the transition and the large thermal hysteresis are not very sensitive to sample crystallinity,<sup>47-50</sup> as is evident by the similar shape of the capacitance-temperature curves obtained with polymorphous samples,<sup>55</sup> LB films,<sup>43</sup> and high quality crystals.<sup>59</sup>

Although the locations of the capacitance peaks in the different samples gives some indication of interaction between layers of different compositions, the shapes of the heating peaks are even more revealing. Consider the shapes of the heating peaks for the multilayer and mixture samples, as shown in Figure 3.9c-f. The Period 20 multilayer sample shows a broad plateau in the capacitance on heating, whereas the Period 10 sample shows a narrower plateau and the Period 2 and mixture samples show rounded peaks. The expected dependence of the capacitance on temperature in an ideal non-interacting sample can be calculated by treating the layers with different compositions as capacitors connected in series. Applying this idealization to the data in Figure 3.9a and b yields the dashed line shown in Figure 3.9c. This line would apply to any of the multilayer structures if the layers are not interacting. The calculation yields a broad plateau very similar to the one in the data for the Period 20 sample, indicating that the Period 20 sample behaves as two independent films with little evident interaction between them, consistent with the above analysis of the x-ray data. (The calculated capacitance is lower than that measured in the Period 20 sample. Previous measurements have shown some variation in sample capacitance, probably a result of sample-to-sample variations in film thickness and electrode coverage.<sup>46</sup>)

The Period 10 sample shows a narrower plateau than expected for a noninteracting sample (i.e., the dashed line in Figure 3.9c), but not a single peak that would indicate a sample with a single transition temperature. It is more consistent with an intermediate situation – a sample consisting of independent, but interacting layers. The phase transition in part of each layer is influenced by interaction with its neighboring layers. This has the effect of raising the effective transition temperature of the adjacent 50:50 layers and lowering the effective transition temperature of the adjacent 80:20 layers and therefore narrowing the plateau compared to that of the noninteracting sample.

The heating peaks of the mixture and Period 2 samples, on the other hand, are relatively narrow, consistent with a film with a single, phase transition. Furthermore, the heating peaks for these samples are much closer to that of the pure 80:20 sample and there is no indication of a peak corresponding to the heating peak of the pure 50:50 sample. The capacitance and x-ray diffraction data from the mixture and Period 2 samples are nearly identical with each other, further supporting the hypothesis that thin multilayers have such strong interaction that they behave as a single composite sample.

#### Summary of results and discussion

The results of the x-ray diffraction and dielectric measurements can be summarized as follows. The Period 20 sample can be considered as two independent films. The temperature dependences of both the x-ray diffraction and capacitance data are consistent with two independent layers exhibiting little or no interaction. On the other end

of the range, both the Period 2 and mixture samples behave like a composite system with a single ferroelectric-paraelectric phase diagram. The Period 10 sample, on the other hand, exhibits both composite behavior and distinct features of 80:20 and 50:50 copolymers. This suggests that the effective interaction length is approximately the thickness of one of the material layers, or about 11 nm, corresponding to one of the four distinct material layers of the Period 10 sample.

An alternate explanation for the composite behavior observed with the Period 2 and Period 10 samples is that the layers intermixed in some way, perhaps during LB deposition or during annealing. Layer mixing during deposition might arise from gaps in individual layers, but our studies show that individual layers are continuous<sup>60,48,53</sup> and that films of only 1 or 2 LB layers usually make good capacitors,<sup>16,61,62</sup> indicating that gaps and pinholes are uncommon. The film transfer ratio during constant-pressure deposition is consistently near 1:1, which rules out significant layer mixing or thickness variation due to removal of previous layers. The x-ray diffraction measurements at the annealing temperature show that the samples were never melted, so there was no chance of mixing in the melt, when the polymer chains are mobile. Also, melted films recrystallize into needles with completely different orientation, losing their (110) orientation.<sup>48,53</sup> Because of the length and stiffness of the chains, they do not readily diffuse through each other in the solid state. This process would require highly unlikely cooperative motions of dozens to hundreds of formula units in multiple chains.

To test the sample stability during annealing, and put an upper limit on interlayer diffusion, we made additional annealing studies on the Period 10 and Period 20 samples after all the other measurements were completed. Since the initial annealing time was 2 hrs, we subjected the Period 10 and Period 20 samples at 135 °C to two additional annealing cycles of 20 hrs and one of 200 hrs. (This is in addition to several hours spent at elevated temperature during the synchrotron studies.) If these long annealing times led to greater inter-diffusion, we would expect both greatly decreased peak intensities (due to the larger amount of defects resulting from inter-diffusion) and, in the case of the period 20 sample, a smearing of the two resolvable ferroelectric peaks (see Figure 3.6c). The two 20 hr and the 200 hr annealing cycles did produce some decrease in the intensity of the 50:50 x-ray diffraction peak in the Period 20 sample by amounts of 10% after 40 hrs, to 20% after an additional 200 hrs. Similarly, the Period 10 sample exhibited decreases of 15% and 34% after 40 hrs and 200 hrs, respectively. The positions of the two ferroelectric peaks from the Period 20 sample were insensitive to the extra annealing, and both peaks are clearly resolvable even after a total of 240 hours of annealing. These extended annealing studies shows that even after 100 times longer annealing there is little or no change in the Period 20 sample, so that it seems very unlikely that the period 10 sample suffered diffusion effects after only two hours of annealing. Taken together, all the annealing studies allow us to conclude that it is unlikely that the observed composite behavior is due to inter-diffusion of the 80:20 and 50:50 multilayers.

### 3.5. Conclusions

The capacitance and x-ray diffraction data in the multilayer samples establishes a progression consistent with an interaction length of approximately 11 nm. (This is larger than the interaction length of  $\leq 4$  nm estimated for interactions between the VDF copolymer and Cu phthalocyanine particles in a nanocomposite.<sup>34</sup>) The Period 20 sample shows little or no interaction between the relatively thick films of pure 50:50 and 80:20 copolymer. The Period 10 sample exhibits behavior intermediate between that of noninteracting films and a composite film. The Period 2 sample behaves as a composite sample, nearly identical in structure and behavior to that of the mixture sample.

We note that the lower critical temperature,  $T_0$ , and the higher critical temperature  $T_1$  occur in two different regimes. At and below  $T_0$  the samples are all fully ferroelectric. Hence all the interactions occur between ferroelectric phases of the 50:50 and 80:20 materials. Between  $T_0$  and  $T_1$ , there exists a heterogeneous mixture of ferroelectric and paraelectric regions. In this regime, one can envisage an interaction driven by the polarization of the ferroelectric phase on the paraelectric regions, thereby increasing  $T_1$  and/or changing the transition rate as compared to the pure samples.

In ferroelectric thin films, there are two general interaction mechanisms – mechanical and electrostatic. Both are connected with boundary conditions and are most pronounced in systems with a first-order ferroelectric phase transition. Mechanical interaction arising from stress is common in epitaxial systems, where the interaction

length is the distance over which strain is relaxed, usually through accumulation of dislocations.<sup>12,29</sup> For the VDF copolymers, the lattice constants perpendicular to the polymer chain are 10% smaller in the ferroelectric phase than in the paraelectric phase. For example, the compressive stress of an 80:20 layer in its ferroelectric phase, with its smaller lattice spacing, on a 50:50 layer in its paraelectric phase would tend to stabilize the ferroelectric phase of the 50:50 material, and raise its transition temperature. This effect is also observed in high-pressure studies, where the transition temperature of the VDF copolymers increases linearly with the application of hydrostatic pressure.<sup>63</sup>

Electrostatic interactions arise from the boundary conditions on the electric displacement. In a multilayer capacitor containing both ferroelectric and paraelectric layers, surface charge on the ferroelectric layer produces an electric field in the paraelectric layer, which in turn tends to polarize the paraelectric layer, stabilizing the ferroelectric state, and raising the transition temperature of the paraelectric layer. This effect is also observed in applied-field studies, where the transition temperature of the VDF copolymers increases linearly with the application an external electric field.<sup>50</sup>

With either mechanism, mechanical or electrostatic, the phase transition and critical temperatures for the Period 10, Period 2 and mixture samples can be described as follows. For the Period 10 sample, the value of  $T_0 = 9 \pm 4$  °C. For non interacting layers, the x-ray peaks should be additive. A simple model in which the experimental intensities of the pure 80:20 and the pure 50:50 sample as a function of temperature are added

together gives an extrapolated  $T_0$  value  $2.5 \pm 3$  °C, which is fairly close to  $T_0 = 9 \pm 4$  °C. This indicates that in the ferroelectric phase, there is little or no interaction in the Period 10 sample. The much lower  $T_0$ s of the Period 2 and the mixture samples is a strong indication of the existence of interaction in these samples in the ferroelectric phase. The Period 10, the Period 2, and the mixture have similar transition rates over the entire transition region with the peak intensities changing at a rate of approximately  $0.008 \pm 0.002 (\text{°C})^{-1}$ . This could be interpreted as evidence that in this mixed paraelectric-ferroelectric phase region, the interaction has a fairly long length scale and is insensitive to the shorter period.

In summary, studies of ferroelectric-paraelectric phase transition temperature in multilayers consisting of ferroelectric VDF copolymers with different compositions, and therefore different phase transition temperatures, show clear evidence of interaction between the two copolymers, with an estimated interaction length of 11 nm. The main evidence for this conclusion is the observation that samples with a layer thickness thicker than 11 nm exhibit little or no interaction, while thinner samples exhibit interaction and the thinnest sample exhibits composite behavior nearly identical to a mixture sample. The transition from independent to interacting to composite behavior has not been reported before with ferroelectric multilayers. This begins a new approach to the study of polarization correlations in ferroelectric systems. It also offers new opportunities for materials engineering afforded by the ability to control the transition temperature and the breadth of the coexistence region. For example, ferroelectric polymers make a good

acoustic match to aqueous environments and are therefore useful for ultrasonic imaging and for sonar, where the temperature of the environment is nearly constant.



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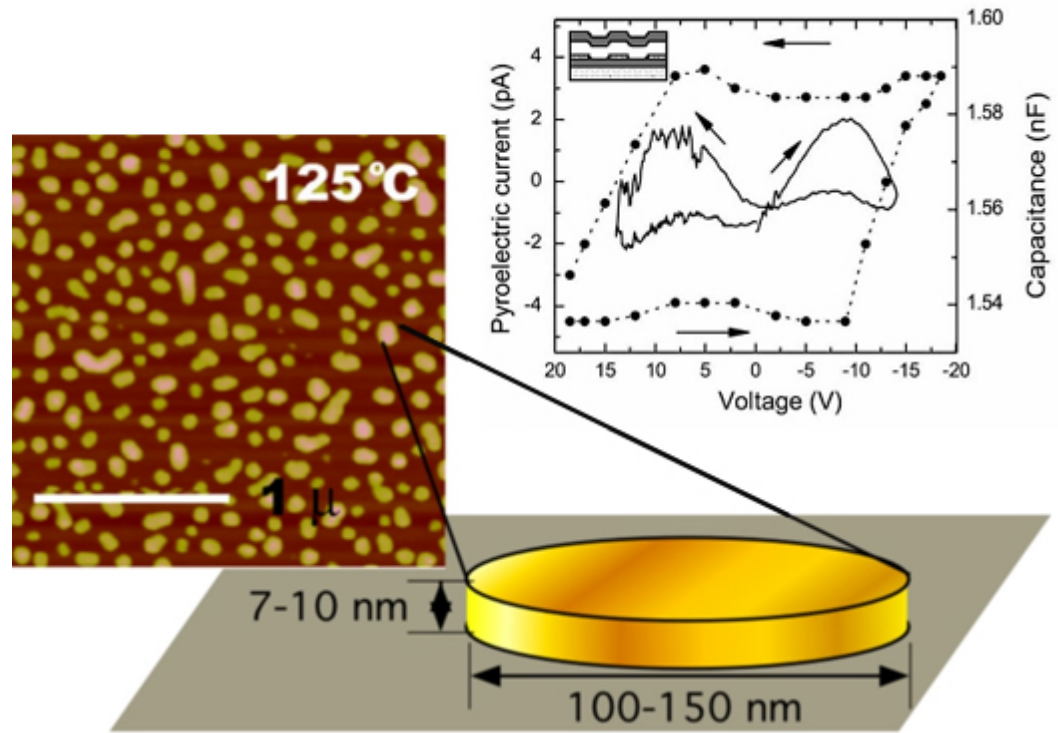
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## Chapter 4 Polarization Switching of Nanomesas

### 4.1 Introduction

As introduced in earlier chapters, nanomesas are disk-shaped nanostructures with dimension of 100 nm in diameter and 9 nm in thickness, developed through self-assembly during annealing. Observation of nanomesa formation presented in section 2.5 revealed that the active formation of nanomesas from a 1 LB layer film of 70:30 copolymer started at 60 °C (see Fig. 2.15) and ended between 120 °C ~ 135 °C during annealing. Prior studies done by Bai *et al.* characterized the properties of nanomesas formed after annealing at 125 °C for 1 hour.<sup>1</sup> They probed nanomesas macroscopically through X-ray diffraction, capacitance vs. temperature measurement (CT), capacitance butterfly curves (CV), and pyroelectric current measurements.<sup>1,2</sup> In their study, XRD peaks of nanomesa samples showed stronger intensity compared to an annealed 20 LB layer thin film, which implied good crystallinity of nanomesas. CT measurement on a nanomesa-capacitor of 50:50 copolymer showed the ferroelectric-to-paraelectric (paraelectric-to-ferroelectric) transition at 63 °C (50 °C). CV and pyroelectric current ( $I_p$ ) measurements on the same nanomesa-capacitor sample showed polarization switching (Fig. 4.1), and the polarization reversal occurred at approximately  $\pm 13 \sim 14$  V. Observation of the phase transition and the polarization switching evidently proved the ferroelectricity of nanomesas in average.



**Figure 4.1** shows AFM images of nanomesas and their average dimensions, modeled as a thin disk. The plot at the upper right of the figure shows a hysteresis in the pyroelectric current and butterfly curve measured from a nanomesa capacitor film, consisting of nanomesas formed from a 3 LB layer film of P(VDF-TrFE) 70:30 copolymer, and a 4 LB layer of polyethylene with the top and bottom aluminum electrodes. The schematic sample configuration of the nanomesas is shown at the upper left corner of the plot. The figures are reused with permission from Mengjun Bai, *Applied Physics Letters*, **85**, 3528 (2004). Copyright 2004, American Institute of Physics.

In contrast to the previous studies, which probed only the average behavior of nanomesas, the main goal of this project is to study the electromechanical and switching properties of individual nanomesas. The fact that nanomesas are disk-shaped and nanoscale in size could possibly open new paths for designing memory devices out of them, and other ferroelectric applications. Thus, direct investigation on individual nanomesas is necessary. To make a direct approach at the nanoscale of the individual nanomesas, a scanning probe microscopy (SPM) system is the best technique to apply.

