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THE SECOND GENERATION OF THE CCCM SYSTEM FOR IN-VITRO CARDIAC TISSUE ENGINEERING

By

Mai Dung Thi Nguyen B.S., the Oklahoma University, 1999 M.S., the University of Louisville, 2010

A Dissertation Submitted to the Graduate Faculty of J.B. Speed School of Engineering, the University of Louisville, in Partial Fulfillment of the Requirements for the Degree of

Doctor of Philosophy

Mechanical Engineering Department University of Louisville Louisville, KY

August, 2014

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A Dissertation Approved on June 17, 2014 By the following Dissertation Committee:

Dr. Guruprasad Giridharan, Director

Dr. Thomas Berfield, Co-chair

Dr. Bradley B. Keller

Dr. Palaniappan Sethu

Dr. Stuart Williams

Dr. Ayman El-Baz

DEDICATION

This dissertation is gratefully dedicated

to

my lovely deceased aunt, Say Nguyen,

my biological family,

and the Dominican Sisters of Peace

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My deepest gratitude goes to Dr. Bradley Keller, Dr. Guruprasad Giridharan, and Dr. Palaniappan Sethu, who welcomed me and provided tremendous opportunities to explore my career with trust, encouragement, consistent advice, and challenges. With their guidance, my project moved far beyond my imagination. I also would like to thank Dr. Thomas Berfield and Dr. Steward Williams, who were so generous with their time to serve as my dissertation committee. I am grateful to their wisdom, ideas, and support.

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ABSTRACT

THE SECOND GENERATION OF CCCM SYSTEM FOR IN-VITRO

CARDIAC TISSUE ENGINEERING

Mai Dung Thi Nguyen

June 17, 2014

Cardiovascular disease is the leading cause of death worldwide. When a myocardial infarction occurs, scar tissue compensates the damaged myocardial tissue. This scar tissue increases the stiffness of the heart tissue, reduces the heart's function, and finally leads to the heart failure (HF) disease. To have the tissue engraftment, in-vitro cardiac tissue should have the same properties as the native mature cardiac tissue. However, current *in-vitro* cell culture technologies fail to accurately recreate the *in-vivo* like mechanically physiological environment for *in-vitro* cardiac tissue culture, and therefore, fail to regenerate the *in-vivo* like mature cardiac tissue. Hence, a microfluidic cardiac cell culture model (CCCM) system was developed to better recreate the cellular environment and advance cardiac regeneration. CCCM system replicates the hemodynamic loading and unloading conditions occurring inside the left ventricle of a heart. With this system, different pressures of human heart conditions may be replicated for a variety of clinical and physiologic conditions. For proof-of-concept, embryonic chick cardiac cells with normal heart condition were applied. Compared to the tissue cultured in a static condition, tissues stimulated in the CCCM system achieved an in-vivo like cardiac

matured phenotype, had higher proliferating rate, showed more maturity, and expressed more contractile proteins. These results demonstrated that the CCCM system can be used to study the behavior of cardiomyocytes in different mechanical heart conditions and to create mature cardiac tissue which will benefit cardiac tissue transplant for HF.

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CHAPTER 1 INTRODUCTION

1.1. CARDIOVASCULAR DISEASE (CVD)

The basic components of the cardiovascular system are the heart, blood vessels (arteries, capillaries, and veins), autonomic innervation of the heart and vasculature, and the circulating blood. The heart acts as a pump to circulate blood through the lungs to oxygenate, and through the arteries to deliver oxygen and nutrients to the entire body. When blood is delivered to tissues, the oxygen and carbon dioxide are exchanged. The deoxygenated blood is then returned to the heart via veins, and finally to the lungs, helping dispose of carbon dioxide and other waste products.

Cardiovascular Disease (CVD) collectively refers to abnormalities associated with various components of the cardiovascular system and covers over 60 disorders relating to the heart and vascular system. CVD is the leading cause of death in the United States, which is higher than the next four leading causes of death combined.¹ Statistics from the American Heart Associate (AHA) indicate that about 81 million people or 1/4th of the population suffer from some form of CVD in the United States. This includes high blood pressure ~ 74.5 million; coronary heart disease ~ 17.6 million; stroke ~ 6.4 million; congenital cardiovascular defects ~ 650,000 to 1.3 million; and heart failure ~ 5.8 million.² Based on the article: "Heart Disease and Stroke 2010 Update" from AHA, it

was estimated that the total indirect and direct cost due to CVD and stroke in 2010 would be ~ 503.2 billion dollars, placing a severe burden on the economy and diminishing the quality of life for several thousands of people.²⁻⁴

CVD can be classified into two major categories based on disorders of the heart or the vascular system. Disorders of the heart include conditions such as angina pectoris, arrhythmias, cardiomyopathy, congestive heart failure, and congenital heart disease. Disorders of the vascular system, on the other hand, include conditions such as aortic aneurysms, arteriosclerosis, high blood pressure, stroke, and transient ischemia.^{1, 5} Coronary heart disease is the most common type of CVD. It is a condition which fatty deposits build up inside the inner walls of coronary arteries, creating blockages of the arteries. These blockages reduce the blood flow, causing a pain or discomfort in the chest, heart failure (HF) and heart attacks. In atherosclerosis,, the arteries become thicker or harden; and the inner wall of the arteries becomes narrower due to the deposits of fat, cholesterol or other substances. This narrowed passage can block the blood flow and lead to heart attacks and strokes. Strokes occur when the blood vessels to the brain are occluded or broken. As a result, brain cells begin to die due to lack of oxygen and nutrition.²⁻⁴ Stroke usually relates closely to high blood pressure, which happens when the pressure inside the vessels is higher than the normal range, which is about 120/80mmHg. High blood pressure can cause HF, stroke, kidney failure, or other health problems. The end stage for different CVDs is HF (Fig.1.1) which occurs when the heart fails to pump sufficient blood through the body. The body, therefore, does not get enough oxygen and nutrients. HF may develop slowly over time, and if not treated, can

cause life-threatening conditions, including pulmonary edema, failure of brain, kidney and other major organs, and myocardial infarction.⁶⁻⁹



Figure 1.1: Heart Failure is the end-stage of dysfunctional cardiovascular system existing for a long term.

