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# Verification of Grouting Effectiveness Using 3-D Seismic Tomography

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VERIFICATION OF GROUTING EFFECTIVENESS  
USING 3-D SEISMIC TOMOGRAPHY

by

CHRISTOPHER MICHAEL LYNCH

B.S., University of Colorado at Boulder, 2011

A thesis submitted to the  
Faculty of the Graduate School of the  
University of Colorado in partial fulfillment  
of the requirement for the degree of  
Master of Science

Department of Civil and Environmental Engineering

2011

This thesis entitled:  
Verification of Grouting using 3-D Seismic Tomography

written by Christopher Michael Lynch  
has been approved by the Department of Civil and Environmental Engineering

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Professor John McCartney (committee chair)

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Professor Ronald Pak

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Mr. Matthew DeMarco

Date \_\_\_\_\_

The final copy of this thesis has been examined by the signatories, and we  
Find that both the content and the form meet the acceptable presentation standards  
Of scholarly work in the above mentioned discipline.

Christopher Michael Lynch (M.S. Civil Engineering, Department of Civil, Environmental, and Architectural Engineering)

Verification of Grouting using 3-D Seismic Tomography

Thesis directed by Professor John McCartney, Ph.D., P.E.

## **ABSTRACT**

Compaction grouting is one of the most common ground improvement techniques in geotechnical practice. Traditional quality assurance methods for compaction grouting typically involve evaluation of grout injection parameters and intrusive point measurements. An issue with these methods is that they may not reflect the entire treated soil volume. A geophysics-based evaluation method such as 3-D seismic tomography provides an alternative technique to evaluate the volumetric improvement of soil profiles before and after compaction grouting. Specifically, 3-D seismic tomographic images can be used to visualize and quantify the distribution in compression wave (p-wave) velocities to measure and estimate spatial variations in improvement of subsurface materials in a rapid, non-intrusive, and inexpensive manner.

3-D seismic tomography was applied in this study to two roadway rehabilitation projects to investigate its suitability in quality assurance programs for shallow grouting of poor roadway subgrades. This study presents the details of these projects as well as related grouting field operations, seismic data collection procedures, and raw 3-D seismic tomography results. Several analytical methods are proposed to interpret the tomography results to quantify the degree of improvement in the seismic velocity distributions at the sites following grouting. The potential applications of 3-D seismic tomography for verifying effectiveness of future compaction grouting projects is explored and recommendations are made based on lessons learned.

## **DEDICATION**

This thesis is dedicated to my grandfather, Marshall Cappelloni, for inspiring me to think creatively and work tirelessly, and to my parents Thomas and Barbara Lynch, without whose support this endeavor would not have been possible.

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## 1. INTRODUCTION

Compaction grouting is a widely used soil improvement technique in geotechnical engineering practice. In this technique, cementitious grout is injected under pressure through boreholes into the subsurface with the goals of filling voids and densifying the surrounding soil profile. The costs associated with grouting can be significant for owners, especially when injected grout quantities exceed the initial estimated quantities. These costs are encumbered further due to difficulties in verifying the magnitude of improvement resulting from compaction grouting. The main objective of this thesis is to address the problem of verification by evaluating the use of 3-D seismic tomography to infer the volumetric improvement in soil behavior from compaction and void-fill grouting. Three-dimensional seismic tomographic can be used to visualize and quantify the distribution in compression wave (p-wave) velocities in order to measure and estimate spatial variations in improvement of subsurface materials. Compression waves may also be referred to as seismic, or primary waves, and are the fastest-traveling of all direct body waves.

Specifically, 3-D seismic tomographic evaluations were performed at to two roadway rehabilitation projects which employed compaction and void-fill grouting to stabilize loose and deteriorating regions of subgrade soils. Case Study 1 is located in Zion National Park, Utah, and Case Study 2 is located along a section of Arizona State Route 88 northeast of Phoenix, AZ, referred to as “Apache Trail.” Both sites were constructed nearly a century ago. Geotechnical issues have arisen at these sites because cut and fill techniques were used to traverse the mountainous terrain, resulting in relatively shallow depths to bedrock from approximately 0.6 to 6.0 meters (2 to 20 feet) with relatively poor drainage. The soils at the two sites, which consist mostly of silty to sandy gravels with some cobbles and boulders, provide a particular challenge



for compaction grouting do to their variable saturation. Accordingly, these sites were found to be good candidates for the use of seismic evaluation for compaction grouting verification as opposed to traditional verification approaches such as standard penetration testing (SPT) or cone penetration testing (CPT).

Seismic data resulting from the surveys before and after grouting operations were processed using commercial tomographic software. Several analytical techniques were used in this study to evaluate the seismic data to assess the quality of ground improvement. The results of these analyses were also interpreted based on the known grout quantities injected at each site.

Chapter 2 provides a brief overview of ground improvement, with a review of grouting methods and applications, including relevant information relating to site investigation, applications, design, equipment, and procedures. Chapter 3 provides an introduction to geophysical testing methods, including an overview of conventional 2-D seismic refraction methods as well as relatively new 3-D seismic tomography methods. This chapter also provides a background on the calculations incorporated into the software used to process the seismic data as part of this investigation (GSR3D), along with an overview of prior applications of this software to other civil engineering problems including other compaction grouting verification studies.

The details of the project at Zion National Park (Case Study 1) are documented in Chapter 4, while the details of the project at Apache Trail (Case Study 2) are documented in Chapter 5. The seismic tomography results from these two sites are presented in Chapter 6, along with the details of the processing procedures and characterization of the tomography and difference tomography calculations. The analytical techniques developed to use the 3-D seismic tomography results to verify the quality of grouting at these two sites are presented in Chapter 7.

This chapter also includes a comparison of results from this study with those from a previously documented 2-D seismic refraction investigation at the Apache Trail site (AMEC 2007).

Recommendations for potential future applications of these methods based on the lessons learned from the investigation design and seismic data collection and processing are summarized in Chapter 8. The conclusions of this study and lessons learned are summarized in Chapter 9. This thesis also includes several appendices. Location maps for the two projects are presented in Appendix A, along with plan drawing detail sheets from the project files to permit a better understanding of the site layouts. Layouts of the geophysical equipment arrangements are presented in Appendix B. Typical raw seismic tomography results are included in Appendix C and seismic difference tomography results are included in Appendix D. Finally, ray densities calculated for the tomography generated can be found in Appendix E. The results in Appendices C, D and E provide additional information to support the discussion in Chapters 8 and 9.

## **2. GROUND IMPROVEMENT**

The main motivations for ground improvement are to address site-specific issues such as excessive surface settlement, erosion, excessive seepage, or weak zones. Settlement usually occurs due to changes in the state of stress due to increased foundation load magnitudes, changes in groundwater elevation, seismic loading, or excavations adjacent to existing foundations leading to decreased embedment depth and confining pressure. Erosion can occur beneath a foundation due to flow of surface water, as well as at greater depths due to piping in embankments or failure of sewers and storm drains. Preexisting or developing voids beneath foundations or within embankments can also result in particle mobility and destabilization of soil structure, ultimately resulting in settlement problems.

Ground improvement techniques have become increasingly accepted by engineers as a means of mitigating problematic soils determined to have either low bearing capacity or high settlement potential. Some of the typical goals of ground improvement methods are to increase soil density (and therefore frictional strength, stiffness, etc.), fill voids within the soil mass, improve drainage conditions or create a barrier to natural groundwater flow, and control or prevent settlement.

Compaction grouting is a ground improvement method that has been used successfully for decades (Warner 2003) for a variety of applications, including improvement of soil conditions at undeveloped sites and stabilization of historic structures where settlement was found or predicted to be unacceptably large. Advances in technology, equipment, and admixtures have allowed compaction grouting to be applied to a broad range of geotechnical problems. A considerable record of case histories, many providing quantitative verification of improvement, indicates that compaction grouting is a reliable technique for ground improvement and settlement control. Additionally, ground improvement technologies have been shown (Spaulding et al. 2008) to have

significantly lower carbon footprints compared to certain conventional foundation approaches, which is often a question of interest in sustainability analyses.

Many types of grouting are currently employed in practice, covering a variety of grout materials and injection procedures. USACE (2008) released an engineering and design manual titled *Grouting Technology*, which provides technical criteria and guidance for grouting applications for civil works, covering procedures, materials, equipment, and applications of the many proven grouting methods available. Bruce and Dugnani (1994) summarized some of the most common grouting practices utilized in the United States, providing additional historical perspective to some of the advances made in this field.

### **2.1. Void-Fill Grouting**

While not the most common method of grouting available today, void-fill grouting has a descriptively simple goal. Where voids, or cavities, are known or suspected to exist within a soil mass, this technique aims primarily to fill and stabilize these openings with a mixture of grout. Cavities can exist as continuous channels resulting from removal or abandonment of pipes, large voids resulting from mining operations, large voids common in lava tube or karstic environments, or eroded material resulting from flow of water. Warner (2004) described the fastest and least costly method of void filling using commercially available concrete pumps with ready-mixed concrete or mortar. Since the primary objective of void-fill grouting programs is the filling of existing cavities more than the compaction of loose material surrounding the injected grout, little research has been found relating to the verification of such programs, other than field monitoring used to observe whether the problems originally related to the cavities ceased following grouting. Holmquist et al. (2003) summarized void-fill grouting procedures

and verification methods used to mitigate mine subsidence due to abandoned underground coal mines.

## **2.2. Compaction Grouting**

Compaction grouting refers to a ground improvement method that is used to increase soil density (and therefore frictional strength, stiffness, etc.), while filling or closing voids within the soil mass, improving drainage conditions or creating a barrier to natural groundwater flow, and controlling or preventing excessive settlements. The only major grouting technology to have originated in the United States, compaction grouting has been described as a “uniquely American” ground improvement method (Baker et al. 1983), pioneered on the West Coast of the United States in the 1950’s to repair settled structures. This method has been successfully used for decades to improve soil conditions at undeveloped sites and to stabilize and retrofit historic structures where settlement was found or predicted to be unacceptably large. Compaction grouting refers to the process by which low-slump, typically less than 2.5 cm (1 in), grout is injected underground at modest pressures, usually between 700 and 3500 kPa (100 and 500 psi). A complete review of compaction grouting has recently been presented by the American Society of Civil Engineers (ASCE 2010), providing an overview of grouting mechanics, investigations, design, procedures, analysis, and applications for the technique. In an effort to promote good practice in compaction grouting, the *Compaction Grouting Consensus Guide* (ASCE 2010) was released by the Geo-Institute of the American Society of Civil Engineers. That document provided the following general summary of the compaction grouting process:

“Compaction grouting is a ground improvement technique that improves the strength and/or stiffness of the ground by slow and controlled injection of low-mobility grout. The soil is displaced and compacted as the grout mass expands. Provided the injection process progresses in a controlled fashion, the grout material remains as a growing mass within the ground and does not permeate or fracture the soil. This behavior enables

consistent densification around the expanding grout mass, resulting in stiff inclusions of grout surrounded by soil of increased density.”

Compaction grouting is typically achieved by sequencing the injection locations from primary to secondary, and sometimes to tertiary borings, arranged in a repeating pattern across the area to be improved. Mitigation of historic structures is costly, especially if the structure must be impacted, making compaction grouting a cost-effective method for improving foundation stability without adversely impacting structural or aesthetic aspects. Warner (2010) presented a useful outline of important factors to consider for the use of compaction grouting, summarized in Table 2.1, gathered from nearly sixty years of personal experience in the application of this method. Adbelrahman et al. (2003) provided a useful list of advantages and disadvantages to performing compaction grouting, summarized in Table 2.2. Compaction grouting may also be referred to as limited mobility or limited mobility displacement grouting, giving emphasis to the fact that the low-slump (< 1 in.) grout used in the process is not intended to intersperse within the surrounding soil.

**Table 2.1. Guidelines for design of compaction grouting programs (after Warner 2010)**

<b>Investigation</b>	<b>Planning</b>	<b>Rules for Proper Performance</b>
<ul style="list-style-type: none"> <li>• Soil Type / Grain Size Distribution</li> <li>• Consolidation Properties</li> <li>• Moisture Content</li> <li>• Permeability</li> <li>• Depth to Competent Strata</li> <li>• Grout Confinement</li> </ul>	<ul style="list-style-type: none"> <li>• Acceptable Grout Hole Size Range</li> <li>• Upstage, Downstage, or Combined</li> <li>• Grout Mix / Aggregate Gradation</li> <li>• No Clay or Admixtures</li> <li>• Refusal Criteria (surface displacement, maximum pressure or volume)</li> <li>• Leveling Requirements and Accuracy</li> </ul>	<ol style="list-style-type: none"> <li>1. Start on Competent Formation</li> <li>2. Acceptable Grout Rheology</li> <li>3. Appropriate Pumping Rate (&lt; 8 psi/min.)</li> <li>4. Proper Injection Sequence</li> <li>5. Good Surface Monitoring</li> </ol>

**Table 2.2. Advantages and disadvantages of compaction grouting applications (after Abdelrahman et al. 2003)**

<i>Advantages</i>	<i>Disadvantages</i>
• Minimum disturbance to structures and surrounding ground	• Relatively ineffective at shallow depths (low confining pressures)
• Minimum risk during construction	• Prohibitive costs for problem soils at great depths
• Supports all portions of a structure	• Possibly ineffective adjacent to unsupported slopes
• Loose/problem soil can be treated irrespective of depths or thickness of layers	• Challenging to verify improvement
• Can be combined with other methods	• Danger of filling underground pipes with grout
• No harmful vibrations to nearby structures/utilities	• Effectiveness questionable in saturated clays
• Reduction in liquefaction potential	• Expense

Some of the more favorable ground conditions for this technique are zones of loose material that may have originated due to poor construction practices or developed over time due to movement of groundwater or inadequate drainage design. Grout is injected through boreholes at various depths into this loose material to create bulbs of grout due to the low mobility of the grout mix used. These bulbs not only densify surrounding soil, but under ideal conditions can result in columns of grout.

### ***2.2.1. Applications of Compaction Grouting***

Compaction grouting has been applied to address a wide range of civil engineering challenges over the last several decades, during which time a considerable body of knowledge has developed to support the usefulness of the techniques. Typical applications include leveling of structures to correct differential settlement, ground improvement prior to construction, reduction of liquefaction potential (Baez and Henry 1993; Boulanger and Hayden 1995; Miller and Roycroft 2004; Orense 2008), sinkhole remediation in karstic environments, and ground

stabilization of eroding or collapsing soils (Strauss et al. 2004; Welsh and Burke 2009; Haramy et al. 2009).

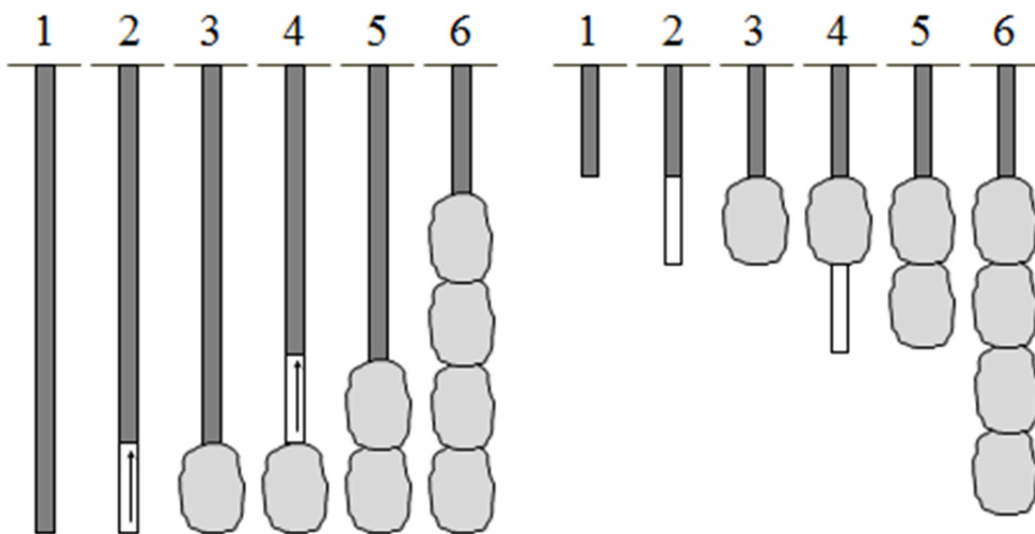
Mitchell et al. (1998) provided a comprehensive summary of ground improvement methods available for remediation of both open and constrained sites, where compaction grouting was recommended for both constrained and/or developed sites, and was described as effective to unlimited depths in any rapidly consolidating, compressible soil (including loose sand). Advantages cited by the authors included controllable treatment zones, suitability to soils containing fines, as well as limited prior experience required. Limitations noted included high cost and post-treatment loss of pre-stress with time following compaction grouting. Design considerations for compaction grouting are relatively straightforward and based upon several decades of experience. Bandimere (1999) and Warner (2004) provide some useful additional resources for assisting in the design of compaction grouting programs. Rheology has been defined by Warner (2007) generally as “the study of plastic flow of materials,” adding that the term refers to the properties of a grout in both the fresh and hardened state resulting from the initial mix design, including any admixtures used, and the mix procedures followed. Warner has long been a proponent of the influence of grout rheology on the effectiveness of grouting programs. Muller and Bruce (2000) also provide a useful overview of the equipment commonly used for compaction grouting operations.

### ***2.2.2. Field Procedures***

Weaver (2000) provided a valuable comparison of common “rules of thumb” followed by both American and European grouting contractors for compaction grouting. Figure 2.1 shows two different construction procedures that can be used for grouting, based on the advancement of the injected grout column. The simplest, fastest, and cheapest method is known as bottom-up,



where the casing is advanced to the full depth of the zone to be treated, with grouting proceeding upward in stages as the casing is removed, usually until insufficient confinement is obtained. For situations where greater improvement is required at shallow depths (1-3 m), or where surface heave must be carefully controlled, the top-down method can be used. The additional time and costs involved in the top-down method, as each stage must be re-drilled to advance the casing to the next stage, are offset by the grouting verification provided by drilling as well as the increased confinement at the surface. A combination of the two methods has also been used successfully, with the first stage being injected at the most shallow depth, and the remaining stages advancing upward from the deepest depth as in the bottom-up method.



**Figure 2.1. (a) Bottom-up, and (b) top-down compaction grouting (after ASCE, 2010)**

### **2.2.3. *Mechanics of Soil Compaction***

A thorough understanding of compaction grouting operations can be developed through consideration of soil mechanics principles, relevant soil properties, and stress-strain relationships governing soil behavior during grouting. Graf (1969, 1992), Brown and Warner (1973) and

Wong (1974) provided some of the earliest published reviews of the compaction grouting process, beginning the discussion surrounding the analysis methods of interest. More recent works have built upon some of the earlier theories proposed, including experience gained from decades of application of this technique. An alternative theory for compaction grouting design was presented by Schmertmann and Henry (1992) to protect surface construction from local zones of settlement due to sinkholes. This design concept was based on lateral stress increases and enhanced soil shear arching ability that results from lateral volume displacement during grouting.

Kleyner and Krizek (1995) proposed a mathematical model to describe the physical process that occurs as grout consolidates under applied pressure and expels excess water into the surrounding soil. While this work was focused toward applications involving bore-injected minipiles and grouted anchors, the model allowed for the calculation of average degree of consolidation as a function of time for the grout prior to set, and increases in borehole radius. A laboratory testing program allowed for validation of the model under a variety of conditions.

Perhaps the most complete mechanistic model developed for compaction grouting was introduced by Yang and Zou (2009). The theoretical basis for this model considered a spherical cavity expansion and conical shear failure zone occurring above the grout bulb as in earlier theories. A Mohr-Coulomb yield criterion was incorporated as the initial yield function, and limiting grouting pressures were determined according to a strain-softening elastic-plastic model based on conventional triaxial compression tests. Analytical solutions to the compaction grouting process were presented, and found to agree reasonably well, showing potential for the method to optimize the design of compaction grouting operations.

### **2.3. Grouting Verification Methods**

Verification of the grouting process can be considered important for a number of reasons. To the engineer, perhaps of greatest interest is whether the grouting program designed and carried out indeed performed as intended, resulting in the desired outcome in the properties of the soil being treated. Additionally, verification can ensure that the grout injected into the ground actually improved the targeted area, which can particularly be a concern where the soil being treated overlies highly fractured bedrock or karstic terrain, where injected grout can possibly migrate through these features away from the targeted soil. Hydrofracturing of the soil, where high injection pressures can cause brittle fracturing of the soil resulting in lenses or “wings” of grout instead of the bulbs intended, is also a significant concern during compaction grouting, limiting the allowable injection pressures and rates. Frequently, the only records that exist for the quantities of injected grout are the manual logs recorded by the grouting contractor, necessitating careful inspector attention to confirm. For these and many other reasons, reliable and cost-effective methods are desired to verify the achievement of grouting programs.

A considerable record of case histories, many providing quantitative results of improvement, indicates that compaction grouting can be used successfully for ground improvement and settlement control. One challenge with the use of compaction grouting for soil improvement is the quality assurance testing needed to verify that the target soil volume has been improved.

Verification methods available for use in grouting operations cover a wide range of technologies. ASCE (1995) published a thorough review of available grouting verification methods, including case histories highlighting advantages and disadvantages to the various methods available at the time. Several relationships have been proposed for verification of grouting based on changes in soil properties such as void ratio, density, and relative density.

### 2.3.1. Effectiveness Assessment Methods

Schmertmann & Henry (1992) presented a design approach for compaction grouting based on lateral stress changes and volumetric strains developing within soil as a result of compaction grouting. Following the results of centrifuge modeling tests to study the effects of grout composition, depth and injection rate on grout bulb developments, Nichols and Goodings (2000) presented a shape factor,  $S_{\psi}$ , to describe grout bulb geometry, as follows:

$$S_{\psi} = \frac{L_{Bulb}}{B_{Bulb}} \quad (2.1)$$

where L is the overall length of the grouted bulb and B is the diameter of the bulb at the grout depth. The grouting intensity number (GIN) has been a widely-used verification method for grouting. While different forms of the equation can be found in the literature, Perkins and Harris (2003) provided a form of the GIN relationship specific to compaction grouting, as follows:

$$GIN = \frac{Take \times Pressure}{(C \times Distance^2)} \quad (2.2)$$

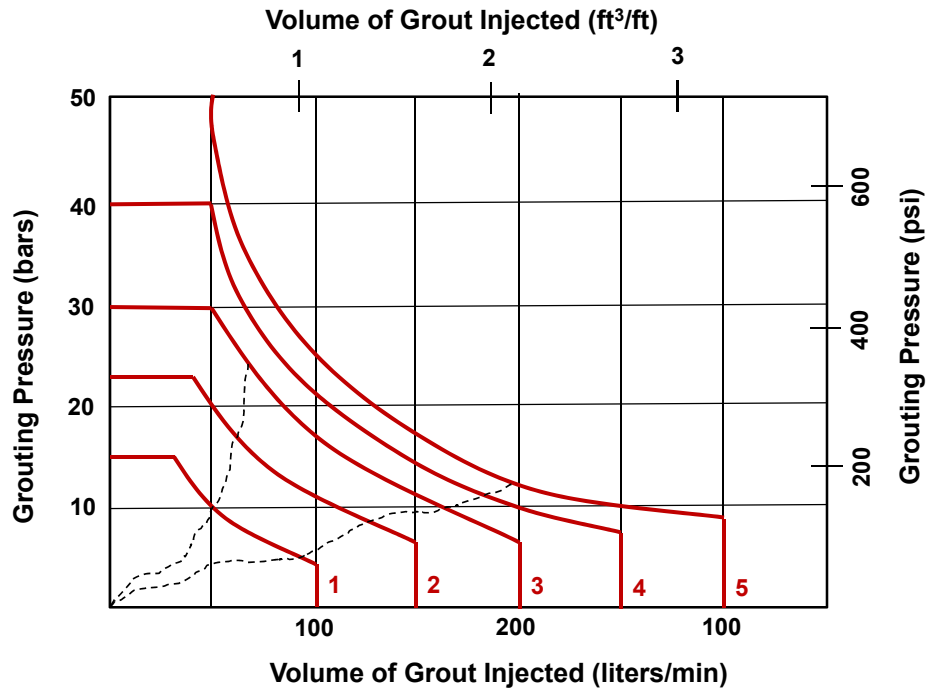
where *Take* = Grout take (ft<sup>3</sup>)

*Pressure* = Peak injection pressure (psi)

*Distance* = Center to center distance between holes (ft)

*C* = Site specific constant (typically ~ 0.75)

Warner (2004) describes the use of grouting intensity numbers to allow for real-time monitoring of grout injection. For a single stable grout, injected at a uniform rate, curves corresponding to chosen GIN limitations can be developed, as shown in Figure 2.2. Pressure and volume injection parameters can then be monitored to determine when the specified grouting intensity number is reached.



**Figure 2.2. Parabolic GIN curves with typical pressure-volume relationships. Dashed lines indicate possible paths followed during grouting. (after Warner, 2004)**

Batsu et al. (2009) investigated methods to allow for the prediction of heave during inclined compaction grouting based on the elastic continuum approach. Ground heave was found to increase non-linearly with increase in inclination, with the increase initially sharp for small inclination values, followed by a decreasing rate of increase at larger inclinations. For larger injection depths,  $c_o/d > 10$ , where  $c_o$  is the depth to the center and  $d$  the diameter of the injected grout, beyond inclinations of  $70^\circ$ , increases in heave with changes in inclination were found to become insignificant.

### **2.3.2. Geotechnical Field Testing**

Standard Penetration Test (SPT) or Cone Penetration Test (CPT) measurements before and after ground treatment are the most commonly used field testing quality assurance methods for compaction grouting. The primary issue with these methods is that they only quantify the degree

of improvement at point locations and do not reflect the improvement of the soil from a volumetric basis. Additionally, site conditions may prevent access of the large equipment required to perform these tests, availability may be limited, and high mobilization costs may make these methods financially unachievable, especially for smaller projects.

Baez and Henry (1993) described verification methods used for a compaction grouting program designed to densify a layer of very loose sand to silty sand underlying a dam. Corrected SPT values obtained following grouting ranged between 11 and 38, compared to an average of 4 before treatment. Where post-grouting SPT values were found to be lower than required, a quaternary (fourth) injection phase was applied. Boulanger and Hayden (1995) conducted a collective review of case histories on improvement of liquefiable soils by compaction grouting, where significant increases in CPT penetration (tip) resistance were achieved for soils ranging from slightly silty sand to silt. Observations included changes in penetration resistance for increases in elapsed time following grout injection, as well as due to differences in field procedures followed, most notably bottom-up versus top-down techniques. For most situations, Boulanger and Hayden recommended that the bottom-up method could be effectively used at shallow depths, provided appropriate procedures are followed (multi-phase approach, decreased spacing between injections). Miller and Roycroft (2004) concluded that compaction grouting could be effectively used to mitigate liquefaction of susceptible soils and to create a buttress zone to protect structures. Their analysis included CPT results gathered for a variety of different injection spacings, which allowed for a quantification of liquefaction potential and factors of safety at different depths throughout the soil profile both before and after compaction grouting. They found densification to be achieved in all cases considered in their study, with maximum benefits occurring for sands at 1.5 m (5 ft) injection spacing.

Orense (2008) compiled a more recent review of two case histories on compaction grouting, finding improvements in strength and lateral earth pressure of the soil, in addition to SPT values, as a result of compaction grouting. Strauss et al. (2004) successfully utilized compaction grouting to mitigate settlement occurring due to weak alluvium beneath highway approach fills after performing a test program to verify effectiveness and establish minimum improvement requirements. Welsh and Burke (2009) provided some recent examples of effective applications of compaction grouting for settlement remediation due to erosion and piping resulting from unsealed joints in storm drains below a freeway in California. Their work also described the use of compaction grouting for liquefaction mitigation in Japan following the 1995 Kobe earthquake, and for the prevention of sinkhole development in karstic regions of Pennsylvania.

### ***2.3.3. Laboratory Testing***

Nichols and Goodings (2000) performed small-scale model compaction grouting tests in a geotechnical centrifuge to investigate the soil response to a single-stage grout bulb injection in dry uniform sand at various depths. The effects of grout composition (rheology) on grout bulb development and shape were also explored, with results indicating the shape of the injected grout bulb to be a function of overburden pressure. For a particular grouting condition, an upper limit to grout bulb size was observed, with soil deformations similar to those occurring for deep uplift anchors, disagreeing with the conical shear failure theories suggested by Graf (1969, 1992) and Wong (1974). Following additions of either clay or flyash to the grout mix lessened the ability of the mixture to sustain high pressures.

El-Kelesh and Matsui (2008) carried out double-wall calibration chamber model tests for compaction grouting, capable of independent control of stress and boundary conditions. Monitoring of injected grout volume, pressure, vertical deformations, and vertical and lateral

stresses indicated two distinct stages during grouting. Pre-heaving behavior (prior to soil surface displacement) was characterized by increasing injection pressure, lateral stress, and densification. With continued injection, the upheaving stage consisted of increased rates of surface displacement at relatively constant injection pressure and decreased rates of lateral stress increase and densification. Following injection, imparted lateral stress experienced relaxation. Further tests utilizing this equipment are expected to be completed to further examine the mechanisms and effectiveness of compaction grouting for different soil and grouting conditions.

#### ***2.3.4. Test Injection and Excavation Programs***

Some of the earliest research on quality assurance methods for compaction grouting verification involved full-scale field excavations (Brown and Warner 1973; Warner 2003). Excavations of grouted masses have provided some valuable insights into the mechanisms occurring during grout injection, including the influence of variations in grout rheology and injection parameters. Following a test excavation program, Warner et al. (1992) defined the grout travel index as follows:

$$\textit{Grout travel index} = \frac{\textit{Minimum radial travel}}{\textit{Minimum colum radius}} \quad (2.3)$$

This study found that by plotting injected grout volumes as a function of the grout travel index, further understanding can be established regarding the effectiveness of the grouting and resulting densification of the soil mass. These studies indicated that for many cases, significant amounts of grout were found at greater depths than that of the grout hole, and that injection rates greater than about 1.5 ft<sup>3</sup> (0.04 m<sup>3</sup>) per minute had an adverse effect on grouting effectiveness.

#### ***2.3.5. Instrumentation during Injection***

The application of real-time data logging instrumentation has been shown by Geraci (2007) to provide continuous and precise monitoring of injection parameters during compaction grouting,



allowing for identification of high grout take regions, potential equipment malfunctions, and detailed analysis of soil response. Grout properties and injection parameters that can be monitored using these methods include viscosity, pressure, and flow rate.

Schuyler and Gularte (2008) successfully incorporated tiltmeters, which measure rotation, to monitor the movement of a bridge deck during compaction grouting beneath the bridge foundation. After correcting the tiltmeter output to account for diurnal thermal expansion and contraction of the bridge deck, the instrumentation allowed for immediate notification of vertical movement of the foundation, indicating the maximum improvement had been reached. This case demonstrates how grouting verification criteria can be established indirectly, without the measurement of grout injection parameters or changes in soil properties, through instrumentation of the ground surface or adjacent structures.

Simple devices such as crack gauges, or more sophisticated devices such as strain gauges, could be installed along sensitive structures, which would allow for the continuous visual or electronic monitoring of strain or movement of the structure. Surveying methods can also be employed, allowing for periodic verification of the position of a structure or the elevation of a roadway surface. One of the most simple and reliable devices that can accomplish monitoring of elevation change is a basic water manometer, but traditional and laser-based surveying instruments have also been successfully utilized to accomplish this task.

### ***2.3.6. Post-Earthquake Observations***

Mitchell et al. (1995) presented a considerable study of case histories from sites where ground improvement methods had been subjected to real life earthquake events. Performance data from 32 cases, most of which were found in Japan or Southern California, indicated that improved ground experiences significantly less settlement, lateral displacement, and associated damages

than untreated ground. Five sites studied provided pre- and post-densification  $(N_1)_{60}$  values, which correlated well to standard cyclic stress ratio to  $(N_1)_{60}$  relationships. The observation was made that ground improvement should extend a sufficient lateral distance beyond the perimeter of the structure to be protected to minimize displacements and resulting damages. This work also provided recommendations for future research in this field, suggesting more focus be given to developing understanding of the effects of combined improvement methods.

Hausler and Sitar (2001) presented a summary of more than 90 case histories relating to the performance of improved sites, collected from 14 earthquakes in Japan, Taiwan, Turkey, and the United States. For the two compaction grouting sites studied, one was classified as having acceptable performance, and one as unacceptable. Unacceptable performance designations resulting either from excessive ground deformations in the presence of a severe lateral spreading hazard or because of an insufficient depth of remediation.

### ***2.3.7. 3-D Seismic Tomography***

Although the available literature on injection monitoring and SPT-CPT testing show that these techniques are important tools to use as part of a quality assurance program, they only provide point measurements. An alternative approach is through the use of 3-D seismic tomography, a volumetric, three-dimensional, non-destructive geophysics-based evaluation method. 3-D seismic tomography uses seismic refraction of compression waves (p-waves) to determine the depths and seismic velocities of subsurface layers using a seismic wave generated at the surface. Further discussion of this method can be found in Chapter 3 following a brief overview of geophysical methods in general.