There are various different kinds of SPM developed to probe different types of interaction between the probe and the sample surfaces such as Atomic Force Microscopy (AFM), Scanning Tunneling Microscopy (STM), Magnetic Force Microscopy (MFM), and Piezoresponse Force Microscopy (PFM). Among those, PFM is a primary tool for imaging and characterizing ferroelectric materials at nanoscale;<sup>3,4,5,6</sup> therefore, it is highly suitable for the goal of our study. In addition to PFM, there is an advanced application of PFM called switching spectroscopy PFM (SS-PFM), used for our study. SS-PFM is a powerful tool to reveal a local switching property of ferroelectric samples.<sup>7,8,9</sup>

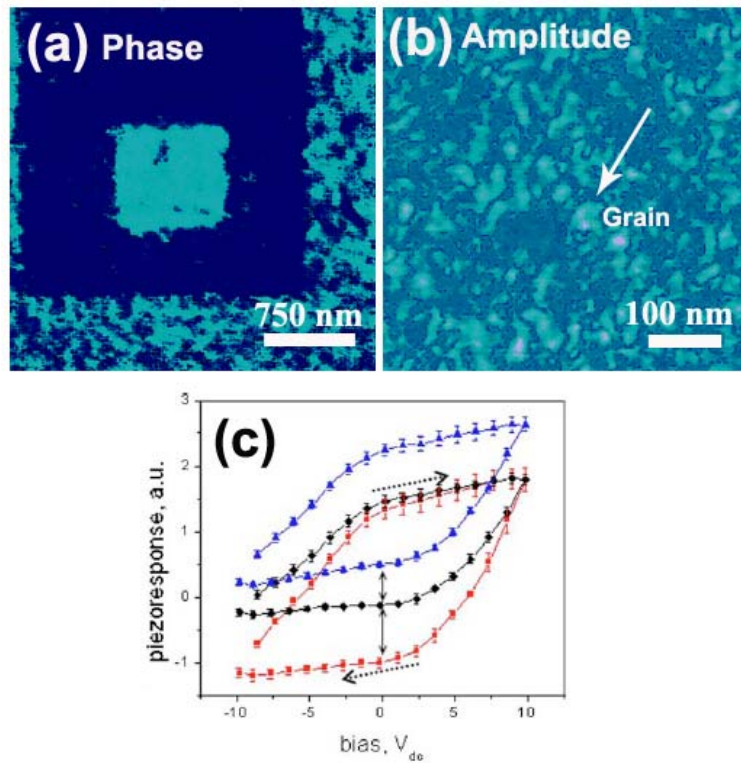
For this study we have used PFM and SS-PFM facilities at the Center for Nanophase Materials Sciences (CNMS) at Oak Ridge National Laboratory (ORNL) in collaboration with Dr. Kalinin *et al.*. Prior to this nanomesa study, investigation on copolymer thin films<sup>10</sup> already started using the system. The thin film study showed that we could switch the films of 70:30 copolymer consisting 10 LB layers corresponding to

approximately 18 nm with  $\pm 10$  V (Fig. 4.2a), and the boundary of oppositely polarized sample area revealed grain types of switching unit about 25-50 nm in size (Fig. 4.2b). Also, well-behaving hysteresis loops were obtained from most of the probed sample area (Fig. 4.2c).

Inspired from the prior study, we planned to obtain PFM images of oppositely polarized individual nanomesas and piezoelectric switching hysteresis loops from local areas within an individual nanomesa with SS-PFM. These results would clearly show ferroelectric properties of individual nanomesas. In following sections of this chapter, results that we obtained will be presented in detail after a brief description of sample preparation.

## 4.2 Sample Preparation

Nanomesa samples were prepared by annealing thin films of 70:30 copolymer consisting 1 LB layer at 135 °C for 2 hours. The heating and cooling rate for the annealing procedure was 1 °C/min (The detailed LB film deposition process on the trough can be found in section 1.3.). The sample substrate used for this study was Si wafer with crystal orientation (100). For convenient sample grounding, aluminum electrodes were deposited at the back of the Si substrates where the metal sample holder makes a direct contact with the samples. The DC resistances of the Al electrodes were initially in a range of 50 ~ 100 k $\Omega$  as the electrodes were deposited, and the resistances were lowered to a range of 5 ~ 10 K $\Omega$  after a day of baking in the oven at 200 °C.



**Figure 4.2** (a) and (b) are PFM images and (c) are piezoresponse hysteresis loops obtained from 10 LB layer film of P(VDF-TrFE 70:30) deposited on HOPG. The figures are reused with permission from B. J. Rodriguez, *Applied Physics Letters*, **90**, 122904 (2007). Copyright 2007 American Institute of Physics.



### 4.3 Polarization Switching Observation with PFM

In this section firstly principles of PFM scanning will be introduced, and then the results of PFM study will be presented and discussed.

#### 4.3.1. Principles of PFM Scanning

PFM measurement is an additional measurement to AFM. During AFM measurement, an external AC field with a frequency  $\omega$  will be applied to the AFM tip, coated with conductive material, and then AFM will provide additional images of the electromechanical response of the sample, which are called amplitude and phase images of piezoresponse on top of the topographic AFM image. For PFM application, AFM runs in contact mode so that the oscillating piezoresponse can be separated from the constant topographic signal using lock-in technique. Now, let us look at this procedure in detail.

#### *Elements for the PFM*

The PFM system consists of a commercial AFM system (Veeco MultiMode NS-III A) equipped with additional function generators and lock-in amplifiers, and external signal generation and data acquisition electronics.<sup>8,9,10</sup> Also, a custom-built electrically shielded sample holder was used for direct tip biasing and to avoid capacitive crosstalk by bypassing the SPM electronics. The probes used for the study are MikroMasch models CSC37A, CSC37B, and CSC38A coated with Cr-Au and with nominal spring constants of 0.35 N/m, 0.30 N/m, and 0.03 N/m, respectively. For temperature control, the Veeco

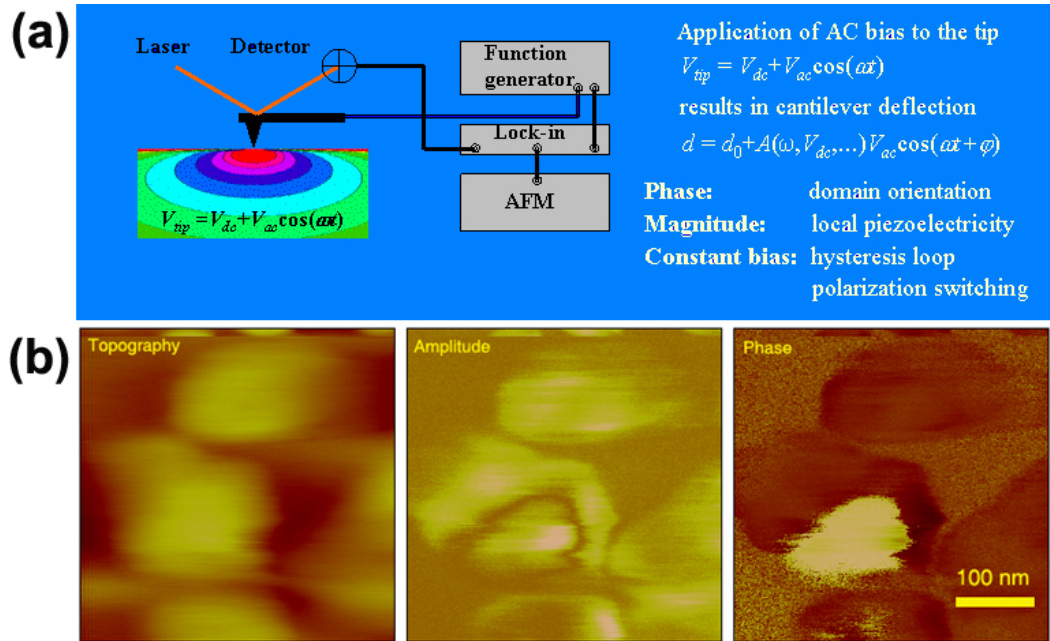
Multimode NS-III A has attachable heating and cooling elements. The temperature range the system could be held stable within 1 °C over the range 0 °C to 135 °C.

### Topographic Image

First of all, in contact mode AFM, the interaction between the tip and the surface results in the deflection of the cantilever, which thus acts as a force sensor.<sup>6</sup> The topography, the AFM image, is recorded by keeping the relative interaction force between the tip and the sample surface constant through the entire image. The relative force is controlled by a set-point voltage of the cantilever position detector, which corresponds to the degree of the deflection of the cantilever due to the tip-sample interaction. To keep the deflection constant, the vertical position of the cantilever base moves according to the topography of the sample surface, providing a topographic image. For imaging nanomesas, the set-point voltage was an order of one tenth V, which corresponds to a tip force of an order of 1 nN when the spring constant of the tip is approximately 0.3 N/m.

### Piezoresponse Images

Now, let us look at how the contact mode AFM is applied to PFM imaging (Fig. 4.3a). Ferroelectric materials exhibit piezoelectricity, which is an electromechanical coupling response.<sup>11</sup> The presence of a stress  $X_{jk}$  in piezoelectric materials induces a change in the surface charge density  $\sigma_i$  of the material,<sup>12,13</sup> and they show the following linear relationship.



**Figure 4.3** (a) is a schematic configuration of the PFM system; this figure is from S. V. Kalinin group [website http://nanotransprot.ornl.gov](http://nanotransprot.ornl.gov); (b) is an example of a set of PFM images; the topography, the amplitude, and the phase. Figure 4.3a is reused with permission from S. V. Kalinin.

$$\sigma_i = d_{ijk}^{direct} X_{jk} \quad (4.1)$$

where  $d_{ijk}^{direct}$  is the piezoelectric coefficient of the material. This is called the direct piezoelectric effect. Conversely, applying an electric field  $E_k$  to the material causes strain  $x_{ij}$ , expressed as

$$x_{ij} = d_{kij}^{converse} E_k \quad (4.2)$$

where  $d_{kij}^{converse}$  are the converse piezoelectric coefficients of the material, and this is called the converse piezoelectric effect.<sup>12,13</sup> PFM is based on the detection of bias-induced surface deformation (strain), the converse piezoelectric effect, and the process is as follows.

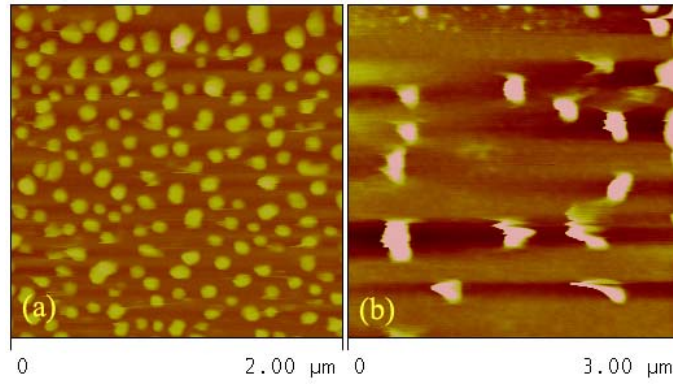
During the contact mode AFM scanning, an external AC voltage of a frequency  $\omega$  is applied to the tip by using the function generator. The AC voltage on the tip produces an AC field in the sample. This electric field will produce a sample deformation,  $d \sim A \cos(\omega t + \varphi)$  according to the converse piezoelectric effect if the sample is piezoelectric<sup>5,6,7</sup>. Note that the sample must have a counter electrode. In this PFM scanning, adapted to AFM, the signal, detected as a cantilever position, contains both topography (the position of the cantilever base) and the piezoresponse  $A \cos(\omega t + \varphi)$  (oscillation part of the signal) from the sample. The piezoresponse signal, followed the same frequency  $\omega$  of the applied field, thus this piezo part of the signal can be separated out by using the lock-in amplifier, referenced to  $\omega$ . The oscillating part of the signal,

sorted out by a lock-in, will be sent to the main control program of the microscope through auxiliary channels, and be recorded as two complementary PFM images; one as the amplitude, and the other as the phase. As a matter of fact, a PFM measurement provides three images in total; the usual AFM topography, plus the amplitude and the phase of the piezoresponse of the sample (Fig. 4.3b).

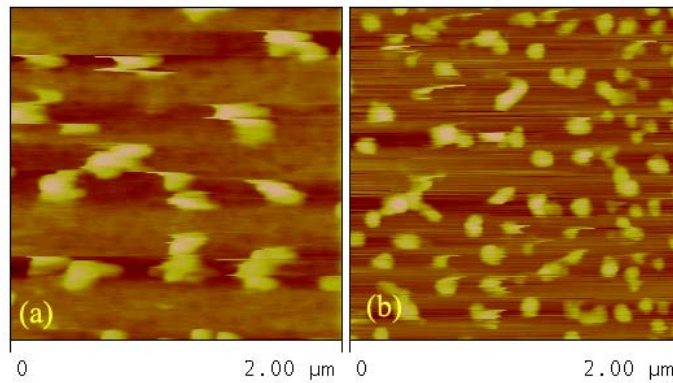
### 4.3.2 Scanning Conditions and Issues in PFM

Before we try to record images of switched nanomesas as our goal, we first needed to test PFM scanning conditions. In this section, the PFM scanning conditions and the issues that we faced during test-scans will be discussed before we look into the main results of the PFM study. Throughout the tests, the morphological modification of nanomesas was a major issue. It is known that AFM imaging in contact mode can be destructive when the tip-sample distance is below 1 nm.<sup>6</sup> However, the modification in PFM imaging cannot be attributed entirely to the contact mode AFM. The softness of nanomesas is another fundamental cause of the morphological modification of nanomesas. Having these fundamental issues, we focused to reduce the degree of the modification, and followings are the effects of scan conditions on nanomesa modification.

1) AC Bias: First of all, the effect of AC bias amplitude on the sample modification was tested by comparing images recorded with and without AC bias at room temperature. The test showed strong effect of AC bias (Fig. 4.4). The image recorded without AC bias (Fig. 4.4a) shows nanomesas almost the same as they were formed.



**Figure 4.4** shows topography of nanomesas obtained from PFM scanning; (a) with zero bias at room temperature; (b) with AC voltage of 5 V<sub>p.p.</sub> at 650 kHz at room temperature.



**Figure 4.5** shows topography images of PFM taken; (a) at room temp with AC bias of 4 V<sub>p.p.</sub> at 890 kHz; (b) at 0 °C with AC bias 5 V<sub>p.p.</sub> at 570 kHz.

However the image recorded with AC bias of 5  $V_{p,p.}$  and 650 kHz shows an extreme modification (Fig. 4.4b). It seems that nanomesas were dragged by the tip and spread over the sample surface. We tested scanning with lower bias, however, with lower bias, it was not clear if we were getting good piezoresponse from nanomesas when it is lower than 3  $V_{p,p.}$ . Therefore, we decided to find other compensatory conditions to reduce the modification maintaining AC bias of in a range of 4~5  $V_{p,p.}$ .

2) Temperature and frequency of AC bias: Lowering the scanning temperature lessened the morphology modification as the effect is shown in Figure 4.5. The lowest stable temperature we could reach with the cooling element of the system was 0 °C; we had water condensation problem going below 0 °C. We suspect the reason why lowering temperature helped to prevent the modification is based on the following assumption. A temperature increase between the tip and nanomesas may occur during contact mode scanning, this temperature increase could exacerbates the sample modification according to the fact that copolymer film flows in paraelectric phase<sup>1,2</sup>, manifested as film separation. The active film separation starts at 60 °C (section 2.5). Therefore, lowering the scanning temperature could help nanomesas remain in ferroelectric phase and prevent the possible exacerbation in paraelectric phase of nanomesas. However, this assumption has not been tested.