1.2. TREATMENT OF HEART FAILURE

Heart Failure (HF) is a chronic disease, therefore, the treatment for HF needs lifelong management, which includes changes in living habits, medication, and assist devices to augment heart function. ^{7, 10, 11} The only cure for end- stage heart failure is total heart transplantation.

Drug therapy is usually used for the initial stage of the HF. Depending on the stage and symptoms of HF, a single or combination of different medications are applied. The most common drugs used for treatment of HF include Angiotensin-converting enzyme inhibitors, or Angiotensin II receptor blockers, Digoxin (Lanoxin), Beta blockers, Diuretics, and Aldosterone antagonists.¹² Angiotensin-converting enzyme inhibitors or

Angiotensin II receptor blockers dilate the arteries and improve blood flow, therefore, decrease the workload on the heart. Digoxin helps to strengthen the contraction of heart muscle and slow the heartbeat. Beta blockers reduce the heart rate and pressure. Diuretics enhance urination frequency to keep from the fluid building up in the body, especially in the lungs. Aldosterone antagonists help the heart work better.

When the HF advances to a more serious stage, devices that optimize myocardial function may be used for the treatment. For example, implantable cardioverterdefibrillators are used for monitoring the heart rhythm. Cardiac resynchronization therapy, or biventricular pacing, are used to help the heart pump efficiently by sending timed electrical impulses to the heart's ventricles for contraction. Mechanical circulatory support devices (left ventricular assist devices (LVAD)) that unload the native ventricle are used as a bridge to transplantation or as destination therapy in patients with severe HF that are refractory to medical therapy.¹³ LVADs are mechanical pumps designed to transport blood from the left ventricle through the body.

Heart transplant is a palliative therapy used for a subset of pediatric and adult patients with progressive and irreversible HF. A healthier heart from a donor is replaced for the failing diseased heart.¹⁴ However, people undergoing heart transplant face high risks of the rejection of the donor heart, infection, artery problems, medication side effects and the potential high risk of cancer due to the immune-suppressant medications.¹⁴ In addition, due to the shortage of donors, people who need heart transplants experience a long waiting times. Heart transplant or LVAD are currently the only options for the end-

stage HF. However, due to the lack of donors and the complications associated with immunosuppressive treatments as well as many high risks occurred during surgery, scientists and surgeons continue to search for new strategies to treat the HF.

1.3. THE HEART

1.3.1. Overview of the formation of the heart in the embryo

The heart is one of the first functioning organs formed during the embryonic period, both in bird and mammalian embryos.^{15, 16} The heart derives from the anterior mesoderm, the middle embryonic layer. First, one group of the mesodermal cells differentiate into precardiac cells, which later transform into myocardial, endothelial and smooth muscle cells. These mesodermal precardiac cells migrate and form the primitive linear heart tube, which includes the inner endothelial, cardiac jelly, and external myocardial layers. Another population of cardiac cells differentiates into cardiac myocytes, smooth muscle cells, and endothelial cells.^{17, 18} Then, the primitive straight heart tube loops and folds into an S-shape, followed by the convergence process. During this convergence phase, the formation of trabeculae begins; and hemodynamic stimulation plays an important role in modulating the trabecular patterning and development.¹⁹ The heart surface area, myocardial mass and wall stiffness increase as a result of this trabecular formation. At the end of this formation, the trabecular compaction begins, which contributes to the formation of ventricular septum and the thickness of the ventricular compact layer. At this time, the separation between the atria and ventricles, via the inlet segment, occurs and the formation of atria and ventricle develops.^{17, 20} Following the convergence is the wedging process. The modification of valves, such as the aortic valve or atria-ventricular valves, occurs; and the separation of left and right atria and ventricles is completed to

form a regular 4-chamber heart. ^{15, 19, 20, 19} Any abnormality during these processes can lead to heart congenital heart defects.

A complete 4-chamber heart, through one organ, functions as two pumps coupled to one another in a series. The right pump receives deoxygenated blood from the entire body and pumps it to the lungs for oxygen-carbon dioxide exchange, while the left pump receives the oxygenated blood from the lung and then delivers this oxygenated blood to the entire body. As a result, the pressure in the right pump is lower than in the left pump. However, to perform pumping function, both the left and right pumps need to match their output volume.

1.3.2. Gross anatomy of the heart

Each side of a heart has a main pumping chamber (the ventricle), a holding chamber (the atria), and two valves to prevent back flow (Fig. 1.2.). The valve between the right atria and right ventricle is the tricuspid valve and between the left atria and left ventricle is the mitral valve.^{21, 22} These valves prevent the retrograde flow of blood back into the atrium when the ventricles contract. The pulmonic valve and aortic valve in the right and left ventricle respectively prevent the blood in the pulmonary artery and aorta from flowing back to the right and left ventricle when these ventricles relax. The two ventricles share a common wall (septum) and electrical system to stimulate and control the timing of native ventricular contraction.