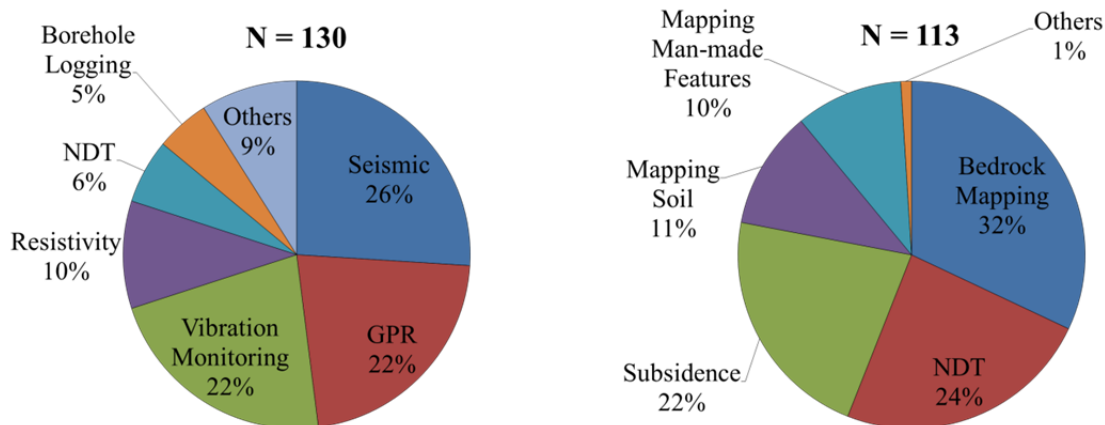
### 3. BACKGROUND ON GEOPHYSICAL METHODS

The field of geophysics has been defined as “the science of applying the principles of physics to investigations relating to the structure and properties of the earth” (CLFHD 2003) in order to measure physical properties of interest as well as characterize their distribution. A wide variety of geophysical technologies are available to engineers today, several of which could potentially be used for verification of grouting. Applications of geophysical imaging, as well as nondestructive test (NDT) methods, have seen significant increase and acceptance in recent years, due largely to their ability to rapidly and accurately gather information of interest to engineers. A brief listing of geophysical methods that have been applied to transportation engineering investigations is provided here to give the reader an understanding of the variety of technologies available within this field, but this list is by no means definitive or complete.

- Surface Geophysical Methods
  - Potential Field Methods: Magnetic, Gravity
  - Seismic Methods: Seismic Refraction, Seismic Reflection, Surface Wave Methods (Spectral Analysis of Surface Waves (SASW), Multi-Channel Analysis of Surface Waves (MASW))
  - Electrical Methods: Self-Potential (SP), Equipotential and Mise-a-la-Masse, Resistivity, Induced Polarization
  - Electromagnetic Methods: Frequency Domain Electromagnetic, Time-Domain Electromagnetic, Ground-Penetrating Radar, Very Low-Frequency (VLF), Seismoelectrical, Metal Detectors
  - Nuclear Methods: Nuclear Magnetic Resonance (NMR)
  
- Borehole Geophysical Methods
  - Electrical Methods
  - Nuclear Logging
  - Acoustic Logging
  - Flow Logging
  - Hydrophysical Logging
  - Well-Completion Logging
  - Hole-to-Hole Logging
  - Cross-hole Seismic

Several publications can be found that comprehensively detail the various geophysical methods available to engineers, summarizing relevant background theory along with informative figures, tables, and case studies. One of the earliest, from the United States Army Corps of Engineers, titled *Geophysical Exploration for Engineering and Environmental Investigations* (USACE 1995), was intended to provide an introduction to geophysical exploration for engineering, geological, and environmental investigations. A more recent publication titled *Application of Geophysical Methods to Highway Related Problems* (CFLHD 2003) was intended to be used as a technical manual and focused on providing information for both traditional geophysical as well as emerging non-destructive testing (NDT) methods to geotechnical and highway engineers for various transportation engineering applications. The most recent publication of this type was published by the Center for Geotechnical Practice and Research, titled *Geophysical Primer for Geotechnical Engineers* (Rutledge et al. 2005), and also included a sample of geophysical contractors, equipment suppliers, and available software.

The National Cooperative Highway Research Program released a document titled *Synthesis 357: Use of Geophysics for Transportation Projects* (NCHRP 2006), which reported on “current knowledge and practice, without the detailed directions usually found in handbooks or design manuals.” U.S. State and Canadian provincial departments of transportation (DOTs) and U.S. federal transportation agencies were surveyed to primarily investigate which agencies were using geophysics and for what purposes, limiting the scope to how geophysical methods were being applied by geotechnical engineers during highway planning and construction activities. Figure 3.1 illustrates responses received regarding the most commonly used geophysical methods and applications within the agencies responding to the survey.



**Figure 3.1. (L) Most commonly used geophysical methods; and (R) most common applications of geophysics among state DOTs and selected federal and Canadian transportation agencies (after NCHRP, 2006)**

### 3.1. Seismic Methods

Seismic refraction is generally considered an efficient, cost-effective, and non-destructive method that can be used in a wide-variety of applications to characterize subsurface materials. This technique has been applied in the fields of petroleum, mining, geotechnical, environmental and hydrological engineering, to name a few, over the last several decades for a seemingly unlimited variety of subsurface characterization needs.

Seismic refraction can be defined as a geophysical method used to determine the depths and seismic velocities of subsurface layers using a seismic wave generated at the surface. Normally, low frequency seismic energy is emitted by a seismic source such as a sledgehammer and collected using geophones, which measure the arrival of the seismic wave, typically at a location some distance away from the location where the wave was introduced. Successful application and processing of traditional 2-D seismic refraction relies on the assumptions that seismic wave velocities increase with depth through the subsurface profile and boundaries between subsurface

layers are generally planar. One of the most significant limitations to the seismic refraction approach is introduced by the groundwater table. The compressional, or seismic, wave propagation speed through water is typically 1450 m/s (4750 ft/s) and is temperature-dependent. When saturated soils are encountered by a seismic wave, the true p-wave velocity through the soil medium is obscured by the high p-wave velocity of the water.

### 3.1.1. *Properties of Geomaterials Recoverable from Seismic Methods*

The three-dimensional equation of motion for an elastic solid can be derived through force equilibrium as described by Kramer (1996). Simplification of the force equilibrium equations results in the following three equations of motion for an elastic solid:

$$\rho \frac{\partial^2 u}{\partial t^2} = f_x + \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + \frac{\partial \sigma_{xz}}{\partial z} \quad (3.1)$$

$$\rho \frac{\partial^2 v}{\partial t^2} = f_y + \frac{\partial \sigma_{yx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{yz}}{\partial z} \quad (3.2)$$

$$\rho \frac{\partial^2 w}{\partial t^2} = f_z + \frac{\partial \sigma_{zx}}{\partial x} + \frac{\partial \sigma_{zy}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} \quad (3.3)$$

where  $u$ ,  $v$ , and  $w$  represent displacements in the x-, y-, and z-directions, respectively, and  $f$  represents the body forces per unit volume acting in each direction (generally gravity only). Considering body forces to be negligible, these three relationships can be simplified to the following alternate form:

$$\rho \frac{\partial^2 u_i}{\partial t^2} = \frac{\partial \sigma_{ij}}{\partial x_j} \quad (3.4)$$

where  $i$  and  $j$  equal (1,2,3) or (x,y,z), depending on the convention chosen. The equation of motion describes the propagation of stress waves within an elastic soil region, which advance in all three directions along a spherical shell, or wavefront, from the source location. Compression waves, the fastest-moving of all seismic waves, are the easiest to detect, as they arrive first at

observation points, typically geophones. The equation of motion can be combined with strain-displacement and constitutive (stress-strain) relationships to fully characterize the behavior of wave propagation in three dimensions.

For isotropic stress states, compression, also known as primary or seismic wave, speed  $v_c$  can be related to shear modulus  $G$ , Young's modulus  $E$ , density  $\rho$ , and Poisson's ratio  $\mu$  as follows:

$$v_p = v_c = \sqrt{\frac{G(2-2\mu)}{\rho(1-2\mu)}} = \sqrt{\frac{E(1-\mu)}{(1+\mu)(1-2\mu)}} \quad (3.5)$$

As values of a soil's seismic wave propagation velocity have been shown to be directly related to shear modulus and density, some consideration to how these values are determined should be given. Hardin and Drnevich (1972) have shown  $G$  to depend on void ratio  $e$ , overconsolidation ratio (OCR), and mean effective stress  $\sigma'_{mean}$  of a soil, as follows for angular soils

$$G = 1230 \frac{(2.973-e)^2}{1+e} (OCR)^k (\sigma'_{mean})^{1/2} \quad (3.6)$$

where  $G$  and  $\sigma'_{mean}$  are in units of psi, and the value determined for  $G$  is at a shear strain  $\gamma$  equal to  $10^{-4}\%$ . According to this relationship, for nonplastic soils ( $PI=0$ ), the value of  $k$  is equal to zero. Hardin and Drnevich (1972) also provided the following simplified hyperbolic model describing the relationship between the shear modulus at a given shear strain and the maximum shear modulus, which occurs at small strains less than approximately  $10^{-4}\%$

$$\frac{G}{G_{max}} = \frac{1}{1+\frac{\gamma}{\gamma_r}} \quad (3.7)$$

where  $\gamma_r$  is defined as the reference strain, which serves as a reference value for different values of shear strain, and is equal to the ratio between ultimate shear stress  $\tau_{ult}$  and  $G_{max}$  for a soil.

Seismic refraction methods can be considered a low-strain test for determination of seismic soil properties (Kramer 1996), where shear strains developed are typically less than  $10^{-4}\%$ , which

are not large enough to induce significant non-linear stress-strain behavior in the soil. Seed and Idriss (1970) proposed a more simplified relationship between shear modulus and confining pressure, based on the soil type and relative density as follows for sands:

$$G = 1000K_{2,max}(\sigma'_{mean})^{1/2} \quad (3.8)$$

where  $G$  and  $\sigma'_{mean}$  are in units of psf, and where

$$K_{2,max} = f(D_r) = 15 + 0.6D_r \quad (3.9)$$

for sands, with  $D_r$  given in percent. For silts and gravels,  $K_{2,max}$  is multiplied by factors of 0.6 and 2.0, respectively, according to this relationship. Through these various relationships for shear modulus  $G$ , estimates can be made of the values of the seismic wave propagation velocity  $v_c$ . We can see from these relationships that the values of  $G$  are strongly tied to both effective stress and density (or void ratio). So, for ground improvement methods having the objective of densifying soil, increases in values of both density and shear modulus can be expected.

Many years of experience in performing seismic refraction studies have resulted in a variety of empirical charts providing typical seismic p-wave velocities of various geomaterials, such as the ranges provided in Table 3.1. Excavation equipment manufacturers (Anon. 1987; Anon. 1988) have also provided charts relating rippability of soils and rocks to seismic p-wave velocities, which are commonly cited in the literature. More recently, Rucker and Ferguson (2006) observed correlations between seismic velocities and soil cementation stage classifications resulting from three projects in Arizona.



**Table 3.1. Range of Velocities for Compressional Waves in Soil and Rock  
(after ASTM D5777-00)**

Materials	Velocity	
	ft/s	m/s
<b>Natural Soil and Rock</b>		
Weathered surface material	800 to 2000	240 to 610
Gravel or dry sand	1500 to 3000	460 to 915
Sand (saturated)	4000 to 6000	1220 to 1830
Clay (saturated)	3000 to 9000	915 to 2750
Water*	4700 to 5500	1430 to 1665
Sea water*	4800 to 5000	1460 to 1525
Sandstone	6000 to 13000	1830 to 3960
Shale	9000 to 14000	2750 to 4270
Chalk	6000 to 13000	1830 to 3960
Limestone	7000 to 20000	2134 to 6100
Granite	15000 to 19000	4575 to 5800
Metamorphic rock	10000 to 23000	3050 to 7000

\*Depending on temperature and salt content.

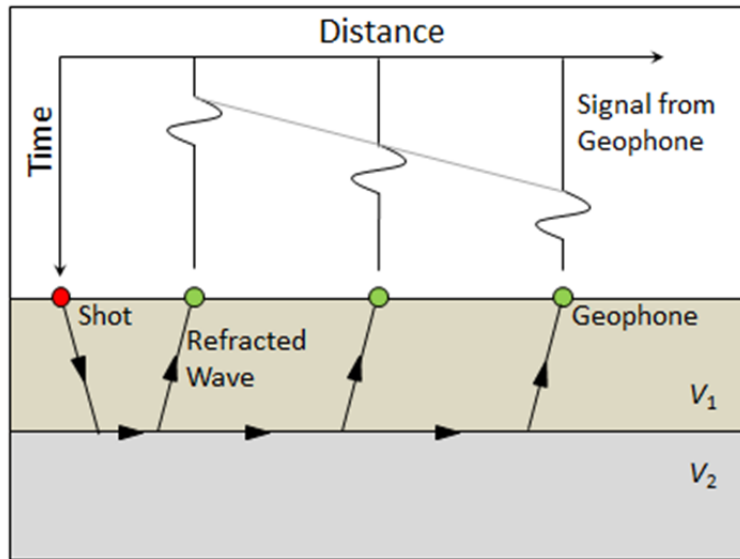
### 3.1.2. 2-D vs. 3-D Geophysical Methods

Conventional 2-D seismic refraction is based upon wave theory as related to plane waves. Huygen's principle describes the refraction of an incident ray upon a boundary between two media of different seismic velocities. The most elementary relation describing this refraction phenomenon is the law of refraction, or Snell's Law, which can be attributed to the field of optics, and is analogous to the refraction of a seismic wave across a boundary. This relationship is described as follows:

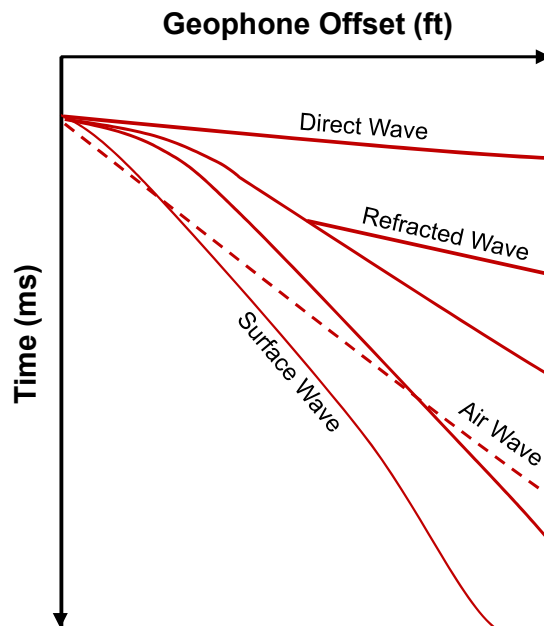
$$\frac{\sin\alpha_1}{\sin\alpha_2} = \frac{v_1}{v_2} \quad (3.10)$$

where  $\alpha_1$  and  $\alpha_2$  are the angles made with the normal to the boundary by the incident and refracted rays, and  $v_1$  and  $v_2$  are the seismic velocities of the incident and refracted rays, respectively. This relationship forms the basis for traditional 2-D seismic refraction interpretation, which can be extended to multiple layers of increasing velocity with depth. Figure 3.2 provides a simple illustration of the principles fundamental to 2-D seismic refraction procedures, where an incident wave is recorded at different times by geophones arranged in a

straight line radiating outward from the source location. Figure 3.3 shows a typical distribution of arrival times for surface, body, and air waves within a travel-time plot recorded by 2-D geophones during a seismic refraction survey.



**Figure 3.2.** Simplified seismic refraction process showing reflected waves and arrivals as recorded by geophones.

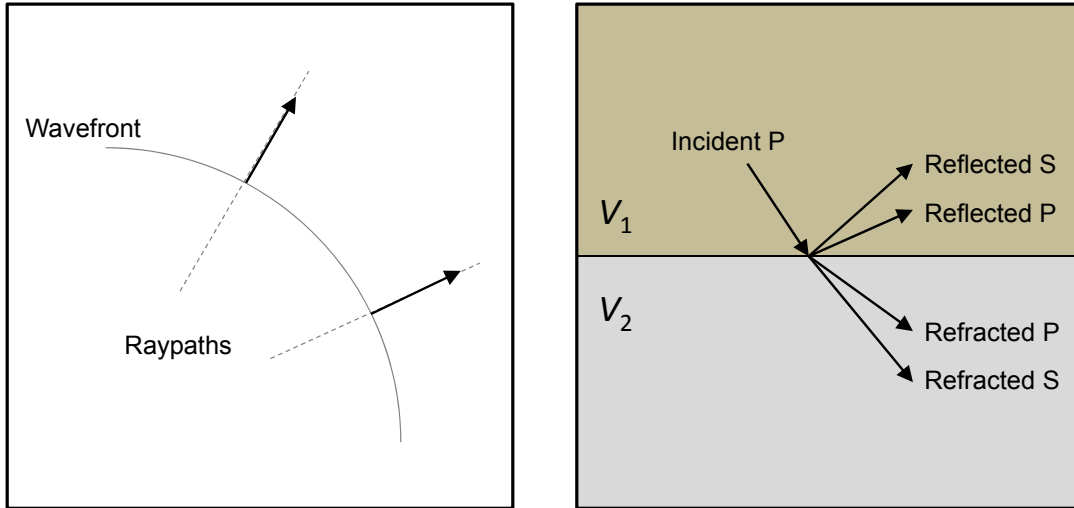


**Figure 3.3.** A comprehensive interpretation of body-, air-, and surface-wave events on seismic travel-time plots (after Park et al. 2001).

Pseudo 3-D seismic processing marked the next step in seismic tomography and has been described by Sirles et al. (2006). Two case histories started by collecting seismic data using standard 2-D seismic refraction field procedures, from which “data were processed using 2-D tomography inversion, then calibrated 3-D models were generated through interpolation.”

Additional clarification regarding the nature of propagating wavefronts and wave reflection and refraction is provided in Figure 3.4. For propagating p-waves, the waves of interest for 3-D seismic surveys, raypaths describe the path traveled by the normal to the surface of the seismic wave as propagation occurs. For a wave traveling in either two or three dimensions, raypaths can either be straight or curved depending on the materials and therefore wave velocities encountered. Also, as shown in Figure 3.4, an incident p-wave will both refract and reflect at a boundary between materials having different seismic velocities. Depending on the type of incident wave, different refracted and reflected waves will be created. Kramer (1996) provides further discussion on the nature of wave reflection and refraction.

Sirles et al. (2006) defined a ray as “a region in the model that has the highest contribution to the first arrival time, and typically descends from the source at the ground surface to higher velocity layers before ascending to the surface receiver(s).” This definition relates to the predecessor to the software used for tomography generation as part of this study, GSR3D. A complete review of seismic wave propagation and ray theory has been provided by Červený (2001).



**Figure 3.4. (L) Illustration of raypaths normal to the surface of a propagating wavefront and (R) reflected and refracted waves resulting from an incident p-wave.**

### ***3-D Seismic Tomography***

ASCE (1995) defines tomography as “an analytical technique for evaluating geophysical data such as the speed and amplitude of sound waves traveling through the earth, or electrical resistivity, radar frequency and signal strength.” The roots of tomographic imaging can be traced to the medical imaging profession, where computed tomography (CT) scans, computerized axial tomography (CAT) scans and magnetic resonance imaging (MRI) have become commonplace terms in medical practice.

Whereas these types of medical tomography methods are often used to image bone or soft tissue structure in the human body, the term seismic tomography refers to a more specific area of tomographic imaging used to estimate engineering properties of different materials such as soils and produce graphical representations of their distribution. Propagating velocities of compression waves (p-waves) are the most common properties recovered directly through seismic refraction analysis. The term 3-D seismic tomography therefore describes the use of

seismic refraction data collection methods for three-dimensional analysis and quantification of seismic velocities.

The 3-D seismic methods employed in this study are based upon wave propagation theory. In the three-dimensional domain, the seismic energy imparted by a source at the surface will travel through the ground along a wavefront. This wavefront will propagate through different materials, adjusting for the different velocities encountered by the wave. For 3-D seismic tomographic methods, the arrival times of this wavefront can be measured at any point along (or below) the ground surface, instead of simply in a straight line at the surface as with 2-D refraction methods, to more completely characterize the variation of seismic velocity in the material in question.

Fermat's principle was proposed by the 17<sup>th</sup> Century French mathematician Pierre de Fermat to explain the behavior of seismic raypaths at an interface. When applied to seismology and seismic tomography, the principle states that:

$$t = \int_A^B \frac{dl}{v} = \textit{minimum} \quad (3.11)$$

where  $t$  is the travel-time of the ray,  $A$  and  $B$  are two points along the travel path of the ray,  $dl$  is the elemental distance along a raypath, and  $v$  is the seismic velocity over that elemental distance. Fermat's principle states that of the many possible paths between two points, a ray will travel along the path that will result in the minimum possible travel time (Lowrie 1997).

Three-dimensional wave propagation methods generally begin by dividing a 3-D initial velocity model into small grids. Raypaths are then traced between sources and receivers to develop calculated travel times. These calculated times are then compared to known or measured travel times obtained through the actual seismic survey. The following linearized inverse problem can then be solved for each cell:

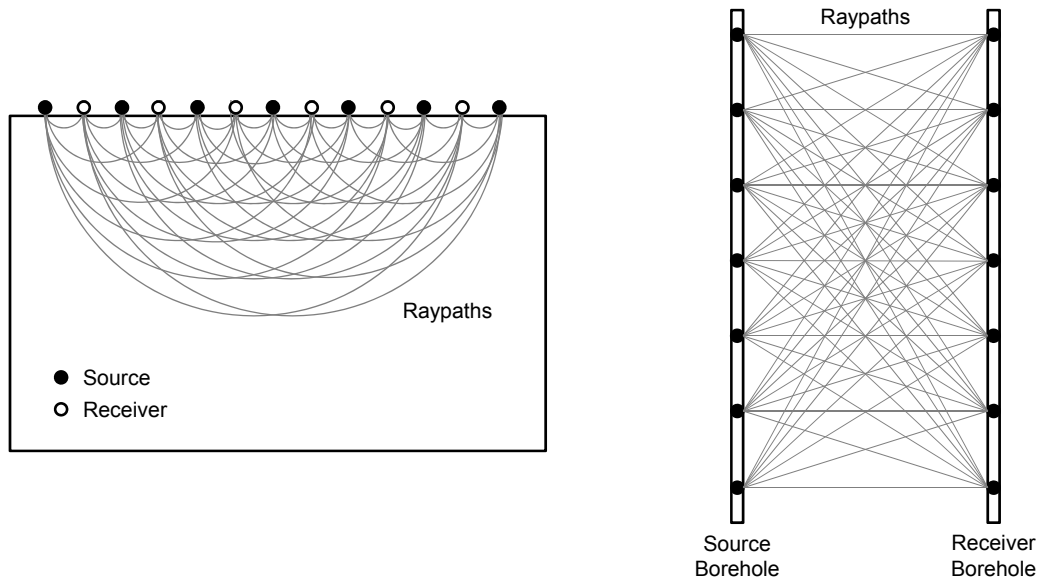
$$(t_{calculated} - t_{measured})_i = \sum_{j=1}^n L_{ij} \delta \left( \frac{1}{v} \right)_j \quad (3.12)$$

where  $L_{ij}$  is the length of the  $i$ 'th ray in the  $j$ 'th grid cell and  $\delta \left( \frac{1}{v} \right)_j$  is the change to be applied to the velocity model in the  $j$ 'th grid cell, sometimes referred to as the change in slowness, or inverse of velocity. The velocity model can then be updated iteratively following this procedure until the solution providing a minimum difference between calculated and measured travel times is obtained, providing the final velocity model.

Three-dimensional first-arrival-time tomography methods were used by Zelt et al. (2006) to process 3-D shallow seismic data collected as part of an environmental remediation investigation, where the 3-D seismic refraction-based method used was found to be relatively simple, quick, and inexpensive, with less-subjective analysis and interpretation, when compared to 3-D seismic reflection methods.

Another method which can be used to obtain 3-D seismic tomography involves the use of subsurface source and receivers located in boreholes, also referred to as down-hole or cross-hole methods. This technique has been successfully used to investigate an active sinkhole causing property damage in a residential neighborhood (FHWA CFLHD 2003), detect abandoned coal mines beneath a retaining wall, and verify the effectiveness of jet-grouting beneath a bridge pier foundation (Hanson et al. 2000). Figure 3.5 illustrates typical source and receiver layouts between both surface and subsurface methods, which would allow for 2-D tomography generation. The linear raypaths shown for the subsurface arrangement would only be accurate for a constant-velocity model where no refraction would occur. Additional geophone lines or boreholes would allow for 3-D tomography to be created. Cross-hole sonic logging (CSL), which is a non-destructive evaluation method used to evaluate the integrity of drilled shaft

foundations, can also be used to develop 3-D seismic tomography. Haramy (2006) also showed that 3-D CSL methods could be used to successfully determine seismic velocity differences before and after grouting of drilled shafts which were found to have defects.



**Figure 3.5. Source and receiver locations along with raypath coverage for typical (L) surface seismic and (R) subsurface seismic surveys.**

Data collection for true 3-D seismic tomography investigations follows many of the same procedures as those used during conventional 2-D seismic refraction. The most significant difference relates to the layout of the geophones and shot locations. During conventional 2-D or pseudo 3-D seismic surveys, geophones are arranged in a single line, and shots are recorded from locations in some arrangement surrounding or within that line. For true 3-D seismic investigations, a grid of geophones and shot locations is established, so that a single shot is recorded by all geophones simultaneously, resulting in decreased required field data collection time and increased resolution and data confidence compared to pseudo 3-D surveys, at the

expense of increased overhead costs related to the additional equipment required to image the same volume of soil.

### ***3.1.3. GSR3D Seismic Tomography Software***

A recently-developed software package known as GSR3D, developed by Geostructural Seismic Research, Inc., was used to process the data collected at the two sites and produce three-dimensional tomographic images representing the seismic velocities before and after grouting. The GSR3D software package has been successfully proven for a variety of civil engineering applications, including the location of a collapsed tunnel, detection of abandoned coal mines, location of scour zones within an embankment dam, location of utility pipes beneath a concrete roadway, and determination of 3-D bedrock topography.

This proprietary software integrates automatic signal processing techniques, numerical modeling procedures, and finite difference wave propagation methods to quickly obtain high resolution, accurate 3-D ground images from shallow seismic data. Sirles et al. (2006) describes the numerical modeling approach that makes up the GSR3D analysis, combining the discrete element method with particle flow code (DEM-PFC). The predecessor to GSR3D was known as the *Geostructural Analysis Package (GAP)*, which received use in fields outside of geotechnical engineering, such as structural engineering. The GAP package has been used extensively to evaluate the structural capacity of drilled shaft foundations (Haramy 2006), but its potential use in the fields of chemical, thermodynamic, and groundwater flows have also been proposed (Sirles et al. 2006). This computational method allows for simultaneous processing of many source and receiver combinations in arbitrary configurations, located either along the ground surface or in boreholes.

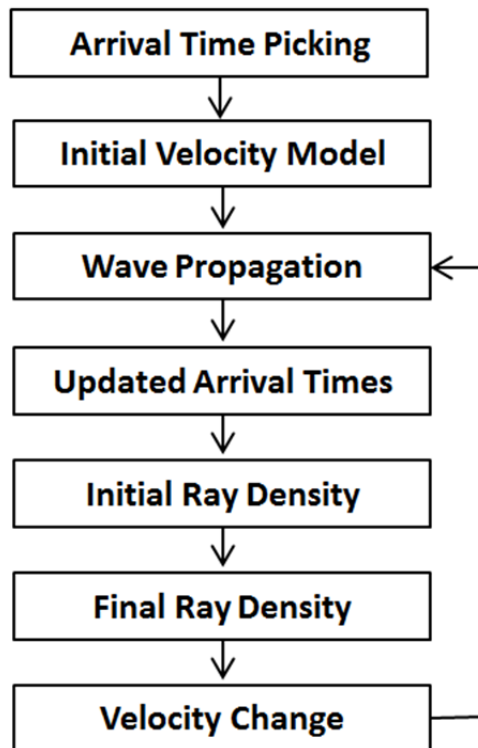


The software estimates travel times by propagating waves across a model of constant initial velocity using wave front normal vector interpolation following a modified Eikonal method, which are then compared to the travel times determined from the seismic shot record. Sample picks of compression wave first arrivals can be combined with time, frequency, and velocity filters and a multi-dimensional B-Spline interpolation network (BIN) to determine first arrivals accounting for waveform shape, source/receiver distance, and adjacent picks, resulting in automatic and consistent travel time picks. Waves are then propagated from each source and each receiver to determine regions in the velocity model having the most significant effect on the travel time and rational functions of incremental resolution are generated from these regions for the tomographic inversion.

The arrival times for each element are added to the corresponding source arrival function for each ray to characterize the Fresnel zone. Differences in arrivals from the model were iteratively corrected using a corresponding Fresnel zone density function allowing for rapid convergence. Model elements are ordered in a compact tetrahedral packing consisting of spherical elements of equal radius connected by links of equal length. The model resolution is incrementally increased for each iteration and quickly converges to the solution of minimum travel time error with minimum velocity variation, providing consistent results. The resulting 3-D tomograms can then be sliced and contoured from a variety of perspectives to allow for visualization of the velocity structure. Figure 3.6 illustrates a simplified flow diagram describing the processing routine followed during tomography calculation by GSR3D.

Boundary conditions for the tomography models generated by GSR3D cannot be specified by the user, and the results of different boundary conditions on the results were unable to be verified for this study. As waves which are propagated through the model do not have the ability to

reflect along the model boundaries, there is not chance that the calculated arrival time can be influenced by these boundary reflections. The tomographic volume can therefore be considered as a region within an infinite elastic half space. Also, as the calculated seismic wave arrival times are determined from the propagation of seismic wavefronts and not their reflections, only the arrival of this wavefront will have an influence on the resulting tomography, and any other potential waves, such as shear waves that arrive at later times, are not considered.



**Figure 3.6. Simplified processing procedure utilized by GSR3D.**

### ***Assumptions and Limitations of GSR3D***

An average value for the initial starting velocity of the model is determined based on the average distances between shot and receiver locations and the arrival times determined through the auto-picking process. This process is often referred to as straight-line average velocity determination. For regions having no raypath density, no procedure exists for updating the

seismic velocities from this initial velocity approximation. Therefore, in many areas of the final tomography model, the initial velocity approximation may be reported. This is especially evident at the greatest depths and at the boundaries of the models, where it often appears that a velocity inversion (higher velocity layers above lower velocity layers) exist, which is not probable due to the known stratigraphy of the subsurface layers.

Auto-picker results and manual training picks do not always agree with complete accuracy. However, the benefits of decreased influences from fatigue when performing manual picking of shots can be said to outweigh the losses from the disagreement between auto-picker and manual training picks. Geometric data entered for the geophone and shot locations are automatically rounded to the nearest integer within the GSR3D software. Regardless of the accuracy maintained when performing surveys of geophone and shot locations, the tomographic processing will be performed using integer values for the x, y, and z coordinates. This rounding can potentially result in uncertainties in the calculated velocities. Resolutions reported by the program are also limited to integer values, which prevents the identification of grouted regions of nominal size less than 1 ft or 1 m, depending on which units are chosen when performing the calculations.

Edge effects, or regions along the boundaries of the tomographic volume having lower raypath densities, are reported in the same way as higher raypath density regions. This fact can potentially be misleading to users of this type of seismic tomography program who do not fully understand this limitation.

### ***GSR3D Historical Case Study #1: Rocky Mountain National Park***

One of the first studies involving the use of 3-D seismic tomography for the assessment of compaction grouting effectiveness as part of roadway stabilization projects took place during the

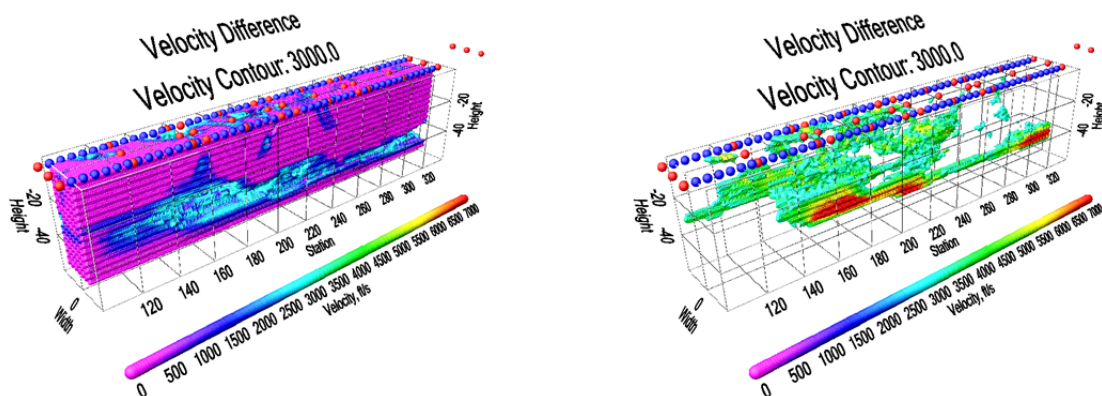
summer of 2007. Engineers with FHWA-CFLHD were tasked with rehabilitating a failed culvert that had been causing significant roadway settlement and cracking along Trail Ridge Road in Rocky Mountain National Park. The GSR3D program was investigated to determine seismic tomography before and after ground improvement at the site. Compaction grouting was used to stabilize roadway settlement caused by piping of fines from the subgrade due to a failed culvert. Before and after grouting, seismic data was collected using a sledgehammer impact on the ground surface as the input source while the refracted waves at different distances from the source were measured using geophones. The GSR3D program was used to interpret the arrival times of different waves at the different geophones. The method proved effective in producing pre- and post-grouting volumetric velocity difference images allowing for a more thorough assessment of ground improvement at the site. Further details relating to the site, the grouting operations carried out for the roadway remediation, and the seismic tomography investigation can be found in Haramy et al. (2009).