3) The frequency and amplitude of the applied bias: Both the frequency and the amplitude of AC bias were manually tuned by monitoring the line scanning. With

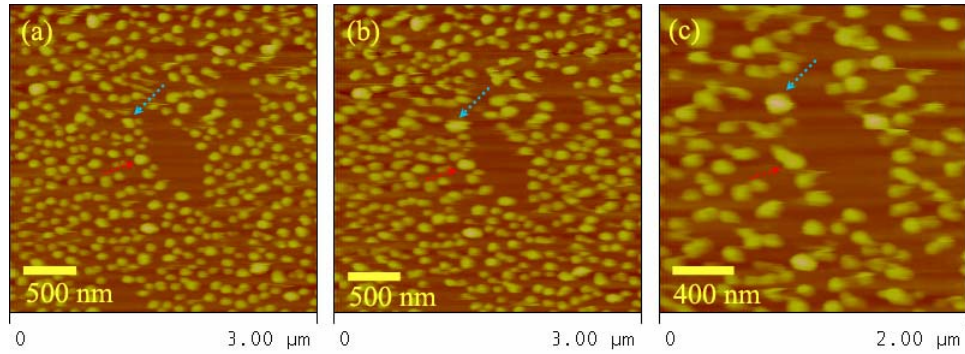
frequency of order of hundreds kHz and amplitude in the range of 4~5  $V_{p,p.}$ . PFM images were obtained. The modification was insensitive to the tested frequency and the amplitude of the AC bias. Note that the PFM study on the thin continuous films of copolymer used the same bias amplitude 4~5  $V_{p,p.}$ <sup>10</sup>

4) The scan angle, lines, size, and rate: The scan angle did not show apparent influence to the sample modification, but the scan lines, size, and rate showed their effects on the modification. Their common cause of the modification was due to repetitive contacts between the tip and nanomesas, which is inevitable in contact mode imaging. The more the frequent contacts are, the worse the modification is (Fig. 4.6). To obtain images of reasonable resolution we made scans consisting of 256 or 512 scanning lines. Having this scan line restriction, the modification problem becomes more serious when the scan area is smaller than 1 micron. This problem was compensated by increasing the scan rate. The scan rate was approximately 2 ~ 3 lines per second to obtain good images from a 1~2 micron size of scan area. (Fig. 4.7)

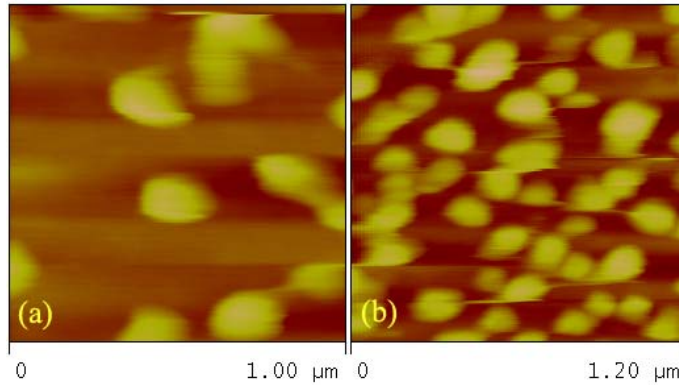
### 4.3.3. PFM measurements and results

As mentioned at the beginning of the chapter, the main goal for the project is to study ferroelectric properties of individual nanomesas. Obtaining piezoresponse from nanomesas is not sufficient to prove ferroelectric properties of nanomesas.





**Figure 4.6** shows three consecutively recorded AFM images over the same sample area; (a) first, (b) second (c) the third scan. The nanomesas indicated with the red and blue arrows show changes in their morphology.



**Figure 4.7** shows Topography images recorded during PFM scanning on two different areas in the same sample. Both (a) and (b) were recorded under similar conditions, and then; (a) at the scan rate of 1.6 Hz (1.6 lines/second); (b) at the rate of 2.5 Hz

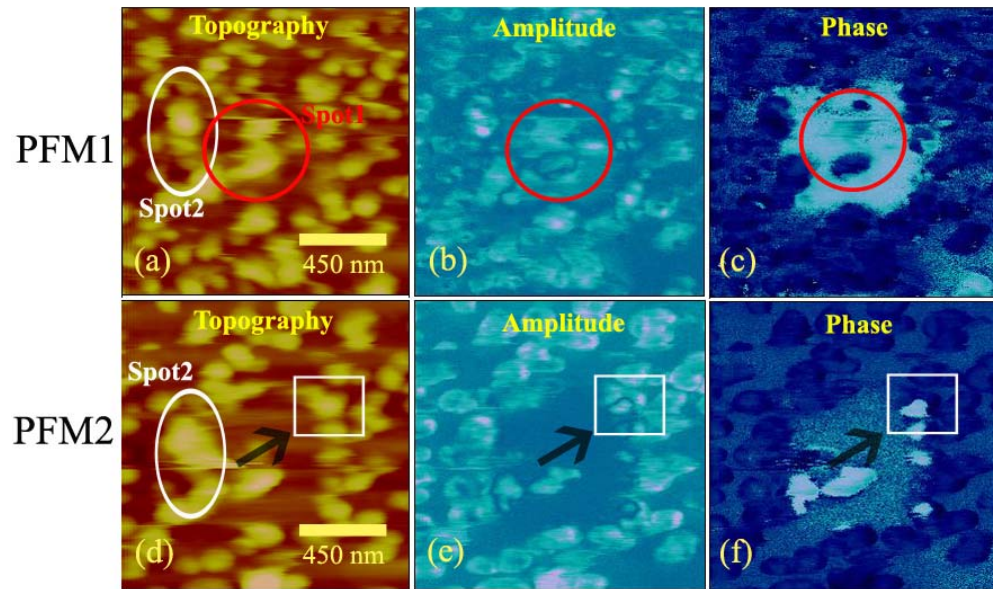
The property distinguishing ferroelectric materials from other piezoelectric materials is having switchable spontaneous polarization. Therefore, we should present the switching properties of individual nanomesas to prove their ferroelectricity.

According to our purpose, we planned to obtain PFM images of oppositely switched nanomesas by recording images after polarizing them with opposite polarity of DC voltages as the previous thin film PFM study showed the switching properties of the thin film (Fig. 4.2a). The results are shown in Figure 4.8. In addition to this switching property of nanomesas, we have observed some detailed structures within individual nanomesas shown in Figures 4.9 through 4.12. The focus of the analysis on the detailed structures was whether they are domains or not.

#### *PFM Results 1: Nanomesa Switching*

In Figure 4.8 two sets of PFM images are shown; namely PFM1 and PFM2. These two sets were obtained from the same sample area with following steps. Firstly, a square of size 600 nm, was scanned with a DC tip bias at +7 V, and then image set PFM1 was measured over a larger area, a square of size 1.5  $\mu\text{m}$ . After obtaining image set PFM1, the same polarizing procedure was repeated on the same area of the sample but with a dc bias of -7 V, and then the image set PFM2 was recorded.

First, we can notice some degree of modification on nanomesas in these two sets of PFM images.



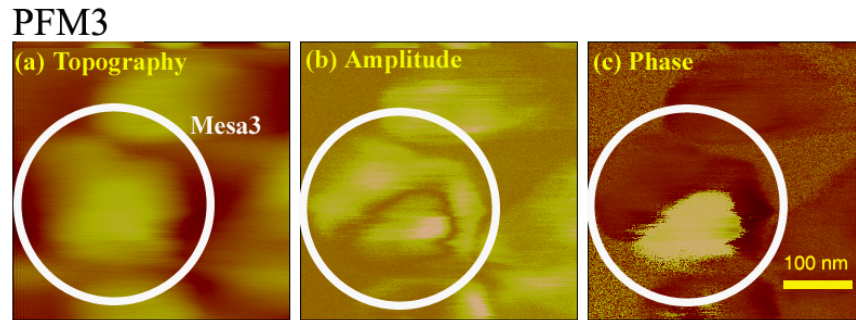
**Figure 4.8** shows two sets of PFM images recorded over the same region. (a) and (d) show topography, (b) and (e) amplitude, and (c) and (f) phase. A 600 nm square area at the center of the image area, was polarized with + 7 V and -7 V for PFM1 and PFM2, respectively. Some specific features are specially marked with circles and squares and arrows for discussion.

The area, circled with red line (spot1) shows severe modification due to an applied bias during scanning since this area is at the center of the image where previously scanned with  $\pm 7$  V bias. Topography of nanomesas in this red-circled area shows significant distortion (see Fig. 4.8a), and the corresponding area in amplitude (Fig. 4.8b) and phase (Fig. 4.8c) images are not following the topography. The area, circled with white line in Figure 4.8d is an example of the modification due to repetitive scans compared to the same area in Figure 4.8a since PFM2 was recorded after PFM1 on the same area. Also, we can notice in these white-circled areas that there has been a scanning drift between PFM1 and PFM2; the white-circled area in Fig. 4.8d is lower in y position compared to the same area in Fig. 4.8a.

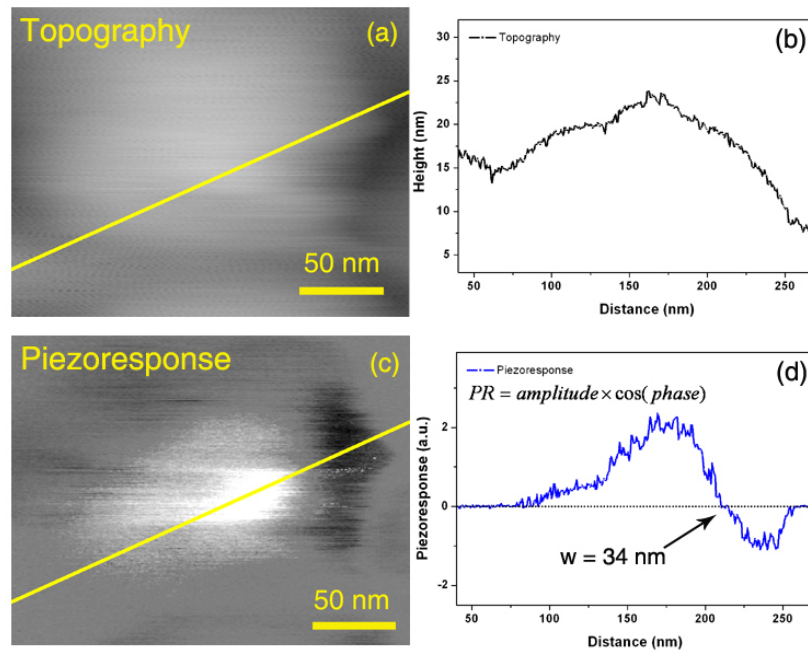
Despite the modifications described above, these two sets of PFM images clearly showed oppositely polarized nanomesas. At the center of Fig. 4.8c and Fig 4.8f, we can see nanomesas in the positive (dark color) phase and in the negative (bright color) phase, respectively. We named the dark color phase as the positive phase and the bright color phase as the negative phase<sup>a</sup> since they were obtained after polarizing with the positive and the negative bias, respectively. This piezoresponse of opposite polarities proved that the individual nanomesas could be switched; therefore they were anticipated to be ferroelectric. Additionally, we observed nanomesas that contained both the positive and negative phase within one nanomesa in these set of PFM. Those nanomesas are at the right edge of the 600 nm square of the polarized area, as indicated with the black arrow.

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<sup>a</sup> This is the relative phase. Determination of the absolute phase was not possible in this measurement.



**Figure 4.9** shows a set of PFM, named as PFM3 recorded from the area indicated with a white square in PFM2 of Fig. 4.8. The circled nanomesa is called Mesa3 for discussions.



**Figure 4.10** (a) and (c) are the topography and mixed piezoresponse of Mesa3 marked in Figure 4.9; (b) a line scan of topography of Mesa3 indicated with a yellow line in (a); (d) shows a line scan of a mixed piezoresponse of Mesa3 indicated with the yellow line in (c); (c) is the calculated mixed piezoresponse (PR) image using the equation shown in (d).

This led us to question whether nanomesa can contain multiple domains or not. To investigate this, we recorded another PFM image over the target area, squared with white line in PFM2, and the image is shown in Figure 4.9, namely PFM3.

### PFM Results 2: Domains

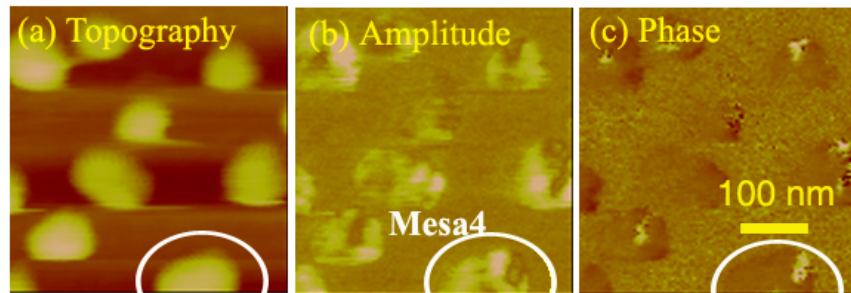
To test whether the boundary shown in PFM3 is domain boundary or not we examined the dimension of the nanomesa, circled with white line and named as Mesa3. The maximum length across Mesa3 is approximately 250 nm, which is more than twice the size of the typical nanomesa. The maximum length across the bright phase region in Mesa3 is approximately 140 nm. (These dimensions are measured from the amplitude image.) These dimensions suggest Mesa3 may consist of two or more nanomesas. In other words two nanomesas were merged during annealing or by the tip during scanning. To make sure this conclusion we did following test.

In general, the amplitude images of PFM show a minimum value at the domain boundary between two opposite polarization.<sup>6,10</sup> To see if the boundary we see in the amplitude image of PFM3 (Fig. 4.9b) is a true domain boundary, we tested it with the imaging resolution method. The principle of the imaging method is that the width of the transition from positive to negative piezoresponse determines the PFM imaging resolution,<sup>6,10</sup> and the procedure is as follows. We firstly generated the mixed piezoresponse,  $PR = amplitude \times \cos(phase)$  for the PFM image of Mesa3 (Fig. 4.10d), and then a selected line profile of the mixed piezoresponse across the boundary as

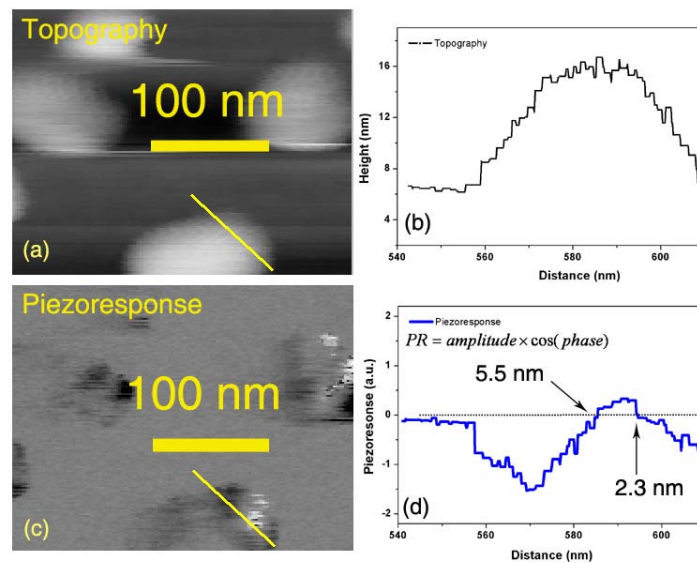
indicated with yellow line in Figure 4.10d was fit to the domain-wall profile function,  $R(x) = R_- + (R_+ - R_-) \tanh[(x - x_0)/(w/2)]$ , where  $R_+$  ( $R_-$ ) is the response on the left (right) of the domain wall centered at  $x_0$  and  $w$  is the width of the domain wall.<sup>6,14</sup> According to the fit result, the imaging resolution (i.e., the domain wall width) of the yellow line profile (Fig. 4.10d) was determined as 34 nm. The determined value 34 nm as PFM imaging resolution is unreasonable since it is more than 30 % of typical nanomesa size. Also, the boundary width in the amplitude image of Mesa3 is clearly visible and it is directly measured as 8 nm from the amplitude image (Fig. 4.9b). This, in fact, agrees well with the imaging resolution 5 nm obtained from the previous thin film PFM study.<sup>10</sup> Therefore, this test confirmed that the boundary in Mesa3 is not a domain boundary, but a physical boundary of two merged nanomesas suggested by the dimension analysis.