Figure 1.2: Schematic image of the heart gross anatomy. (*http://healthinformation.4arabs.com/heart/2.html*)

Deoxygenated blood from the vena cava system flows to the heart and is held in the right atria. When the tricuspid valve opens, the blood flows into the right ventricle in order to be pumped to the lung where the exchange of carbonate-oxygen in the blood occurs. Through the pulmonary artery, the oxygenated blood is then brought to the left atria and finally is pumped into the left ventricle when the mitral valve opens. The contraction of the left ventricle pumps the blood into the aorta from where blood is delivered throughout the body. Due to the vascular resistances and pressures being higher in the systemic circulation than the pulmonary circulation, the left ventricle generates more force to pump. Therefore, the muscle wall of the left ventricle is thicker than the right ventricle. Atria act as a booster pump and hence the walls of the atria are also much thinner than the ventricles.^{21, 22}

1.3.3. Working of the heart

The heart, consists of two atria and two ventricles, is the organ responsible for pumping blood throughout the body. The electrical signals generated in the sino atrial node travel through a signal transduction pathway to stimulate the heart tissue. In response to this, the upper then lower chambers of the heart contract sequentially, first both atria, then the ventricles. The working principle of the right heart side is similar to the left heart.

A pumping cycle of the heart can also be divided into two main periods: the diastolic and systolic periods. The diastolic period starts when the aortic valve closes and the muscles begin to relax. The diastolic period ends when the mitral valve closes after filling the blood from the atrium to the ventricle. The systolic period then starts when the mitral valve closes and the muscle begins to contract. This period ends when the aortic valve closes after the blood in the ventricle is ejected to the aorta.²¹⁻²³

The relationship between pressure and volume, especially for the left ventricle (LV) chamber, can be divided into four phases: the ventricular filling or diastole, isovolumic contraction, ejection, and isovolumic relaxation (Fig.1.3.).²¹⁻²⁴ During the ventricular filling phase, the relaxation of the heart muscles reaches the maximum level. Therefore, when the blood from the atria continues to fill in the ventricle, the pressure of the ventricle goes up gradually and the blood volume is increased significantly, which is represented by phase 'a' on the pressure-volume loop. When the ventricle pressure reaches a certain level, the muscles contract.²⁴ The pressure inside the ventricle at this point is higher than the atria. As a result, the mitral valve closes, but this pressure is not

sufficient to open the aortic valve. Because all valves are closed, the pressure is increased dramatically while the volume remains the same. This phase is called the isovolumic contraction phase (phase b). At this point, the ventricle begins to contract until the pressure inside the ventricle chamber exceeds the aortic pressure; then the aortic valve opens. The blood inside the left ventricle is then ejected to the aorta, causing a decrease in volume (phase c). However, since the ventricle is still contracting, the pressure inside the ventricle keeps increasing until it reaches its peak, then, decreases when the ventricle begins to relax. The ventricular pressure begins to drop until the pressure in the aorta finally becomes larger than in the ventricle, causing the closure of the aorta valve. The relaxation of the ventricle plus the closure of valves greatly reduces the pressure inside the ventricle while the volume remains unchanged with no blood going in or out of the ventricle. This phase (phase d) generates a vertical line (isovolumic relaxation phase) on the diagram B (Fig.1.3.). When the pressure inside the LV is lower than the left atria pressure, the mitral valve opens and the LV is again filled with blood. The next cardiac cycle begins.²¹⁻²⁴

During normal adult conditions, the human heart rate is about 70 ± 10 beats per minute (bpm). The stroke volume is about 60 ± 10 mL/beat and the left ventricular systolic peak pressure approximates of 120 ± 10 mmHg. The left ventricular end diastolic pressure ranges from 5-12 mmHg. ^{25, 26}. Stroke volume is the volume of blood ejected for each beat. Heart rates vary during fetal development and are then higher in the neonatal and adult heart.



Figure 1.3: Relationship between pressure and volume during the pump cycle of the heart. (A) Cardiac cycle diagram and (B) Pressure-Volume Loop. (a) Diastolic filling phase, (b) Isovolumic phase, (c) ejecting phase, and (d) Isovolumic relaxation phase.

1.4. HEART AT CELLULAR LEVEL

1.4.1. Cellular organization of cardiac tissue

Unlike other tissue, in the early development, embryonic cardiac tissue has a high ability for both differentiation and proliferation.²⁷⁻²⁹ This high proliferation and differentiation makes the vertebrate heart quickly transformed from a single two-layer straight tube into a four-chamber heart.³⁰ Cardiac morphogenesis occurs during the embryonic period, between weeks 4 to 8 in human pregnancy, or between days 2-10 in the chick embryo.¹⁶ DNA synthesis reaches the high rate during this cardiac morphogenesis; and the cardiac conduction system as well as coronary vascular system develops in late morphogenesis.^{16, 31} However, when entering the neonatal period, cardiomyoctes reduce their proliferating rate to focus more on producing contractile proteins; hence, becoming functional cardiacmoyctes.³² Therefore, cardiomyocyte differentiation occurs to adapt the

subsequent of hemodynamic pressure/volume loading and unloading, resulting in an increase in size or causing cell hypertrophy. During this hypertrophic process, the amount of protein contents (especially contractile proteins) per individual cell increases with a little change in cell number.^{33, 34} After birth, cardiomyocytes lose their ability to proliferate.