**Figure 3.7. Photographs showing (L) differential settlement of roadway and (R) compaction grouting operations at Rocky Mountain N.P.**

Some of the primary concerns in developing the compaction grouting program at this site resulted from the potential for damage to sensitive historic structures in close proximity to the

injection locations. Maximum displacement limits were imposed for the existing stone guard wall and a dry-stacked stone armored slope below the roadway and surrounding the culvert outlet. For the armored slope, a maximum vertical movement of 40 mm was allowed, with the mortared stone guard wall restricted to a maximum vertical movement of 20 mm to reduce the potential for cracking. To reduce possible heave of the roadway surface, compaction grouting was performed prior to the removal and replacement of pavement. This first-known case of the application of seismic tomographic methods for verification of grouting for roadway stabilization projects was based upon the pseudo 3-D, or 2.5-D, seismic tomography method, as described by Sirles et al. (2006). A single seismic line containing 24 geophones was deployed in four separate locations, during each of which shots were collected. The seismic data collected was later combined into a 3-D volume representing a combination of the four smaller volumes resulting from each of the four seismic lines collected in the field, to finally produce the pseudo 3-D volumetric seismic tomography images as shown in Figure 3.8. Further discussion of the data collection and processing methods used to develop this 2.5-D seismic tomography approach are provided by Sirles et al. (2006).



**Figure 3.8. Pseudo 3-D difference tomography from Rocky Mountain N.P. compaction grouting site, showing seismic velocity differences (L) less than 3000 ft/s and (R) greater than 3000 ft/s, on a scale of 0 to 7000 ft/s.**

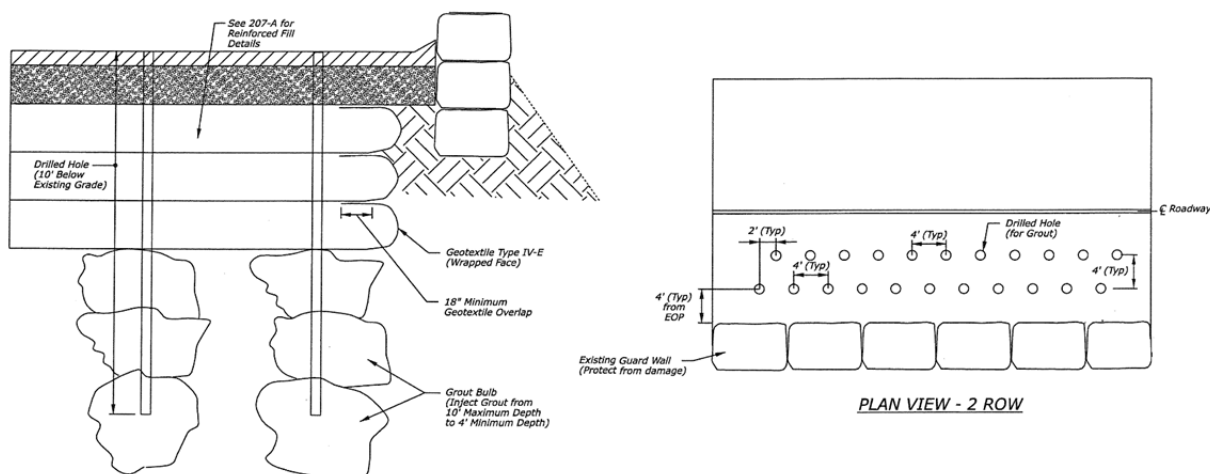
From the results shown in Figure 3.8, the 3-D difference tomography shows considerable increases in seismic velocities in the vicinity of the failed culvert. Records of the injected grout volumes, which show the highest grout injections near the midpoint of the volume, correlate well with the results of the seismic tomography. These results can be considered reasonable, as the highest degree of improvement could be expected near the midpoint of the volume where the failed culvert pipe was located, and the surrounding soils were believed to have been eroded and deteriorated. The existence of negative velocity differences in the resulting difference tomography is unknown, as the scales chosen for Figure 3.8 only displays positive velocity differences.

#### **4. CASE STUDY 1: ZION NATIONAL PARK**

The first site is located along the Zion-Mt. Carmel Highway, in Zion National Park, Utah, where excessive pavement subsidence and severe pavement cracking occurred. Initially, damage was attributed primarily to a large ancient landslide extending through three of the switchbacks approaching the Zion-Mt. Carmel Tunnel. On further investigation, roadway damage has been attributed to areas of very loose embankment material and open voids. Compaction grouting of this loose subsurface material was selected as the best remediation method to stabilize the subsiding embankment zones, and grouting was carried out following bottom-up procedures. Additionally, subsurface drainage improvements were completed in conjunction with excavation of the top 1 m (3 ft) of roadway and replacement with geosynthetic-reinforced fill. Two compaction grouting locations were chosen for conducting the 3-D seismic tomography based on site access and high anticipated grout takes. Uncorrected SPT values ranging from 5 to 14 (very loose to medium dense) were documented at these sites prior to grouting.

During compaction grouting, dial gauges were used to visually monitor and record minimum and maximum injection pressures and a water manometer was used to detect ground heave. Grout takes were recorded by counting the number of strokes of the grout pump cylinder, which was calibrated to the cubic foot. Following grouting, the upper 1 m (3 ft) of the road surface was excavated to allow for replacement with reinforced compacted fill. This excavation revealed asphalt thicknesses as much as 1 m (3 ft) along the centerline and as much as 1.5 m (5 ft) or more along the shoulder. Previous boreholes showed asphalt thicknesses of only 0.13 to 0.25 m (5 to 10 inches), indicating more settlement had occurred at this location and there was a potential inversion of the subsurface density profile. Compaction grouting was performed on a staggered

1.2 m (4 ft) pattern to depths up to 3 m (10 ft). Figure 4.1 provides a typical construction detail for the compaction grouting layout, and Table 4.1 summarizes quantities.



**Figure 4.1. Typical compaction grouting profile and layout at Zion National Park.**

**Table 4.1. Compaction grouting summary for Zion N.P.**

<i>Location</i>	<i>Stationing</i>	<i>Number of Injection Holes<sup>1</sup></i>	<i>Total Grout Casing</i>	<i>Total Grout Volume</i>
			<i>m (ft)</i>	<i>m<sup>3</sup> (yd<sup>3</sup>)</i>
1	172+54 – 174+10	79[8]	203(664)	3.2(4.2)
2	177+26 – 179+37	107[14]	204(670)	11.7(15.3)

<sup>1</sup> Number in brackets indicates number of holes where casing could not be advanced to minimum depth of 3 ft (1 m)

#### 4.1. Soils and Site Conditions

As previously mentioned, the soils at the locations studied at Zion National Park can be broadly described as loosely consolidated poorly-graded fine sands with some gravel and large boulders up to 15 ft (4.6 m) in diameter. A complete review of the sites studied has been previously reported by Yeh and Associates, Inc. (2008; 2009), including geological background and the results of a subsurface investigation performed at this project location.



An important observation made at the site was an existing 18 in. (46 cm) corrugated metal pipe (CMP) culvert located at approximate stationing 178+00, aligned perpendicularly to the roadway alignment, which corresponds closely to the midpoint of grid #2. However, this culvert appeared to follow along the top of bedrock, and therefore, identifying this pipe in the tomography results was anticipated to be very unlikely, as the pipe would be difficult to differentiate between the bedrock boundary. As shown later in Chapter 6, the resolutions calculated by the GSR3D software for the tomography at grid #2 were 2 ft (0.6 m), which is larger than the diameter of this pipe.

Figure 4.2 also provides some illustration of the problems observed at the roadway surface in the vicinity of the grouting and seismic survey locations. In some areas of the roadway, large voids were present in the pavement, which, according to Park Service personnel, had to repeatedly be filled by Park maintenance staff to prevent the traveling public from exposure to an unsafe situation. In other areas, small holes were observed in the pavement ranging from approximately 2 to 5 cm in diameter, which upon closer inspection, connected to much deeper and larger voids immediately below the pavement, indicating a highly unstable base situation.



**Figure 4.2. Voids beneath roadway surface daylighting at Zion N.P.: (L) Large void opening resembling a pothole, more than 0.5 m (1.5 ft) in width; and (R) small hole in pavement surface observed to open to a much larger void beneath pavement.**

## **4.2. Pre-Grouting Geophysical Investigation**

For both sites, two 24-channel Geode seismographs manufactured by Geometrics were used to collect and process the information received from 48, 4.5 Hz vertical geophones. The seismographs were powered by 12V automotive batteries and data was viewed and stored using a battery-powered laptop PC. A 7 kg (16 lb) sledge hammer equipped with a “triggering” sensor was used as a seismic source. The hammer was impacted upon an aluminum strike plate with sufficient energy to produce good quality readings at every geophone, as determined by observation of the shot record immediately following every shot. A triggering sensor sent a signal to the data recorder to begin recording as soon as impact occurred.

At the Zion sites, the 48 geophones were arranged in three lines of 16 geophones, with typically 1.8 m (6 ft) spacing between lines. Two different in-line spacings, 1.5- and 3-m (5- and 10-ft), were investigated to assess possible improvements in resolution achieved by the alternate spacings. At the Apache Trail sites, four lines of 12 geophones were used, utilizing landstreamers with 5-foot in-line spacing with either 3 or 4-foot spacing between lines.

Shot and geophone locations were surveyed to allow for relocation during the post-grouting survey. Activities including rock ripping, roadway pulverization, and heavy equipment traffic were occurring in the immediate vicinity of the planned survey at the Zion site, requiring carefully-timed shots or multiple shots to achieve satisfactory seismic arrival times based on signal-to-noise ratios. An average of 70 in-line shots per geophone layout was obtained at Zion, and 45 mid-line shots per layout at Apache Trail.

Zonge International, Inc. of Lakewood, Colorado was contracted as part of the Zion National Park investigation to provide geophysical data collection support. In addition, the Contractor provided manual picks of seismic first arrival times for each raypath between source and receiver

for the pre- and post-grouting 3-D seismic surveys, and final presentation of 3-D seismic tomography processing results in a report format. Further discussion of the results contained within the report from the Contractor is provided in Chapter 7, to which results obtained by this investigation are compared.

The road surface had been milled prior to arrival at the site, and loose granular material was found along the shoulder adjacent to the walls. Spike attachments were used on the geophones for the shoulder locations, where the spikes were pushed into the granular material and degraded asphalt. Tripod plates were attached to the geophones for the locations within lanes where the receivers could simply be set upon the road surface, with good agreement observed between signals from the spike and tripod plate attachments.

**Table 4.2. Source and receiver summary for Zion N.P. pre-grouting seismic survey.<sup>1</sup>**

<b>Site</b>	<b>Sources (Shots)</b>	<b>Receivers (Geophones)</b>	<b>Raypaths</b>
1.10	69	48	3312
1.5.1	66	48	3168
1.5.2	66	48	3168
2.10	69	48	3312
2.5.1	66	48	3168
2.5.2	65	48	3120

<sup>1</sup> Location of sources and receivers were not identical for Grid #1 between pre- and post-grouting surveys, due to retaining wall work at time of post-grouting survey.

**4.2.1. Site #1 Grid Layout (172+54 – 174+04)**

Layout of a rectangular coordinate axis for the first grid began with the placement of two stakes near an existing control point, at approximately 171+40, 19 ft Lt. A temporary stake numbered P1 was placed near an existing survey control point to serve as a basis for distance measurements to grid corners, and a second stake P2 was used to align P1 to visually locate the corner of the first grid along the roadway. This method was employed due to the fact that the

only surveying equipment that could be secured in the field was a hand level and stadia rod. A tape measure was used to pull measurements from P1 to A1 and A2, the nearest corners of the coordinate grid established for grid #1. Point A2 was located near the inside corner of the masonry retaining wall adjacent to the roadway at this location.

A length of 150 ft (45.7 m) was then pulled using the tape measure along the inside face of the wall, which was nearly linear, from point A2 to point A4, the third grid corner. The fourth grid corner, point A3, was then located by pulling a 3-4-5 square triangle from the line connecting A2 to A4, resulting in a rectangular grid. The line connecting A1 to A3 served as the positive x-axis and the line connecting A1 to A2 as the positive y-axis, with the positive z direction measured upward normal to the roadway surface. The slope of the surface for the first grid was assumed to be constant, resulting in a planar geophone location layout. Appendix B provides diagrams of the layouts of geophones and source locations for the single 10-ft geophone spacing and both 5-ft geophone spacings at the first grid location. These three separate layouts were referred to as 1.10, 1.5.1, and 1.5.2. For each of the layouts, a total of 48 geophones were arranged in three lines of sixteen geophones, with an intermediate line of geophone locations was established 6 ft (1.8 m) between the first and third lines.



**Figure 4.3. Layouts of the (L) 10-ft (3-m) geophone spacing for grid #1 and (R) 5-ft (1.5-m) geophone spacing for grid #1 at Zion N.P. during pre-grouting seismic data collection.**

The grid was marked out with spray paint at geophone and sourcing locations and masonry nails were driven into the remaining pavement at the named grid corners. A USGS benchmark was located at the west entrance to the Mt. Zion Tunnel, approximately 1550 ft east of the previously mentioned control point. A hand level and stadia rod were used to establish elevations from the known elevation of this benchmark to the grid corners and control points.

#### **4.2.2. Site #2 Grid Layout (177+26 – 178+76)**

The layout for the second grid was more complicated than the first, due to the curved alignment of the roadway at the selected location. While the first survey location was along a fairly straight roadway segment, the second was located along a curve. Similar procedures were followed, with more care taken to record and lay out geophones and sourcing locations. A rectangular grid was established following the same procedures as those used for the first survey location, with distances to grid corners recorded based on the control points established and known fixed features at the site. Parallel lines were then marked every five feet in the x-direction along this grid. Geophones were then set up along a pattern that maintained either a 5- or 10-ft x-direction spacing, depending on the grid being surveyed, but the y-coordinates

varied for each x-coordinate depending on the alignment of the roadway at that location. In other words, each geophone at a given x-coordinate was translated by the same distance in the y-direction, maintaining equal spacings of 6 feet in the y-direction as those used in the first grid layout. The single 10-ft in-line geophone layout and two 5-ft in-line geophone layouts were referred to as layouts 2.10, 2.5.1, and 2.5.2 for grid #2, following the same naming convention used for grid #1. Diagrams illustrating these layouts can also be found in Appendix B, and Figure 4.4 shows the curved alignment of the grid #2 and geophone layout for the 10-ft (3-m) geophone spacing.



**Figure 4.4. Layout of the 10 ft (3.0 m) geophone spacing at Zion N.P. grid #2 during (L) pre-grouting and (R) post-grouting seismic data collection.**

#### ***4.2.3. Equipment and Data Collection***

Two 24 channel geode seismographs manufactured by Geometrics of San Jose, California were used to collect and process the information received from the geophones, as shown in Figure 4.5. Each of the seismographs was powered by a 12V automotive battery, and data output was recorded using a ruggedized laptop PC. Built into the seismograph operating software are signal observation tools to monitor each geophone, which was used to verify satisfactory operation of each geophone and recording of synthesized noise prior to data collection.



**Figure 4.5. Twenty-four channel Geometrics Geode seismograph.**

A 12 lb. sledge hammer equipped with a “triggering” device was used as a seismic source. The hammer was impacted upon an aluminum plate, both shown in Figure 4.6, with sufficient energy to produce good quality readings at every geophone, as determined by the contracted geophysicist. The trigger sent a signal to the data recorder to begin recording as soon as impact occurred. Shot records recorded by the seismograph were stored to the laptop hard drive, which were later transferred to another system for first arrival picking and tomographic analysis.



**Figure 4.6. (L) Sledge hammer; and (R) aluminum strike plate.**

Construction work took place between 8pm and 8am, with closure of the road beginning at the intersection of Scenic Drive and Zion-Mount Carmel Highway. Excavation involving frequent rock ripping, material placement, and heavy equipment traffic were all taking place in the immediate vicinity of the planned survey, preventing work from being performed the first night of the visit. Data collection efforts were completed for grid #1 the following morning, with traffic control arranged for one lane beginning at 8am. Flaggers alternated traffic in either direction while equipment was being set up along the grid and checked. Once data collection was ready to begin, flaggers were instructed to hold traffic in both directions. Authorization was given from the Project Manager that traffic could be held in both directions for up to 30 minutes at a time, but typical traffic delays during data collection lasted 10 to 15 minutes, after which traffic was allowed to pass.

Data collection at grid #2 proved to be much easier, as no construction activities were planned for the following night. Some effort was required to convince project management to agree to provide flaggers to keep the road closed, while allowing for any necessary access by construction crew, to allow for data collection. A second project was underway east of the tunnel, inside the park, which was also operating on night shifts involving complete closure of the road. Once the necessary arrangements were made, data collection was able to proceed smoothly throughout the night.

Time requirements for the data collection can be summarized considering the conditions existing in the field at the time. Establishing the two grids, including six total geophysical layouts, was accomplished in approximately 5 hours using the manual tape-measure and hand-level methods described previously. For data collection for the three layouts at grid #1, where traffic control was maintained in the adjoining lane, approximately six hours were required.



Data collection was accomplished at grid #2 in approximately half the time as was needed at grid #1 due to the removal of delays resulting from traffic and construction activities.

### **4.3. Observation of Compaction Grouting**

The purpose of this site visit was primarily to observe compaction grouting being performed and to gather as much information as possible concerning methods and procedures followed, materials and grout mixes used, and any successes or difficulties encountered relating to this technique. This information will then be considered in upcoming revisions to the current compaction grouting (and general grouting) specification, otherwise referred to here as S270.

A 3D seismic refraction survey had previously been performed at this project site at segments 172+54 to 174+04 and 177+26 to 178+76 by CFL staff and Zonge Geophysics. These two locations are relatively straight sections of road, supported by historic stone masonry walls, that have been experiencing pavement subsidence and cracking, which is believed to be caused by the loose condition of the roadway fill and possible washing out of material beneath the roadway. The stone walls contain no provisions to allow for drainage of subsurface water that may accumulate behind the wall, and the presence of open void spaces is also suspected in these locations. Due to scheduling conflicts, a site visit could not be arranged to enable observation of compaction grouting at these specific locations. Several other locations along the Zion-Mt. Carmel Highway have experienced similar problems as the locations studied in the geophysical survey and have also been specified in the plans for compaction grouting. On the nights which the inspection took place, compaction grouting was being performed from stations 114+96 to 118+65. Here the road begins at a straight segment which enters into a switchback progressing uphill and ahead station, supported by a historic stone masonry wall similar to those found at the locations studied in the geophysical survey.

**Table 4.3. Grouting location summary for Zion N.P.**

Station	to	Station	Side	Rows	Grouting Type	Geophysical Survey?	Observation of Grouting?
114+96	to	118+65	RT	1	Compaction	None	Yes
166+42	to	168+68	RT	2	Compaction	None	No
172+54	to	174+10	LT	2	Compaction	172+54 to 174+04	No
177+26	to	179+37	LT	2	Compaction	177+26 to 178+76	No
183+82	to	186+64	LT	2	Permeation	None	No

This location was the last location where compaction grouting was to be performed. During compaction grouting at the three other locations, less than expected grout takes (i.e., injected grout volumes) were observed. Ken Baumgartner, Project Manager from CH2MHill, requested a site visit from Tom Allen, the contracted geotechnical engineer from Yeh & Associates, to investigate some of these issues and make any possible recommendations. After speaking with the crew from DrillTech, and looking over the drilling and grouting logs from the evening of Mr. Allen’s visit, it appears as though Mr. Allen requested compaction grouting be performed in the middle of segment 114+96 to 118+65, along the beginning and into the middle of the switchback. Mr. Allen instructed DrillTech employees to try slight variations to their procedure, including “drying” and “wetting” of the grout mix, with no noticeable change in results. The contract documents specified a maximum slump of 1.5 in (3.8 cm), and during our observations, this mixture resulted in clogging of the grout hoses and couplings on several occasions, especially if held under high pressures at one location for too long. DrillTech employees commented that this requirement was a bit too “dry,” and that a 2 to 3 in (5.1 to 7.6 cm) slump is typical, even ideal, for compaction grouting for the given conditions. While the Contractor’s claim may have been true based on their experiences, no guidance has been found in the literature suggesting a grout slump greater than 2 in (5.1 cm) should be used for compaction grouting.

#### ***4.3.1. Equipment and Methods***

An unusual technique was used to install the 2-in (5-cm) inside diameter (I.D.) steel casings, involving a sacrificial conical steel tip, inserted into the end of the casing and temporarily attached using one wrap of duct tape. These steel tips were said to have been manufactured by DrillTech at their shop. The 10.5-ft (3.2-m) casings with tips were driven to the required 10 ft (3.1 m) depth, unless refusal occurred, using a Hyundai 140W-7A excavator with a pneumatic driving attachment. The casings were then backed out of the borehole several inches using either an automatic hydraulic “casing puller” or a manually-operated lever-based remover. A steel rod a few feet longer than the casing was then inserted into the casing and rammed against the sacrificial tip to remove it from the casing. The rod was then held in place and the casing backed out a few more inches, checking that the rod remained in place while the casing moved to ensure removal of the tip. Casing installation advanced ahead of the grouting operations, and stopped when an adequately large group of casings had been installed. Casings locations were laid out using a tape measure, measuring from the inside of the stone wall and adjacent holes and marked out with spray paint.

Grout was mixed using a series of equipment specialized for grouting operations, trucked to the site from DrillTech’s California yard. When looking over the grouting logs provided by CH2MHill prior to our arrival at the site, an equipment change was noticed. During the first night of compaction grouting, it was discovered that the equipment originally brought in by DrillTech was not performing adequately, as no grout takes were being recorded for the first several holes. DrillTech staff informed us that a replacement batch plant and pump were brought in from GeoGrout, Inc. and casings were again driven and compaction grouting re-performed at those hole locations. While the GeoGrout equipment seemed to perform adequately, further

inquiry into this equipment change may be required. A truck-mounted generator provided electricity and a water tank fed water through a custom-designed water pump to both the batch plant and a water hose used mostly for tools and equipment cleaning. Mixing of cement, water, and sand aggregate was accomplished using a trailer-mounted batch plant that supplied mixed grout to the concrete pump using an auger-type mixer. A Reed B20 concrete pump fed the mixed grout through high-pressure grout lines to a large-radius bend coupling which was then attached to the casing. A dial gauge was fitted to the bend and packed with grease that could be periodically flushed using a zerk fitting to prevent grout from entering the gauge.

The cement used in the grout mix was Commercial Grade Quikrete Type II-V, 94 lb. bags, that “complies with current ASTM C-150 and Federal Specifications for Portland cement.” The compaction grouting proposal originally submitted by DrillTech states, “compaction grout will be composed of a uniform mixture of fine aggregate, Portland cement and water. Use of natural or artificial clay-type substances as additives to improve flow or pumpability of the low mobility grout shall not be allowed. Fine aggregate shall consist of well-graded silty sand with 100% passing the 3/8 in (9.5 mm) screen and between 18% and 30% passing the #200 screen. Portland cement and/or flyash may be added to make up a deficiency in fines content. Material having a plastic index will not be used.” The actual proportion of cement used in the mix was unable to be verified in the field.

Monitoring of vertical displacement, or heave, was accomplished using both a water tube manometer and a laser-based system consisting of a Leica Rod-Eye Classic and Leica Rugby 100. Heave displacement was only checked when relatively large grout takes were observed. Lateral, or horizontal, displacements of the wall were never checked, and no reflective markers

were ever observed as described in the DrillTech proposal. No cracking of the stone wall was ever observed.

#### ***4.3.2. Additional Observations***

On the first night of our observation, the employee chosen to operate the pump switch and record the grouting logs informed us that he had just arrived on the project site, and had never operated this kind of equipment before. The result was that on the first hole being grouted, the pump was not shut off following proper procedures, and the coupling escaped from the grip of the grouters, and fell to the ground, breaking a dial gauge. No calibration stickers or serial numbers were observed on any of the dial gauges used. The calibration sticker found on the laser level was expired.

At the majority of holes grouted, maximum recorded injection pressure per the logs was 500 psi, while pressures of 650 psi or greater were commonly observed on the gauge. When driving some casings, difficult conditions were encountered, possibly due to encountering of bedrock or boulders. During driving of some holes, the casing was seen to move laterally, creating an oblong-shaped hole. When these casings were removed, mostly following successful grouting, they were usually significantly bent.

Several mistakes were noticed in the compaction grouting submittal from the Contractor (Drilltech). On Sheet D-03 of these plans, beginning station 114+96 was mistakenly labeled 114+69. In this segment, from 114+96 to 118+65, compaction grouting was intended to be performed using one row of grouting locations, while the proposal and what was actually constructed followed the two row procedure. This error resulted in driven casing quantities roughly double the original estimate, with a yet unknown effect on the injected grout quantity.

In the permeation grouting proposal submitted while at the site, sheet D-07 shows a single row of grouting locations instead of the specified two rows as in the plans.

Ground cracking extending between adjacent holes on a line was observed following casing driving and compaction grouting. The depths of these cracks are unknown. On some holes where larger grout takes were recorded, whether the grout was entering existing voids or these cracks was uncertain.

#### ***4.3.3. Comments and Suggestions from Contractor***

The Contractor (Project Manager for DrillTech, Rick Quiles) was kind enough to share some thoughts and experience concerning the grouting operations at Zion National Park, which are paraphrased below.

- A spherical zone of influence is created around the point of injection, having a diameter about equal to the depth of injection below the ground surface. This zone causes a “pitcher’s mound” effect when grouting near the surface.
- At depths less than about 10 ft (3 m), insufficient overburden pressures exist to develop resistance to injection pressures during compaction grouting.
- Placing too many restrictions, or procedure-based specifications, on Contractors is a bad idea. If during grouting, attempting methods different than what is specified is believed to produce better results, the Contractor is bound to the conditions in the specifications. Sometimes Contractors end up having to continue using a procedure or grout mix they know is not working effectively or is not the most appropriate for the site conditions.

#### ***4.3.4. For Further Consideration***

From some of the observations made on this trip, the need for further investigation into the use of slump measurements for grouting applications has become clear. For several reasons, the

applicability of a slump measurement for ensuring a proper grout mix can be questioned. One reason has to do with the different stress conditions existing in the grout during slump testing and grout injection. During slump tests, gravitational forces are the only forces acting upon the slump cylinder. However, during injection, particularly during compaction grouting, much higher pressures act upon the grout, undoubtedly resulting in a different material behavior than under gravitational loading only. Whereas gravitational forces may not be of sufficient magnitude to induce shearing in the grout cylinder, the large forces encountered during injection are likely to produce a fluid condition in the grout. This argument calls into question the use of slump measurements alone. As pointed out by Warner (2004), an additional issue relating to the use of slump measurements has to do with the inclusion of fine-grained or cohesive soils, in the grout mix. Increasing the fraction of cohesive material would have the result of decreasing the apparent slump, which could mislead one into thinking that the mix had become “drier,” or having lower moisture content, while moisture had in fact never changed. While the DrillTech proposal specifies a maximum amount of fines to be used in the grout mix (18-30% passing the #200 screen), no testing of this material ever seems to have been performed.

The other significant issue that became clear during this trip relates to the methods used during grouting to monitor injection parameters such as pressure, injection rate, and total grout take. The contractor monitored and recorded minimum and maximum injection pressures using a dial gauge. Grout takes were recorded by counting the number of strokes of the grout pump cylinders, which were said to have been calibrated. At each hole, the total strokes were counted, and the number divided by four to evenly distribute the take across the four separate stages. At one point when the remote pump switch line was severed, pump strokes were visually counted until the line could be reconnected. Continuous and real-time computer monitoring of these

parameters would decrease the chances of human error in these situations, and show how injection parameters varied with time and depth.

#### **4.3.5. Reinforced Fill (177+26 to 179+37)**

At one of the segments being studied as part of the geophysical investigation, the excavation had been completed the night before we arrived, allowing some photographs to be taken and observations to be made. Perhaps most interesting about the excavation was the very deep areas of asphalt pavement that remained visible even after milling and 3 ft (1 m) of excavation. Greater than 2-ft (0.6-m) asphalt thicknesses were present at the centerline, increasing toward the stone wall, as shown in Figure 4.7. These observations were postulated to have the unexpected result of showing decreases in p-wave velocities for the reinforced fill zones once the post-grouting geophysical survey is performed. Nuclear density testing logs for the compacted fill placed at this location show placed wet densities ranging from 138 to 145 lb/ft<sup>3</sup>, at moisture contents of between 5.4 and 6.2%. Fill was placed in the excavation in 9 inch lifts separated by geotextile fabric as specified in the plans with multiple passes of a smooth drum vibratory roller compactor.



**Figure 4.7. Asphalt thickness greater than 1 m (3 ft) observed at Zion N. P. site due to repeated maintenance patching to correct settlement.**



#### **4.4. Post-Grouting Geophysical Investigation**

Nearly identical procedures as employed during the pre-grouting seismic survey were followed for the post-grouting survey, with a few notable exceptions. At each of the grids, the masonry retaining walls which had been specified for removal and replacement in the plans were discovered to have been removed during the course of construction, but not yet completely reset. As these walls were still in the process of being reset at the time of arrival to complete the post-grouting survey, and large trenches approximately one to two feet deep remained adjacent to the walls, minor modifications to the grid layouts had to be made in order to complete the data collection within the narrow time window available. Instead of 6 ft (1.8 m) spacings between geophone lines, 5 ft (1.5 m) spacings were used to narrow the grids. At grid #1, the alignment of the grid was skewed slightly to allow for the best possible relocation and coverage of the targeted soil volume considering the unexpected conditions at the site.

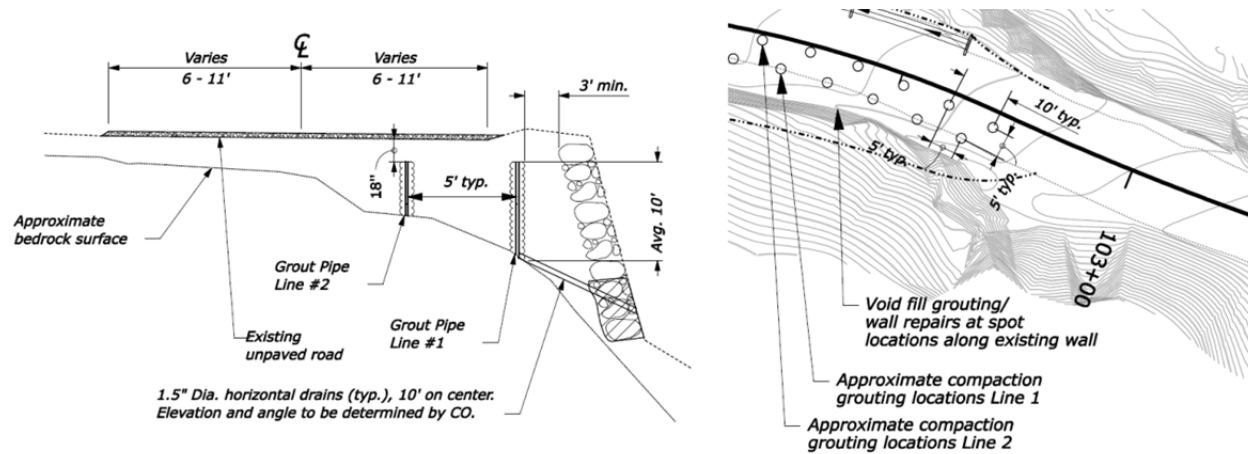
Data collection proceeded easily once the grids were relocated and modified as required, with similar access and scheduling challenges encountered during the pre-grouting survey. Similar time requirements for data collection were also noted between the pre- and post-grouting surveys.

## **5. CASE STUDY 2: APACHE TRAIL, TONTO NATIONAL FOREST**

The second site studied as part of this research is located along the Apache Trail, within Tonto National Forest in Arizona. The Apache Trail traverses the Superstition Mountains and connects Apache Junction, on the eastern edge of the Greater Phoenix area, with Theodore Roosevelt Lake. Similar problems as observed at the Zion site have plagued this road for many years, and a combined void-fill grouting and compaction grouting program was designed to stabilize areas showing evidence of void development from piping of material within loose roadway fill material and subsidence beneath both the road surface and adjoining retaining walls. One of the most sensitive concerns in performing compaction grouting on this project, and guiding the selection of associated performance criteria, was possible disturbance to historic dry-stacked stone retaining walls.

While traditional high-pressure, low-slump compaction grouting was originally specified in the plans as the primary method of filling potential voids and densifying zones of loose soil, concerns about possibly damaging the historic dry stacked retaining walls necessitated the inclusion of strict monitoring criteria, particularly for displacement of the wall faces and the maximum allowable grouting pressure. Similarly to the grouting at Zion, casings were installed to relatively shallow depths from 2 to 17 ft (0.6 to 5.2 m). The first several holes that were attempted to be grouted using the compaction grouting technique were quickly advanced upstage without taking significant grout quantities. Following some changes, the greatest results were obtained by increasing the water-cement ratio of the grout and filling the holes strictly by gravitational pressure, or hydraulic head. A water to cement ratio of 0.77 by weight (1.17 by volume) was chosen, along with an equal weight of fly ash to cement, to which small amounts of

retarding and thixotropic admixtures were added. Figure 5.1 provides a typical construction detail for the compaction grouting layout, and Table 5.1 summarizes grouting quantities.