Now, let us look at another PFM image of nanomesas with interesting detailed structures. Figure 14.11 shows PFM images (PFM4) recorded with a fresh tip without any polarization treatment. The level of modification seems very low, and nanomesas show detailed structures within individual nanomesas, and this time, the scale of the detailed structures were smaller in scale compared to Mesa3 case. We again applied the imaging resolution method to test if the detailed structures in PFM4 were domains similarly as we tested Mesa3.

## PFM4



**Figure 4.11** shows a set of PFM images showing nanomesas with interesting domain structures. One specific nanomesa is marked with the white circle and named Mesa4.



**Figure 4.12** (a) and (c) are the topography and mixed piezoresponse images of Mesa4, which was marked in Figure 4.11; (b) a line scan of topography of Mesa4 indicated with a yellow line in (a); (d) shows a line scan of a mixed piezoresponse of Mesa4 indicated with the yellow line in (c); (c) is the calculated mixed piezoresponse (PR) image using the equation given in the text.



First, we magnified the bottom right corner of Figure 14.11 (where the circled nanomesa, Mesa4 is positioned) and presented the magnified images in Figure 14.12; the topography (a), the mixed piezoresponse (c), and their line profiles (b) and (d), respectively. The widths of the domain walls within Mesa4 were determined as approximately 2.3 nm and 5.5 nm as indicated in Figure 4.12d. This value is close to the resolution 5 nm, obtained from the previous thin film PFM study.<sup>10</sup> This convinces us that the imaging resolution obtained from Mesa4 is real, and therefore, they are domains. As a matter of fact, we can conclude that nanomesas can contain multiple domains, even though it is not clear at this point whether the domains were developed during nanomesa formation or during PFM scanning.

#### **4.4 Polarization Switching Observation with SS-PFM**

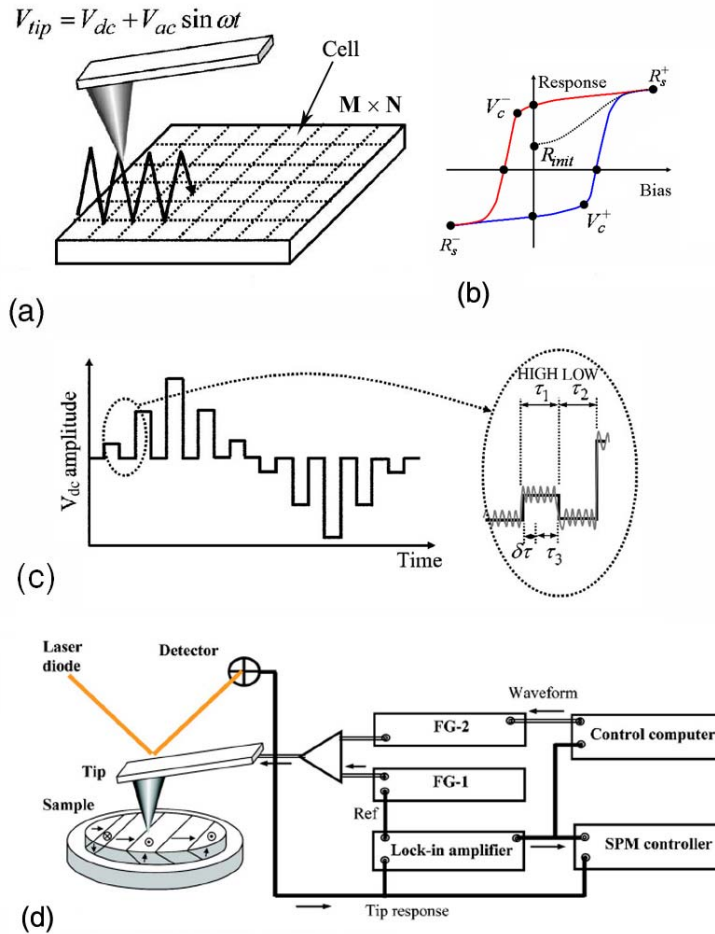
In the previous PFM study section we have observed that individual nanomesas are switchable with  $\pm 7$  V bias suggesting possible ferroelectricity, and can contain multiple domains within one nanomesa. Now, in this section a confirmed switching property of nanomesas, resulted in piezoresponse switching hysteresis loops are presented. The switching hysteresis loops have been obtained using SS-PFM, and how SS-PFM records the loops will be introduced first.

##### **4.4.1 Principles of SS-PFM scanning**

SS-PFM is an advanced application of PFM. SS-PFM is configured in the force volume imaging mode. From SS-PFM measurements we can obtain a two dimensional

image map consisting of an array of  $M \times N$  local piezoelectric switching hysteresis loops from a scanned area. SS-PFM is configured in force volume imaging mode of Veeco MultiMode NS-III A AFM system.

In the force volume imaging mode, the microscope collects an array of  $M \times N$  force curves from a targeted scan area, divided into  $M \times N$  grids, then the force curves are mapped out as a two dimensional (2D) image. (The force curve is a function of the approach-retract travel distance of the tip, recorded as the cantilever deflection according to the tip-surface interaction force, and the more detailed information about the force volume imaging can be found in the manual of Veeco MultiMode NS-III A and the website of Veeco).<sup>15,16</sup> SS-PFM is developed by adapting this functionality to PFM. Therefore, we can obtain an array of  $M \times N$  local piezoelectric switching hysteresis loops with SS-PFM analogous to the force curves with AFM. For SS-PFM measurement, an additional function generator (Fig. 4.13d) needs to be added to the PFM system to apply the switching bias to the scanning tip to obtain piezoelectric switching loops, the piezoresponse as a function of applied bias (switching bias) at each cell (Fig. 4.13b). The switching bias is a series of voltage pulses (Fig. 4.13c) that are combined with the small AC piezoresponse bias (see inset to Fig. 4.13c).



**Figure 4.13** (a) shows an array of  $M \times N$  cells in SS-PFM images; (b) is a schematic plot of a standard switching hysteresis loop; (c) shows the waveform of voltage pulses used for SS-PFM scanning; (d) is a schematic configuration of SS-PFM system. The figures are reused with permission from S. Jesse, *Review of Scientific Instruments*, **77**, 073702 (2006) and *Applied Physics Letters*, **88**, 061908 (2006). Copyright 2006, American Institute of Physics.

Now, let us look at how SS-PFM works in detail. During SS-PFM scanning, the tip moves from one point to the next in a step motion according to the scan conditions: a step size  $l$ , a number of steps,  $M$  (in  $x$  direction) and  $N$  (in  $y$  direction), and a scan rate, the time taken at each cell. Thus, the entire image consists of  $M \times N$  small areas of size  $l \times l$  so called a cell. At each cell, the series of voltage pulses (Fig. 4.13c) are applied in sequence, each followed by a piezo measurement, and thus local hysteresis loops are obtained. The pulse polarizes the local area when it is on for an order of few milliseconds, and then the piezoresponse from the local area is recorded when the pulse is off. A number of hysteresis loops can be repeatedly taken at one location, however too many repeats will increase the total scanning time enormously since a typical SS-PFM measurement consists of an order of thousand cells. Typically 2 cycles of hysteresis loops were recorded at each cell. The obtained hysteresis loops from each cell are analyzed during scanning by fitting to a standard hysteresis loop shape as follows.

The fitting software firstly calculates the average of the 2 cycles of hysteresis, and the averaged switching loop is fit with the Boltzmann sigma functions (Eq. 4.3 and 4.4) which represents the standard shape of hysteresis loops.<sup>8</sup>

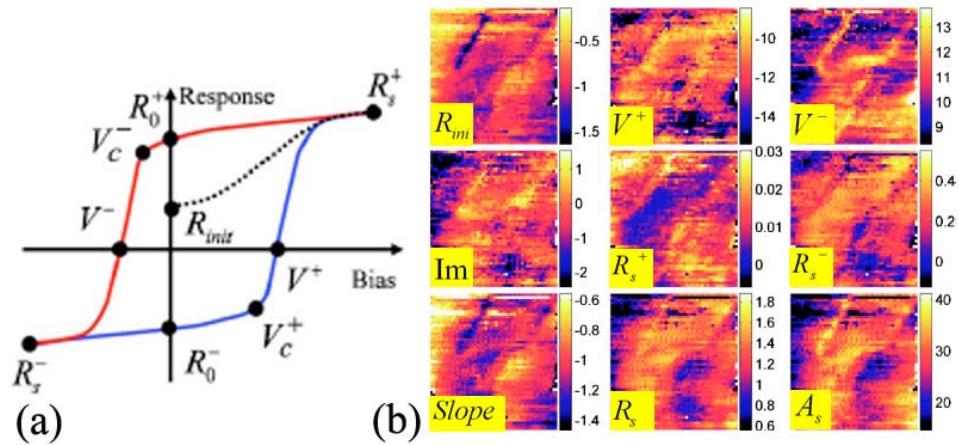
$$R^+(V) = a_1 - a_2 \left[ 1 + \exp\left(\frac{V - a_3}{a_5}\right) \right]^{-1} + Va_6 \quad (4.3)$$

$$R^-(V) = a_1 - a_2 \left[ 1 + \exp\left(\frac{V - a_4}{a_5}\right) \right]^{-1} + Va_6 \quad (4.4)$$

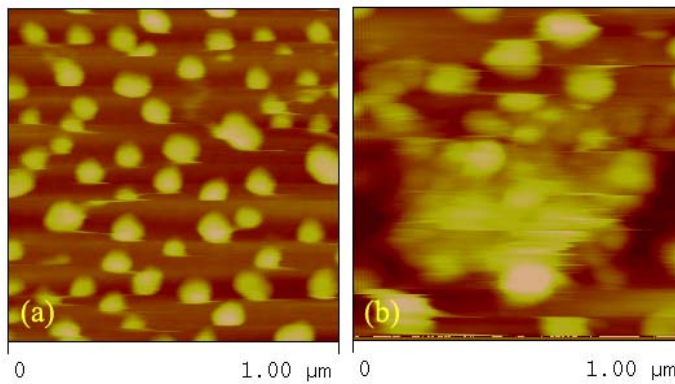
$R^+(V)$  and  $R^-(V)$  in above equations are piezoresponse as a function of bias in forwarding direction (from negative to positive bias, +) and in the reverse direction (from positive to negative bias, -), respectively. By using the six fitted coefficients  $a_1 \sim a_6$  in the fitting function, 9 characteristic parameters of the switching loop (Fig. 4.14a) are determined for each cell, and then mapped out for the entire scan area (Figure 4.14b). The characteristic parameters are the initial piezoresponse  $R_{ini}$ , the coercive biases  $V^+ = a_4$  and  $V^- = a_3$ , the saturation responses  $R_s^+ = a_1$  and  $R_s^- = a_1 - a_2$ , the switchable polarization  $R_s = a_2$ , the imprint  $Im = (a_3 + a_4)/2$ , the slope of the loop  $a_6$ , and the work of switching  $A_s = a_2(a_4 - a_3)/2$ . This curve fit processing software was developed by Jesse *et al.*. The SS-PFM method and the fitting procedure can be found in detail in their papers.<sup>8,9</sup>

#### 4.4.2 Scanning conditions and Issues in SS-PFM

Now let us look at the scanning conditions and issues in switching spectroscopy PFM (SS-PFM). Similar to PFM, SS-PFM showed morphological modification on nanomesas. As shown in Figure 4.15, nanomesas were significantly distorted after a SS-PFM scan. In this scan the amplitude of the AC bias was  $4 V_{p,p}$ , and the maximum DC pulse for to the switching loop measurement was  $10 V_{dc}$ . Since we have already observed that the degree of modification is strongly affected by an applied bias in PFM measurements (see section 4.3.2), we lowered both the amplitude of AC bias and the maximum value for the DC pulse to  $1 \sim 2 V_{p,p}$  and  $7 \sim 7.5 V_{p,p}$ , respectively.



**Figure 4.14** (a) is a schematic switching hysteresis loop, labeled with the switching characteristic parameters; (b) is a set of SS-PFM images, consisting of 9 maps. Each map shows the indicated property of the sample surfaces, probed with SS-PFM probe. The figures are reused with permission from S. Jesse, *Review of Scientific Instruments*, **77**, 073702 (2006) and S. Jesse, *Applied Physics Letters*, **88**, 061908 (2006). Copyright 2006, American Institute of Physics.



**Figure 4.15** shows topography images obtained from PFM scanning (a) before (b) after SS-PFM scanning.

With the lowered bias, we were able to improve the modification problem involved in SS-PFM, and these values were used for all results SS-PFM measurements presented in this dissertation.

Other scanning conditions we checked were the total number of cells ( $M \times N$ ), the size of the cells and scan area, and the number of steps of switching bias pulses for one cycle of a switching loop. These conditions were related to the resolution of the image map, and the scanning time of SS-PFM. Assigning more cells to a scan could give us higher resolution of image maps in principle; however, the tip drift problem became significant as the increased cells resulted in a longer scanning time. For example, we observed 7 % of drift in one direction after a 40-min SS-PFM scan; therefore, we needed to choose cell numbers considering both the image map resolution, and the total scanning time. The typical values of the scan conditions that we used are as follows; the total number of cells is 900 ~1600, the size of cells 12~15 nm, the scanned area ~500 nm<sup>2</sup>, the number of pulse steps is 48, and the typical number of cycles of the hysteresis loops at each cell is 2. It takes approximately a few seconds to complete two switching loops with 48 switching bias steps in a loop, thus approximately 0.5 ~1 hour for a scan consisting 30×30 cells.

#### **4.4.3 SS-PFM Results and Discussion**

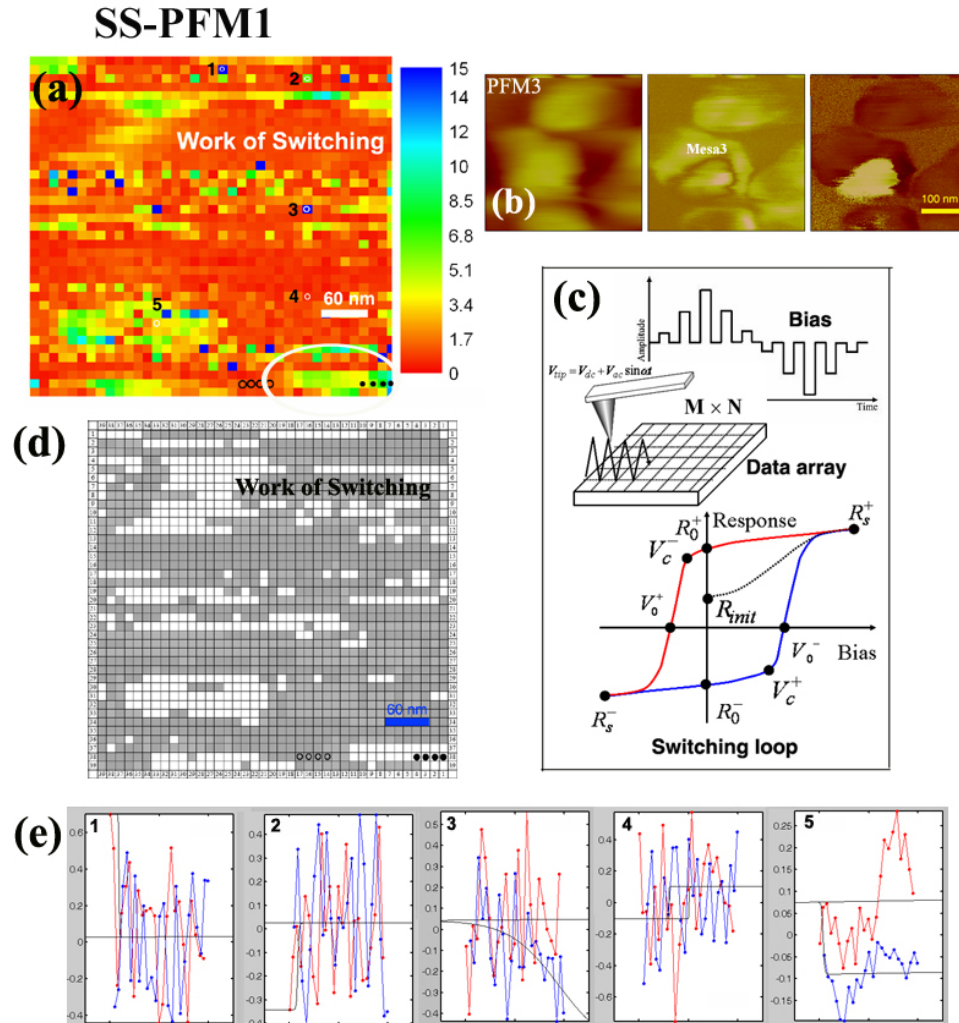
In the PFM study section (section 4.3), we have observed that the piezoresponse of individual nanomesas is switchable, indicating that they are ferroelectric. In this

section SS-PFM results (SS-PFM1 and SS-PFM2) are presented, and the results show clear switching hysteresis loops from nanomesas indicating they are ferroelectric.