The embryonic cardium is composed of three different major cell layers: an inner single cell endocardial layer, a loose connective tissue layer and the layer of cardiomyocyte muscle cells (or myocardium layer).^{14, 21, 22, 35} During the morphogenesis, via proliferation and differentiation of cardiomyocytes, these three layers are quickly transformed into a 3D trabecular myocardium. (Fig. 1.4.A) This trabecular and compact myocardium continues to increase in mass and number in order to form a solid mature myocardium to sustain the transmural pressure due to the hemodynamic loading and unloading applied on the inner side of the cardiac muscle wall.¹⁶ Hence, the developing of this solid mature myocardium promotes the myocardium function.^{36, 37} To perform this function, under the effect of mechanical load, mature cardiomyocyte and myofibril arrange in parallel.³⁵

Cardiomyocytes are the cells that make up the heart muscle and have the ability to contract spontaneously. To perform their function in synchrony, cardiomyocytes need to align and establish end to end cell-cell contacts. (Fig.1.4B and C). Smooth muscle cells form a contiguous layer over the cardiomyocytes, and finally a layer of endothelial cells line the myocardium providing shear protection. Besides these major cell types, cardiac

tissues are also composed of cardiac fibroblasts. Cardiac fibroblasts relate to heart remodeling, therefore, play a critical role in heart hypertrophy and heart failure.³⁸



Figure 1.4: Cardiac tissue. [A] Schematic layers of the heart walls; [B] Histological image of ventricular wall; [C] Arrangement of cardiomyocytes in the cardiac muscle. ([A] ³⁹; [B] http://www.studyblue.com/notes/note/n/histology-medi-1000/deck/938131; [C]:http://www.studyblue.com/notes/note/n/tissue-lab-3-muscle-and-nervous-tissue/deck/2179334)

Hemodynamic stimulation is one of the major exogenous factors regulating cardiac morphogenesis. To adapt mechanical loading and unloading, the myocardium increases the cell size with protein contents, especially the contractile regulating proteins.^{16, 40} Myofibril is the contractile structure of cardiac muscle. Myofibrils are composed of sarcomeres or the contractile unit. ^{41, 42} At the beginning, when the cardiac muscle cells differentiate, all the sarcomeric proteins randomly diffuse in the cytoplasm. By the time of linear-heart-tube formation, due to mechanical stimulations, myocytes begin to beat or contract, causing myofibrils to rapidly arrange into a highly organized network in order to synchronize the contractions throughout. A sarcomere unit is composed of 3 major components: thin filament, thick filament, and Z band. (Fig. 1.5) Thick filaments arrange in parallel to the thin filaments. Myosin heavy chain proteins are on the thick filament and bind to F-actin of the thin filament during the contraction. Thin filament is composed of F-actin, troponins, and tropomyosin. During the contraction, thick and thin filament slide along each other. Titin filament connects the thick filaments to the Z band and acts as an elastic spring during the myocyte contraction. The Z band connects the sarcomere units in series.⁴²⁻⁴⁴ The contraction is controlled by the interaction between the myosin heavy chain on the thick filament and the binding site of the F-actin molecules, which is the major component of the thin filament. This binding activity depends on the sensitivities of Ca²⁺ to the tropomyosin-troponin complex.⁴⁵ Alpha-actinin, a component of Z band, serve as the anchor for F-actin to Z band, as well as the connection to neighbor sarcomere.⁴⁶ The mechanism of the contraction will be discussed in the section 1.4.2.



Figure 1.5: Simplified schematic model of mature myofibril. [A] Myofibril; [B] Ultrastructure of a relaxing sarcomere; [C] Ultrastructure of a contracting sarcomere. The magnitude and duration of stretch and contraction in a cardiac tissue depends on the preload and afterload conditions. In the heart, specifically in the left ventricle, preload

refers to the condition when the filling of the blood inside the ventricle causes the stretch of the ventricular wall during the diastolic phase. Afterload refers to the aortic resistance that the system needs to overcome in order to pump blood out of the ventricle via opening of the aortic valve.²² This directly affects the contractile force that needs to be generated by cardiomyocytes. Overcoming the aortic pressure opens the aortic valve for ejecting the blood into the aorta.

Preload pressure increases slowly when blood filling to the chamber during diastole increases, which creates greater systolic pressure for the subsequent contractions due to the preload sensitivity of the native ventricle. This systolic pressure continues to increase until its maximum systolic pressure is reached at the optimal preload. At a constant preload, higher systolic pressure can be obtained through ventricular contraction by raising the afterload condition such as increasing the aortic pressure.²² However, if the afterload pressure or the resistance keeps increasing, the ventricle cannot create enough force to open the aortic valve to push the blood out of the heart. At this point, the systolic phase is totally isovolumic. Preload and afterload pressures, as a result, depend on the vascular system and the behavior of the heart including peripheral resistance, the frequency of the heart's contraction, and change of the stroke volume.²²

1.4.2. Cellular response to mechanical signals

When a mechanical stimulus is applied to the extracellular matrix (ECM), the cells detect this mechanical stimulus via mechanoreceptors. These mechanoreceptors are located in the plasma membrane connecting the extracellular and intracellular regions of the cells, traducing the mechanical signals from the outside to the inside of the cell.^{23, 47} Once the signal is transmitted inside of the cell, the signal triggers biochemical changes via signaling transduction pathway, enhances the formation of sarcomere, and alters structure of the cytoskeleton directly.^{23, 47}