**Figure 5.1. Typical grouting profile and layout at Apache Trail Wall 1.**

**Table 5.1. Grouting summary for Apache Trail.**

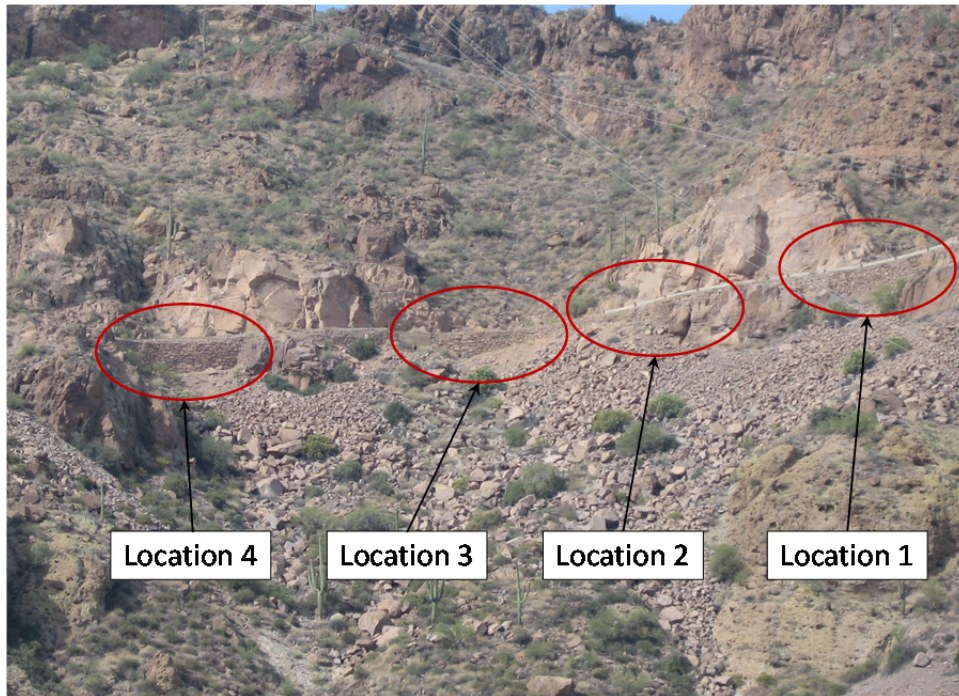
<i>Location</i>	<i>Stationing</i>	<i>Number of Injection Holes<sup>1</sup></i>	<i>Total Grout Casing</i>	<i>Total Grout Volume</i>
			<i>m (ft)</i>	<i>m<sup>3</sup> (yd<sup>3</sup>)</i>
Wall 1	100+00 – 102+71	27[6]	54(176)	14.5(19)
Wall 3	300+00 – 304+64	92[17]	197(647)	117(153)

<sup>1</sup> Number in brackets indicates number of holes where drilling was completed but no grout injected

### 5.1. Soils and Site Conditions

Conditions at the Apache Trail site were relatively similar to those encountered at Zion National Park, with the most significant variance being the different roadway surfaces in place. While at Zion, asphalt pavement thickness ranging from several inches to several feet existed at the seismic survey locations, the roadway surface along the portion of Apache Trail studied consisted of dense, compacted decomposed granite material. Figures 5.2 and 5.3 provide some perspective into the terrain and conditions existing at the Apache Trail site. A more detailed

analysis of the site conditions, including geotechnical evaluations of the roadway and stone retaining walls, has been reported by AMEC (2007) in a previous study.



**Figure 5.2. Panoramic photograph showing locations 1 to 4, from right to left, along Wall 3 at Apache Trail, with stationing advanced from approximately 300+00 at the right to 304+50 at the left.**



**Figure 5.3. Photographs of Apache Trail retaining walls: clockwise from top left: (1) Location 1; (2) Location 2; (3) Location 3; (4) and (5) Location 5, Wall 1; (6) large void daylighting at the roadway surface at Location 4.**

## 5.2. Pre-Grouting Geophysical Investigation

Landstreamers, connected arrays of geophones designed primarily to be towed along the ground, were incorporated for the Apache Trail investigation as shown in Figure 5.4. These geophone arrays were chosen based on their flexibility in placement and relocation in the field, a choice that was supported by the good agreement found by van der Veen et al. (2001) between signals received using traditional geophones and landstreamers. The main advantages of using landstreamers for at this site were the significant reductions in time and effort required to place sensors and gather seismic data, as well as the ability to quickly move the line in the event that traffic was required to pass the narrow roadway. Four profiles of Geostuff landstreamers, consisting of twelve 4.5-Hz vertical geophones spaced 1.5 m (5 ft) apart, allowed for prompt relocation of receivers when moving between sites and clearing passing traffic. A minimum of 45 shots for each site were placed along the centerlines between adjacent landstreamers and off-end of the lines. Two 24-channel Geometrics Geode seismographs, as shown in Figure 5.4, were used for this investigation as well. Diagrams illustrating the layout of geophones and shots for each of the five locations are provided in Appendix B for further reference.

Due to the relatively shallow depths to bedrock at both sites and the close spacings of geophones, arrival times were relatively small. In these situations, the addition of a delay, or pre-trigger geophone signal record, provided a longer baseline signal to consider during data interpretation and resulted in easier to distinguish arrival times. The use of geophone tripod bases and landstreamers with geophones mounted to baseplates both allowed for successful identification of compression wave arrival times, often without requiring shot stacking. Background noise from nearby construction activities during data collection was addressed by stacking consecutive shot records from the same location when noise became significant.



**Figure 5.4. (L) Laptop, seismograph, and battery setup; and (R) geophones deployed on landstreamers at Apache Trail.**

**Table 5.2. Source and receiver summary for Apache Trail**

Site	Sources (Shots)	Receivers (Geophones)	Raypaths
1	45	48	2160
2	45	48	2160
3	45	48	2160
4	45	48	2160
5	59	48	2832

Locations were chosen for this investigation based primarily upon the layout of the historic dry-stacked masonry retaining walls in the vicinity of the planned grouting operations. The grid layout chosen was centered at the midpoint of the tallest sections of these walls, and aligned as close as possible along the roadway surface near the walls. As the greatest depths of fill material were expected to exist at these locations, the greatest potential for grout takes was anticipated here, a hypothesis that had been supported by evidence gathered in previous studies of these segments of Apache Trail and the walls of concern.

### 5.3. Observation of Compaction Grouting

Due to scheduling conflicts, the frequently-changing construction schedule, and the need to plan any travel to this site well in advance, the author was unable to personally attend the compaction grouting operations. The grout mix that was finally chosen for the Apache Trail grouting can be found in Table 5.3. A thixotropic admixture and foam were added to this mix design, with amounts determined based on site conditions. The retarding admixture used was Eucon DS, manufactured by Euclid Concrete Admixtures, and the thixotropic admixture used was Rheomac VMA 362, manufactured by BASF. The grout mixture shown corresponds to a water-to-cement ratio of 0.77 by weight and 1.17 by volume.

**Table 5.3. Grout mix used at Apache Trail.**

<b>Masonry Sand</b>	1350 lb
<b>Top Soil (Silt)</b>	1350 lb
<b>Cement</b>	432 lb
<b>Fly Ash</b>	432 lb
<b>Retarder</b>	24 oz
<b>Water</b>	40 gal

Additionally, the grouting plan initially outlined in the plans specified three lines of grouting points along both Wall 1 and Wall 3. Due to higher than expected grout takes during grouting along lines 1 and 2 (line 1 being nearest to the outboard stone retaining wall), grouting line 3 was abandoned to avoid significantly exceeding the estimated grout and hole casing quantities.

### 5.4. Post-Grouting Geophysical Investigation

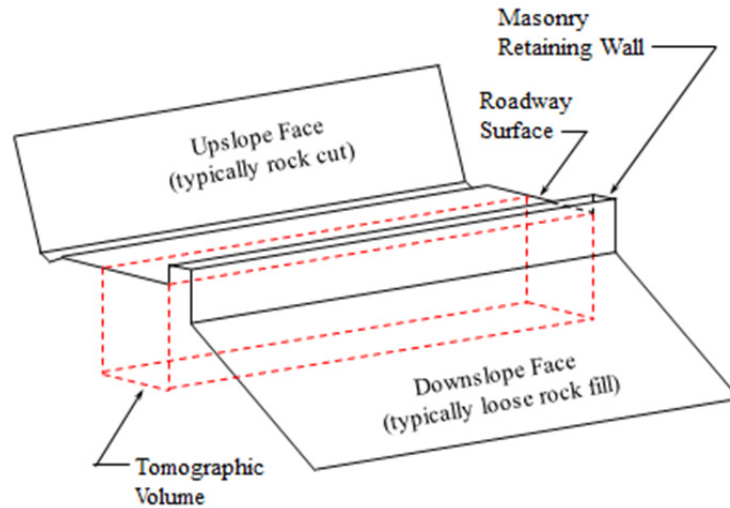
Identical procedures were followed during post-grouting data collection as were employed during the pre-grouting survey, with the exception that shot locations which were no longer accessible due to the reduced two-person crew had to be abandoned. The choice to leave out these shot locations was determined in advance, and no significant reduction in the quality of the investigation was anticipated as a consequence.



## 6. RESULTS

Once the seismic data had been collected from the pre- and post-grouting investigations at each of the sites, and the geometries of the geophone and source locations determined from the surveying information, 3-D seismic tomography images were developed using the GSR3D software package. Select pre- and post-grouting seismic tomography from the sites surveyed is provided in Appendix C, seismic difference tomography can be found in Appendix D, and ray densities are presented in Appendix E for each of the locations.

Figure 6.1 provides a schematic which helps orient the viewer as to the perspectives given for all tomography developed for this study. While different origins and directions of coordinate axes were chosen for the Zion N.P. and Apache Trail relative to the adjacent retaining walls at the sites due to conditions in the field, the viewing perspective for the tomography is maintained consistently throughout this report with respect to viewing angle. This allows the viewer to better understand the conditions nearer to the retaining wall structures, which were of primary concern when performing grouting at these sites. Additionally, the most severe signs of settlement and roadway damage were observed along the outboard traffic lanes at these sites, which correspond to the nearer side of the tomography as presented here.



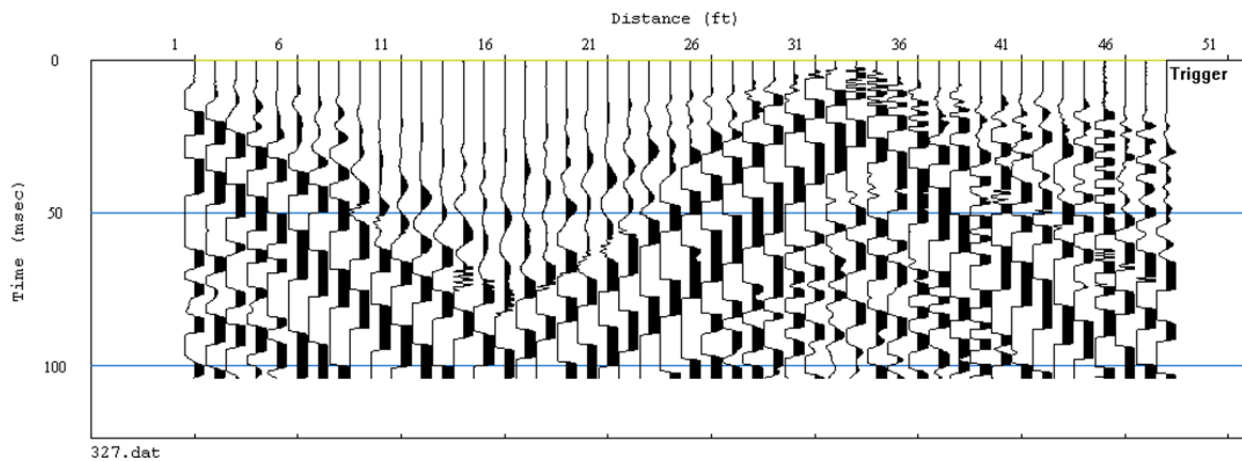
**Figure 6.1. Schematic illustrating the viewing perspective for the tomography generated for both Zion N.P. and Apache Trail sites, relative to the typical site conditions.**

### **6.1. Zion National Park Results**

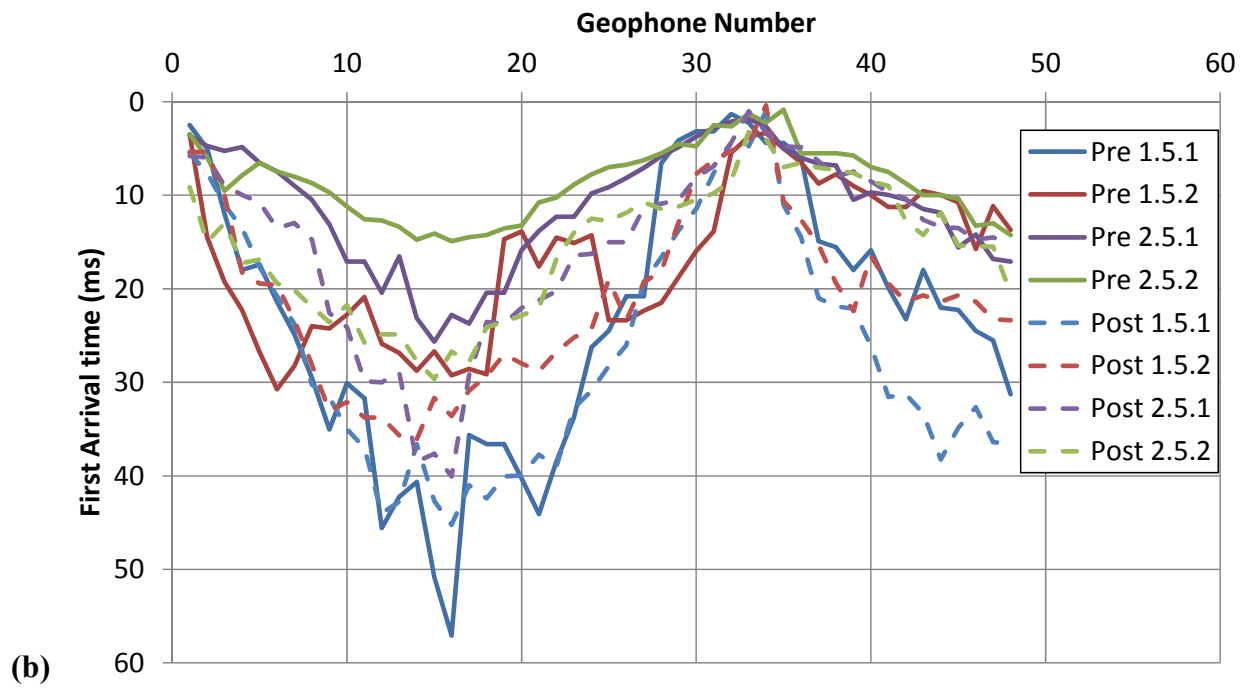
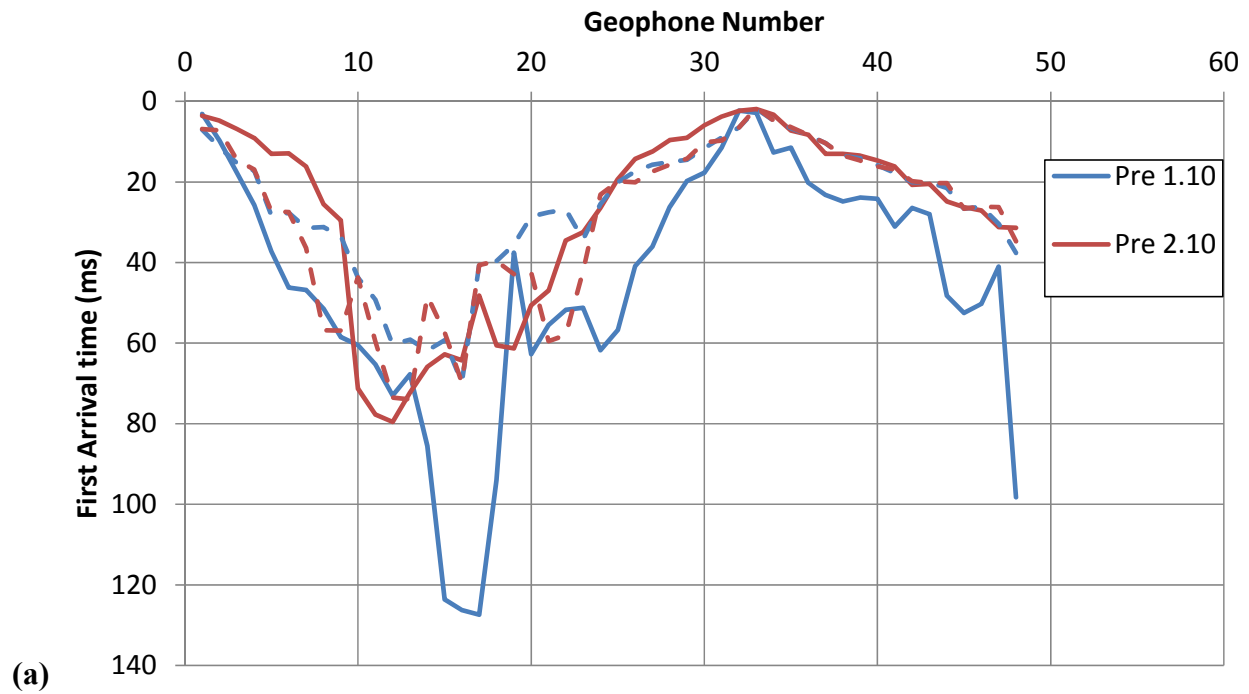
Consistent procedures were followed for processing of the 3-D seismic data collection during the field investigations for both Zion and Apache Trail sites. In order to obtain the maximum benefit of the automated first arrival picker integrated within the GSR3D package, while allowing for some degree of user influence in consideration of the picks, the full capabilities allowed by the software for entry of training picks into the autopicker feature was utilized. The following process was determined after several different procedures were investigated for determination of the first arrival times for the approximately 64,000 raypaths resulting from the pre- and post-grouting surveys at both sites. Figure 6.2 shows a typical shot record collected from the pre-grouting survey at layout 1.5.2 at Zion. The seismic data collection and viewing software accompanying the seismographs included software called SeisImager2D which allowed for auto and manual picking of seismic first arrival times. This software was used to develop manual picks for selected shot locations, which remained consistent in relation to the position within grid layout for each of the layouts. These manual picks, resulting from one shot at each

layout, were entered manually as training picks into the GSR3D program for use in the autopicking procedure.

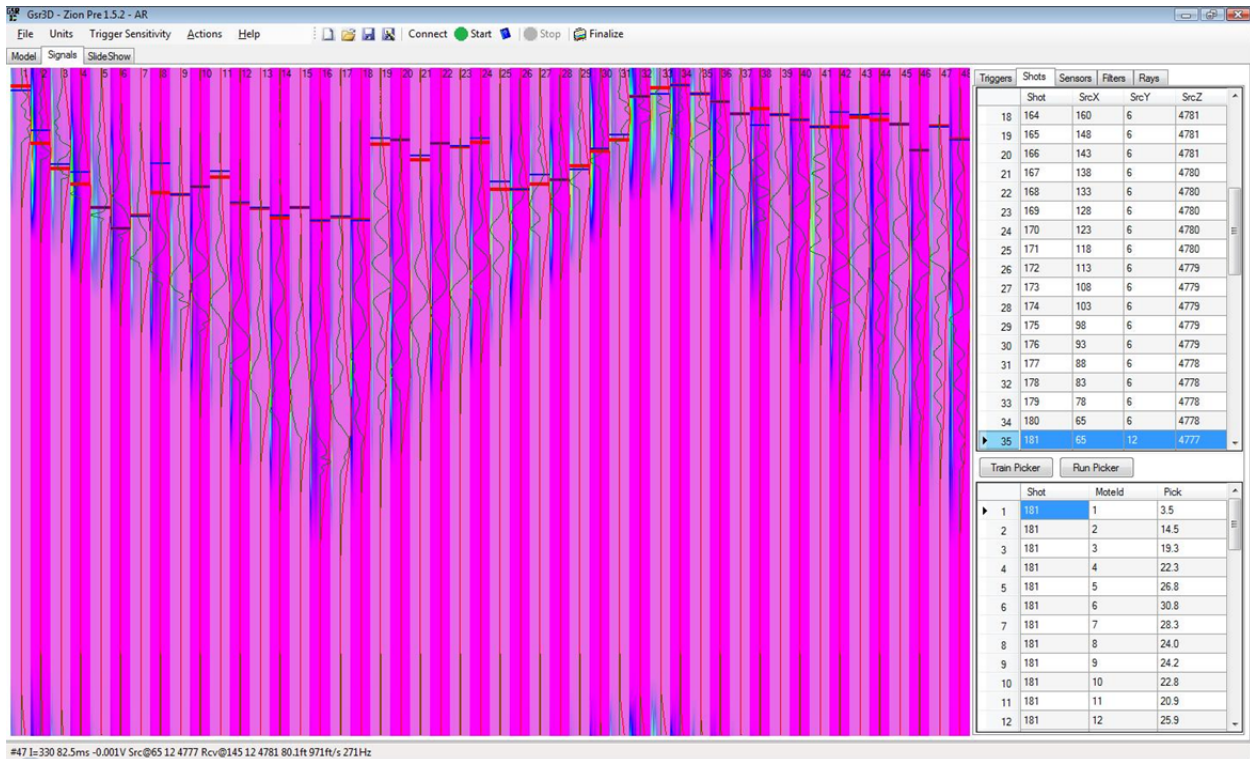
Figure 6.3 shows overviews of the training picks used for generation of the 3-D seismic tomography at the Zion sites. A general trend can be observed in this figure, where significant increases in arrival times occurred following grouting for the 5-ft (1.5-m) geophone spacings, which may have resulted from decreases in seismic velocities following grouting. The opposite trend is generally observed for the 10-ft (3-m) geophone spacing layouts, where decreases in arrival times can be noted, which would suggest increased seismic velocities within the subsurface materials. It should be noted, however, that due to the circumstances encountered during data collection, as previously mentioned, the locations of shots and geophones for both grids were not able to be maintained completely between the pre- and post-grouting surveys, but the relative locations used for the training shots were held consistent.



**Figure 6.2. Typical shot record for 3-D layout 2.5.1 at Zion N.P., with clearly distinguishable first arrivals.**



**Figure 6.3. Manual training picks used for GSR-3D autopicker for Zion sites: (a) 10-ft (3-m) geophone spacing; and (b) 5-ft (1.5-m) geophone spacing.**



**Figure 6.4. Typical screenshot showing manual training picks (in red) and resulting trained autopicks (in blue) used processing of seismic data for Zion pre-grouting location 1.5.2.**

Red picks shown in Figure 6.4 were determined using SeisImager2D, and entered into GSR3D as example picks for one shot. The train picker and run picker commands were then executed within GSR3D, resulting in the final picks shown in blue. The shot record above is shown for Zion pre-grouting location 1.5.2.

Tomography calculated for the Zion and Apache Trail locations was plotted using Matlab software, to allow for a variety of situations to be considered, and to determine the most effective means of presenting the results possible. The GSR3D software contains a fast, consistent, and automated tomography generation tool, which creates 3-D perspective views and 2-D slices of the velocity models calculated by the program, saving the images created to separate folders on the computer's hard drive. However, GSR3D does not typically allow for the computation of

difference tomography, although the software does have this capability. To allow for the calculation and plotting of the difference tomography, as discussed in the next section, and to maintain consistency in the tomography presented in this study, the powerful 3-D visualization and matrix computation abilities of Matlab were used to plot the pre- and post-grouting tomography instead. GSR3D creates a data file following tomography calculation that contains a table consisting of the nodes which make up the tomography. At each node, the value of the determined seismic velocity and ray density is reported along with the x-, y-, and z-coordinates of each node. This table could then be easily plotted using different Matlab functions to create the tomography for each location. A 3-D scatter plot was chosen to represent the data, with spheres of equal radius centered at the node location, colored with respect to a specified colorbar, or scale, depending on the data being plotted.

Pre- and post-grouting tomography for the Zion locations, showing only seismic velocities less than 500 m/s can be found in Appendix C. These representations of the tomography were found to provide a simple comparison between pre- and post-grouting tomography, while considering ray densities, as discussed later in this chapter. For most of the Zion locations, less points below this threshold velocity can be observed following grouting, suggesting a decrease in the regions of lowest-velocity due to grouting. At some locations, unexpected increases in the number of points below the threshold velocity can be observed, which are attempted to be explained in later sections.

### ***6.1.1. Difference Tomography***

Difference tomography was calculated from the pre- and post-grouting tomography as follows:

$$v_{c,diff} = v_{c,post} - v_{c,pre} \quad (6.1)$$

where  $v_{c,diff}$  refers to the seismic velocity difference and  $v_{c,post}$  and  $v_{c,pre}$  refer to the seismic velocities resulting from the post- and pre-grouting tomography, respectively. Upon examination of the data points calculated for the tomography at the Zion sites, the discovery was made that data points did not exist at the same coordinates within the overlapping volumes between the pre- and post-grouting models. A simple Matlab routine was written to read the pre- and post-grouting tomography output, consider the locations of the data points in each, and compute the seismic velocity differences between points falling within a specified distance tolerance. For each site and instrumentation geometry, a variety of tolerances were considered to provide the most representative number of difference tomography points possible. A summary of the tomography output for each of the Zion sites is provided in Table 6.1, and the difference tomography in Table 6.2. Reasonable numbers of data points were obtained according to this procedure for most sites, with the exception of sites 1.5.2 and 2.5.1, where higher disagreement between the locations of the pre- and post-grouting data points was found.

**Table 6.1. Pre- and post-grouting tomography summary for Zion N.P.**

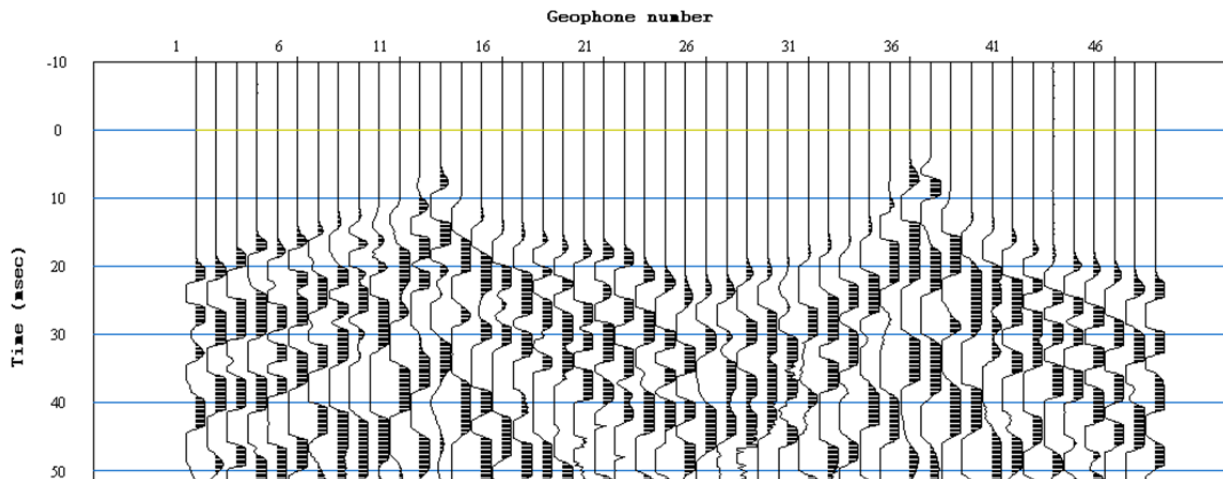
Site	Pre-Grouting Tomography		Post-Grouting Tomography	
	Data Points	Resolution, m (ft)	Data Points	Resolution, m (ft)
1.10	34682	0.6 (2)	34639	0.6 (2)
1.5.1	82989	0.3 (1)	78936	0.3 (1)
1.5.2	86306	0.3 (1)	82158	0.3 (1)
2.10	54427	0.6 (2)	49181	0.6 (2)
2.5.1	16921	0.6 (2)	15833	0.6 (2)
2.5.2	17675	0.6 (2)	15907	0.6 (2)

**Table 6.2. Difference tomography calculation summary for Zion N.P.**

Site	Tolerance ft. (cm)	Minimum Tomography Data Points for Difference Calculation	Resulting Difference Tomography Data Points
1.10	0.75 (22.9)	34639	28313
1.5.1	0.50 (15.2)	78936	63045
1.5.2	0.60 (18.3)	82158	<b>187755</b>
2.10	0.50 (15.2)	49181	49156
2.5.1	1.00 (30.5)	15833	<b>2617</b>
2.5.2	0.50 (15.2)	15907	15896

## 6.2. Apache Trail Results

The same procedures were followed for this study for the processing of 3-D seismic tomography for the Apache Trail sites as was used for the Zion sites. Similarly, Figure 6.5 shows a typical shot record recorded for a location at Apache Trail, illustrating the addition of the pre-trigger geophone record, or delay, added to improve the determination of first arrival times. Figure 6.6 displays the manual training picks entered into the GSR3D program for the autopicking analysis, from which a general trend of decreased arrival times can be observed suggesting increases in seismic velocities.



**Figure 6.5. Typical shot record for 3-D layout at Apache Trail, with clear first arrivals and pre-trigger delay interval shown.**



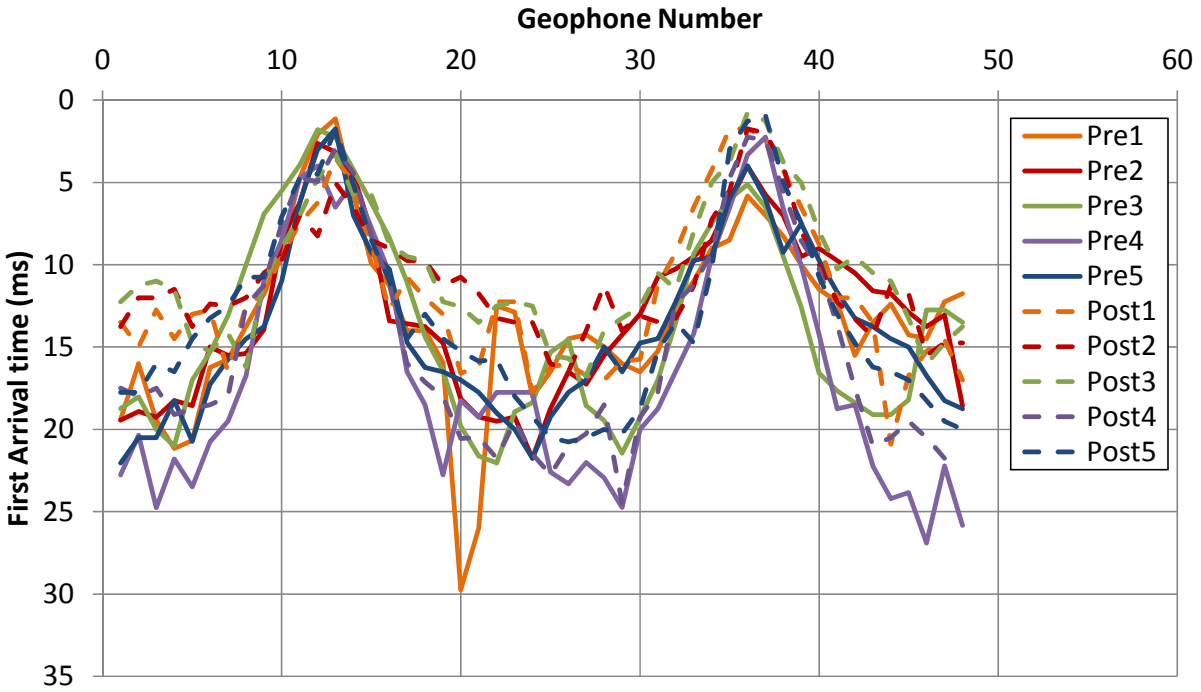


Figure 6.6. Manual training picks used for GSR-3D autopicker for Apache Trail sites.

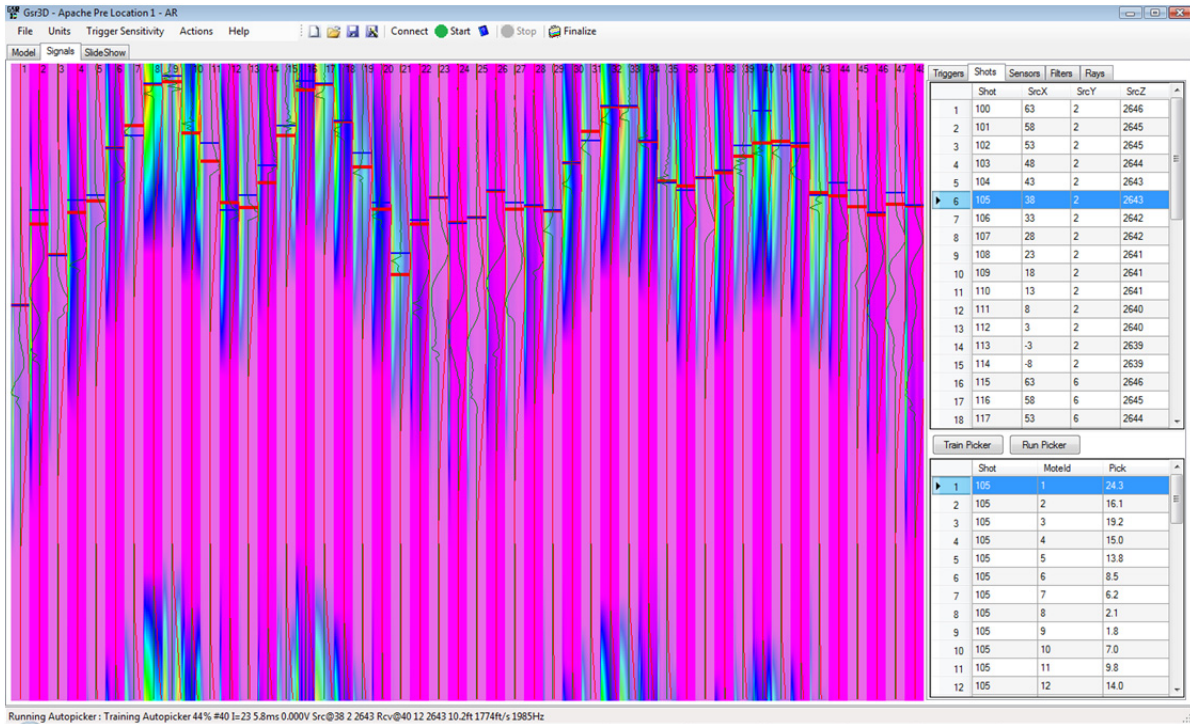


Figure 6.7. Typical screenshot showing manual training picks (in red) and resulting trained autopicks (in blue) for Apache Trail pre-grouting location 1.