SS-PFM1 image (Fig 4.16a) is a work of switching map, consisted of 1600 cells, each with a size of  $12 \times 12 \text{ nm}^2$ , over a square of size 480 nm that we obtained from vicinity of the sample area shown in Figure 4.16b. Due to the morphological modification and the tip drift during scanning, a perfect topographical match between the PFM image (Fig. 4.16b) and the SS-PFM image (Fig. 4.16a) is not expected between scans. AC bias of  $1.5 V_{p,p}$ , 678 kHz was used for piezoresponse measurement, and the maximum magnitude of DC bias pulse of 7 V was used for switching loops.

Figure 4.16c reminds us how the SS-PFM image was obtained, as described in section 4.2 (Fig. 4.13). The procedure can be briefly recalled as following. During SS-PFM scanning, switching loops from each cell was obtained, and the loops were fitted to the standard hysteresis loop shape (Fig. 4.16c), and the fitted characteristic parameters of the loops (see Figure 4.16c or Fig. 4.5a) were recorded as 2-dimensional image maps (Fig. 4.5b). Among 9 image maps, the map of the work of switching is selectively chosen to present our work. The reason is because the work of switching map is a useful guide to distinguish nanomesa regions from non-nanomesa region on the map since the work of switching corresponds to the area of the switching loop.

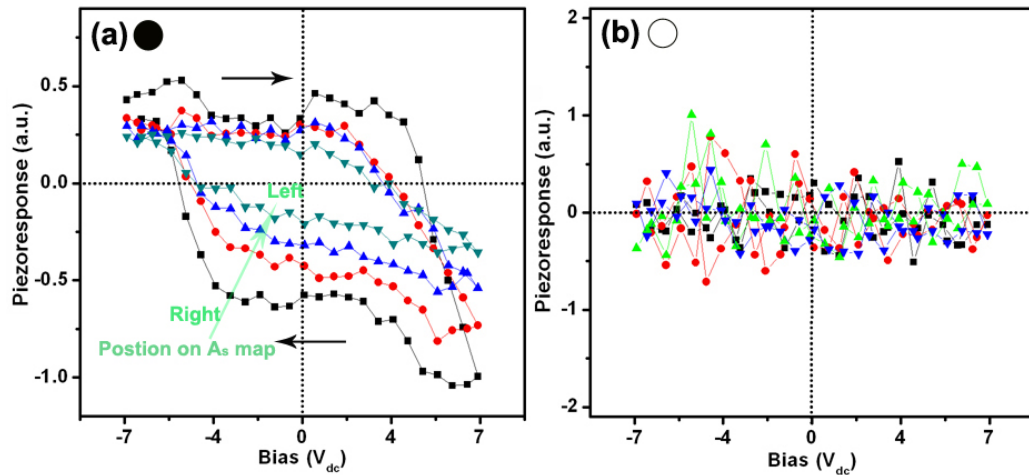




**Figure 4.16** shows: (a) a work of switching map obtained from SS-PFM1; (b) a PFM image recorded before SS-PFM1; (c) schematic plots of DC bias pulses, data array of SS-PFM, and a switching loop; (d) a simplified form of the work of switching map in (a); (e) examples of bad fitting results on null hysteresis loops. The size of the cell is  $12 \times 12 \text{ nm}^2$ , the total number of cells 1600. Figure 4.16c is reused with permission from S. Jesse, *Review of Scientific Instruments*, **77**, 073702 (2006) and S. Jesse, *Applied Physics Letters*, **88**, 061908 (2006). Copyright 2006, American Institute of Physics.

In other words, we will obtain hysteresis loops with non-zero work of switching value (called as an open loop, Fig. 4.17a) from nanomesa area, and no piezoresponse, resulted in zero work of switching value (called as a closed loop, Fig. 4.17b) from the non-nanomesa areas. As we expected SS-PFM1 clearly presents nanomesa areas (yellow and green in color) and non-nanomesa areas (red in color).

However, we need to note that there were a number of loops were not fit correctly because of a poor signal-to-noise ratio in some loops, and the examples are shown in Figure 4.16e. Each example in Figure 4.16e is numbered, and the cells where the bad fits are from are also marked with the same number of the example on SS-PFM1 (Fig. 4.16a). The work of switching for the loops 1, 2, and 3 (Fig. 4.16e) have been fitted to high work of switching values even though they are closed loop, and the loop 4 (Fig. 4.16e) were fitted as a small loop. This type of bad fit contributes to the non-zero background value in the  $A_s$  map. In the case of the loop 5, the bad fit result seems to be originated from the irregular shape of the loop. To exclude the bad fits for our analysis, we made a manual version of the  $A_s$  map shown in Figure 4.16d. In this simplified manual map nanomesa regions (open loops) and non-nanomesa regions (closed loops) are indicated as white and gray, respectively after examining the hysteresis loops individually. In fact, the fit version (Fig. 4.16a) and the manual version (Fig. 4.16d) match well indicating bad fits are not many. The  $A_s$  map (Fig. 4.16a) shows the detailed variation within the nanomesa region with colors, and the simple manual map (Fig. 4.16d) shows a clear boundary between well-behaving loops and the background (noisy or closed loops).



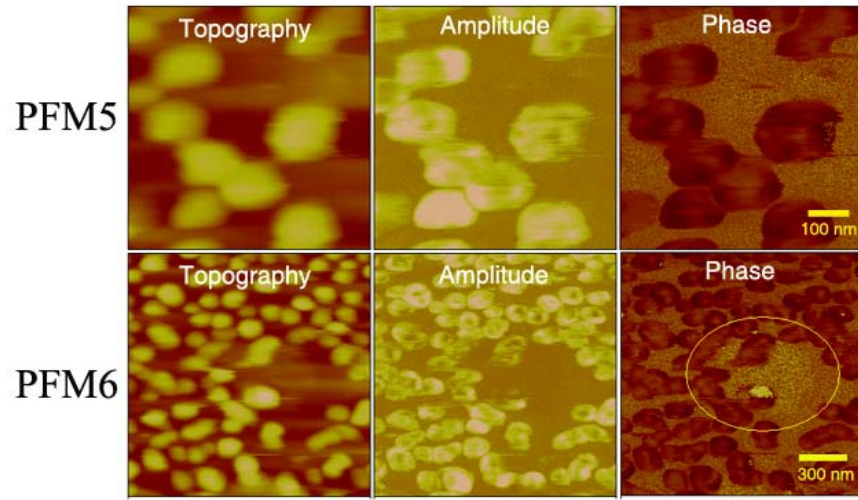
**Figure 4.17** shows individual hysteresis loops from indicated area on the work of switching map shown in Figure 4.16 (a) and (d); (a) from the cells, marked with solid circles; (b) from the cells, marked with hollow circles. One cycle of switching loop is consist of 48 pulses and one cycle takes about 1.2 sec

Now let us look at the actual hysteresis loops from the  $A_s$  map. The examples of switching loops are presented in Figure 4.17. The loops shown in Figure 4.17a are from the nanomesa region, indicated with solid circles ● at the bottom right corner on the  $A_s$  map (Fig 4.16a and d). The loops shown in Figure 4.17b are from non-nanomesa region, indicated with hollow circles ○ near the center of the bottom on Fig 4.16a and d. One can notice the clear contrast between them. The well-behaved loops show a gradual decrease in the work of switching value towards to the center of the nanomesa (towards the left corner on the map, Fig. 4. 16a and d) as labeled in Figure 4.17a. However, whether this is from intrinsic properties of nanomesas or from scanning effects, or both, is not clear at this point. Further investigation is needed to clarify it. Well-behaved loops similar to the ones presented in Figure 4.17a can be found from areas in green color scale on the  $A_s$  map. The average coercive voltage for the well-behaved loops is approximately 4 V, and

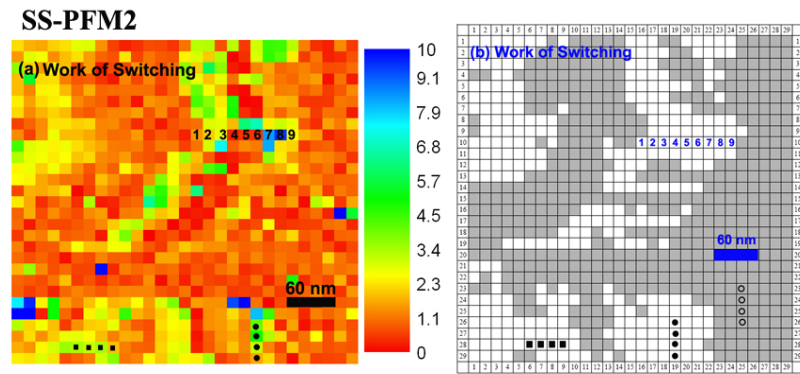
the average height of the nanomesas after modification are ranged between 9~15 nm. From this, the determined coercive field is approximately 250 ~ 450 MV/cm. A 10 LB layer continuous PVDF copolymer film of on graphite film studied with the same SS-PFM system showed the coercive field was approximately 250 MV/cm,<sup>10</sup> which shows good agreement with our results. The thickness of the 10 LB layer continuous film is approximately 18 nm.

Another set of PFM and SS-PFM measurements recorded from a fresh spot of the same sample with which SS-PFM1 was obtained, and they are presented in Fig 18 to 21. Two sets of PFM images namely PFM 5 and PFM6, respectively (Fig. 4.18) are images recorded before and after the SS-PFM measurement namely SS-PFM2. The work of switching map obtained from SS-PFM2 is shown in Figure 4.19. PFM5, the circled area of PFM6 and the  $A_s$  map of SS-PFM2 show a fair topographic match to one another. The cell size of SS-PFM2 is  $15 \times 15 \text{ nm}^2$ , and the scanned area is a square of 450 nm. Examples of well-behaving switching loops and closed loops from SS-PFM2 are shown in Figure 4.20 in a similar fashion as described for SS-PFM1. These loops from SS-PFM2 seem qualitatively consistent with the previous ones from SS-PFM1.

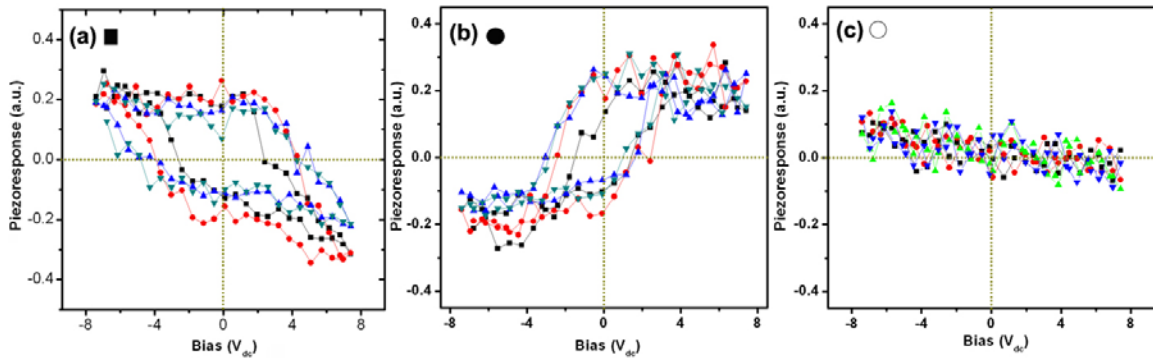
Now, let us note some interesting points. In this set of SS-PFM measurements we have observed the vertical reflection of the hysteresis loops (see Fig. 4.20a and b). This is likely due to the phase shift of the AFM probe, which often happened when the driving frequency is closer to the cantilever resonant frequency or its harmonics.<sup>9</sup>



**Figure 4.18** shows two sets of PFM, named as PFM5 and PFM6. PFM5 and PFM6 were scanned, respectively before and after SS-PFM2 shown in Figure 4.19. The area, circled in the phase image of PFM6 shows a fair matching with SS-PFM2.

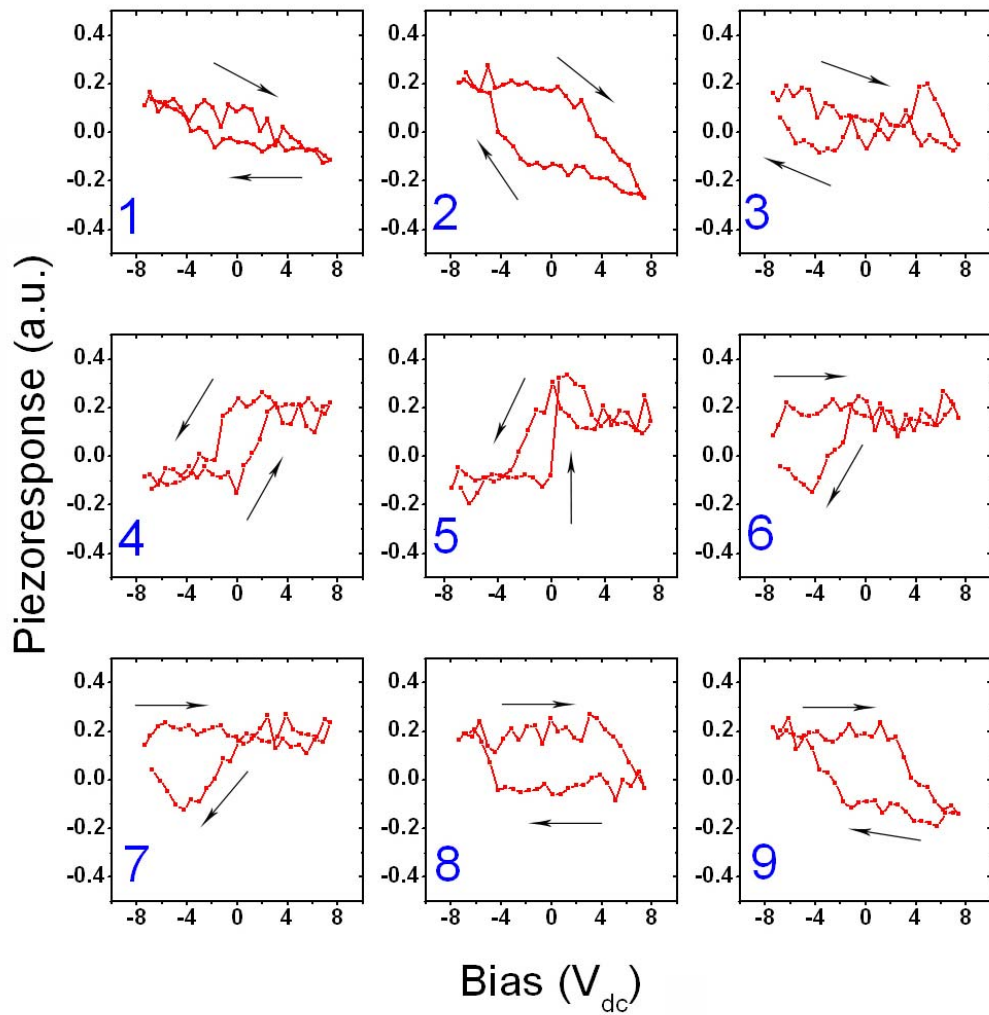


**Figure 4.19** shows; (a) a work of switching ( $A_s$ ) map obtained from SS-PFM2; (b) a simplified form of work of switching map in (a) The size of the cell is  $15 \times 15 \text{ nm}^2$ , the total number of cells 900.