Troponin complex includes troponin C (TnC), troponin I (TnI), and troponin T (TnT). TnC is Ca^{2+} sensitive and has a site for Ca^{2+} binding; TnI is the contractile inhibitor; and TnT is the protein binding to tropomyosin. This troponin complex is strongly associated with the tropomyosin, which regulate the binding of MHC to the thin filament for sarcomeric contraction. ⁴⁸⁻⁵⁰ Binding Ca²⁺ to TnC switches the conformation of TnC from a close position to the open one, allowing the interaction of TnC with TnI to happen. Without this interaction, TnI binds to F-actin at the binding site of MHC; thus, it prevents the bonding between MHC with F-actin. Binding of TnC-TnI releases the binding of TnI-actin and enhances the binding of TnI-TnT, which reveals the binding sites of MHC for MHC attachment. Once MHC attaches to the F-actin, with the ATP hydrolysis occurring during the association of Ca^{2+} with TnC; contraction takes place. ^{41,} ^{50, 51} The relaxation of the sarcomere unit occurs during the dissociation of Ca²⁺-TnC. Ca²⁺ is then transferred back to SR via the SERCA2a pump. In summary, calcium ion will bind to the troponin C, help to deactivate troponin I (inhibitor) and change the formation of TnT in order to reveal the MHC binding site on the thin filament. Once the binding site is opened, myosin heavy chain from the thick filament binds to F-actin. This binding pulls the thin filament of a sarcomere closer to the center, causing the contraction. Titin is a protein connecting the thick filament to the Z band at this point

serves as an elastic spring, keeping the thick filament at the center during this contraction. Alpha actinin, a protein located on the Z bands, helps to connect the thin filament with the sarcomere, as well as to the thin filament of the neighbor sarcomere. Alpha actinin thus contributes to form and maintain the lattice networks among the sarcomere during the relaxing as well as the contracting phases.

Catecholamine affects mechanical performance of the heart tissues through the activation of β-adrenergic receptors (AR) and cardiovascular function can be positively and negatively controlled primarily via adrenergic signaling.⁵²⁻⁵⁴ Under normal physiological conditions, catecholamine induces positive inotropic and lusitropic responses in the heart tissue through β 1-AR-activated pathway. Once the stimulation of β 1-ARs binding with its agonist (ex. isoproterenol) happened, this binding complex activates the formation of cyclic AMP (cAMP). cAMP accumulation rapidly increases which indirectly promotes the phosphorylation of PLB, and enhances the cardiac contractility. ⁴⁷ Even though the density of β-ARs in utero diminishes during development,⁵⁵ there are shifts in the adrenergic receptor subtypes with increasing dominance by subtype β 1-ARs as cardiomyocytes become more mature under normal physiological condition.^{53, 56} This dominant β 1-ARs, therefore, induces positive inotrope and lusitrope via heart rate and contractility. Under the abnormal physiological condition of the heart, or failing heart, β 1-ARs decreases, and β 2-ARs increases with increasing sensitivity to adrenergic toxicity resulting cardiomyocyte death.⁵⁶

Increasing cAMP promotes the phosphorylation of phospholamban (PLB).⁵⁷ Sarcoplasmic reticulum calcium ATPase2a (SERCA 2a) and PLB are proteins for calcium handling regulation inside the cardiomyocytes (Fig.1.6). These proteins are involved in regulating the contraction-relaxation of the heart muscle. Phosphorylated PLB enhances the activity of SERCA2a by increasing the affinity of Ca²⁺ on SERCA2a. This activated SERCA2a then transports calcium against the gradient from cytoplasm back to sarcoplasmic reticulum (SR) for muscle relaxation.⁵⁸ Phosphorylated PLB (pPLB) releases this inhibitory effect, making the affinity site to Ca²⁺ on SERCA2a more apparent. As a result, the rate of calcium ions influx back to the SR increases, promoting the muscle relaxation and being ready for the next contraction. Without being phosphorylated, PLB binds to SERCA2a, preventing the Ca2+ binding to SERCA2a, and hence becoming an endogenous inhibitor of SERCA2a.



Figure 1.6: Simplified schematic of the biomechanical pathway relating to calcium regulation inside the cell for cardiac contractility.
Sarcomere length, a basic contractile unit of cardiomyocyte, can be affected by the mechanical stimulation.⁵⁹ When the muscle is stretched to a length greater than normal size, new sarcomere units are added rapidly at the end of the muscle fibers.^{60, 61} Unlike the skeletal muscle, small changes in sarcomere length can result large changes in tension generation.^{59, 62, 63} Therefore, increasing the sarcomere length enhances the tension development, which affects the changes both in preload condition and the contractility of the heart.

TnT and Alpha and Beta-Myosin Heavy Chain (α , β -MHC) are proteins involved in cardiac sarcomere function as discussed previously. TnT is one of three troponins binding with tropomyosin. TnT affects the function of thin filaments and the interaction between the thin and thick filaments, regulating cardiac muscle contractility.⁵⁰ Abnormality of this TnT gene can cause sudden death for cardiac patients. ⁴⁵

Myosin heavy chain (MHC) is a major protein expressed in heart tissue during the developmental stage and is responsible for mechanical performance of the heart, especially muscle contractility.⁶⁴⁻⁶⁶ In higher vertebrates, two cardiac isoforms of MHC predominate. β -MHC is expressed mainly during embryogenesis or heart diseases while α -MHC exists dominantly in the adult heart tissue and inhibits the expression of β -MHC. The temporal expression of α and β -MHC is species specific. Interestingly, the distribution of α -MHC expression is correlated with beating rate.⁶⁷

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In addition, the deformation of the cytoskeleton can change the physical properties of the cells and distort the nucleus, as well as the biochemical and molecular events inside the cell, such as gene expression, transcription, translation and protein synthesis. This change also affects physical and chemical communication between cells. Therefore, the structure inside the cell, morphology of cell, and the biochemical aspects of the cell are altered as a result of mechanical stimulus.