### 6.2.1. Difference Tomography

Values for difference tomography were calculated following the same procedures used for the Zion sites, where a Matlab program was used to calculate the velocity differences between pre- and post-grouting tomography data points. However, unlike with the data resulting from the Zion processing, very high agreement observed between the numbers of points and the locations of those points for the Apache Trail tomography. As a result, the velocity differences obtained can be plotted at the actual locations provided by the GSR3D software output, as summarized in Tables 6.3 and 6.4. Final model resolutions of 0.3 m (1 ft) were determined for all sites at Apache Trail, unlike at some of the sites as for the Zion processing.

**Table 6.3. Pre- and post-grouting tomography summary for Apache Trail**

Site	Pre-Grouting Tomography		Post-Grouting Tomography	
	Data Points	Resolution, m (ft)	Data Points	Resolution, m (ft)
1	33572	0.3 (1)	33587	0.3 (1)
2	33972	0.3 (1)	33972	0.3 (1)
3	33844	0.3 (1)	33844	0.3 (1)
4	33202	0.3 (1)	33202	0.3 (1)
5	35273	0.3 (1)	35241	0.3 (1)

**Table 6.4. Difference tomography calculation summary for Apache Trail**

Site	Tolerance ft. (cm)	Minimum Tomography Data Points for Difference Calculation	Resulting Difference Tomography Data Points
1	0 (0)	33572	33571
2	0 (0)	33972	33971
3	0 (0)	33844	33844
4	0 (0)	33202	33201
5	0 (0)	35241	35241

Observations from the resulting difference tomography for the Apache Trail sites, provided in Appendix D, are more consistent than those determined for the Zion difference tomography. A general trend that can be noted relates to the locations of velocity increases compared to

locations of velocity decreases within the tomography. A larger proportion of the velocity increases appear to be found in the central regions of the tomography, compared to the velocity decreases, which appear to be found more along the boundaries of the tomography, where less certainty exists, as discussed further in the next section.

### **6.3. Ray Densities**

Appendix E provides illustrations of the ray densities at each data point, or node, determined by the GSR3D software. Values for the ray densities determined represent the number of raypaths traveling through a given node, following the final velocity iteration step. These images provide some valuable insight into the tomography generated by the software for the case studies considered here. Regions of the tomography model having higher ray densities can be said to have the greater confidence in the seismic velocity determined at those points, as they represent a summation of the individual probabilities that raypaths pass through a given node.

For the ray densities determined at the Apache Trail locations, good agreement between pre- and post-grouting ray densities can be observed, with the exception of Location 4. At this location, a significant region of high ray density occurs in the post-grouting plot but not in the pre-grouting plot. Interestingly, this same region corresponds well with the region of greatest velocity improvement in the difference tomography for Location 4 seen in Appendix D. This may be due to the presence of low-velocity material in this region prior to grouting, around which the seismic wavefront traveled, explaining the lack of raypaths. Following grouting, seismic waves may have been more likely to travel through this region, resulting in increased seismic velocities and ray densities. Potential correlations between increased ray densities and increased seismic velocities are not as apparent for the other locations at Apache Trail.

Another important observation that can be made for all of the Apache Trail locations relates to the correlation between regions found to have no ray density and decreased seismic velocity following grouting. While wavefronts would have been propagated through these regions, updating the seismic velocities at these points would have had little effect on the calculated wavefront arrival times. Therefore, it may be likely that these regions experienced little change in seismic velocity during the iterative process, resulting in final seismic velocities close to those determined for the starting model.

For the Zion locations, some of the unexpected results from the pre-, post-, and difference tomography can potentially be explained by considering plots of the ray densities as shown in Appendix E. For two of the plots, post-grouting 1.10 and post-grouting 1.5.2, nonzero ray densities appear to have been reported for the entire final tomography model, which is not the case for any of the other plots. These abnormalities could have been due to an insufficient number of iterations of the model during processing, as well as the challenges posed by the shallow high-velocity layers present during data collection. For these two sites, the same observation between increased ray densities and increased seismic velocities can be observed as with Apache Trail Location 4, but even more noticeably.

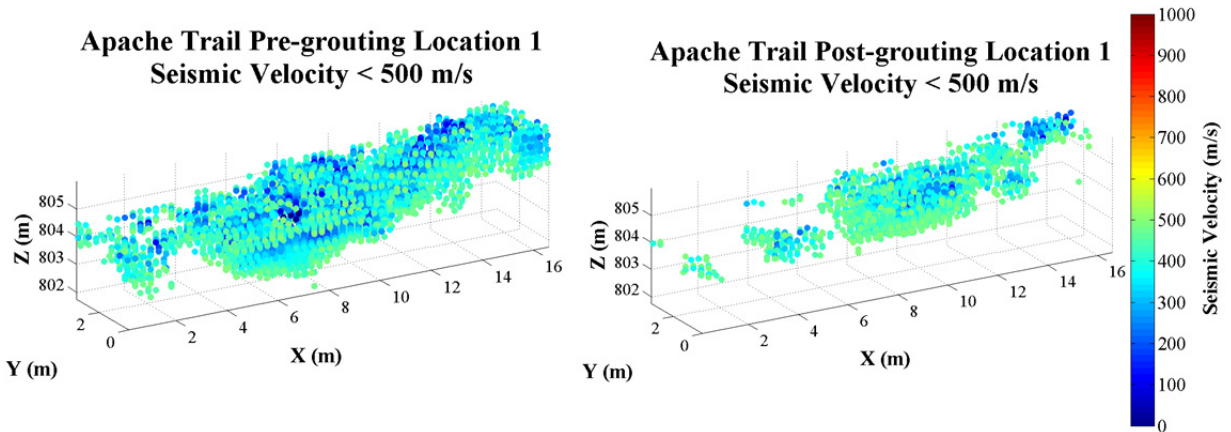
For the remainder of the Zion locations, reasonable agreement between the pre- and post-grouting ray densities can be observed. For these locations, however, the reported ray densities are relatively high and at shallow depths, which correspond to the shallow regions of high-velocity material determined in the pre- and post-grouting tomography and known to have existed in the field.

## **7. DATA ANALYSIS**

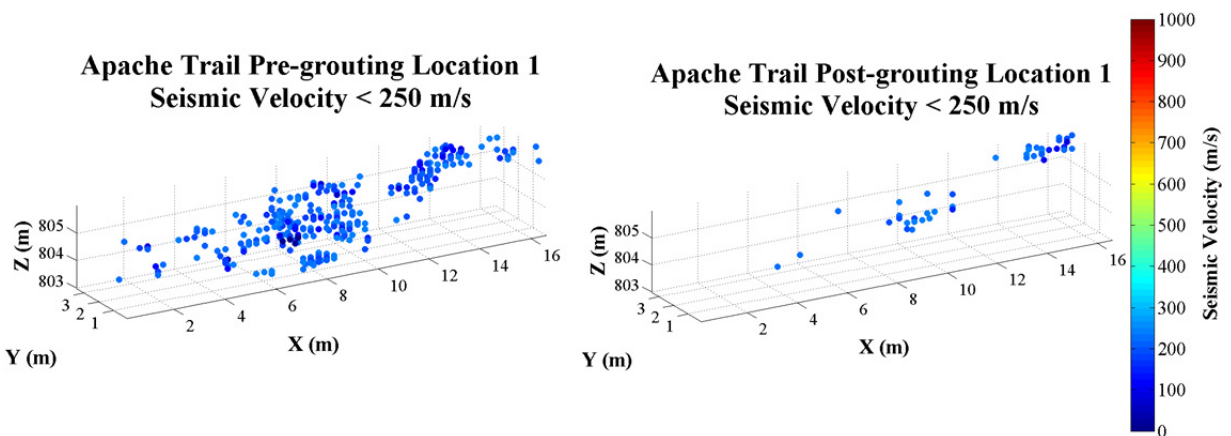
Visualization of 3-D seismic velocity and velocity difference tomography, whether by 2-D slices or by 3-D perspective views, can provide a useful graphical representation of the distribution, both in magnitude and spatially, of areas of concern for grouting and areas showing improvement as a result of grouting. These images alone do not provide engineers or technicians with useful quantitative understanding of these distributions, requiring an investigation into possible methods which could provide this type of information. Several methods are explored to determine their potential usefulness in communicating mathematical and statistical distributions of seismic velocities which make up tomography models like those studied in this investigation.

### **7.1. Improvement of a Target Velocity Range**

One useful method for assessing the effectiveness of grouting operations using pre- and post-grouting tomography is to compare the proportions of the targeted soil mass falling below a velocity of concern both before and after grouting. For Example, Figure 7.1 shows pre- and post-grouting tomography results for Apache Trail Location 1, displaying only those points where the seismic velocity was determined to be less than a threshold value of 500 m/s. From visual observation of these two tomograms, an improvement can be observed due to the decreased number of points falling within the 0 to 500 m/s range. Similar tomography for seismic velocities less than a target velocity of 500 m/s are presented for both the Apache Trail and Zion sites in Appendix C.



**Figure 7.1. Pre- and post-grouting tomography for Apache Trail Location 1, showing data points having seismic velocities less than a targeted velocity of 500 m/s.**



**Figure 7.2. Pre- and post-grouting tomography for Apache Trail Location 1, showing data points having seismic velocities less than a targeted velocity of 250 m/s.**

This concept can be quantified by assessing the percentage of points falling below a target seismic velocity before grouting and comparing the same percentage following grouting. An approach that would allow this degree of improvement to be quantified by the following relationship, where the effectiveness value,  $EV$ , can be described by Equation 7.1 below. Table 7.1 summarizes  $EV$  values for all sites considered as part of this study, showing a considerable

range of values, both positive and negative. Negative values obtained from some sites indicate that more points were present after grouting that fell within the range of 0-500 m/s. This analysis could be repeated for a range of target velocities to investigate possible effects on the values of for different velocity ranges as well as potential trends.

$$EV = \left( \frac{\text{Points below Target Velocity}}{\text{Total Number of Points}} \right)_{Pre} - \left( \frac{\text{Points below Target Velocity}}{\text{Total Number of Points}} \right)_{Post} \quad (7.1)$$

**Table 7.1. Effectiveness values for all sites, with corresponding target velocity range and recorded grout volumes.**

Site	Target Velocity Range, m/s	Pre-grouting (%)	Post-grouting (%)	EV (%)	Total Grout Volume, m <sup>3</sup> (yd <sup>3</sup> )
Zion 1.10	0-500	8.0	1.9	6.0	3.2 (4.2)
Zion 1.5.1	0-500	0.9	13.3	-12.4	1.6 (2.1)
Zion 1.5.2	0-500	3.4	2.2	1.2	1.6 (2.1)
Zion 2.10	0-500	1.8	11.4	-9.6	11.7 (15.3)
Zion 2.5.1	0-500	0.3	1.6	-1.3	5.6 (7.6)
Zion 2.5.2	0-500	0.3	4.5	-4.2	5.6 (7.6)
Apache Trail 1	0-500	8.4	3.7	4.7	18.1 (23.6)
Apache Trail 2	0-500	7.3	4.5	2.7	25.1 (32.8)
Apache Trail 3	0-500	10.7	4.8	5.8	25.8 (33.8)
Apache Trail 4	0-500	4.4	6.4	-1.9	22.2 (29.1)
Apache Trail 5	0-500	7.0	6.7	0.2	7.7 (10.1)

**Table 7.2. Effectiveness values for all sites, with corresponding target velocity range and recorded grout volumes.**

Site	Target Velocity Range, m/s	Pre-grouting (%)	Post-grouting (%)	EV (%)	Total Grout Volume, m <sup>3</sup> (yd <sup>3</sup> )
Zion 1.10	0-250	3.5	1.1	2.4	3.2 (4.2)
Zion 1.5.1	0-250	0.3	0.3	-0.03	1.6 (2.1)
Zion 1.5.2	0-250	3.3	2.2	1.2	1.6 (2.1)
Zion 2.10	0-250	1.0	6.9	-5.9	11.7 (15.3)
Zion 2.5.1	0-250	0.1	1.0	-0.9	5.6 (7.6)
Zion 2.5.2	0-250	0.3	4.5	-4.2	5.6 (7.6)
Apache Trail 1	0-250	0.8	0.1	0.7	18.1 (23.6)
Apache Trail 2	0-250	0.2	0.3	-0.1	25.1 (32.8)
Apache Trail 3	0-250	2.0	0.2	1.8	25.8 (33.8)
Apache Trail 4	0-250	0.3	0.4	-0.1	22.2 (29.1)
Apache Trail 5	0-250	0.2	0.1	0.1	7.7 (10.1)

## 7.2. Seismic Velocity Difference Quantification

In order to provide a more quantitative measure of the degree of improvement resulting from the grouting operations completed at the study sites, several methods were considered. The potential application of any such analysis to a variety of sites, conditions, and tomography models needed to be considered, which lead to the investigation of the most straightforward methods possible that would achieve this goal. For example, due to the complications during the post-grouting seismic data collection at the Zion National Park sites, as mentioned previously, data points resulting from the tomography for the pre- and post-grouting surveys did not align at the same points. This prohibited individual data points from being assessed based on the seismic velocity difference relative to that point. Methods had to be developed which considered the seismic velocity difference relative to some initial measure of the seismic velocity distribution at the site. Equations 7.2 through 7.4 provide relationships that can be used in such situations.

The seismic velocity improvement factor, *SVIF*, can be defined in several different forms. Equations 7.2 through 7.4 describe three possible methods for describing this improvement factor, as follow

$$SVIF_a = \frac{\sum_{j=1}^n (\Delta v_{c,j})}{n} \quad (7.2)$$

where  $\Delta v_{c,j}$  = change in seismic (compression, or p-wave) velocity at each data point

n = number of data points

$$SVIF_b = \frac{\sum_{j=1}^n (\Delta v_{c,j})}{n v_{c,max}^{pre}} \times 100\% \quad (7.3)$$

where  $\Delta v_{c,j}$  = change in seismic (compression, or p-wave) velocity at each data point

$v_{c,max}^{pre}$  = maximum seismic velocity of the pre-grouting model

n = number of data points



$$SVIF_c = \frac{\sum_{j=1}^n (\Delta v_{c,j})}{nv_{c,mean}^{pre}} \times 100\% \quad (7.4)$$

where  $\Delta v_{c,j}$  = change in seismic (compression, or p-wave) velocity at each data point

$v_{c,mean}^{pre}$  = mean seismic velocity of the pre-grouting tomography model

n = number of data points

Assuming that following soil improvement measures, only increases, and no decreases, in compression wave velocity will be observed within a targeted volume, values obtained for the *SVIF* will be greater than zero. Table 7.3 provides a summary of the values obtained for these three forms of the improvement factor relationship for all sites considered as part of this study, along with total grout takes (volumes) recorded within each site.

**Table 7.3. Seismic velocity improvement factors for all sites, along with reported grout volumes injected at each site.**

Site	<i>SVIF<sub>a</sub></i> , m/s	<i>SVIF<sub>b</sub></i> , %	<i>SVIF<sub>c</sub></i> , %	Total Grout Volume, m <sup>3</sup> (yd <sup>3</sup> )
Zion 1.10	454.8	7.7	45.7	3.2 (4.2)
Zion 1.5.1	-9.2	-0.2	-0.8	1.6 (2.1)
Zion 1.5.2	900.7	12.8	64.8	1.6 (2.1)
Zion 2.10	-411.1	-8.4	-33.2	11.7 (15.3)
Zion 2.5.1	-312.2	-11.4	-23.7	5.6 (7.6)
Zion 2.5.2	-424.3	-12.2	-25.8	5.6 (7.6)
Apache Trail 1	30.6	1.3	3.6	18.1 (23.6)
Apache Trail 2	212.1	9.7	26.8	25.1 (32.8)
Apache Trail 3	43.3	1.3	5.2	25.8 (33.8)
Apache Trail 4	-132.2	-2.6	-14.9	22.2 (29.1)
Apache Trail 5	0.8	0.05	0.1	7.7 (10.1)

### 7.2.1. Possible Explanations for Decreased Velocities following Grouting

Several possible explanations can be provided to account for the decreased seismic velocities observed following grouting which are not attributed to the tomography processing methods. Some of these potential reasons include:

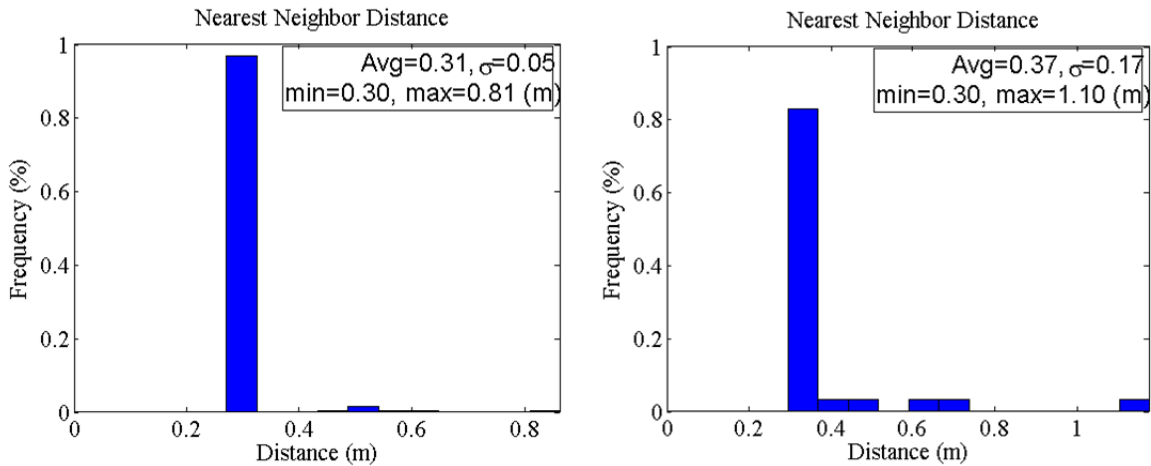
- Vibrations and induced stresses caused by drilling and driving of borehole casings could have potentially disturbed the structure of the soil, including any cementation that might have previously existed within the soil.
- Excavation of thick layers of asphalt (as occurred at Zion sites) and replacement with compacted fill near the surface, could have resulted in replacement with lower velocity (and less dense) material.
- Thick layers of asphalt present near the surface during pre-grouting geophysical data collection (as occurred during Zion data collection) could have had an impact on quality of arrival times determined, although this interaction was unable to be decisively characterized in the analysis, resulting in higher than actual pre-grouting velocities.
- Changes in degree of saturation within the soils between pre- and post-grouting could have resulted in considerable changes in soil properties, especially values of shear modulus  $G$  which is directly related to seismic velocity. Saturation changes could have occurred due to precipitation or watering of the roadway surface which was occurring during construction operations for dust mitigation.
- Based on the fundamental relationships relating seismic p-wave velocity to shear modulus and density, changes in either of the latter two values as a result of grouting can have differing effects on the resulting value of the p-wave velocity for the soil in question. Shear modulus has been shown to be particularly sensitive to applied shear strains, which combined with the possibility of the development of large shear strains during compaction grouting operations, adds additional uncertainty to the final effect of grouting on the p-wave velocity for a soil.

### 7.3. 3-D Spatial Analysis

The primary objective of the grouting carried out for the two case studies considered here was the stabilization of the loosest regions of the roadway subsurface, which correspond to the regions of lowest seismic velocity. One goal of a grouting verification program would be the identification of potentially loose or weak zones that remained following grouting. While the seismic velocity difference quantifications proposed provide an assessment of the average degree of improvement across the entire tomographic volume considered in the analyses, they are unable to account for potential changes in the distributions of these low-velocity regions following grouting.

An alternative approach to assessing the effectiveness of grouting programs by utilizing 3-D tomography information is through three-dimensional spatial analysis methods. Spatial Analysis 3D is a user-friendly, graphical user interface (GUI) integrated with the MatLab environment that allows statistical and visual manipulations of real and simulated three-dimensional spatial point patterns (Eglen et al. 2008; Lofgreen 2011). Analyses included in Spatial Analysis 3D include those derived from the Delaunay tessellation method, including nearest neighbor and Voronoi domain analysis, autocorrelation analysis and its derived density recovery profile, as well as the related K, F, and G-functions. Spatial Analysis 3D was originally developed for the study of neuronal positioning within the central nervous system, but potential future applications in science, engineering, statistics, and mathematics had also been considered. The package was developed out of efforts to quantify the regularity and simulate patterning found in distributions of nerve cells across the retina, due to the dependence of retinal function on uniformity of nerve cell spacing.

Applying the tools available in Spatial Analysis 3D to the data available as part of this study, further quantification of the improvement made through the grouting processes considered can be made. For a set of data points in 2-D, the Delaunay triangulation describes a set of lines connecting each point to its natural neighbors. A single point will have some variable number of natural neighbors, one of them being the shortest (or nearest) neighbor. A Delaunay tessellation is made up by a set of tetrahedral defined by the population of natural neighbors in the 3-D case. The population of nearest neighbor distances thus becomes a useful means to describe the spatial relationship between elements in either a 2-D or 3-D population. Figure 7.3 shows nearest neighbor distance histograms for pre- and post-grouting tomograms having seismic velocities less than 250 m/s, where increases in the average, standard deviation, and maximum distances between points having seismic velocities less than 250 m/s are observed following grouting. These increases can be thought of as greater separations between the loosest or weakest areas of the subsurface following grouting.



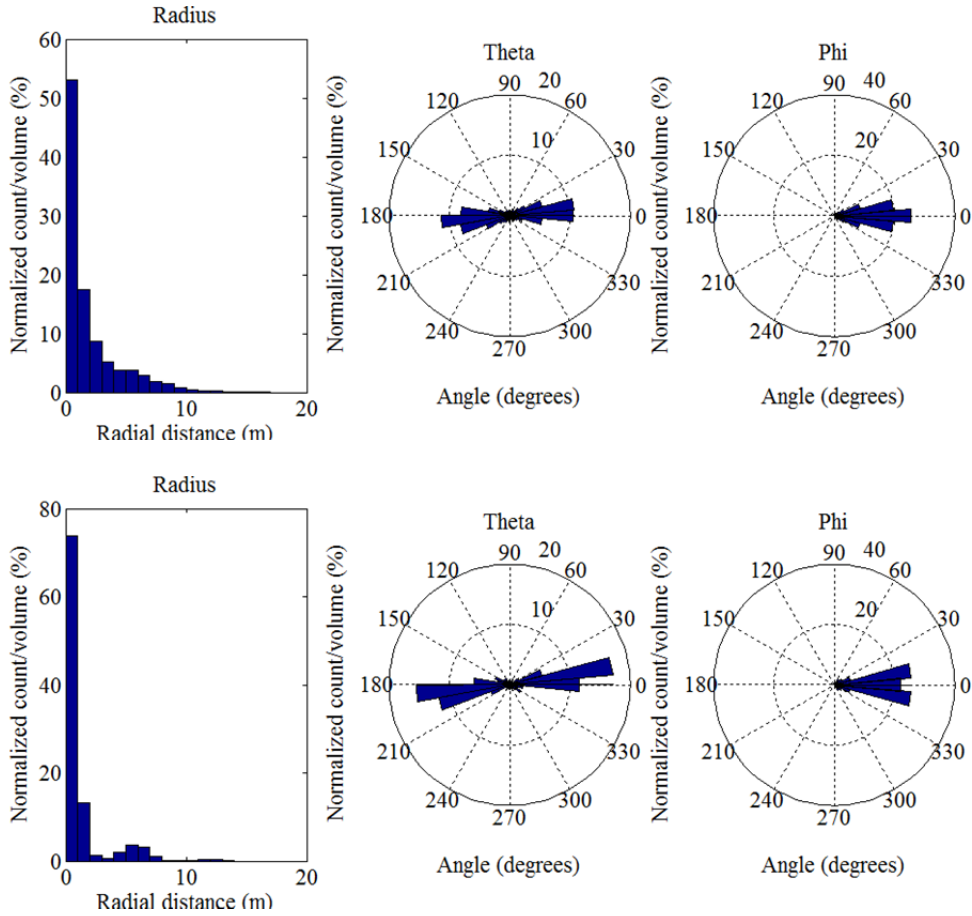
**Figure 7.3. Nearest neighbor distance plots for Apache Trail Location 1 pre-grouting (left) and post-grouting (right) for seismic velocities less than 250 m/s.**

The autocorrelation analysis provides a more robust three-dimensional representation of the spatial distribution of the points in data sets being considered. During the Autocorrelation

calculation, each point is moved to the origin (0,0,0) and all other points are re-plotted with respect to this calculation. The tri-histogram plots shown in Figure 7.4 are one way to communicate the results of an autocorrelation analysis. The leftmost histogram, known as a density recovery plot (DRP), provides a normalized count of radial distances between points per unit volume considered. The *Spatial Analysis 3D User's Guide* provides a further description of the tri-histogram plot:

When looking at the DRP, we are only concerned with the distance these points are from the origin, i.e. radius. There are two additional directions, however, that define the position of the points in such a plot relative to the origin, being azimuthal angle, theta, and elevation angle, phi. Together these three directions, radius, theta, and phi, make up the familiar spherical coordinate system.

For a randomly-spaced set of data, the density recovery plot would consist of bars of constant height for increasing distances from the point of interest. From the results of the autocorrelation analysis performed at Apache Trail Location 1 for seismic velocities less than 250 m/s, as shown in Figure 7.4, increased normalized densities of points can be observed following grouting, with little variation in the angles theta and phi. For this location, the results of both the nearest neighbor distance and autocorrelation analyses can be described as a tighter packing of the regions of lowest seismic velocity, and an increased spacing between those regions, following grouting at the location considered.



**Figure 7.4. Tri-histogram plots for Apache Trail Location 1 pre-grouting (upper) and post-grouting (lower) for seismic velocities less than 250 m/s, showing a closer packing of points following grouting.**

Tables 7.5 and 7.6 provide a summary of percent changes in values resulting from the nearest neighbor and autocorrelation analyses for both Apache Trail and Zion N.P. sites, with percent change defined by the following relationship:

$$\% \text{ Change} = \frac{(\text{Post-grouting value}) - (\text{Pre-grouting value})}{(\text{Pre-grouting value})} \times 100\% \quad (7.5)$$

Values for the nearest neighbor distance and autocorrelation analysis at each of the sites studied are presented in Tables 7.4 and 7.5. From these values, inconsistencies in calculated percent changes are observed for the nearest neighbor distance analysis at the five locations considered at Apache Trail. Better agreement can be observed from the autocorrelation analyses,

where consistent increases were found in point density due to grouting. Therefore, it can be said that for the regions of lowest seismic velocity at these sites, tighter packing of the points, corresponding to the increased densities and therefore smaller region sizes, were found after grouting, but the distances separating these regions of low velocity experienced inconsistent changes. This discrepancy may be due to the paths followed by the injected grout during the void-fill grouting operations. If a higher percentage of the injected grout migrated through an opening or channel within the embankment, the result could potentially be a decrease in the size of the low-velocity region, without a corresponding decrease in the spacing between regions. For an ideal application of compaction grouting, increases in both nearest neighbor distances and autocorrelation analysis parameters would be expected, based on a uniform treatment of the soil volume.

**Table 7.4. Summary of Spatial Analysis 3D nearest neighbor distance analyses for Apache Trail sites, with values shown for percent change from pre- to post-grouting for each parameter, for data sets having seismic velocities less than 250 m/s.**

Site	Nearest Neighbor Distance Analysis (250 m/s Target Velocity), % Change			
	Average (m)	$\sigma$ (m)	Minimum (m)	Maximum (m)
Apache Trail 1	19.4	240.0	0.0	35.8
Apache Trail 2	-14.9	-48.9	0.0	-39.2
Apache Trail 3	38.7	650.0	0.0	137.2
Apache Trail 4	-10.3	11.1	0.0	61.5
Apache Trail 5	0.0	-37.1	0.0	-52.4

**Table 7.5. Summary of Spatial Analysis 3D autocorrelation analyses for Apache Trail sites, with values shown for percent change from pre- to post-grouting for each parameter, for data sets having seismic velocities less than 250 m/s.**

Site	Autocorrelation Analysis (250 m/s Target Velocity), % Change			
	Density (m <sup>-3</sup> )	Critical Density (m <sup>-3</sup> )	Maximum Radius (m)	Reliability Factor
Apache Trail 1	0.075	0.209	1236	36.0
Apache Trail 2	0.174	0.209	933	83.2
Apache Trail 3	0.136	0.209	1013	65.0
Apache Trail 4	0.303	0.231	776	131.0
Apache Trail 5	0.130	0.275	1030	47.0

#### 7.4. Comparison with 2-D Seismic Refraction Results

As part of the previous geotechnical condition survey performed by AMEC Earth and Environmental, Inc. (AMEC 2007), several conventional 2-D seismic refraction surveys were performed in the vicinity of the walls studied as part of this research. The purpose of these seismic refraction surveys was to evaluate the condition of the three walls identified for rehabilitation in the Fish Creek Hill vicinity of Apache Trail, to help evaluate subsurface backfill and foundation conditions. Both 5- and 10-ft (1.5- and 5-m) in-line geophone spacings were used during the seismic refraction data collection, some at the same locations. Four of these lines, as shown in Table 7.6, corresponded with the wall locations selected for 3-D seismic tomography as part of this research.

**Table 7.6. Summary for previous 2-D and new 3-D seismic surveys.**

Wall Number	Corresponding 3-D Site	Line Number
Wall 3	Apache Trail 1	L-9
Wall 3	Apache Trail 3	L-8
Wall 3	Apache Trail 4	L-10
Wall 1	Apache Trail 5	L-4



All surveys referenced in Table 7.6 utilized similar equipment and data collection procedures as those used in this study. Twelve geophones were used in a single 18.3 m (60 ft) long seismic line, with shots placed every 1.5 m (5 ft) between adjacent geophones. The commercially-available software SeisOpt2D was used to process the seismic refraction data. Refraction microtremor (ReMi) data was also collected along these lines, allowing for the inclusion of a shear wave velocity profile with the compression wave velocity results obtained through the 2-D seismic refraction analysis. Further details relating to the surveys performed previously can be found in AMEC (2007).

The resulting distribution of p-wave velocities from the 2-D seismic refraction analysis can be compared to a slice of the 3-D seismic pre-grouting tomography results at the same location to consider potential similarities or differences. Figures 7.5 and 7.6 provide a comparison between the results of these two survey methods for Location 5 at Apache Trail, and Figures 7.7 and 7.8 provide the same comparison for Location 3. Similar trends in the distribution of p-wave velocities can be observed in the 2-D and 3-D tomography models. Several advantages and disadvantages can be extracted from the presentation of the different methods as well. For the case of the 3-D tomography resulting from the GSR3D program, the higher resolution can allow for detection of anomalies such as high or low velocity regions within the soil volume as well as sloping ground surfaces. The output recovered from the SeisOpt2D analysis has the advantages of smaller numbers of velocity values to consider, as well as determination of the approximate depth of investigation resulting from the velocity inversion. For the GSR3D results, interpretation of the likely depth of reliable information is left to the user, which could potentially have unintended results in applications.

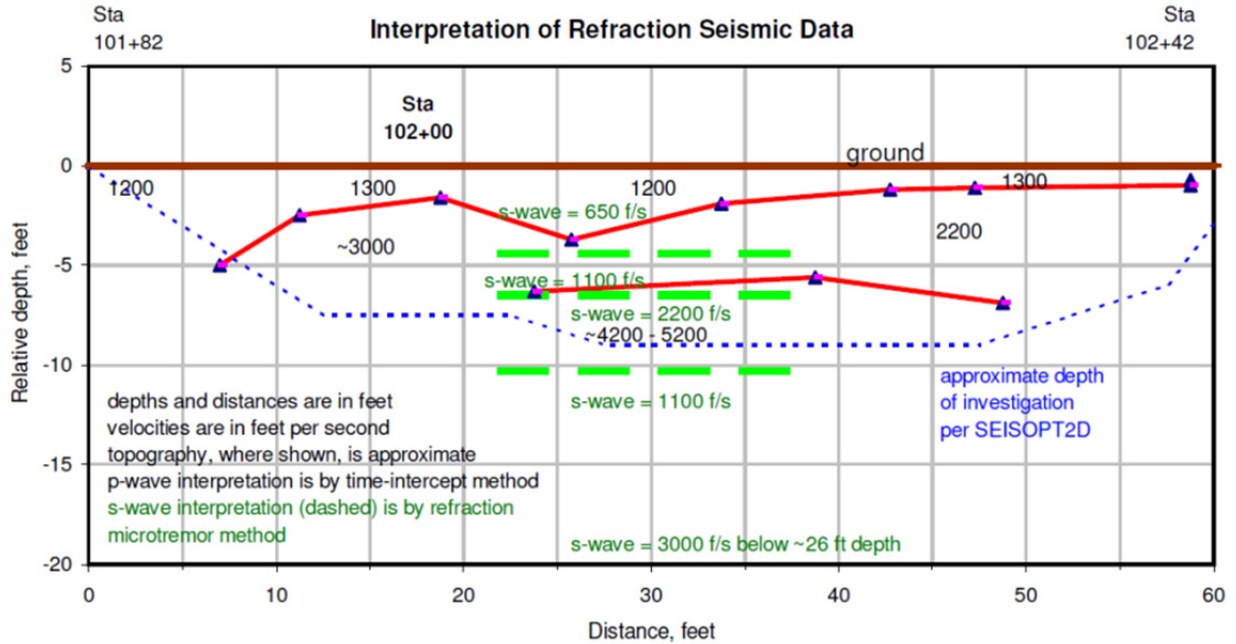


Figure 7.5. Results from 2-D seismic refraction analysis for Line 4 at Apache Trail, as performed previously by AMEC (2007) using SeisOpt2D, which corresponds to Location 5 of the 3-D tomography study performed here.