**Figure 4.20** shows switching loops from the indicated area in Figure 4.19 (a) and (b). One cycle of switching loop consists of 48 pulses and one cycle takes about 1.2 sec, and the maximum bias in this loops are  $\pm 7.5$  V.

Also, various types of switching loops (Fig. 4.21) have been recorded from the sample area, numbered as 1 through 9 in Figure 4.19. The differences in the shapes of these loops shown in Figure 4.21 are very clear and significant in the degree even though they are next to one another merely with the cell size 15 nm. This phenomenon is considered to be originated from a significant modification of that region and the corresponding, modified nanomesa on the top part of the circled area in PFM6 (Fig. 4.18) supports this consideration. Therefore, based on this we can draw a conclusion that the morphological modification complicates the switching properties of the nanomesas, also in that modified region, an instrumental phase shift can occur. The phase shift problem should not be totally ignored and needs careful observation in the future, even though we strongly suspect that it is mainly an instrumental effect.



**Figure 4.21** shows hysteresis loops from area numbered from 1 through 9 in Figure 4.19 (a) and (b). The loops in various types of shape were recorded at every 15 nm in a straight line.

#### 4.5 Conclusion and Discussion

To conclude this PFM and SS-PFM study of polarization switching of nanomesas, we firstly observed suggesting switching property of individual nanomesas by recording PFM images of individual nanomesas, switched in opposite polarities with a dc bias of  $\pm 7$  V. Then, we proved the ferroelectricity of individual nanomesas by obtaining well behaving switching hysteresis loops with SS-PFM from a local area within individual nanomesas as small as 12 ~ 15 nm. The switching loops are clear evident for ferroelectricity. The measured coercive field from the well behaving switching loops is 250 ~ 450 MV/m, which shows good agreement to the continuous copolymer films.<sup>10</sup>

However, throughout the study, we experienced the morphological modification problem of nanomesas during PFM and SS-PFM scanning, and it has remained as an area needs to be investigated in the future. Also, the dynamics of switching loops have not checked in this study. Therefore, in the near future, following investigations can be attempted. For PFM, we can first try to obtain PFM images of nanomesas, less invaded either by conducting PFM at lower than 0 °C or by designing new samples. In the case for the designing new samples, the goal should be lowering the roughness of nanomesa sample surface. Reducing the thickness of nanomesas can be considered, however, it needs to be concerned about how much degree of piezoresponse we would obtain from nanomesas with the reduced thickness. Alternatively, we could find a way to prepare substrates with pockets where nanomesas could sit on could or non-piezoelectric materials, workable with LB technique which can be deposited as capping layers to cover



and protect the nanomesas to make smoother sample surface. In the case of depositing capping layers on the top of nanomesas, it would not be a direct measurement of nanomesas, this will be less invasive method. For SS-PFM we can obtain switching loops from a fixed area within an individual nanomesa, and apply different length of pulses in time and investigate the switching dynamics of individual nanomesas.

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## Appendix A Initial Work for Near Field PSM

Pyroelectric Scanning Microscopy (PSM) has been developed by Dr. Ducharme *et al.* in our lab. PSM system recently reached 500 nm of imaging resolution<sup>1</sup>, and it is anticipated to have better resolution by introducing the near field effect to the system. The imaging resolution 500 nm is an effective demonstration resolution estimated by the minimum size of the distinguishable feature in PSM images. Before presenting the results of the near field effect simulation and some experimental trials, let us look at the background of the PSM system.

### Background

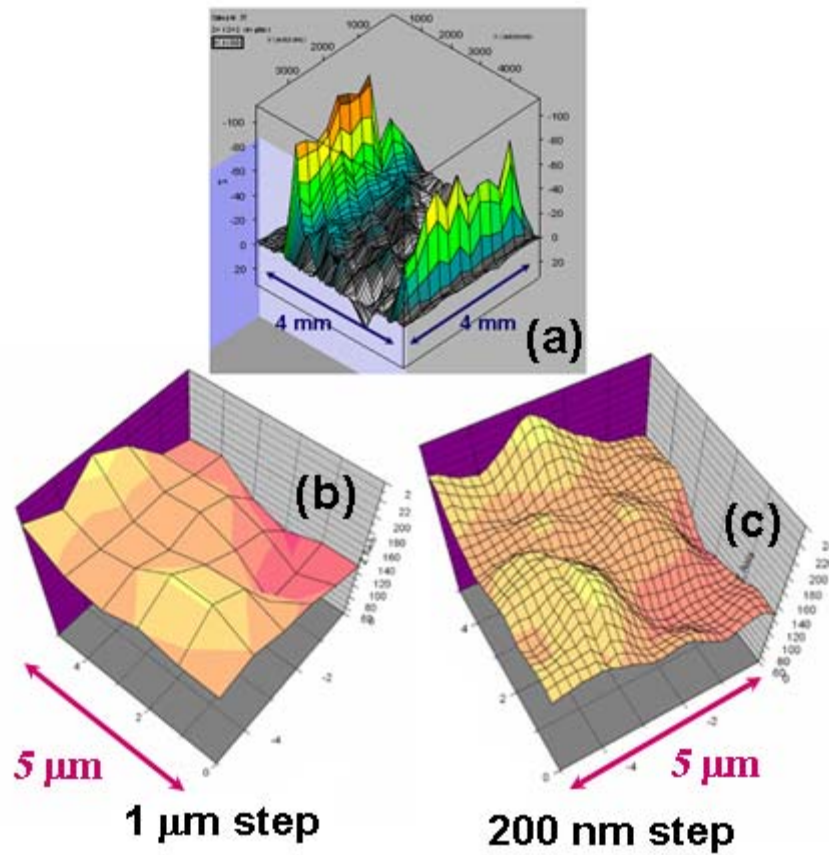
PSM records the pyroelectric current, originated from the electric polarization of the sample (see Chapter 2, p. 31),<sup>2,3</sup> from a unique x-y position in the sample area using a focused laser beam and a computer-controlled positioning system.<sup>4,5,6</sup> An example of a pyroelectric switching current loop has been introduced in chapter 2, which uses the same measurement technique as one implemented to the PSM system. With this technique, originally attributed to Chynoweth<sup>7</sup>, the pyroelectric current was measured by illuminating a sample area with a modulated He-Ne laser beam with an optical chopper at 2 kHz rate (see page chapter2, p32). The modulated laser beam changes the temperature of the illuminated sample area by heating and cooling at a constant rate. The size of the illuminated sample area depends on the beam size of the laser, and the heating and cooling rate depends on the laser modulation frequency, and power of the laser.<sup>4</sup> The He-

Ne laser, used for the pyro-measurement has the wavelength of 633 nm, and the beam width of approximately 0.3 ~ 0.4 mm.

Therefore, PSM was developed by reducing the beam size, and moving the sample by setting it on a positioning system, and then conducting the pyro-measurements under those conditions. The first version of PSM started as a manual control system with micrometer table in 1998,<sup>8</sup> thus the imaging resolution was limited by the positioning. The next version was built on the Melles Griot Nanomover *I*, which has a step resolution as small as 50 nm, and a microscope objective was added the system to reduce the He-Ne laser beam width approximately from 0.3~0.4 mm to 1  $\mu$ m beam size. This second achievement was made by Peterson *et al.*, and they suggested the imaging resolution could be improved further by replacing He-Ne laser with a shorter wave length laser, and by modulating the laser at higher frequency, and by using a better optics to reduce more of the beam width. These suggestions were made based on the following two equations. First one is

$$x_{rms} = (2Dt)^{1/2} \quad (B.1)$$

$x_{rms}$  is the thermal diffusion length of a sample due to the heating and cooling by a pulse laser (modulated laser) with a time period  $t$ , and  $D$  is the thermal diffusivity of the sample, which varies material by material. The thermal diffusion length,  $x_{rms}$  for our sample will limit the imaging resolution because the pyro-current is from polarization change within the heated and cooled area of the sample. Therefore, to reduce  $x_{rms}$ , we should use shorter time period, or a faster modulation frequency.



**Figure B.1** (a) is a PSM image over  $4 \times 4 \text{ (mm)}^2$  area with  $1 \text{ }\mu\text{m}$  steps recorded with the PSM version2; (b) and (c) are PSM image obtained with the recently developed version3 with a blue diode laser. (b) was recorded with  $1 \text{ }\mu\text{m}$  steps, and (c) was recorded with  $200 \text{ nm}$  steps. Figure B.1 (a) is reused with permission from Bradley Peterson, Pyroelectric Imaging in Ultrathin Ferroelectric Films of P(VDF-TrFE), *B.A. Thesis*, University of Nebraska, Lincoln (2003).

The second equation is for the width of the laser focal spot

$$w = \frac{\lambda}{2\pi NA}, \quad NA = \frac{w_0}{2f} \quad (\text{B.2})$$

The original beam width  $w_0$  of the laser can be reduced to  $w$ , if we let the beam pass through a microscope object with a numerical aperture NA. The greater the NA is, the greater the decrease of the beam width, and shorter wavelength will reduce  $w$ .

The recent version of PSM has been developed according to these suggestions. The new PSM system consists of a blue diode laser ( $\lambda = 405$  nm), which is capable of direct modulation up to 5 MHz, and an optical lens system with numerical aperture (NA) 0.85 (see Fig. B.1). The new optical components improved the theoretical resolution from 1  $\mu\text{m}$  to 250 nm. Even though it is an enough resolution for characterizing a large area of thin film capacitors (a square of 1~3 mm), to probe nanometer scale structures such as nanomesas, higher resolution is required. Also, further improving of imaging resolution will make PSM comparable to other scanning probe system such as PFM, and SS-PFM which have become important nanoscale research techniques for ferroelectric materials. Moreover, PSM is a very non-invasive scanning system, even compared to PFM which uses a sharp tip in contact with the sample during scanning.

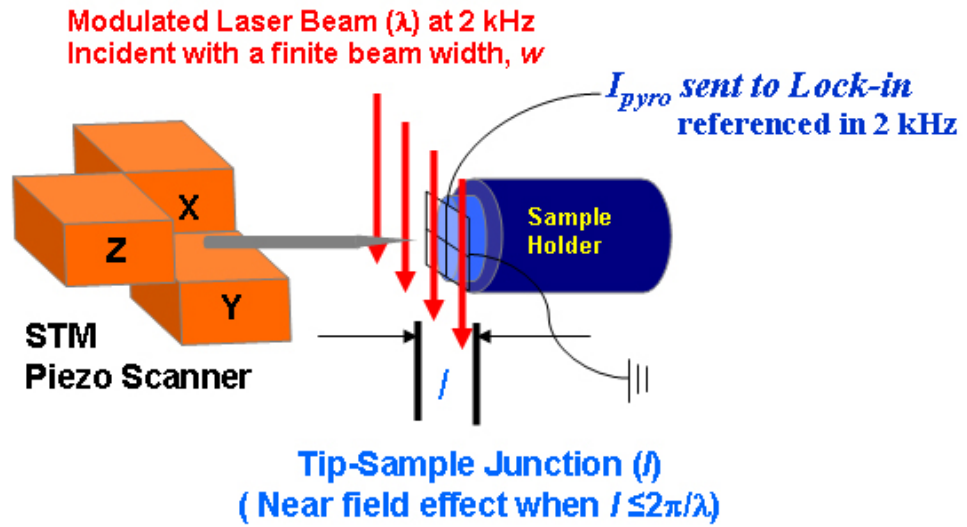
### Near Field Effect

Another means of achieving improved PSM resolution is to use a near-field effect. We propose to implement a PSM system employing a commercialized scanning tunneling microscopy (STM) where near-field illumination is afforded by scattering the

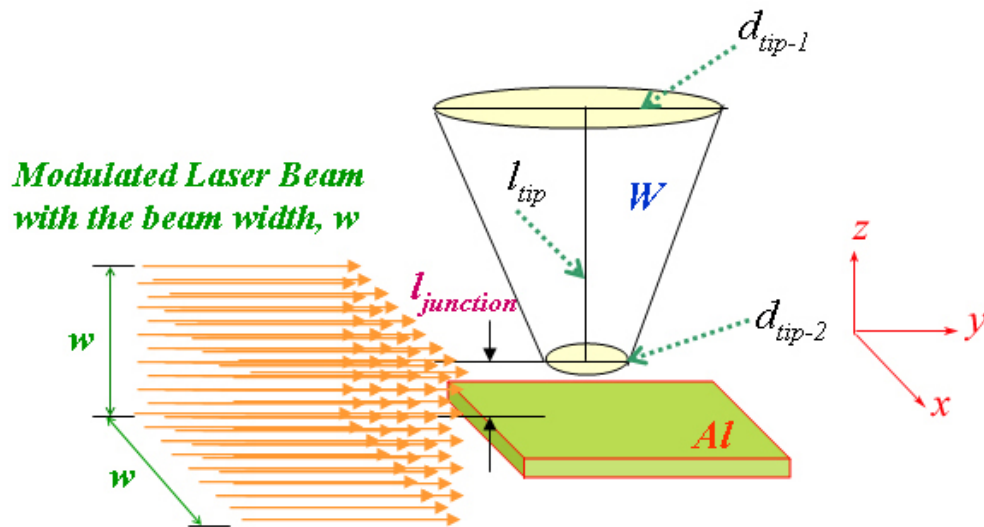
laser beam from the STM tip. The laser beam scattered off of the very sharp STM tip will produce enhanced near-field illumination in a subwavelength region in the proximity of the tip.<sup>9,10,11</sup> The simplified schematic set-up for the near field imaging, combined with the pyro-measurement is shown in Figure B.2. (A more detailed set-up for the pyro measurement and PSM can be found in ref. 3 and 5.) The technique as a whole was not initially successful to obtain a valuable PSM images, because of the relatively low modulation frequency of 1~2 kHz. The experimental trials, however, did show positive feasibility of the method, and the simulation suggested 3  $\mu\text{m}$  beam width can be effectively reduce down to approximately 45 nm, as outlined in the next section. Therefore this suggests that combining the near field effect to PSM system could improve imaging resolution to the next level.

#### 1) Simulation of near-field illumination

The simulation was done with the software HFSS, a commercial implementation of finite-element methods for modeling electromagnetic fields. It is a powerful applications used for antenna design, and complex RF electronic circuit elements design, for example. A simplified model of the simulation parameters is shown in Figure B.3 and the simulation result is shown in Figure B.4. Note that the diagram for the model shown in Figure B.3 is not to scale. The values used for the model were as followings: the wavelength of the light,  $\lambda=633$  nm (He-Ne laser); length of the tungsten (W) tip,  $l_{ip} = 3$   $\mu\text{m}$ ; the dimensions of the tip,  $d_{ip-1}=500$  nm,  $d_{ip-2}=20$  nm; the dimension of the aluminum electrode was  $3\times 3\times 0.05$  ( $\mu\text{m}$ )<sup>3</sup>; the laser beam area was  $3\times 3$  ( $\mu\text{m}$ )<sup>2</sup>;



**Figure B.2** is a simplified schematic set-up for the pyro-measurement combined with STM system to use near field effect and at the same time to obtain PSM images.