To respond to any abnormal condition of mechanical stimulations, such as overpressure or overstretch, the heart begins to remodel itself. The remodeling of the hearts causes an increase in the number of fibroblasts, thickens the heart muscle wall, or enlarges the size of the hearts.^{61, 68, 69} These changes play critical roles in contractility of the cardiac tissue. If the abnormal mechanical stimulus persists, heart remodelling can lead to the cardiac dysfunction (Fig. 1.7)



Figure 1.7: Maladaptive responses due to abnormal mechanical loading leads to the heart failure.

1.5. CONCLUSION

The heart is the central organ within the cardiovascular system and is extremely complex in terms of construction and function. This chapter serves to provide an overview of CVD and the heart structure and function. CVD is a serious health problem and continues to claim millions of lives each year while also diminishing quality of life for several others. However, current treatment options, though beneficial have several limitations. In order to improve the quality of life, researchers therefore continue to search for better options to prevent or treat the CVD.

CHAPTER 2

IN-VITRO MODEL SYSTEMS TO STUDY CARDIAC TISSUE

2.1. NEED FOR CELLULAR-LEVEL STUDIES

The human body consists of sequential levels of structural and functional organization. Cells are the smallest functional units capable of sustaining themselves and consist of various molecular constituents, including bio-molecules like DNA, RNA and proteins. Cells are organized together to form tissue. Organs in the body responsible for specialized functions are made up of one or more types of tissues. Various organs and/or tissues in the body are organized together to form systems (Ex: Cardiovascular, Nervous, or Circulatory). Finally, an organism sustains life due to synergistic working of various systems within the body. Several mechanisms exist to provide feedback and maintain the body's functions within a tight range (homeostasis).

The tradeoff between generations of highly specific molecular information and translation of that information *in-vivo* necessitates investigation at various levels of cellular organizations (Fig.2.1). Cell-based studies are essential to provide highly specific information relating to molecular mediator and the targets for drug discovery, therapy, and tissue generation. Analysis of purified or isolated cell populations free from surrounding cellular and extracellular constituents allows the investigation of sub-cellular mechanisms in great detail, which is not possible in intact tissues.⁷⁰ Study of

heterogeneous mixtures of cells (like in a tissue) often results in unnecessary noise, which significantly deteriorates the quality of information attainable.



Clinical translation

Figure 2.1: Biologic complexity versus clinical translation plot. Human clinical studies are the most relevant, by definition, to clinical translation, but have the least specific whereas cellular level studies provide highly specific information but their relevance to human physiology is low. The *in vitro* cell cellular model devices seek to significantly enhance the relevance of cellular level studies.

Further, cellular level systems that utilize purified cells, allow for convenient analysis, using both destructive and non-destructive techniques. Cells can be imaged using microscopy to study structure, conformation, the expression of intra and extra-cellular

markers, organization of organelles and other details of nuclear and cytoskeletal elements. Low and high-throughput techniques can be used to evaluate gene expression, protein expression and production of metabolites. The effect of a drug can be understood in terms of molecular signaling events that alter cell phenotype and function. High-throughput cell culture, using multi-well plates, can be used to evaluate effects of variables, including concentration of stimulants and time of exposure on cellular function.⁷¹ The flexibility and specificity of information generated from cellular level systems is unparalleled, and is usually an essential first step in any drug discovery study or tissue generation. However, since cell-based studies use isolated cells in a non-physiological environment without mechanisms responsible for homeostasis, the relevance of these studies is limited, and results need to be verified using animal and patient level studies.

In-vitro studies are performed in isolation without the biologic complexity and the paracrine feedback mechanisms present in the body. Therefore, to understand the real and long term effects of a biochemical compound, foreign tissue, drug, or device on an organ or in a system, *in-vivo* evaluation is essential. Animal studies are used to confirm outcomes before application in the human body. Animals are similar in complexity to humans; and the levels of organization are conserved amongst most species. Small animal studies, like study on rats, mice, hamsters and rabbits, are easier to perform due to cost related issues and availability of significant amounts of information and characterization of various systems in animals.^{61, 72} Further, technologies for generation of transgenic animals allows for greater flexibility with design of studies to evaluate

targeted pathways.⁷³ Large animals are physiologically closer to humans and provide improved relevance due to greater similarities in size of organs and function of systems.^{74, 75} Large animals are particularly useful in testing organ/ tissue transplantation or implantable medical devices because the size of their organs is comparable to humans and provides a more accurate representation of the actual situation.

Patient or clinical studies are often the last stage of evaluation for a particular drug or treatment. This follows pre-clinical studies accomplished using *in-vitro* methods and *in*vivo animal studies. Clinical trials allow assessing the safety and effectiveness of a new medicine or device on patients. Clinical studies are divided into phases 0, 1, 2, 3, and 4. Phase 0 trial allows an early evaluation of the pharmacokinetic effects of the candidate drug in humans. This is done by administrating a low dose of the test compound in a short time period. This phase 0 trial doesn't have a therapeutic or treatment purpose; rather, allows the researchers to explore the pharmacological profile of the test compound in human to see if it is appropriate for humans or not.⁷⁶ As a result, it helps to select the potential drug. The disadvantage of this phase is the poor relation between the preclinical and clinical effect of the testing drug.⁷⁷ Phase 1 is the first stage to test the dose effects on human subjects, so the appropriate dose of a certain drug on humans can be found. Phase 2 trials assess how well the drug works and continues to affirm the safety of the drug on large groups. Phase 3 trials are applied on a huge group to see how effective the drug is for a certain type of disease. And finally, phase 4 post-marketing surveillance trials determine potential unanticipated effects of the drug in broader, unselected populations.