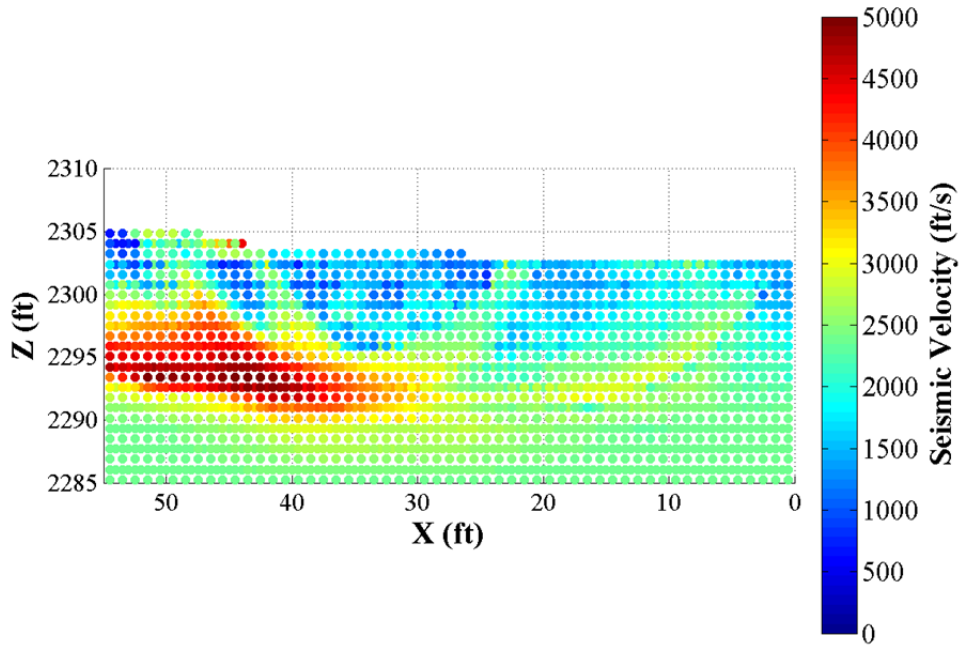


Figure 7.6. 2-D slice of 3-D seismic tomography results from Apache Trail Location 5, shown in the same orientation as the results from the 2-D refraction survey. Slice shown for values of  $-1 \text{ ft} < y < 1 \text{ ft}$  ( $-0.3 \text{ m} < y < 0.3 \text{ m}$ ).

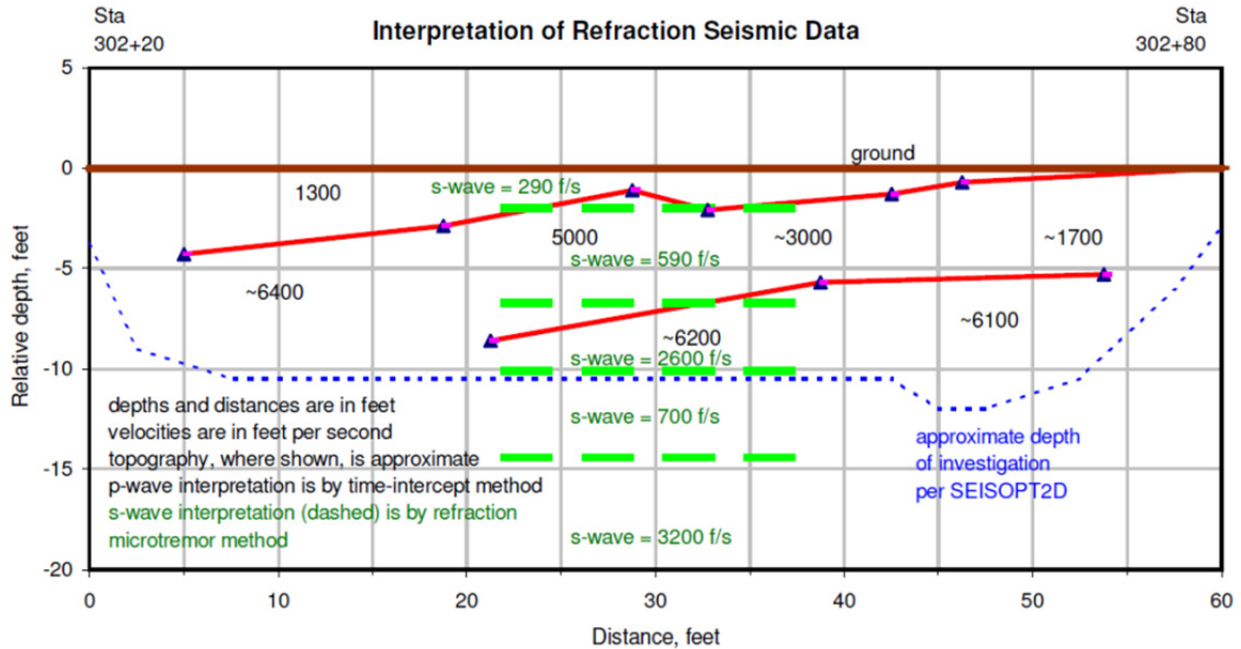


Figure 7.7. Results from 2-D seismic refraction analysis for Line 8 at Apache Trail, as performed previously by AMEC (2007) using SeisOpt2D, which corresponds to Location 3 of the 3-D tomography study performed here.

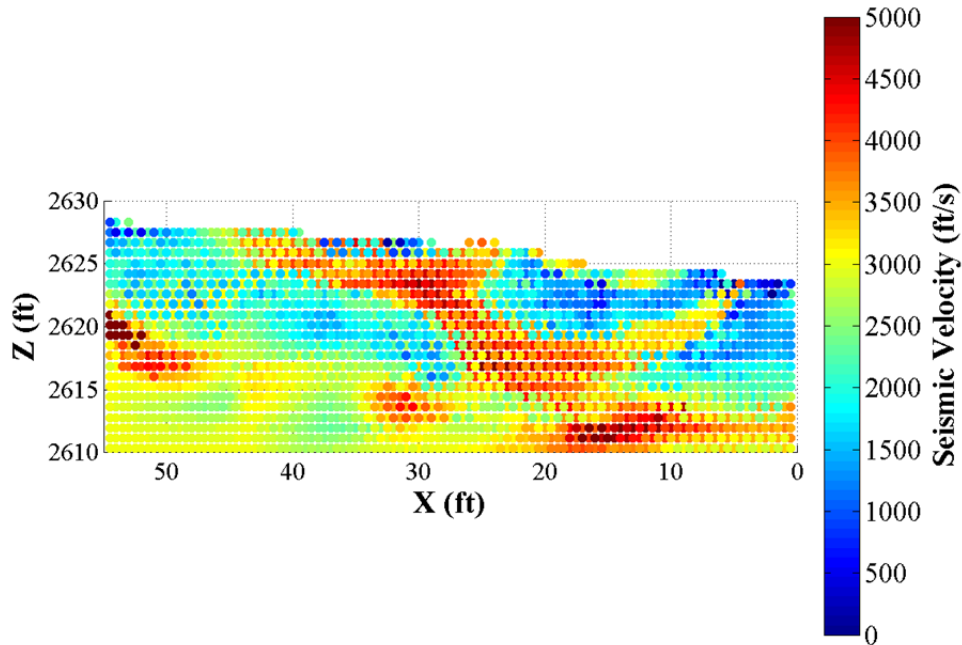


Figure 7.8. 2-D slice of 3-D seismic tomography results from Apache Trail Location 3, shown in the same orientation as the results from the 2-D refraction survey. A slice is shown for values of  $0 < y < 1.5$  ft ( $0 < y < 0.5$  m).

## **7.5. Comparison with Consultant Findings at Zion National Park**

As described in Chapter 4, Zonge International, Inc. was contracted to provide 3-D seismic data collection services for the work performed at Zion National Park. In addition to data collection, Zonge was contracted to provide the raw seismic data collected, and the results of a 3-D seismic tomography analysis for each of the sites studied. The details of their findings are provided by Zonge Project Report #10122 (Zonge 2011). This report summarized that while seismic data obtained was of good quality, first arrivals were obscured by the near-surface high-velocity layers present during both the pre- and post-grouting geophysical surveys. Two separate 3-D seismic tomography processing software packages were investigated to process the data for this report, however, unexpected velocity decreases following grouting were observed using both processing methods.

Manual picking of each of the nearly 40,000 raypath arrival times was completed by the Contractor, with unsatisfactory signal traces discarded. GSR3D was the first program used for the seismic tomography processing, which was also the software used for the separate processing performed for this investigation. However, the Consultant chose to rely on the manual arrival time picks compiled for the collected data and manually enter those picks into the GSR3D software for the analysis, as opposed to the procedure followed for this investigation as described in Chapter 6. The second program investigated, GeoTomCG, is an alternative 3-D seismic tomographic inversion program designed for civil engineering applications. The manual picks chosen by Zonge International, Inc. were again used in the processing of the pre-grouting, post-grouting, and resulting difference tomography. After consideration of the processed 3-D seismic tomography obtained using both of these software packages, the Contractor also found unexpected decreases in seismic velocities throughout a majority of the tomography models

following grouting operations. The Contractor noted that their determination of first arrival times for the collected data was significantly impacted by the interference of “pavement breaks,” which were due to the direct arrivals of the imparted seismic wave traveling through the high-velocity pavement layer at the ground surface. Observations included that the pavement breaks detected within the seismic data were sometimes of higher frequency and sometimes in an opposite direction as the direction of first movement. As a result, in some cases the pavement break magnified the first arrival of the refracted wave and in other cases obscured the arrival, leading to difficulties in obtaining the most accurate possible arrival times to be used in the 3-D seismic processing, and likely contributing to the unexpected results obtained from their investigation.

## **8. RECOMMENDATIONS**

Based on the experience gathered through this study, some general guidelines can be suggested for future investigations employing 3-D seismic tomography surveys for pre- and post-grouting of roadway applications. One of the most critical recommendations that can be made would be to ensure to the highest degree of accuracy possible that locations of geophones and shots are the same for both pre- and post-grouting seismic data collection. Modern surveying instruments can be helpful in minimizing potential placement errors, especially in verifying the locations during post-grouting data collection. Due to potential site changes during construction, either related or not to grouting activities, benchmarks should be located a sufficient distance away from the survey site, or in a location determined to be safe from potential disturbance during construction activities. Adequate flagging and marking of benchmarks used for these purposes may avoid disturbance as well.

Based on the observations made for the pre-, post-, and difference tomography for the case studies considered here, a possible suggestion can be made to improve the difference tomography for investigations concerned with changes in seismic velocities before and after ground improvement. Choosing the same initial, or starting, velocity for the model for the generation of both the pre- and post-grouting tomography constructions could potentially reduce errors in velocity differences and result in a more accurate determination of seismic velocity difference tomography. For the software used in this study, the initial velocities are determined based on an averaging procedure between observed travel times and distances between shots and receivers, which could result in differences in the initial model velocities between pre- and post-grouting investigations. If these velocities are not updated in during the iterative procedure,

seismic velocity differences would be observed. This situation would be of greatest concern in the regions of the tomography having the lowest ray densities, as mentioned previously.

An important question deserving of investigation is whether 2-D seismic methods can be utilized more efficiently than 3-D methods, and whether significant cost differences exist between the two. From the observations made during this study, 3-D seismic tomography methods would be recommended for nearly all cases where 2-D methods may be considered. Cost differences will likely only result from increased data collection requirements for 3-D. For example, traditional 2-D seismic refraction typically employs 12 geophones, 1 seismograph, and from anywhere from 5 to 15 or more shot locations per line. Compared to the 48 geophones, 2 seismographs, and 45 to 69 shot locations per grid used in this study, a greater investment in time and equipment can be observed for the 3-D seismic tomography method as used here. However, 3-D methods can be utilized using smaller quantities and densities of data. Software has been available for the processing of 2-D data for many years, and has experienced many improvements and decreases in cost over that time. While currently, costs associated with 3-D seismic tomography processing may be higher than those associated with 2-D processing, this cost gap may close between the two approaches as additional programs and versions become available.

**Table 8.1. Considerations for and potential limitations to performing 3-D seismic tomography for grouting verification of roadway applications.**

<b>Site Conditions</b>	Saturated soil limitations Pavement thickness (can be variable across a site) Depth to bedrock Adjacent structures, especially historic or sensitive
<b>Environmental</b>	Background noise due to weather (wind), construction or public traffic Impact of noise and vibrations generated during data collection on environment
<b>Access</b>	Maintenance of traffic during data collection Changing site layout, including roadway elevation, due to construction operations
<b>Documentation</b>	Photographs and detailed notes describing shot and receiver locations should be used extensively in addition to surveying
<b>Data Processing</b>	Method of first arrival picks (consistency)
<b>Labor and Equipment</b>	Attempt to use same technicians, engineers, and equipment for pre- and post-grouting seismic investigations

### **8.1. Changes to Design of 3-D Seismic Tomography Grouting Verification Programs**

General guidelines for layout of 3D seismic refraction grids can be proposed based on the experiences gathered during this study. Maintaining straight and parallel lines for all seismic line layouts, regardless of grout injection points or roadway alignment, is highly suggested not only to ease equipment layout but also avoid unnecessary confusion or mistakes made during the data processing stage. While sloping ground surfaces do not create any particular challenges to the 3-D seismic processing methods explored here, maintaining geophone and shot locations in a relatively planar orientation may provide for the most simplified data collection possible, especially at sites with difficult terrain. The benefits obtained from the use of “downslope” shots, those shots collected at the base of the retaining walls like those found at the study sites considered here, may not outweigh the added time, cost, and safety risks associated with their collection. While 3-D seismic tomography processing software such as GSR3D is capable of considering geophone and shot locations at different elevations, maintaining consistency and



simplicity in geophone and shot layouts, with consideration of site specific conditions, is recommended for future investigations.

## **8.2. Cost Comparison between Sites**

Costs for verification of grouting operations based on the methods utilized here will vary widely. Consideration should be given to the most sensitive or critical locations, where grouting operations may be of greatest concern, to select the locations where these verification techniques should be performed. From the experiences gained through this study, costs should not vary considerably for different geophone spacings used, as long as the capacity of the equipment selected (seismic takeout line geophone interval, for example) is not exceeded. For larger geophone spacings, additional time will be required between shot collections due to the larger distances between shots, and accompanying travel between locations, which could potentially be offset by including fewer shots in the survey at the expense of decreased raypath densities.

Significant savings can potentially be realized by using 3-D seismic tomography methods as opposed to conventional methods such as CPT or SPT when the locations being considered for verification are remote or difficult to access. In these cases, mobilization costs for the large or specialized drilling and sampling equipment required for these conventional methods may significantly outweigh those for a seismic investigation.

## **8.3. Effect of Different Geophone Spacings**

One goal of the investigation at the Zion National Park sites was to assess the influence of in-line geophone spacing on the effectiveness of the verification methods used as part of this study. Both 5- and 10-ft (1.5- and 3-m) in-line geophone spacings were used to investigate possible benefits of using smaller geophone spacings to conduct shallow 3-D seismic surveys. Due to the unexpected difficulties encountered at the Zion sites, providing any conclusive

recommendations relating to this question proved more difficult than anticipated. The large regions of decreased velocities observed for many of the Zion tomography models, and the resulting uncertainties associated with those decreases, raised concerns about attempting to provide any definite conclusions as to the influence of geophone spacing on the quality of the results.

Considering that for the sites studied, as nearly identical numbers of geophones and shots were employed, for smaller geophone spacings, higher raypath densities could be expected within the soil volume. This would provide increased resolution and confidence in the final tomography model, as long as confidence in signal and first arrival time quality was certain. Alternatively, the effective depth of a seismic investigation can be said to increase as the largest dimension of the geophone spread increases. Therefore, for any project considering the use of either 2-D or 3-D seismic methods for verification of grouting in the future, tradeoffs will have to be made between the number of geophones and shots used, and the resolutions and depths of the tomography desired.

From the results of this study, some observations can be made between the smaller 5-ft (1.5-m) and larger 10-ft (3-m) in-line geophone spacings used at the Zion locations, with consideration given to some of the unexpected results obtained. A possible advantage of the larger spacings, increased effective depth of investigation, was not observed, as similar depths of reported ray densities can be noted between the different spacings. The depths of the reported ray densities at the Zion locations also corresponds closely with the known shallow depths to bedrock at the site, which will to a large extent limit the effective depth of a seismic investigation. For sites with much deeper soil profiles, some advantage may be obtained by utilizing larger geophone spacings, allowing for longer overall geophone line spreads.

Differences in resolutions between the two spacings were found at one of the grids but not at the other. For grid #1, the larger spacing was found to have a 2-ft (0.6-m) resolution while the smaller spacing resulted in finer 1-ft (0.3-m) resolutions. For grid #2, no difference in resolution was determined for the different spacings, with 2-ft (0.6-m) resolutions determined for both spacings. Further investigation of the potential benefits of alternative geophone spacings for use in these types of shallow 3-D seismic applications is warranted, with the hopes of understanding with more certainty the most efficient geophone spacings and layout to be used for future investigations of this type.

#### **8.4. Improvements to Quality Assurance and Quality Control Programs**

Potential modifications can be made to contracting procedures and plans and specifications relating to 3-D seismic tomography verification of grouting operations to produce the highest quality product for the owner as the result of grouting and verification. Real-time monitoring of injection parameters can be required to be submitted, at a reasonable expense to the contractor performing the work, who may already possess the necessary equipment to collect this data. Better involvement of project managers and geotechnical engineers during compaction grouting operations can ensure that any changes made to the grouting plan during the course of the work are consistent with the overall intention of the grouting program. Prequalification of geophysical contractors can be used in the verification process to ensure the collection of high quality seismic data, consistency in field procedures followed, and reliable tomography processing and presentation. Performance-based payments, in lieu of quantity-based payment structures are also a potential option to be considered in this respect.

Changes to performance-based specifications can be considered for 3-D seismic tomography applications, where one potential method could consider load ratios and pay factors based on

quantitative relationships between pre- and post-grouting tomography, such as the volumetric improvement factors proposed here. The load ratio can be defined as the actual value determined for a particular material property, such as asphalt strength or seismic velocity increase, divided by the desired value of that property following the completion of work. The load ratio can also be substituted by a range of desired material properties resulting from the work performed corresponding to the associated pay factors. Table 8.2 shows one possible structure to such a system, which could be used to adjust payments for work performed based on the results of 3-D seismic tomographic analysis of the site, and can be weighted for different circumstances. Such a system would provide grouting contractors financial incentive to create the greatest amount of improvement possible.

**Table 8.2. Pay scale for potential inclusion into performance-based specifications for grouting work.**

<b>Seismic Volumetric Improvement Factor (SVIF<sub>a</sub>), m/s</b>	<b>Pay Factor</b>
SVIF < -100	0.90
-100 < SVIF < -50	0.95
-50 < SVIF < 50	1.00
50 < SVIF < 100	1.10
SVIF > 100	1.20

As a way to assist engineers in determining whether 3-D seismic tomography-based verification methods should be considered for a given project, a basic framework can be proposed to aid in scoring the sensitivity and potential risks of the project. Such a framework is provided in Tables 8.3 and 8.4. This system can potentially be utilized as a starting point for determining applicable verification methods for different grouting projects, and can easily be modified to consider different scoring criteria or weighing in the scoring process.

**Table 8.3. Scoring rubric framework for grouting programs.**

	Criteria	(1)	(2)	(3)	Points
1	Traffic volume	ADT < X	X < ADT < XX	XX < ADT	
2	Risk to public	Low	Medium	High	
3	Risk to critical lifeline infrastructure	Low	Medium	High	
4	Prequalified compaction grouting contractor	Yes	Yes	No	
5	Historical significance of adjacent structures	Low	Medium	High	
6	Cost of compaction grouting to removal and replacement of soil	Low	Medium	High	
<b>Total Score</b>					

**Table 8.4. Verification method hierarchy for grouting programs.**

		Score	< 3	3-6	7-10	11-14	15-18	>18
<b>Potentially Applicable Verification Method</b>	Manual injection parameter logging		•	•	•	•	•	•
	Ground heave criteria		•	•	•	•	•	•
	Grouting intensity number (GIN)		•	•	•	•	•	•
	Geotechnical field testing (CPT, SPT)					•	•	•
	Test injections with excavation					•	•	•
	Continuous injection parameter monitoring					•	•	•
	3-D seismic tomography					•	•	•

### 8.5. Use of Pre-Grouting Tomography for Design of Grouting Plans

Pre-grouting tomography can potentially be utilized by geotechnical engineers during the grouting design. From the pre-grouting tomography, areas having the lowest seismic velocities can be identified, and grouting operations can be concentrated in the areas most needing improvement. Additionally, areas showing the highest seismic velocities can be avoided in some cases, to prevent these areas from being discovered in the field during grouting and expending

unnecessary time and resources. In situations where bedrock is much shallower than grouting would allow, drilling and driving of casing for unnecessary injection holes can be avoided, reducing costs and maximizing the grouting effectiveness. This method can be achieved as long as the turn-around time required for processing the pre-grouting tomography is relatively quick. Generally, as long as sufficient flexibility is provided in the contracts and specification for the grouting work, the locations of injection holes can be modified prior to the commencement of work, especially if sufficient information is made available in time to warrant modification. This process would, however, require the pre-grouting and post-grouting tomography to be processed and analyzed separately.

## **8.6. Future Work**

One potential question that has arisen as a result of the work performed for this investigation is whether 3-D seismic refraction techniques can be applied to other ground improvement methods such as dynamic or vibro-compaction, or other underground construction operations, as a way to reliably verify effectiveness. While the answers to these questions exist outside the scope of this study, many potentially useful extensions of the technology and data analysis methods explored here can be made in additional areas of ground improvement.

A variety of technologies currently exist for developing 3-D seismic tomography using subsurface sources or receivers (downhole and crosshole seismic). Many of the challenges characteristic to surface-based 3-D tomography methods employed in this study, such as those related to surface layer interference during data collection, are not found in the subsurface-based methods, which often produce higher-quality data due to the decreased influence of environmental factors. Instead of relying upon arrival times to be recovered from refracted waves, down-hole and cross-hole methods can utilize the propagation of direct compression

waves to characterize the spatial variation in wave velocities in three dimensions. The methods explored here for the analysis of pre- and post-grouting data analysis are applicable to any 3-D seismic tomography results regardless of the data collection and processing methods used to develop that tomography.

One potential area for development of future grouting verification technology relates to real-time monitoring. Several challenges must be overcome before real-time 3-D seismic tomography techniques can be practically applied to compaction grouting programs. Many ground improvement methods attempt to achieve densification, or rearrangement, of soil particles, which generally requires energy to be transferred into the soil. This process, whether through vibro- methods, injection of grout, or otherwise, introduces energy into the ground mass, which can influence the seismic wave data collection process. Conflicting noise can result not only from the direct application of the ground improvement, as in dynamic compaction for example, but also from the energy imparted by supporting activities such as equipment or worker movement, which would exist during any real-time seismic data collection efforts.

Further study can also be made into the qualitative methods that can be used to assess the volumetric improvements due to grouting activities, potentially employing more advanced statistical methods than those utilized here. Recommendation is also given to any future work to attempt to secure pre- and post-grouting geotechnical field testing data, such as CPT or SPT, to correlate with the results of the 3-D seismic tomography. Another potentially useful investigation could combine the methods employed here with physical verification methods such as test injection and excavation sites. This would allow the results obtained from the post-grouting tomography to be compared with the actual locations and distributions of injected grout in the ground. Forward modeling techniques can also be employed to include known

velocities into the starting model for specific regions at the start of tomography generation. The velocities and locations for these regions can be obtained through a variety of methods including drilling and sampling during an SPT investigation, correlation with CPT results, or known locations of structures such as retaining walls, foundations, or utilities. While the retaining walls adjacent to the sites considered in this study were not likely to have had an influence on the resulting tomography due to their location outside of the tomographic volume, in some cases, the presence of such structures within the model boundaries would have a considerable influence on the results, which could be considered through the use of forward modeling.

Lastly, based on the observations made during this study, potential relationships between changes in ray densities and changes in velocities before and after grouting could be better understood through further investigation. A useful starting point for such an assessment could involve a redetermination of the tomography for the sites considered here, based on identical initial velocity models for pre- and post-grouting cases. Maintaining a constant initial velocity for the tomography may have significant influence on determined velocity differences, especially velocity decreases, and could potentially increase the overall confidence in the difference tomography through a better knowledge of the relationship between ray densities, initial velocities, and velocity differences.



## 9. CONCLUSION

Successful use of 3-D seismic tomography for assessment of grouting programs for roadway applications does not come without some considerable practical challenges. Potential roadway applications should thoroughly investigate asphalt depths and reconsider seismic use if these depths are significant. Limitations inherent to traditional 2-D seismic refraction, including those related to saturated soils, must also be considered for these investigations. However, the three-dimensional wave propagation method used has been shown to have considerable advantages compared to traditional 2-D seismic refraction analysis, especially for characterization of volumetric improvement resulting from grouting operations. Large amounts of information can be retrieved relatively quickly and processed efficiently when data quality is good, allowing for subsurface characterization in ways that are unachievable by conventional point-based, intrusive testing methods. As for any other tool available to engineers, considerable emphasis should be given to the adequate use of engineering judgment during the interpretation of any results obtained. Familiarity with not only grouting operations and soils and site conditions, but also geophysical and seismic data collection and tomographic processing procedures, are essential prerequisites for successful interpretation of results such as those presented here.

Grouting programs that follow traditional compaction grouting procedures involving the high-pressure injection of grout have shown more promise for this method due to the volumetric improvement created within the soil mass as well as the grout volumes created during the ground improvement process, but confirming this potential through this study proved challenging due to unexpected condition encountered in the field. Where grouting is used to fill voids alone or permeate locally through loose soil, the ability of this 3-D seismic tomography to communicate

the resulting improvement has been shown to be limited, as dimensions of voids filled with grout may be less than the resolution of the tomography. The greatest potential for 3-D seismic tomography lies in complementing traditional quality assurance testing to allow for a more complete understanding of the degree of improvement resulting from grouting, which may be feasible for only the most sensitive or high-risk projects.

The fundamental basis of 3-D seismic tomography technology has been proven through a variety of case studies and conditions to be a viable and useful extension of geophysical methods to civil engineering applications. Significant interest has been noted throughout this study by researchers, contractors, and designers in further developing 3-D tomographic methods for innovative uses. At one time, the rate at which such technologies could advance was largely limited by available computing power and electronic equipment. Today, however, many of those restrictions have been removed through the rapid advancement of computer technologies, abilities, and ease of use. Further advancement of these methods will therefore rely largely on the creativity of geophysicists and engineers, together with the support and encouragement of upper-level management, toward achieving further advancements in understanding and development of this field.

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**APPENDIX A - LOCATION MAPS AND PLAN DRAWINGS**





Figure A.1. Location map of Zion National Park project site.



Figure A.2. Location map of Apache Trail project site.

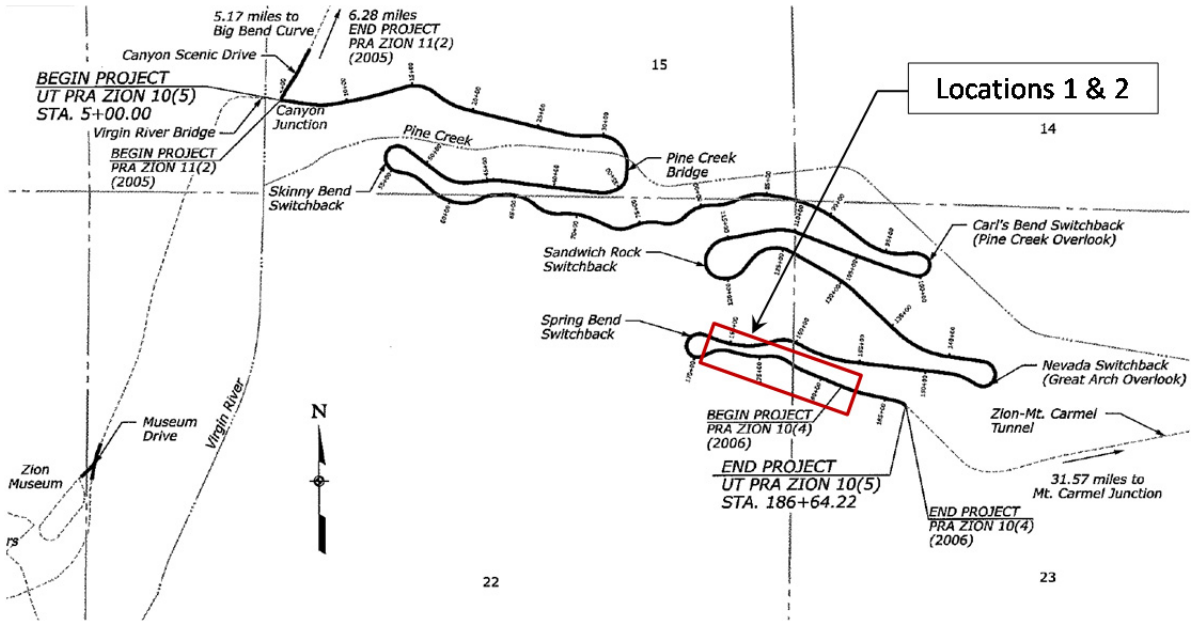


Figure A.3. Plan drawing detail of Zion National Park project site.

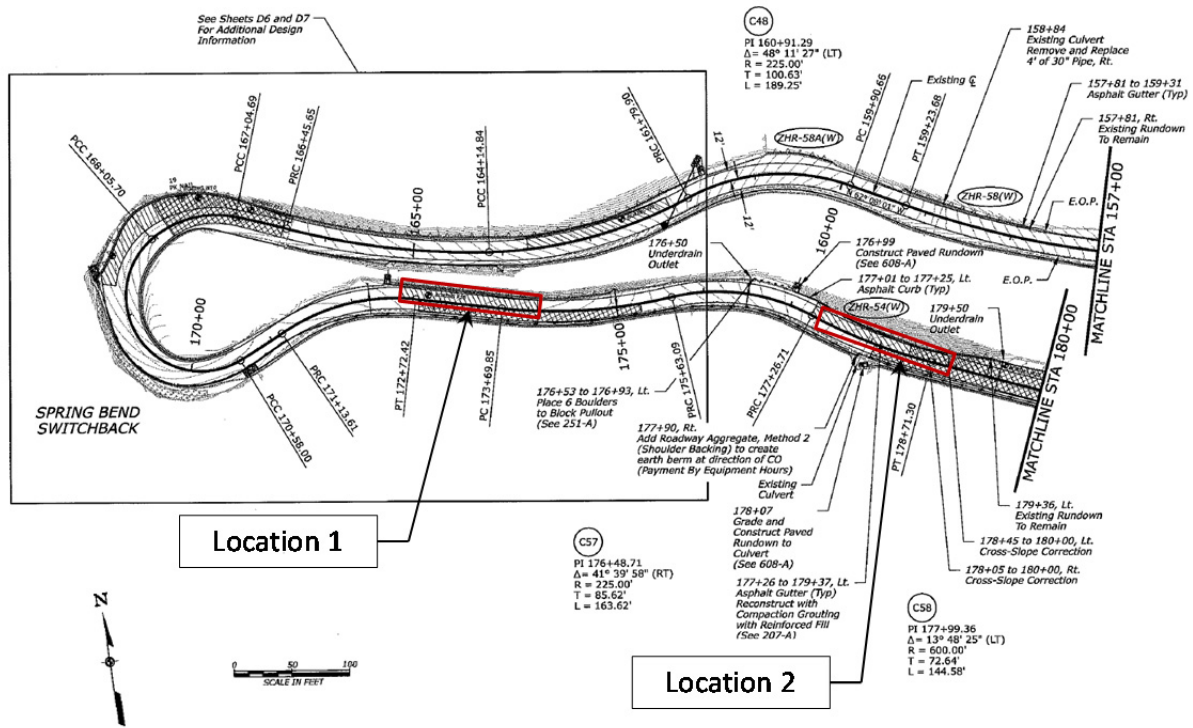


Figure A.4. Plan drawing detail of Zion National Park Locations 1 and 2.