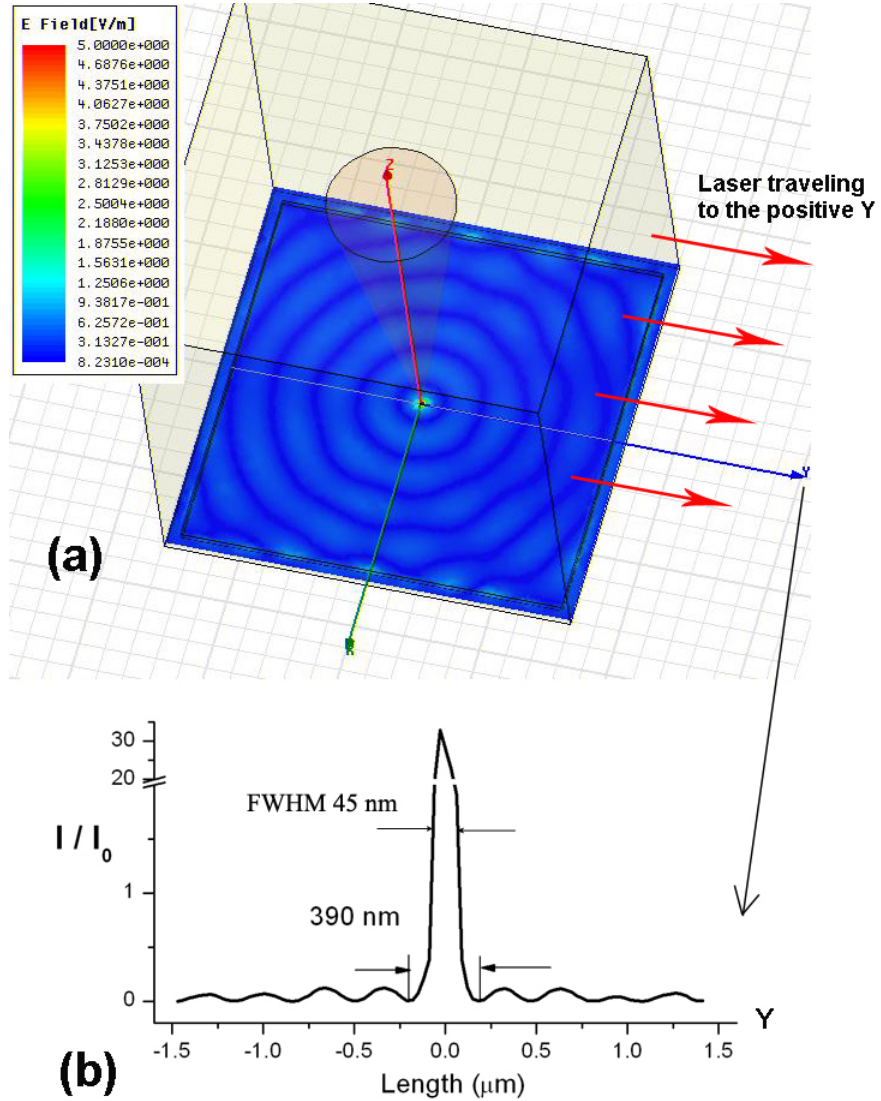


**Figure B.3** is a model used for a near field effect simulation using HFSS.



the tip-sample junction distance  $l_{junction} = 1\text{nm}$ ; and, lastly, the simulation was done within in a volume of  $3 \times 3 \times 3.2 (\mu\text{m})^3$ . The beam is traveling along the positive y direction, and the tip is along the z direction.

As you can see in Figure B.4a, only a small region directly below the tip shows the intensity enhancement effect. The simulation calculates the relative intensity  $I/I_0$ , and Figure B.4b shows the intensity profile on the Y axis. The intensity profile resembles the airy disk, and the first minima falls at approximately  $\pm 180\text{ nm}$ . The region outside of these first minima with respect to the origin point shows the relative intensities below 0.2, while the maximum enhancement at the center is approximately 30 times compared to the  $I_0$ . Therefore we can conclude that HWHM of the dominated first maximum can be considered as the beam width from the near-field effect. We integrated the intensity profile (Fig. B.4b) and then we evaluated two cases, 1) the region of 60 % of the beam intensity lies, 2) the region of 90 % of the beam intensity. The first one gives us approximately 45 nm of beam spot, and the second one approximately 400 nm. This shows that the first maximum has 90 % of power of the incident laser beam. However, we are aware of that this model is too crude since the STM tip we used was not designed but just simply made by cutting with a wire cutter followed by the microscope manual.<sup>12</sup> (We have not yet tried etched STM tips.) However, considering our current goal is improving resolution by a factor of 10 from the 500 nm scale of free-space optics to 50 nm scale, this calculation suggests combining near field effect to the new PSM will be worthwhile.



**Figure B.4** (a) shows the 2D map of the electric field on the Al electrode surface calculated with;  $\lambda=633$  nm; the tungsten (W) tip,  $l_{tip} = 3 \mu\text{m}$ ,  $d_{tip-1}=500$  nm,  $d_{tip-2}=20$  nm; the aluminum electrode  $3 \times 3 \times 0.05 (\mu\text{m})^3$ ; the beam area  $3 \times 3 (\mu\text{m})^2$ ; the tip-sample junction distance  $l_{junction} = 1$  nm; within in a volume of  $3 \times 3 \times 3.2 (\mu\text{m})^3$  in air.

## 2) Experiment

The experimental set-up<sup>1,4</sup> for near-field PSM is shown in Figure B.5. We implemented the pyro-measurement set-up into EasyScan E-STM version 2.0. This STM system had both good and bad aspects in regards of this implementation. This microscope is only built for STM so it was very simple to operate, and the sample-tip junction is open in air, therefore it was fairly easy to align a laser beam to the tip-sample junction. However, it only has maximum scan range of 500 nm, thus changing the scanning spot was very difficult. Also, the EasyScan version 2 was not optimized to connect external electronics into the main system, thus for data acquisition we had to save data manually using a floppy disk drive installed in the lock-in amplifier, SR850 DSP from Stanford Research Systems. Another significant concern was that the tunneling current flow existed in the circuit, because the effect of the tunneling current to the pyro-current circuit has not been studied. Having the unsolved synchronization problem of positioning and data collecting time in addition to the effect of the tunneling current to the system, obtaining meaningful PSM images was not possible with this set-up. However, there are a set of data clearly showing the near field effect, and gives us positive outlook for the application of the near field effect. The results of the first trial of the experiment were as follows.

This data shown in Figure B.6 were collected as follows. Firstly, we made a coarse approach of the sample holder to the tip by hand, and then let the peizo scanner motor do the finer approach.

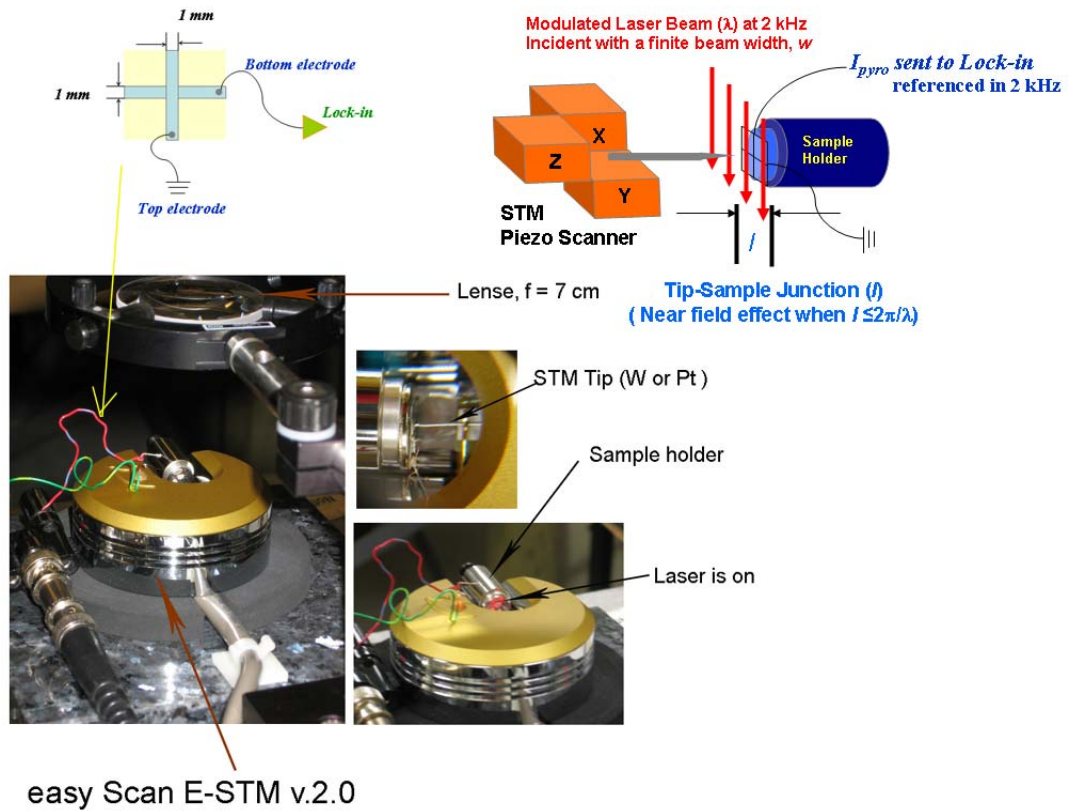


Figure B.5 shows the real experimental set-up we had for the measurements.

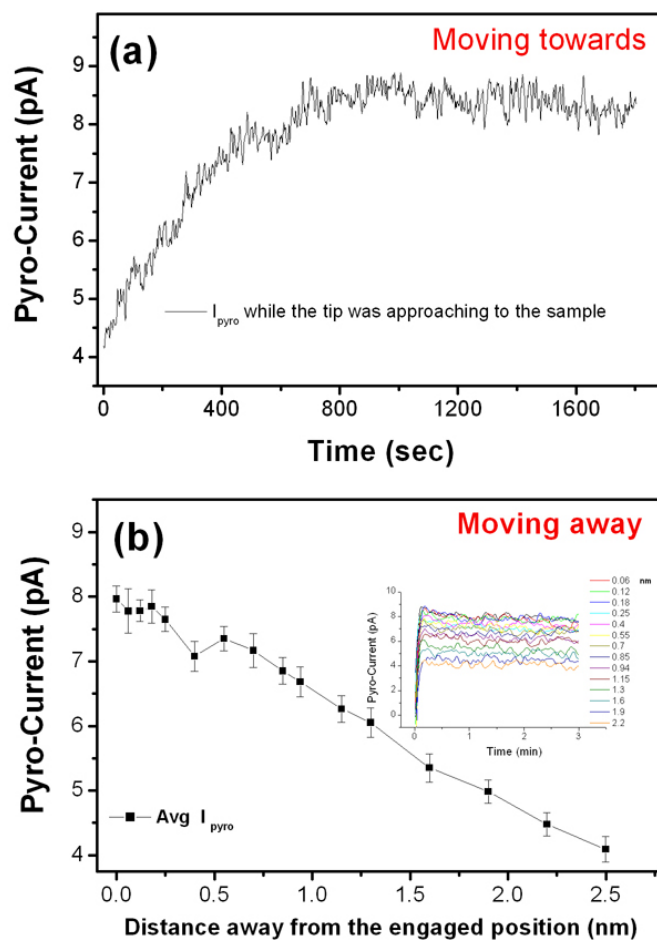


Figure B.6 (a) Pyro-current measured while STM tip was approaching to the sample surface automatically in continuous motion. (b) Pyro-current measured at each step for 3 minutes by controlling the piezo-motor step by step.

After the coarse approach we aligned the laser beam to the proximity of the tip-sample junction, and then we started to collect the Pyro-current during fine approach. The engaging set-point was 0.5 nA for the tunneling current, where the tip stopped approaching in Z and the STM began scanning in x-y. For our experiment, when the scan was engaged, we stopped the x-y scanning, but kept the approached distance z constant. The data shown in Figure B.6a was recorded while the tip was approaching to the sample surface. The total number of steps that the piezo motor made during this data ran is 5,158, and each step was approximately 0.003 nm. The pyro-current increased by approximately 4.5 pA, while the tip-sample junction distance decreased by approximately 1.55 nm. Even though we cannot test the enhancement due to the effect of near field quantitatively, this data illustrates the enhancement effect as an increase trend of the pyroelectric current.

The second set to data shown in Figure B.6b is the test of how the current is stable at each step. After we held the tip at constant tunneling current for 1 min, we retract the tip by controlling the motor step by step, and at each step we collected data for about 3 min with the lock-in time constant about 0.03 second to 1 second, as it shown as a subplot in Figure B.6b. The notable decrease of the Pyro-current began from 0.25 nm away from the initial position, and the decrease of the Pyro-current is inversely proportionally to the distance between the tip and the sample. It is, however, not clear whether the decrease was directly related to the possible decrease of the field enhancement due to the increased the tip-sample distance or not.

### Outlook

Both the simulation and the experiment are very supportive of the idea of adding the near-field effect to the PSM system. To have more accurate prediction, simulation needs to be done with a new model appropriate for the new PSM system. The set of data shown in Figure B. 6 reveals that the coarse approach made by hand was only 2.5 nm away from the typical engaging distance of STM scanning condition, which is approximately 1 nm.<sup>11</sup> The tip-sample distance made by hand was less than 10 nm and the near field effect can be achieved when  $l_{\text{junction}} \leq (\lambda/2\pi)$  (approximately 65 nm range for the blue diode laser, and 100 nm for He-Ne laser)<sup>8</sup>. These two facts suggest us that we could try a simple near-field effect set-up to the PSM system as follow. Add a sharp tip to the optical path of the PSM system (right above the sample surface where the beam is focused), and make a coarse approach of the tip to the sample surface by hand. In this way, we could exclude the tunneling current we had in the experimental set-up presented in this work, and the near-field effect can be easily achieved even though the tip-sample distance will be unresolved.

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- <sup>11</sup> J. Boneberg, *et al, Appl. Phys. A* **67**, 381 (1998)
- <sup>12</sup> Operating Instructions easy Scan E-STM version 2.0, (Nanosurf AG. Switzerland, 2003)



## **Appendix B      Nanoimprints on P(VDF-TrFE 70:30) Copolymer Films**

### *Introduction*

Our ultimate goal is to build a composite film of P(VDF-TrFE) copolymer films with high-dielectric nanoparticles embedded. This type of composite films was predicted to have enhanced electrostriction and dielectric constant of the film due to the exchange coupling between P(VDF-TrFE) copolymer and high-dielectric nanoparticles by Li.<sup>1</sup>

The composite films can be built with many different approaches. For example, the most simple and feasible way is to make composite capacitor samples by spin coating with solutions of copolymers mixed with particles. This is one of the current investigations in our lab. A different approach of constructing the composite sample is presented in this dissertation. The sample configuration that we originally plan to construct is shown in Figure B.1a. To build this sample, firstly we need to deposit LB films of P(VDF-TrFE) copolymer on Si wafer as typical thin films (see Chapter1 and 2), secondly pattern LB films of P(VDF-TrFE) copolymer by imprinting, thirdly deposit high-dielectric nanoparticles onto the imprinted copolymer films, and then finally deposit the cover layer of LB copolymer films. However, this original plan has not yet been achieved. Preparing the patterned copolymer layer by imprinting(Fig. B.1a) is only presented in this appendix.