In conclusion, cell-level studies are highly specific and can be used to investigate molecular mediators and signaling pathways involved in disease processes. These studies cannot be accomplished in patients because of inherent difficulties with isolation of cells and analytical techniques. Animals provide a more appropriate platform for early evaluation as they provide more opportunities for evaluation. To shorten the time between discovery and clinical validation, it is essential that cell-based studies are accomplished in platforms that have physiological relevance. For example: studying cardiac tissue under unloaded static conditions is undesirable since mechanical loading and fluid flow play an important role in maintaining cell structure and phenotype.

2.2. IMPORTANT CONSIDERATIONS FOR CELL-LEVEL METHODS OF CARDIAC TISSUE DEVELOPLMENT AND CHARACTERIZTION

During normal heart function, the myocardium experiences passive stretching and increasing transmural pressure during filling (preload) and actively generates mechanical force with further increase in wall stress during ejection (contraction). Cells in cardiac tissue therefore are under constant physical stimulation and rely on the conversion of these cues into intracellular signals to control cell phenotype and muscle mass during physiologic and pathologic conditions.⁷⁸ Cardiac cells therefore are exposed to periodic stress, strain, and shear.

Physiological heart development and cardiac function rely on the response of cardiac tissue to mechanical stress signals during hemodynamic loading and unloading. These

stresses manifest themselves via changes in cell structure, contractile function and gene expression.⁷² Disruption of this well-balanced stress-sensing machinery due to various pathological conditions results in mechanical dysregulation, cardiac tissue remodeling and heart failure. To achieve physiological relevance, *in-vitro* models must replicate the complex, dynamic *in-vivo* interactions between cardiomyocytes and mechanical stress signals. However, current *in-vitro* models do not incorporate all aspects of mechanical loading and therefore fail to accurately mimic the *in-vivo* cardiac microenvironment.

2.3. REVIEW AND CURRENT STATE OF THE ART

Several animal model studies have proved that hemodynamic mechanical stimulations play significant roles in shaping the formation and ensuring proper heart functions.^{19, 79-84} Therefore, for cardiomyocyte differentiation into functional cardiac tissue, *in-vitro* mechanical stimulation should be included during *in-vitro* cardiac tissue regeneration.

Various clinical studies for cardiac tissue regeneration via transplantation of progenitor or differentiated cell population have been established.⁸⁵⁻⁸⁷ However, the goal of tissue replacement with functional myocardium has not accomplished because a majority of studies apply the direct delivery of undifferentiated cardiac cells to the injured locations.⁸⁸ In addition, the current state of cardiovascular *in-vitro* models is predominantly cultured under conventional static conditions.^{69, 70, 89} Most studies utilize isolated cardiomyocyte cells maintained in two-dimensional culture forming randomly oriented cell-extracellular matrix (ECM) interactions.^{73, 90, 91} Culturing cardiomyocytes in a 2D system does not reflect the physically biological environment that the *in-vivo*

cardiomyocytes experience. As a result, the phenotype and behavior of these 2D cultured cardiomyocytes appear differently from the cardiomyocytes in the *in-vivo* normal conditions.⁹² Cardiomyocyte grown on the 2D condition shows flattened, stellate-shape phenotype instead of a rod-shape phenotype as it is in the *in-vivo* environment. Proliferation rate, differentiation, and DNA synthesis are poor.^{16, 93, 94} The interaction between cell-cell or cell-matrix are limited due to the 2D planar geometry; thus, cell-cell connections are loose, which fails to initiate spontaneous contraction.

There are groups using 3D engineered cardiac constructs to investigate cardiomyocyte maturation, response to drugs, and the effects of genetic defects in ion channels and sarcomeric proteins. The phenotype and molecular regulation and the function of cardiomyocytes in 3D shows more likely resemble the *in-vivo* cardiomycytes. ^{16, 92-100} However, there are a limited number of bioreactors that can generate 3D tissue on a scale relevant for clinical translation. Complex systems that can replicate *in-vitro* mechanical stimulation occurring in the heart are currently unavailable. Accurate replication of the *in-vivo* environment requires consideration of several factors. First, tissue orientation and direction of stretch are critical determinants of cardiac cell signaling; therefore randomly oriented cultures cannot replicate physiological loading. Second, fluid flow is an important factor as shear stress strongly influences endothelial and smooth muscle phenotype but not cardiomyocytes. Third, cyclic build-up of pressure and stretch during preloading are critical determinants that dictate cell structure and function; hence, perfused systems are more representative of the *in-vivo* environment. Fourth,

synchronous contractions ensure ejection of fluid that in turn results in relaxation of builtup pressure and stretch.³⁸

Some of the aforementioned issues have been previously addressed, albeit individually. Patterning techniques like micro-contact printing and lithography to define areas of cell attachment and directional alignment have been accomplished.¹⁰¹⁻¹⁰³ Several groups have cultured cardiac cells under continuous and cyclic loading conditions to mimic *in-vivo* hemodynamic loading.¹⁰⁴⁻¹⁰⁷ Commercial technologies like Flexercell[®] Strain -FX-4000 Flexercell Tension Plus^(TM) (*http://www. flexcellint.com*), which consists of a flexible membrane on which cardiac cells can be plated and then be subject to oscillatory deflections using a vacuum or pressure source, have been used to apply mechanical stretch.^{96, 108} Electrophysiological studies utilize systems such as the IonOptix Myocyte Systems (*http://www.ionoptix.com*) where cardiomyocytes grown on a glass slide are stimulated with an electrical impulse and analyzed for contractility. However, to the best of our knowledge, no *in-vitro* system currently replicates all aspects of cardiac mechanical loading and unloading in the heart.