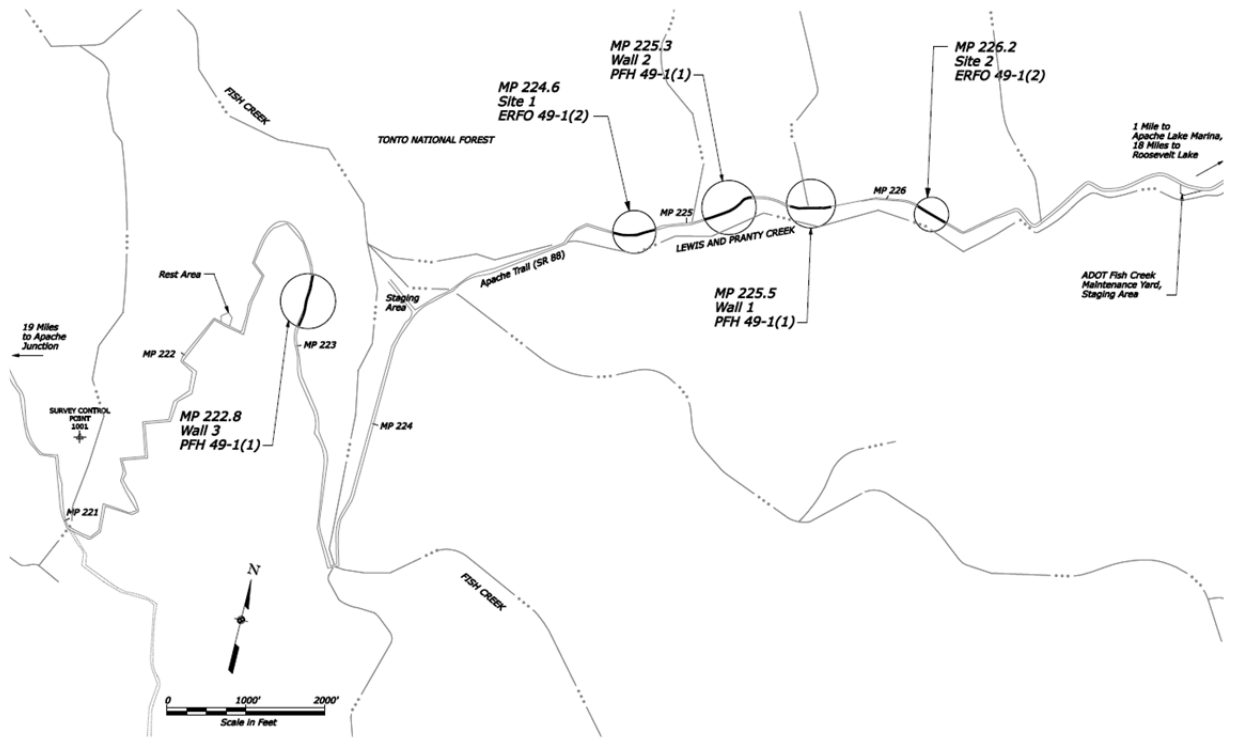


Figure A.5. Plan drawing detail of Apache Trail project site.

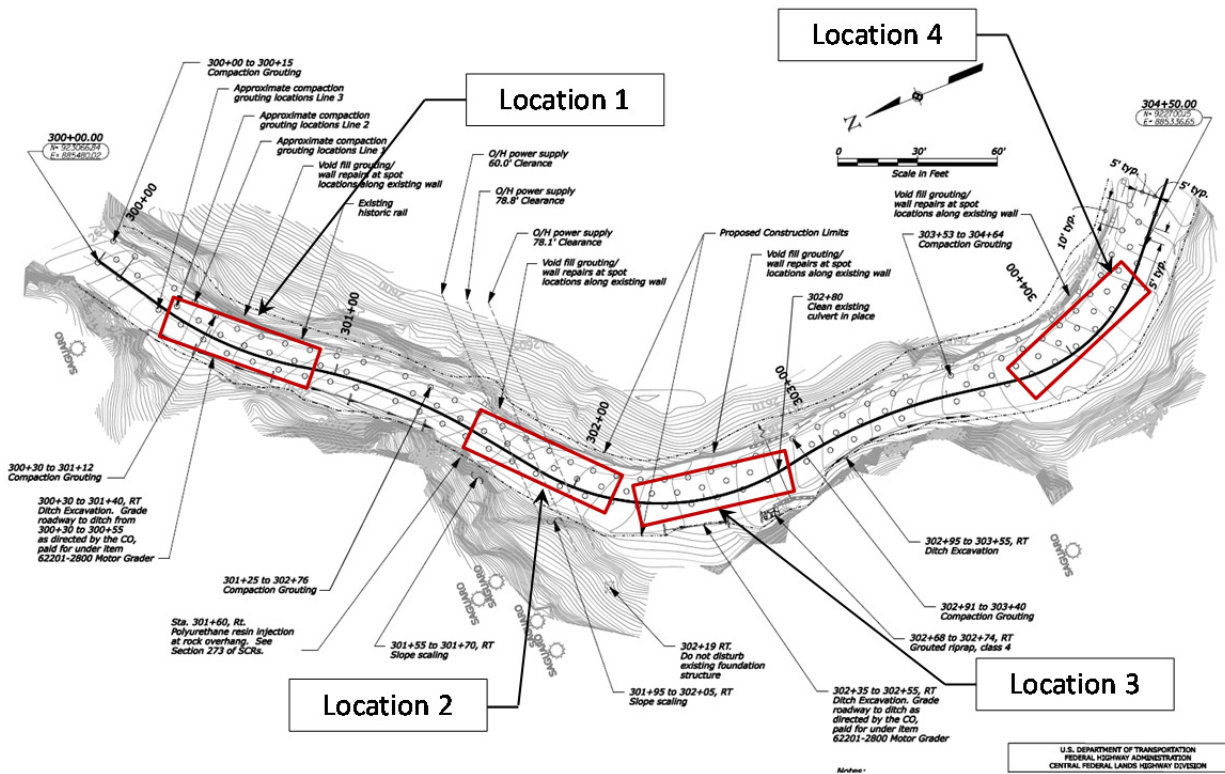


Figure A.6. Plan drawing detail of Apache Trail Locations 1 through 4.

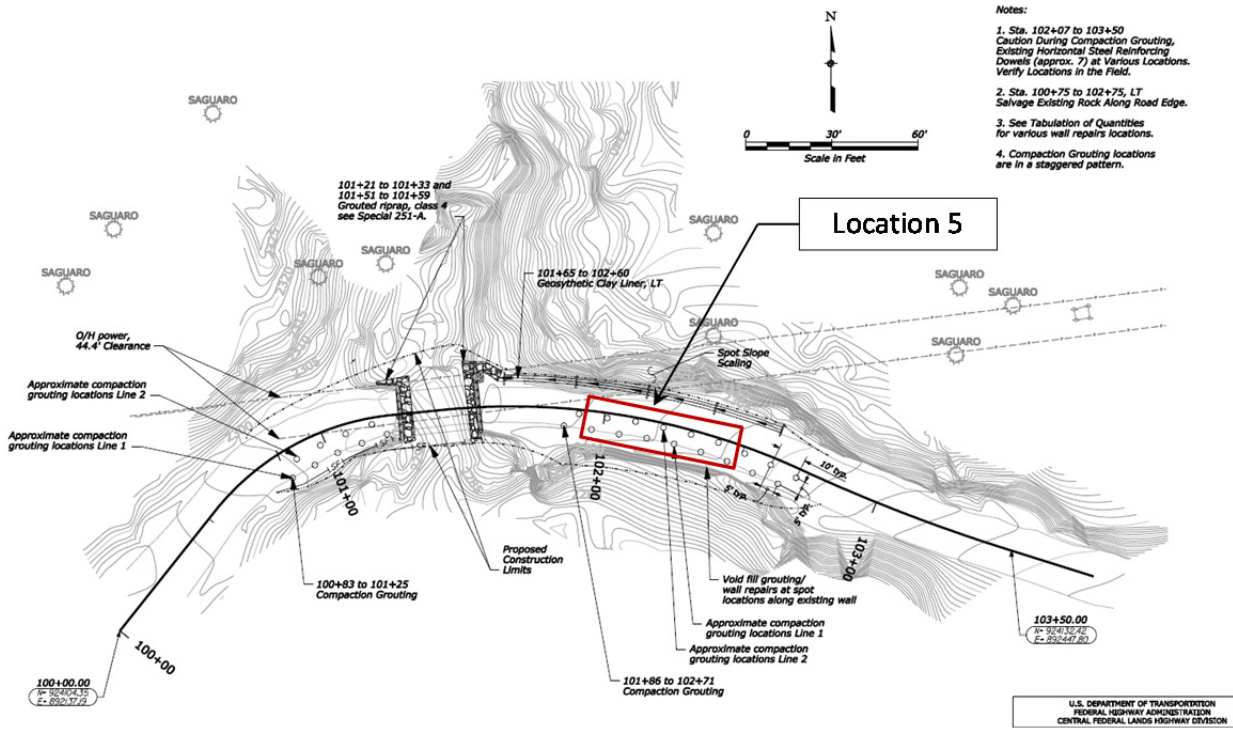
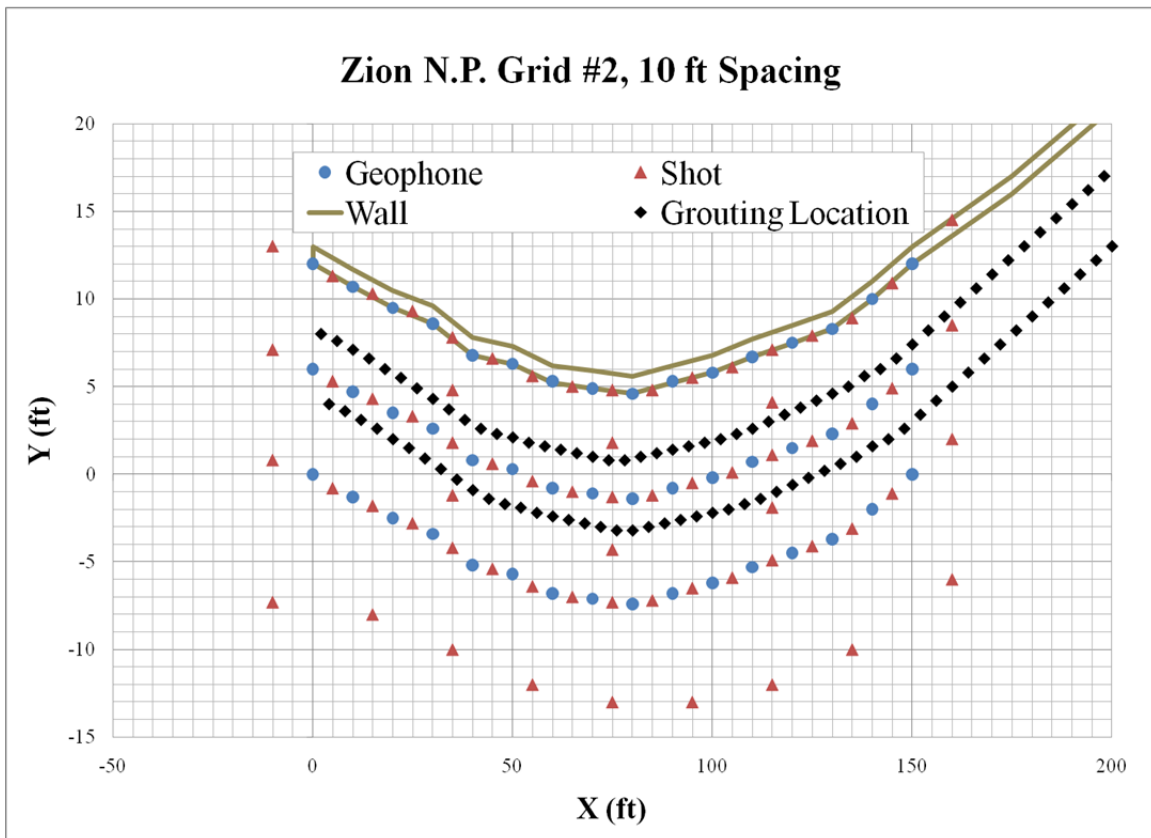
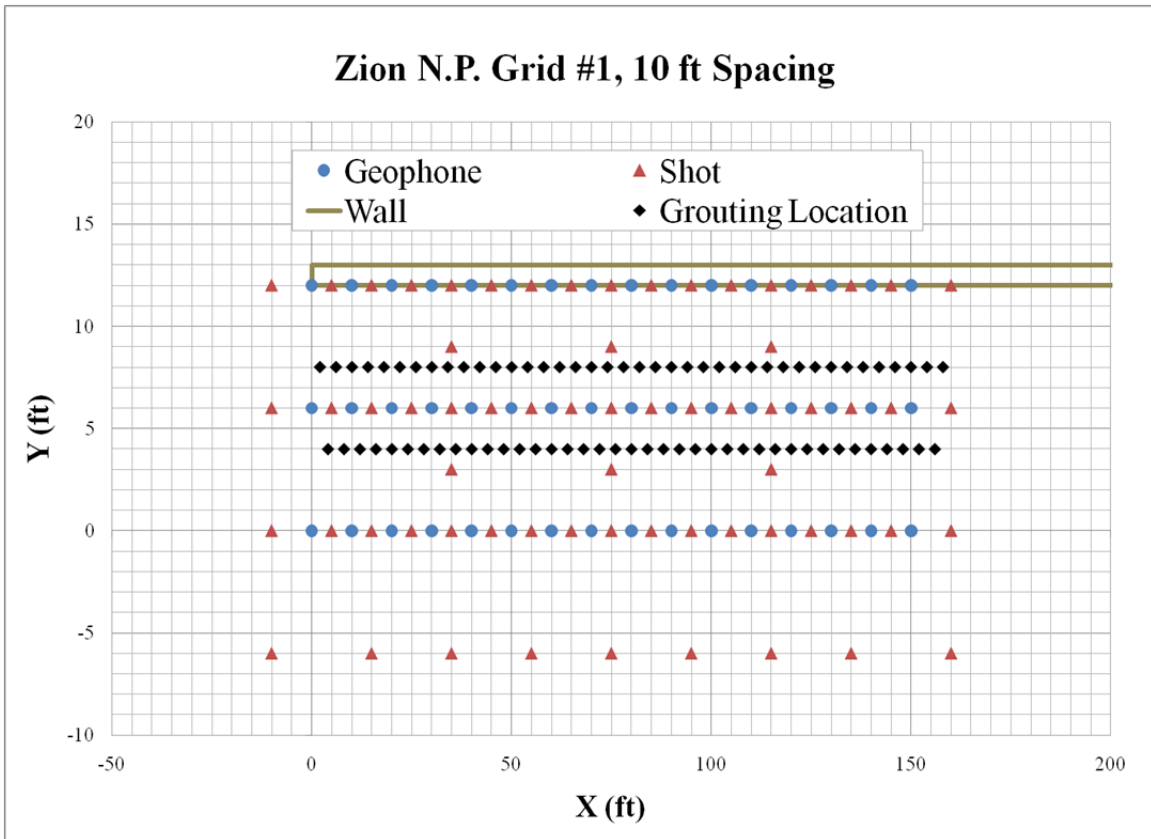
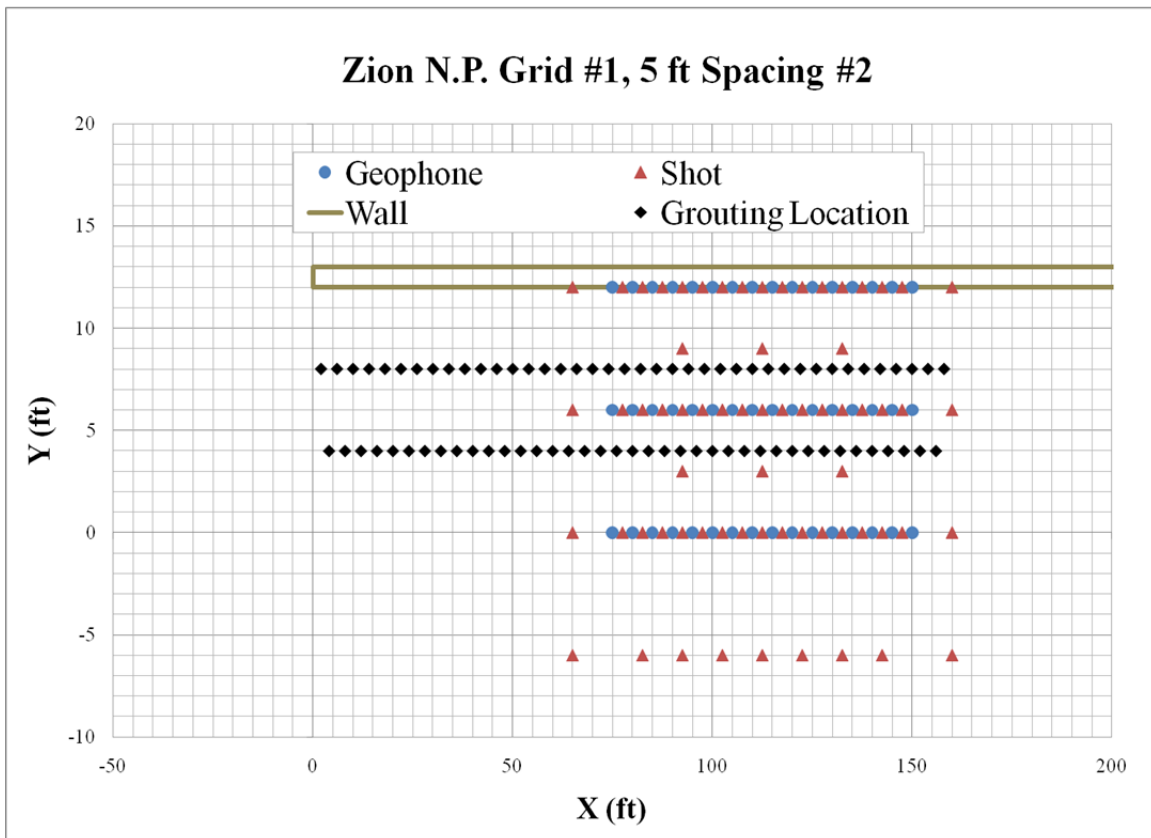
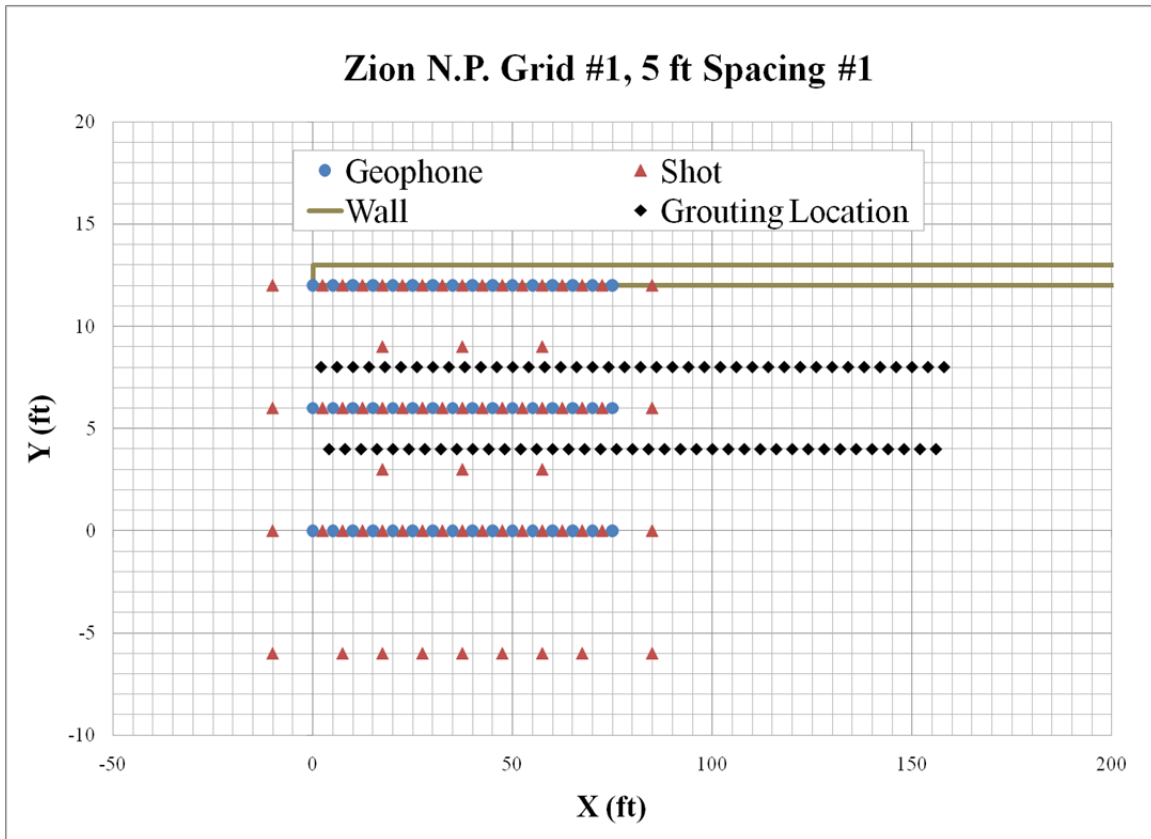


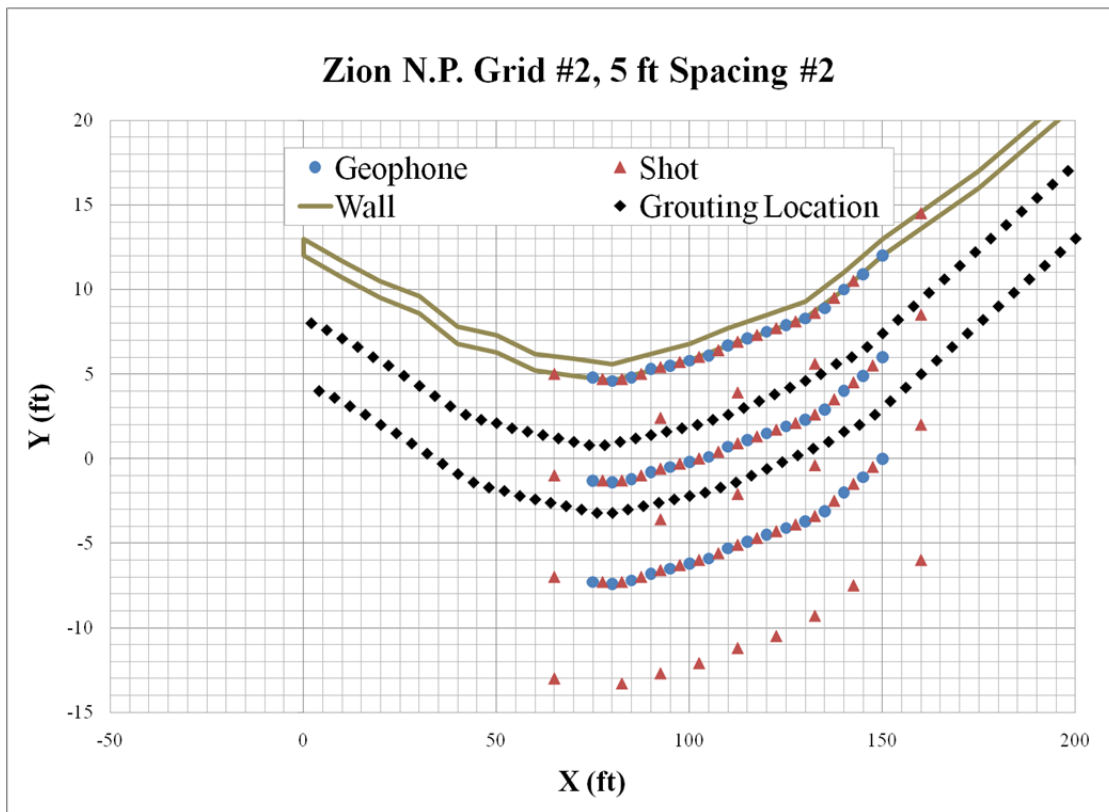
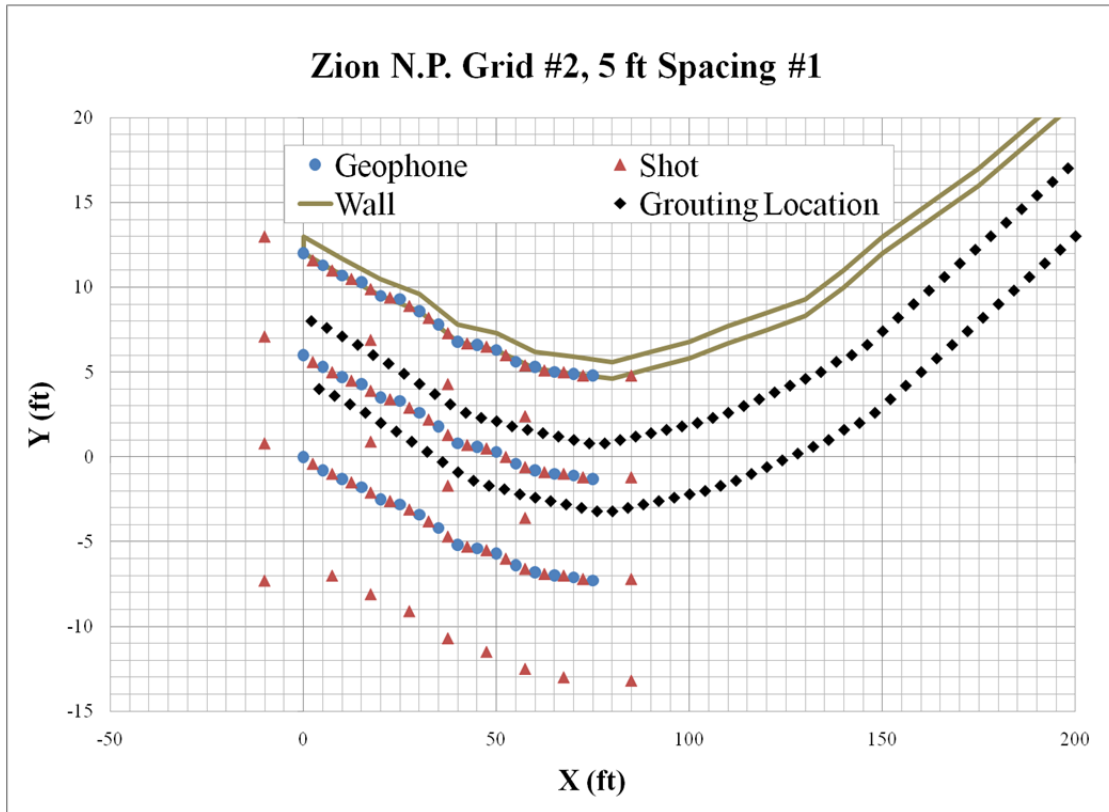
Figure A.7. Plan drawing detail of Apache Trail Location 5.

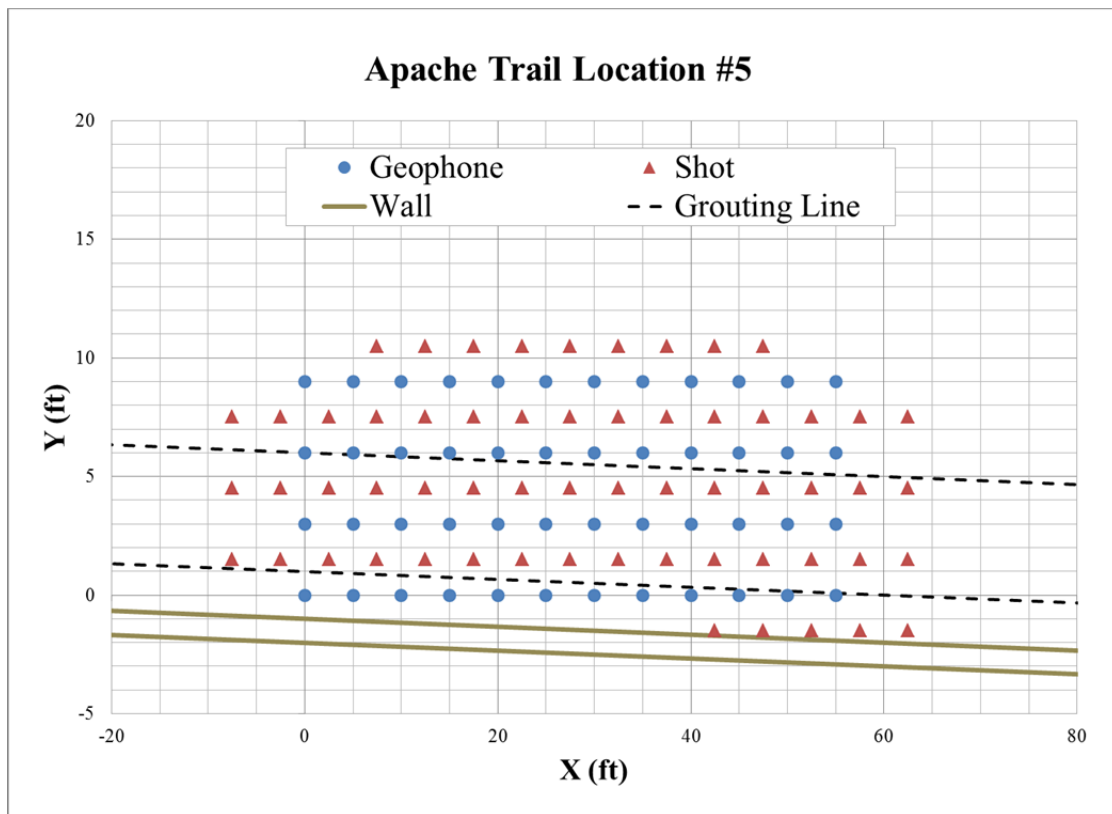
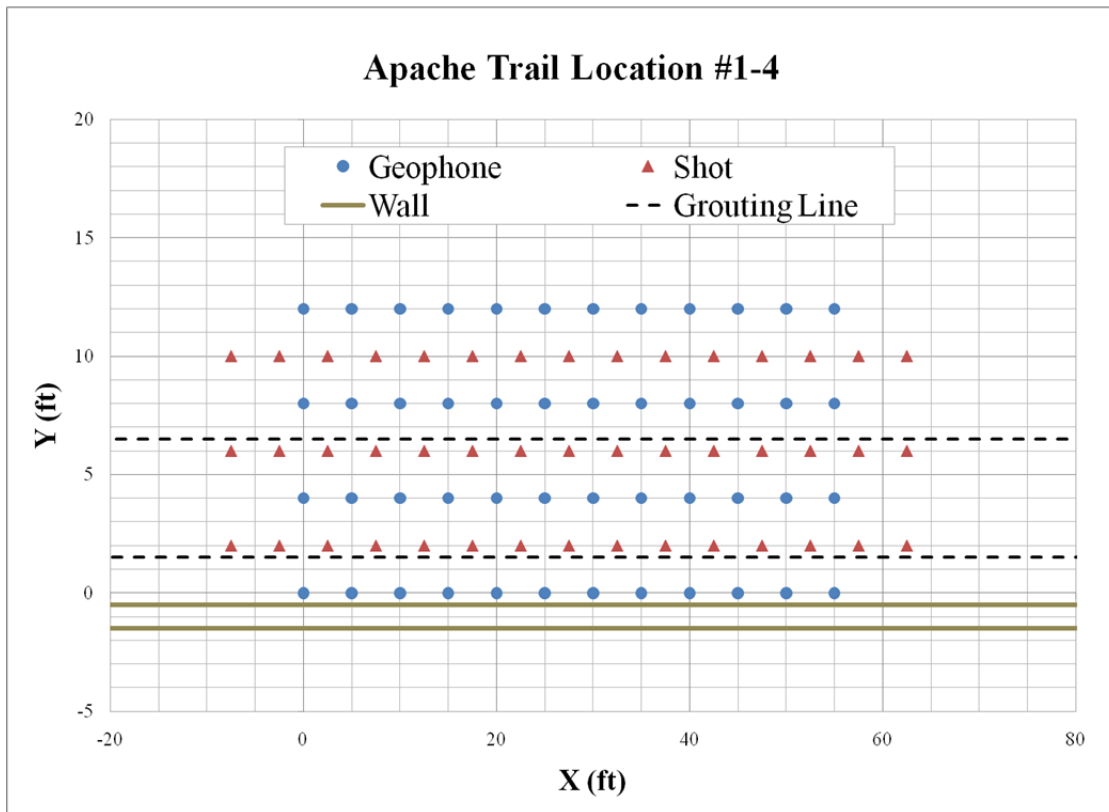
## **APPENDIX B - DATA COLLECTION LAYOUT DIAGRAMS**