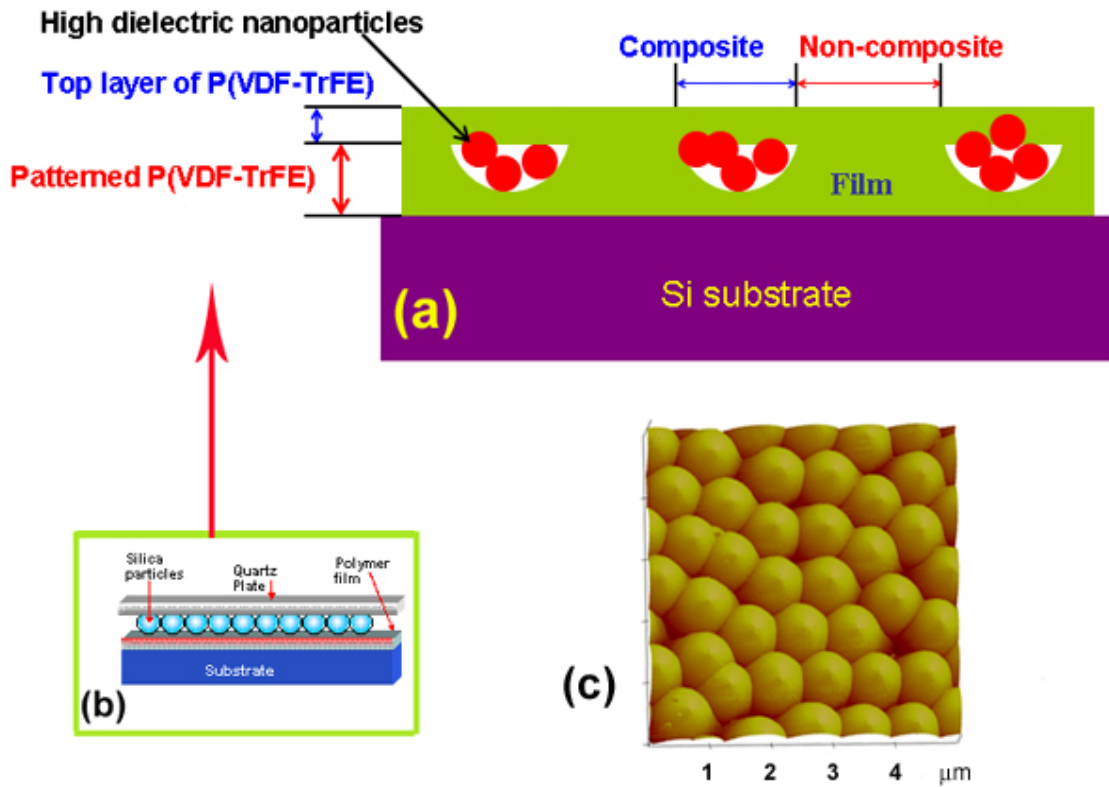
### Samples

First of all, we prepared LB thin films of 70:30 copolymer samples with different numbers of layers; 11, 22, and 33 LB layers, corresponding to approximately 20, 40, and 60 nm in physical thickness, taking account that 1 LB layer is 1.8 nm.<sup>2</sup> All samples were deposited on a Si wafer and annealed at 135 °C for 2 hours before imprinting. The topography change after imprinting was probed with atomic force microscopy (AFM). All AFM scanning was done in tapping mode with a silicon tip with the nominal spring constant  $k = 40$  N/m, and the nominal resonant frequency  $f = 300$  kHz. We also tried scanning electron microscopy (SEM); however, it showed damages on the film after scanning.

### Laser-assisted nanoimprinting with self-assembled nanospheres

To prepare the imprint layer of P(VDF-TrFE) copolymer (Fig B.1a), we used a laser-assisted nanoimprinting with self-assembled nanospheres technique, developed by Dr. Lu in Electrical Engineering at UNL. The procedure will be briefly introduced here, and the detailed information about the technique can be found in Lu's paper.<sup>3</sup> In this technique the imprints are obtained by pressing a self-assembled nanosphere layer deposited on top of a copolymer LB thin film sample, and the degree of imprint can be controlled with a laser pulse assist.

A silica particle solution in water mixed with trinton-X and methanol, in the ratio of 1:400 was used for the self-assembled nanosphere layer.



**Figure B.1** (a) shows a cartoon of a composite film with P(VDF-TrFE) copolymer films matrix with high dielectric nanoparticles: (b) shows the nanoimprint set-up with silica particles dispersed on the film: (c) is an AFM image of the array of remained silica particles after washing. Approximately 6 particles are placed within 5  $\mu\text{m}$ , corresponding to approximately 830 nm in diameter.

The silica particle solution was simply dropped and dispersed on the top of LB films of 70:30 copolymer to make the self-assembled silica nanospheres as shown in Figure B.1c. If we look at the self-assembled array of silica particles in Figure B.1c, approximately 6 silica particles are placed within 5  $\mu\text{m}$ , corresponding to approximately 830 nm in diameter. This is smaller than the labeled value of the purchased silica particles 970 nm. Then, the silica particle solution was dried in the air. The dried silica particle layer was covered with a quartz plate for imprinting as shown in Figure B.1b. The quartz plate (not shown in Figure B.1b) was slightly pressed with a help of a metal plate before the laser pulse illumination was applied. The metal plate weighs approximately 100 g and has a hole at the center about 1 cm in diameter so that laser pulse can reach to the sample surface through the hole. The laser used was a KrF excimer laser with wavelength 249 nm and operated with a pulse duration of 24 ns and the energy density in a range from 0.1 to 100mJ/(cm)<sup>2</sup>. After the imprinting process, the silica particles were washed off in an ultrasonic bath of distilled water. We also tried to imprint with different imprinting conditions as followings.

### Experiments

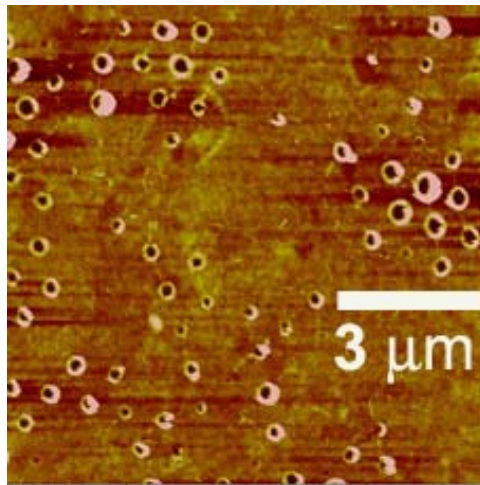
#### **1) Imprinting with laser-assist at room temperature**

Figure B.2 is an atomic force microscopy (AFM) images of imprinted 11 LB layers of 70:30 copolymer sample with 10 ~12 pulses of laser beam with an energy density of 100 mJ/cm<sup>2</sup> at room temperature. A large portion of sample showed irregular coverage, and the size of the dimples were also irregular.

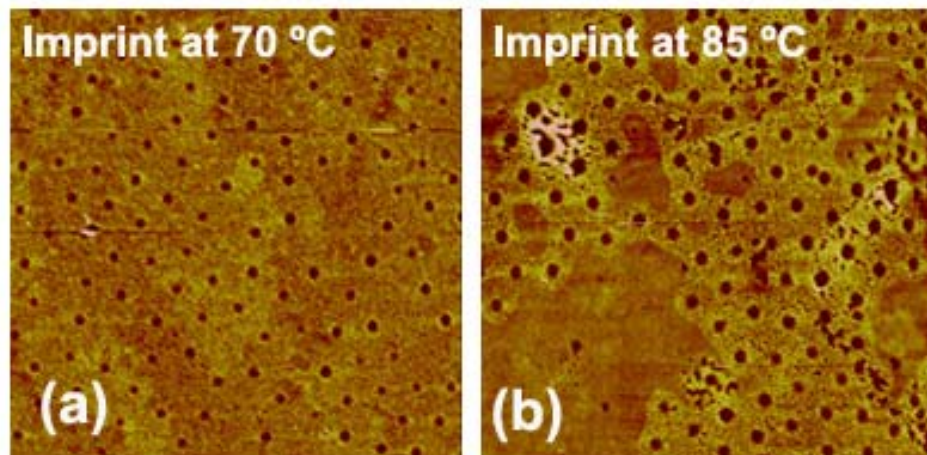
## ***2) Imprinting with laser-assist near $T_C$ of 70:30 copolymer***

Two copolymer samples of 22 LB layers were imprinted with an assist of a pulse laser near the phase transition temperature ( $T_C$ ) of 70:30 copolymer. The phase transition temperature is where copolymers transfer from ferroelectric phase to flowing paraelectric phase, and  $T_C = 100\text{ }^\circ\text{C}$  for 70:30 copolymer. To control the temperature of the sample, the sample was place on top of a temperature controllable hot plate during imprinting. One sample was imprinted with the hot plate temperature at  $70\text{ }^\circ\text{C}$  and the other at  $85\text{ }^\circ\text{C}$ . The imprinting set-up was set in open air, thus a small temperature discrepancy between the sample and the hot plate is expected; however it was not accurately monitored. After the temperature was set, 8 pulses of laser were fired to the samples with an energy density of approximately  $0.12\sim 0.13\text{ mJ/cm}^2$ .

The results from this experiment showed uniform dimples in a fairly regular hexagonal array (Fig. B.3a and c). The average diameter and depths of the imprint at  $70\text{ }^\circ\text{C}$  are  $225 \pm 30\text{ nm}$  and  $12.4 \pm 2\text{ nm}$ , and ones for the imprint at  $85\text{ }^\circ\text{C}$  are  $304 \pm 30\text{ nm}$  and  $24.8 \pm 5\text{ nm}$ . The spacing between dimples is approximately  $850 \pm 50\text{ nm}$  apart consistent well with the sphere diameter  $830\text{ nm}$  determined from the image shown in Figure B.1c. The imprint at  $70\text{ }^\circ\text{C}$  showed less damage on the film under the same energy density of laser beam, this suggests there should an optimal energy of laser at every temperature not to damage sample and at the same time successfully obtain imprints.



**Figure B.2** is an AFM image of nanoimprints on 11 LB layers of 70:30 copolymer film at room temperature with 10 to 12 times of laser pulses with  $100 \text{ mJ/cm}^2$  of the energy density.



**Figure B.3** shows imprints done on 22 LB layers of 70:30 copolymer films: (a) at  $70 \text{ }^\circ\text{C}$ : (b) at  $85 \text{ }^\circ\text{C}$  with 8 times of laser pulses with approximately  $0.12\text{--}0.13 \text{ mJ/cm}^2$  of the energy density.

Also, comparing the experiments 1) and 2), it is apparent that the imprinting at higher temperatures was more effective than applying higher energy density pulses at room temperature for regular patterning. However, there has not been any calculation (or modeling) of the role of the pulsed laser beam in copolymer film nanoimprinting. We can only suspect that the low energy density ( $0.12\sim 0.13$  mJ/cm<sup>2</sup>) of laser pulses should not have much effect on the imprint based on the fact that the imprint done with the laser pulse with much higher energy density ( $100$  mJ/cm<sup>2</sup>) was not successful as shown in the previous section (Fig. B.2).

### ***3) Imprinting during annealing without laser-assist***

Having the importance of imprinting temperature proven, imprinting during annealing was attempted without a laser-assist. The 70:30 copolymer samples of 11, 22, and 33 LB layer films were prepared for nanoimprinting, and then the silica particle layer was deposited to the samples, covered with a quartz plate, and held with the metal weight as described earlier. This time, instead of illuminating laser pulse to the samples prepared for imprinting, they were placed in the oven and heated up to 135 °C slowly and annealed for 1hr and cooled down slowly.

Imprints of all three samples showed nice shape of dimples with interesting rims around them (Fig. B.4a-f). The size of dimples and rims were very regular within a sample, and show a little variation among different samples. Overall dimples are approximately  $280 \pm 50$  nm in diameter, and their spacing between neighbors is

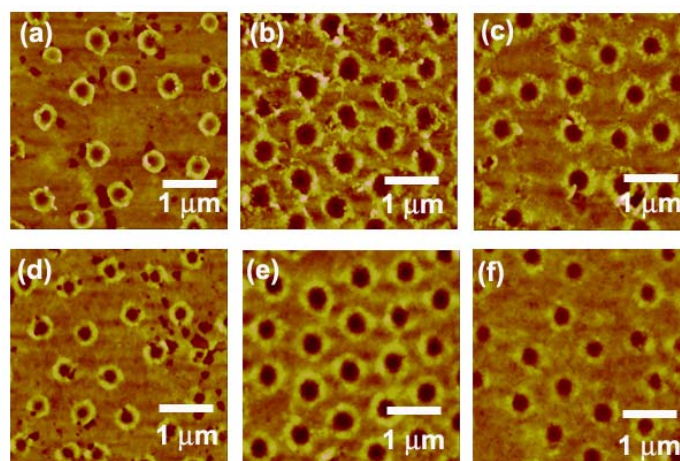
approximately  $850 \pm 50$  nm apart, which is the same as the previous results presented in Experiment 2). The size of the rims is approximately  $140 \pm 20$  nm in width and  $23 \pm 4$  nm height. We reannealed the imprinted samples to check the stability of the imprints. The second annealing was done with the same annealing condition as the first time; in the oven at  $135^\circ$  for 1 hour. The second annealing refined the surface of the imprinted films (see Fig. B.4b, e, and f), however, did not cause any change in dimensions of dimples and rims. As a matter of fact, the stability of the imprint is proven to be very good.

#### ***4) Effect of the silica particles and the metal weight to the imprint***

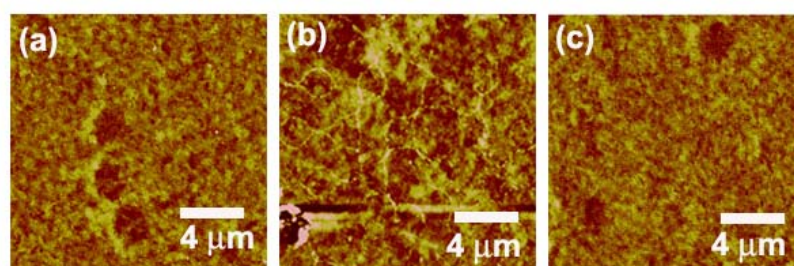
Lastly, we examined the effect of the 100 g of metal plate weight used for the nanoimprint set-up. 11 LB layer of 70:30 copolymer was used for this experiment. Similar to the earlier experiments the silica particle layer was deposited on top of the 11 LB layer of 70:30 copolymer sample, covered with a quartz plate, and held with a metal weight. This time, the sample was left at room temperature for 5 hours without any other assists.

The result shows no drastic topographical change after this experiment, and only few of spots appeared to have some irregularity (Fig B.5). It presumably caused by the mechanical pressure applied by the metal plate to the films.





**Figure B.4** shows imprints on 11 (a and d), 22 (b and e), and 33 (e and f) LB layers of 70:30 copolymer films printed during annealing at 135 ° for 1 hour. The Figures a, b, and c show fresh imprints, and the figures d, e, and f were taken after re-annealing of the imprinted films at 135 ° for 1 hour.



**Figure B.5** shows images of 11 (a), 22 (b), and 33(c) LB layers of 70:30 copolymer films after being pressed with silica particles with the help of 100 g of the metal plate for 5 hours at room temperature.

*Discussion*

We have observed a hexagonal array of shallow dimples imprinted in polymer films as shown in Figure B2 through B4 in this study. However, we cannot conclude what imprint method is the best for building a composite film with high-dielectric nanoparticles since we have not yet built one, and tested its dielectric properties. The work presented here is merely the beginning stage of the construction of the composite films of P(VDF-TrFE) copolymer with high-dielectric nanoparticles. However, if we only evaluate the imprints based on their topography, the imprints made during annealing showed the most regular pattern (Fig. B.4).

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