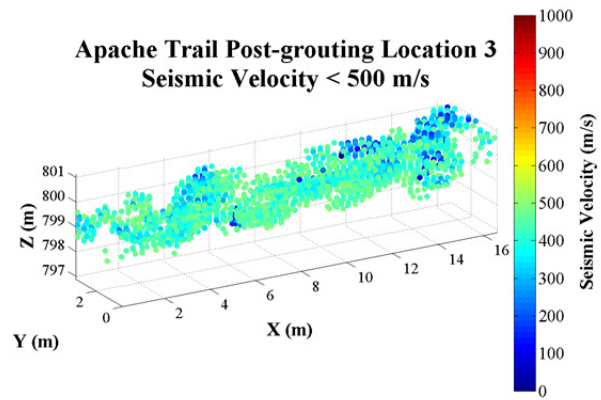
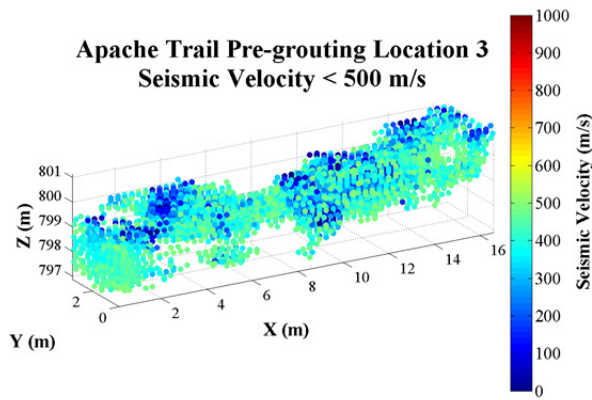
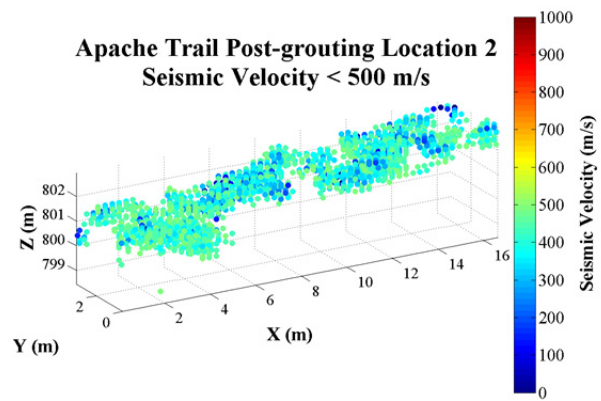
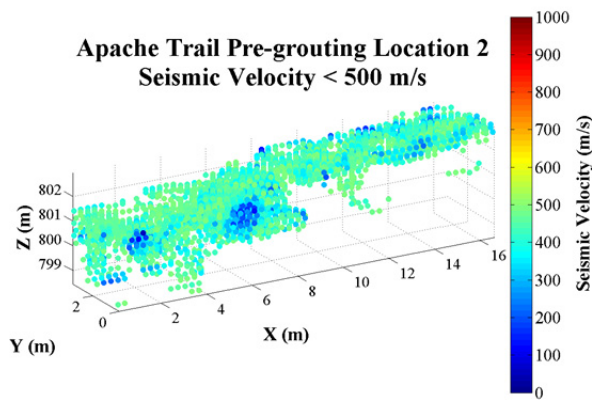
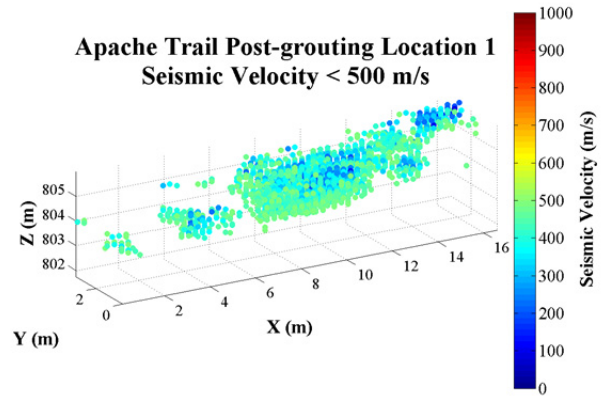
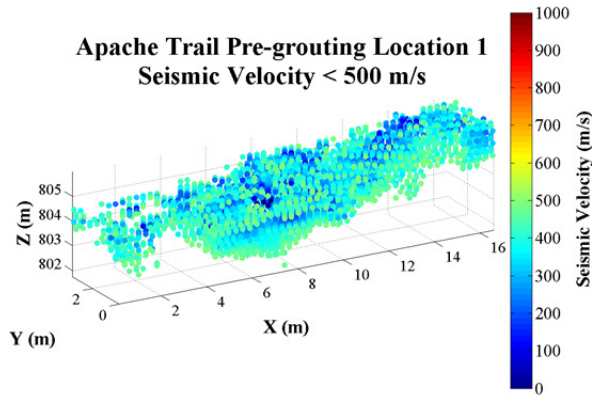


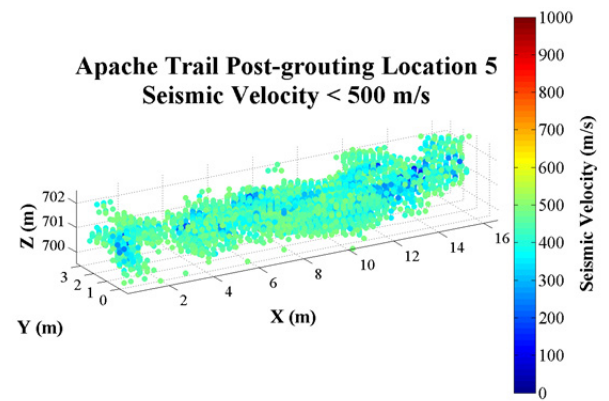
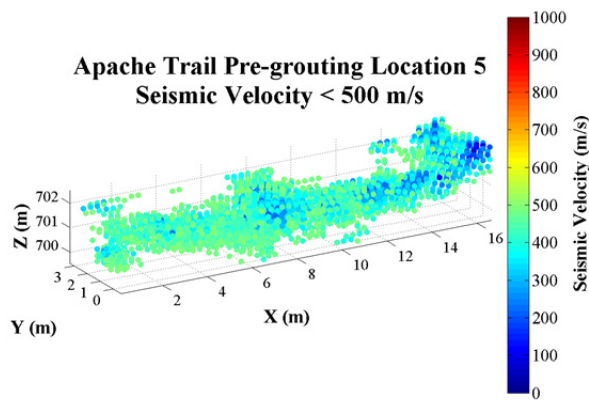
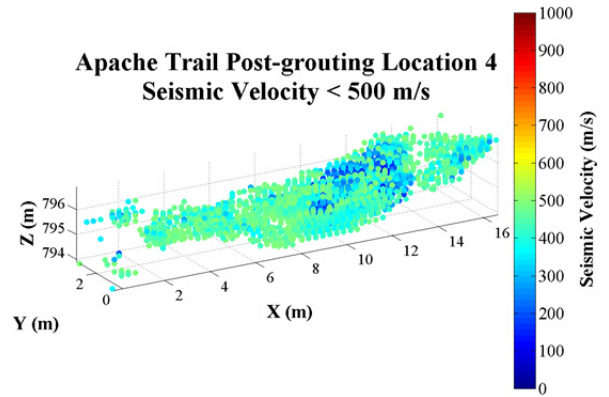
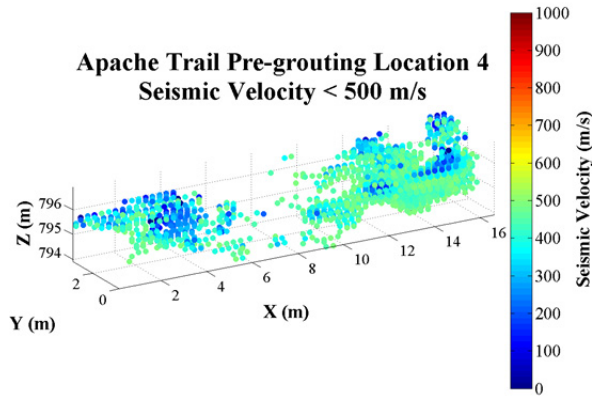


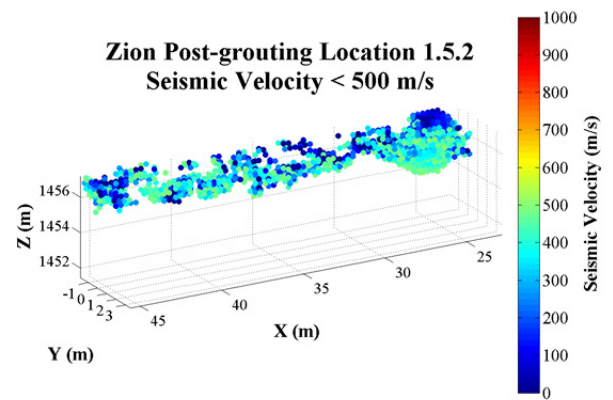
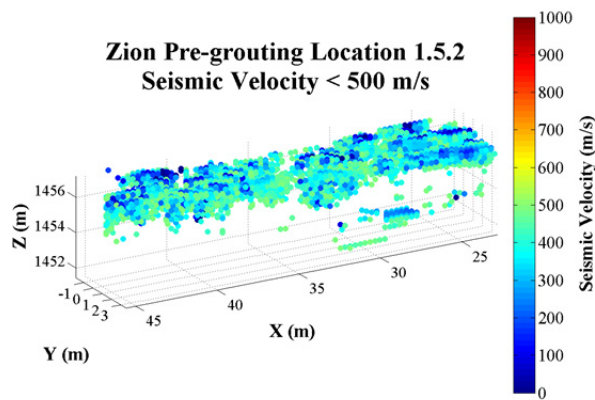
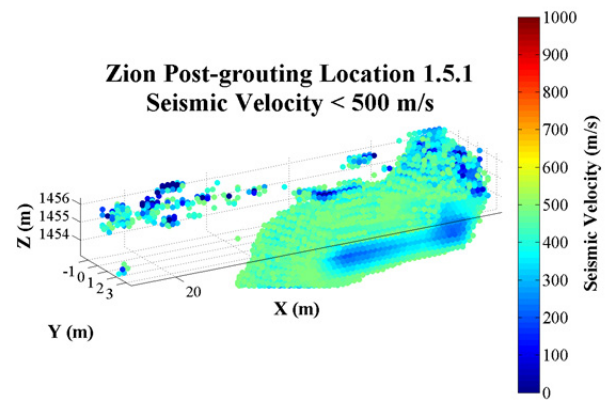
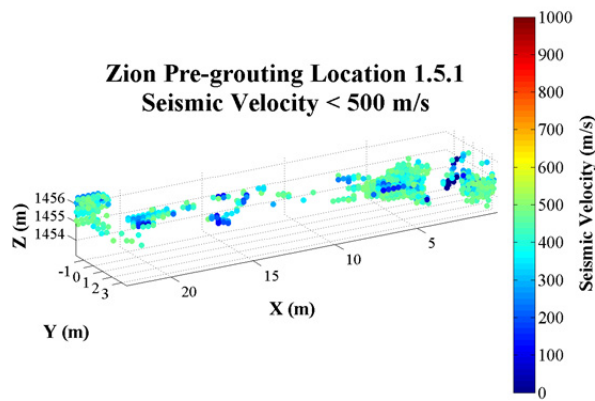
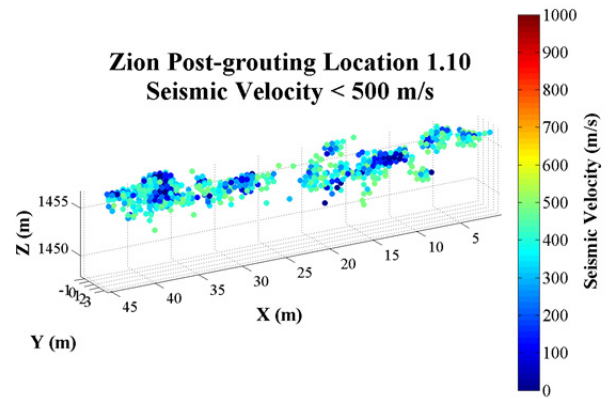
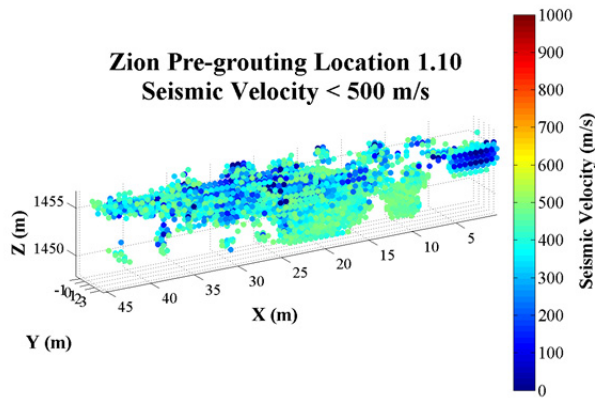




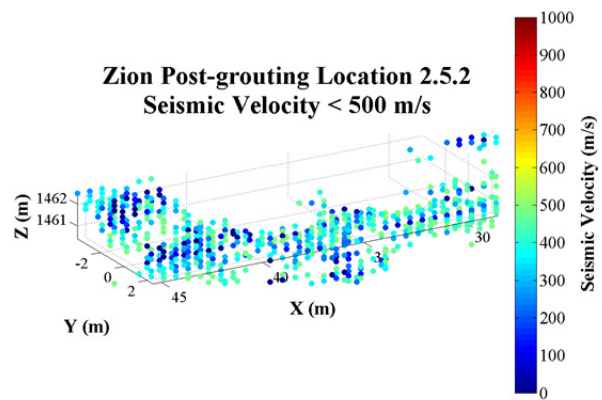
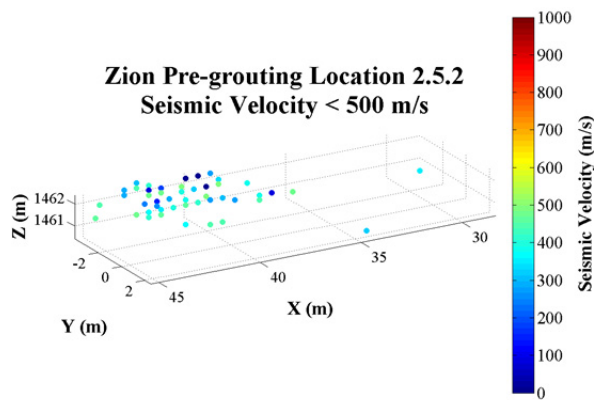
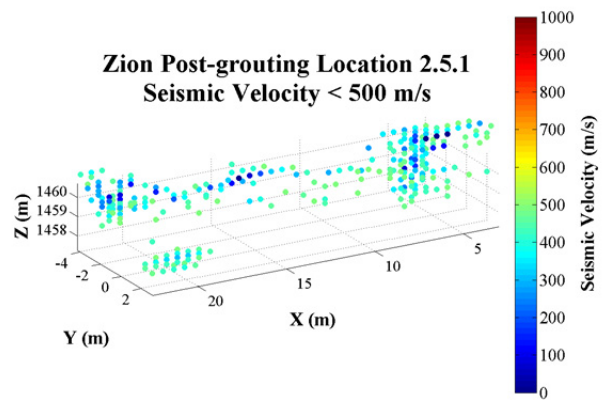
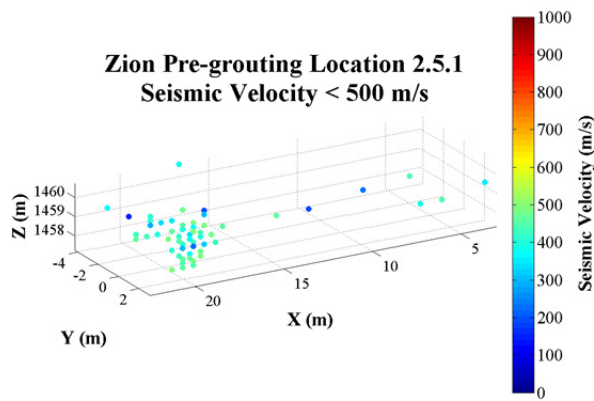
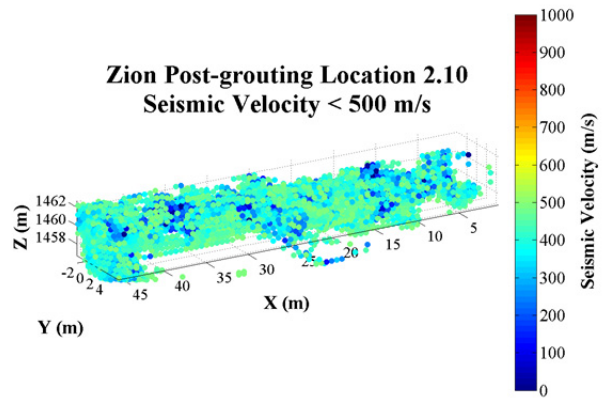
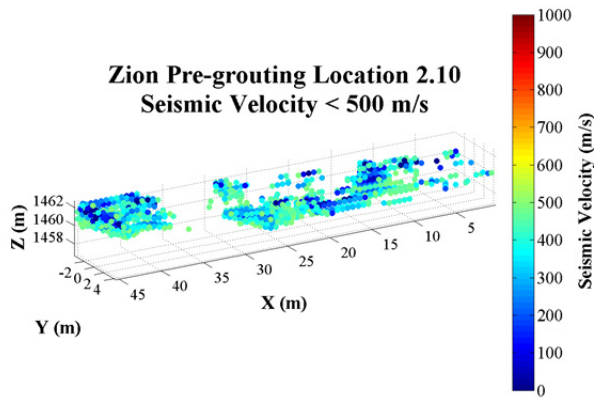
## **APPENDIX C - SEISMIC TOMOGRAPHY**



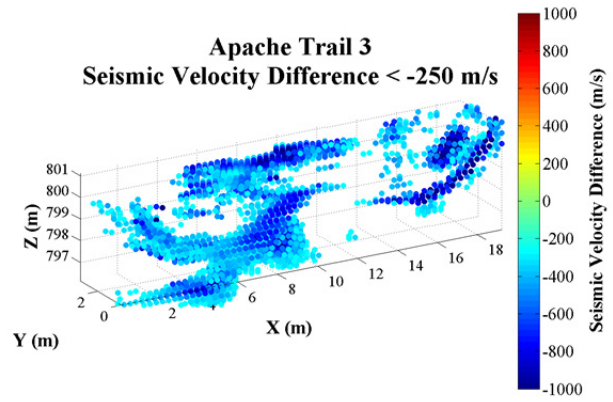
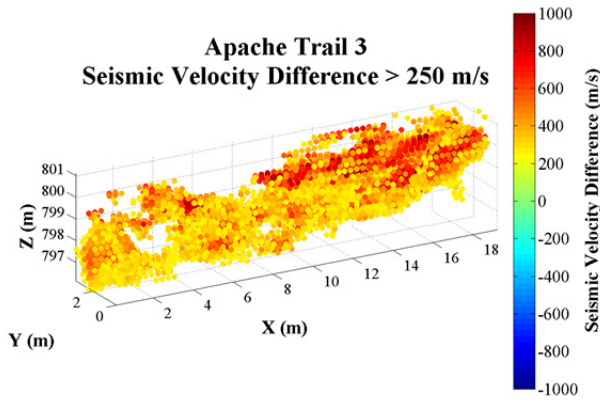
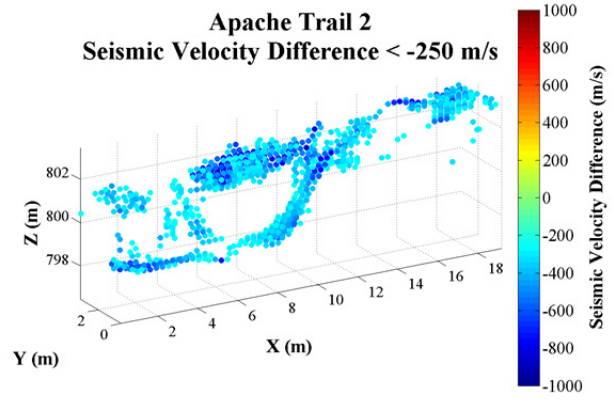
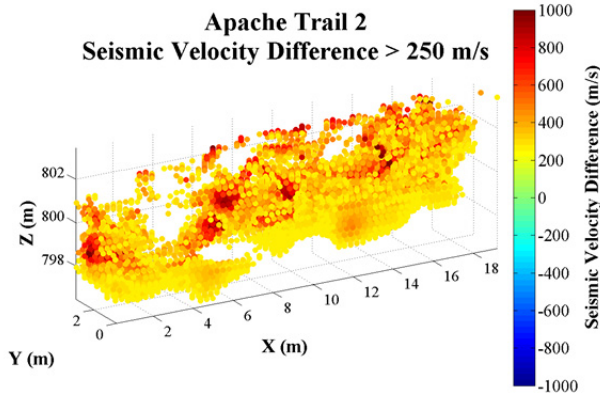
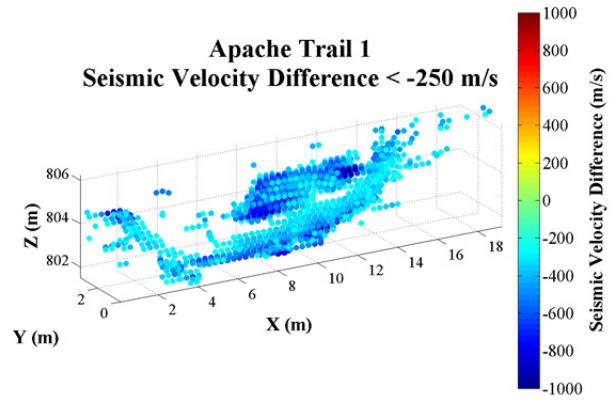
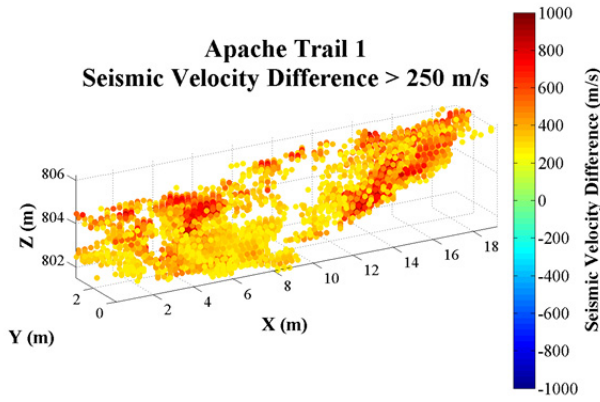


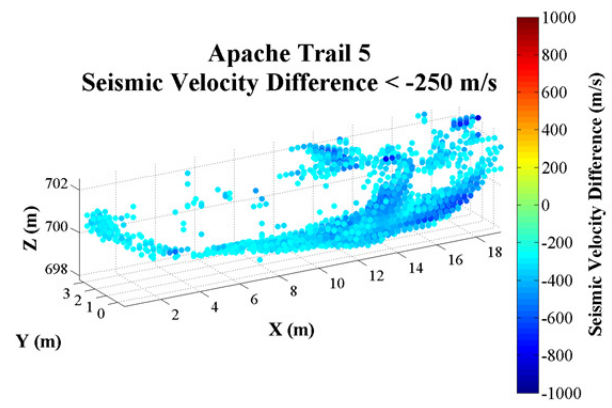
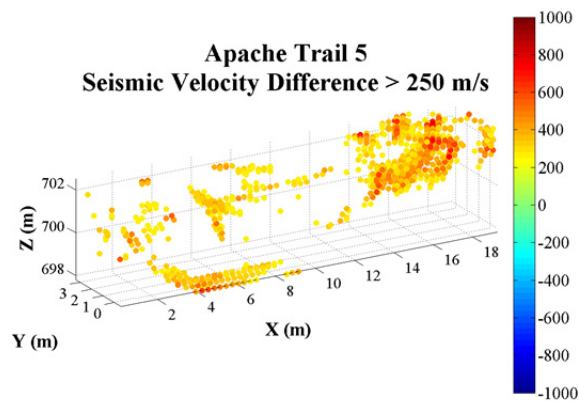
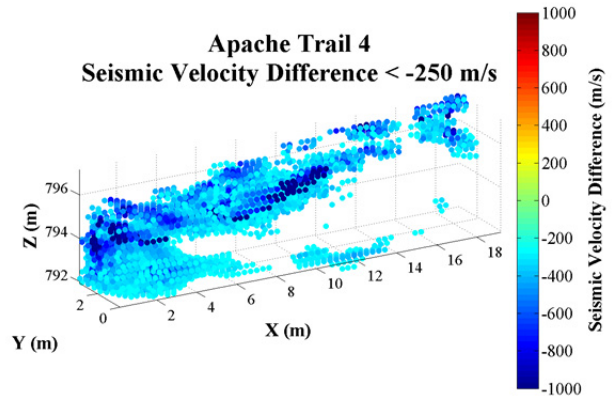
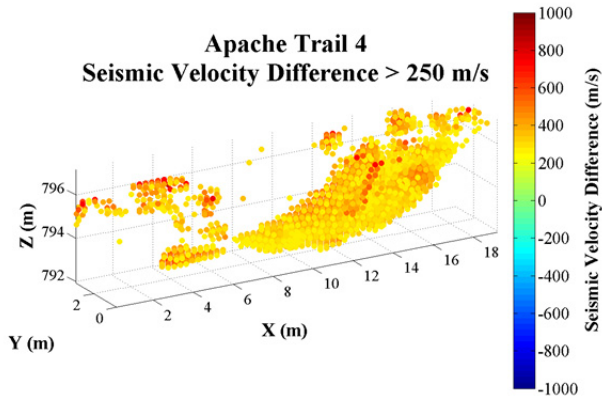


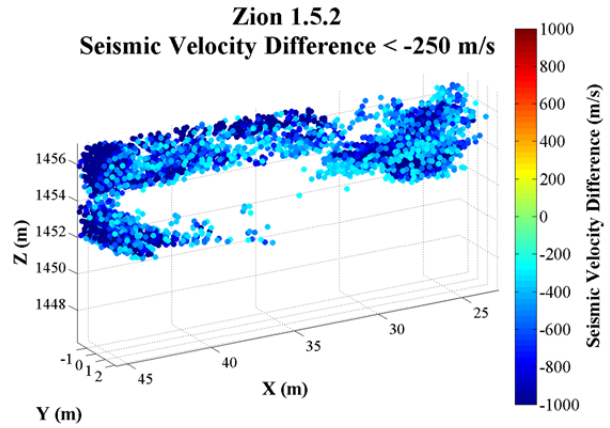
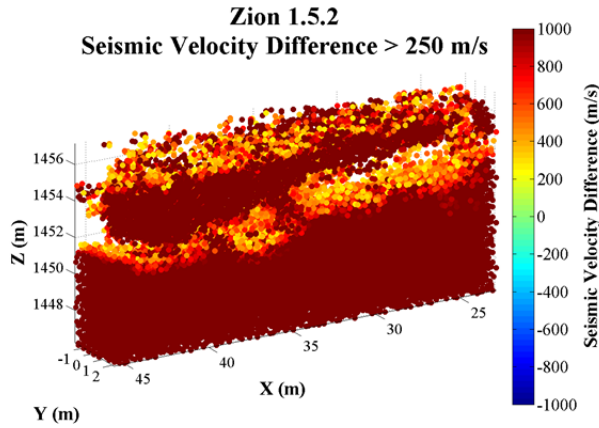
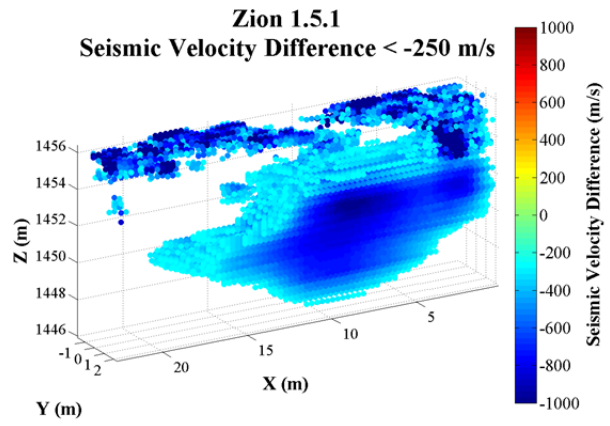
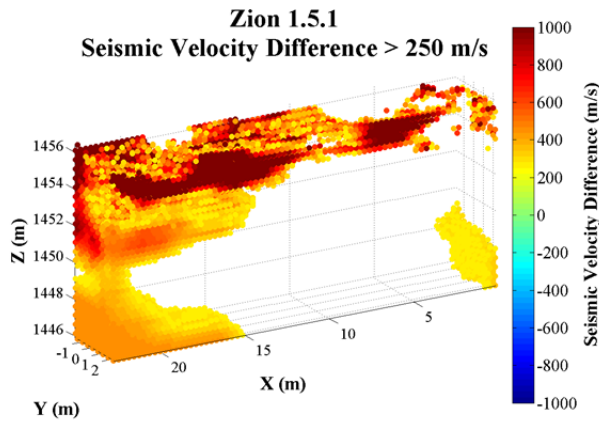
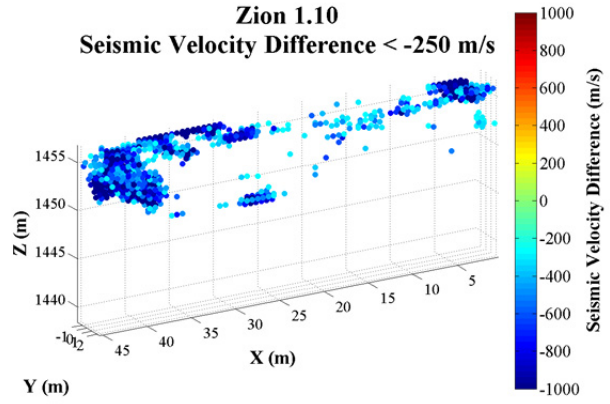
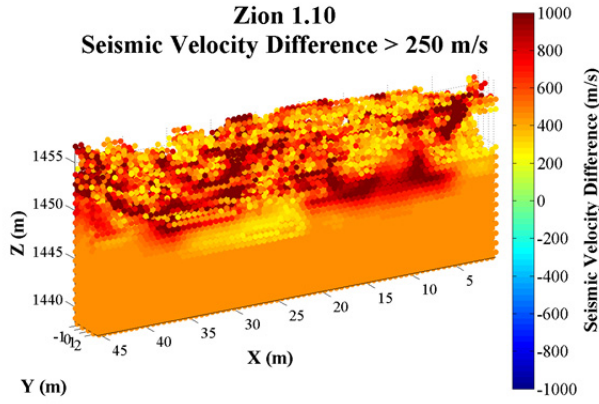


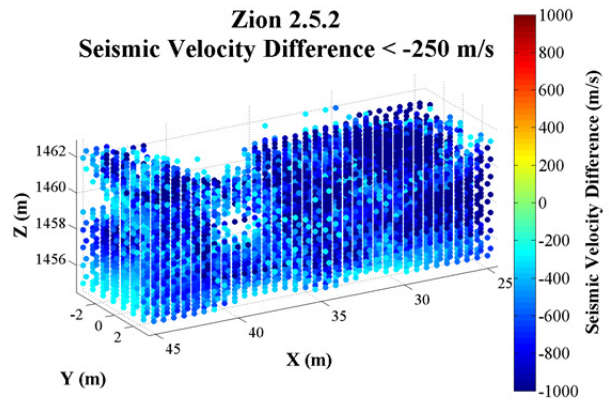
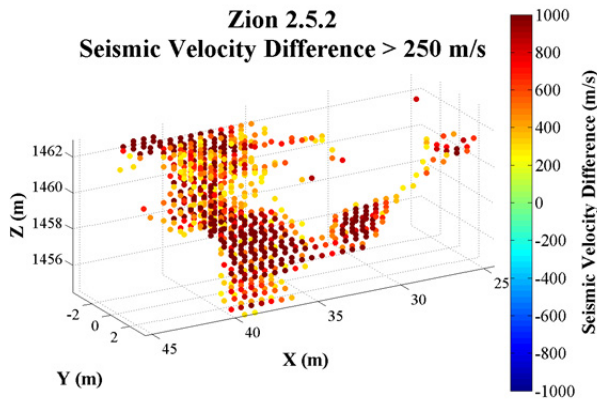
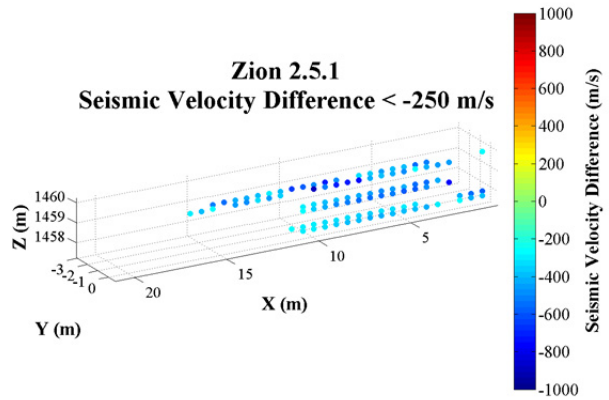
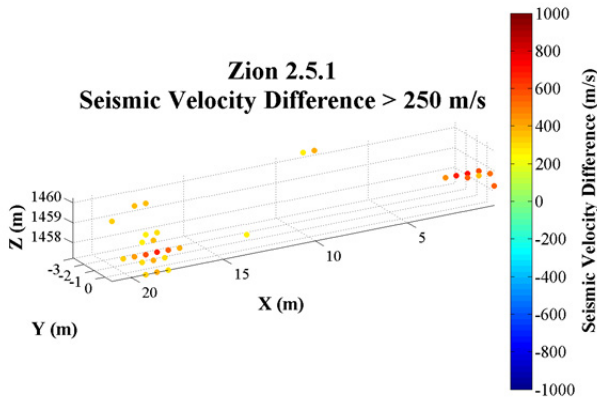
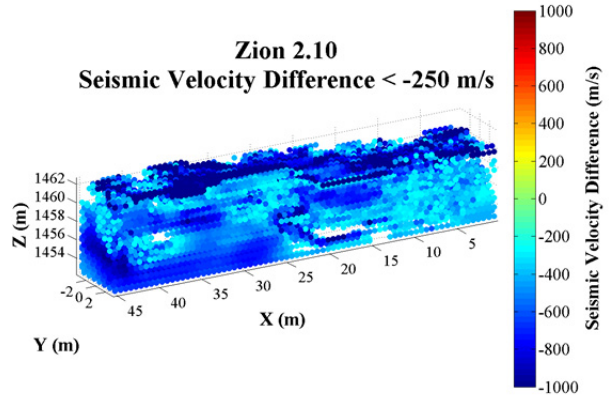
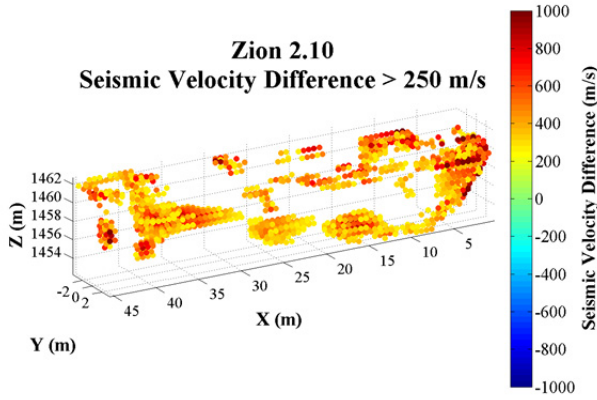


## **APPENDIX D - SEISMIC DIFFERENCE TOMOGRAPHY**









## **APPENDIX E - RAY DENSITIES**