2.4. PHYSIOLOGICALLY RELEVANT SYSTEMS FOR CARDIAC CELL CULTURE

Various manifestations of cardiovascular diseases directly correspond to changes in mechanical behavior of cardiac cells. This, in turn, affects cellular phenotype and function, causing changes like hypertrophy, growth of fibrous tissue, and establishment of random cellular orientation.⁶⁹ For example, in hypertension, the pressure inside the

heart exceeds the normal range due to a high resistance in vascular system and eventually results in hemodynamic overloading of the heart and vasculature. This higher intracardiac and transmural pressure triggers myocytes hypertrophy initially and subsequently can lead to a dilated phenotype associated with myocytes loss. In the long term, this additional stretch weakens the heart muscle, causing heart failure.⁶¹ In the contrast, hypotension refers to the condition where the pressure inside the heart is lower than the normal range due to abnormal filling or ejection or where the arterial vasculature is abnormally dilated. This causes reduced blood circulation and oxygen deprivation to the rest of the body. In response to this oxygen deprivation and reduced nutrient delivery, the heart rate increases, resulting in altered stretch and pressure profiles.

The frequency of the loading determines the ranges for normal and abnormal heart function. For example, in human, bradycardia is a condition where the heart rate is lower than 60 bpm, and tachycardia is another condition characterized by a significantly higher heart rate (>200 bpm) in comparison to normal heart rate (~75 bpm). In response to these abnormal patterns, the heart either lowers or increases the systolic fraction.¹⁰⁹ All of these changes can cause the reorganization of cardiac tissue and it can lead to heart failure or sudden death if it persists long term.¹¹⁰

Finally, due to fluid flow, shear stress can be a significant mechanical cue for cardiac endothelial and cardiac smooth muscle cells. Cardiac endothelial cells contribute to the internal lining of the myocardium and are directly exposed to fluid induced shear stress during hemodynamic loading and unloading. Changes in magnitude, frequency, or

duration of shear stress are crucial for the structure, function and permeability of endothelial cells. Various clinical conditions occur as a result of changes to shear profiles seen by cardiac endothelial cells.

Studying cardiovascular disease requires appropriate cellular level platforms which can be used to culture cells while accurately mimicking mechanical and fluidic loading conditions seen *in-vivo*. In cardiovascular disease, various conditions are associated with distinct mechanical loading profiles and replication of those profiles is critical to ensure proper understanding at the cellular and molecular levels. Mechanical loads experienced by cardiac cells vary as a consequence of dysfunction including pressure, stretch and shear stress, as well as the frequency and duration.

2.5. IN-VITRO TECHNIQUES FOR MECHANICAL STIMULATION OF CELLS

Cells in different tissues experience cyclic compressive loads. Cardiac and vascular tissues are examples of tissue where cells within the tissue are constantly under compressive loading. Replicating this condition *in-vitro* can be accomplished using different techniques such as application gas pressure (hydrostatic compression) directly to the culture system or through the fluid induced loading of the system (pressure loading). These techniques cause direct application of pressure to cells in culture mimicking conditions seen *in-vivo*.

Another commonly seen loading condition in cardiac and vascular tissue is cyclic stretch (and strain). The most common approach to stretch the cells in culture is by growing the

cell on a flexible surface and applying stretch on the surface where the cells are attached. The stretch can be uniaxial, biaxial, and include shear. With the uniaxial stretch, the surface is either rectangular or square and is stretched in one direction either longitudinally to both ends, or is bent/flexed in a four-point bending. With the biaxial stretch, the membrane is circular and the edge of the membrane is fixed. The applied pressure deforms the membrane in both the radial and circumferential directions. However, the strain depends heavily on the location on the membrane, causing the cells on different locations to stretch differently. For example, cells seeded at the center will stretch more than those at the edges. As a result, it is extremely complicated to analyze the data and to interpret the cells behavior. To produce the equi-biaxial strain, the membrane has to slide non-frictionally on a stable plane. On this plane, the stress distribution on the area of the membrane where it is supported by the plane, is symmetrical, creating an isotropic and spatially constant strain.

Finally, cells in different tissues experience shear stress as a consequence of fluid flow. Shear stress is a key mediator of cells phenotype. Shear stress controls alignment and establishes cell-cell contacts, which are important in the formation of tight junctions in ensuring low permeability in vasculature. The velocity, as well as the pattern of the flow, laminar versus turbulent flow for example, can create different shear stress on the cells. Also, viscosity of the fluid is another factor that can increase or decrease shear stress on the cells. In cardiac and vascular tissue, all three of these loads (cyclic pressure, stretch, and shear stress) are experienced simultaneously. Additionally, changes in one or more of these loads have a cascading effect on the entire system. Therefore *in-vitro* models of cardiac tissue need to mimic accurately the combined effects of cyclic pressure, stretch and shear in a pulsatile fashion.

2.6. CONCLUSION

Based on the discussion above, due to the complex nature of the heart and the importance of mechanical loads, an *in-vitro* cellular culture model designed with physiological relevance is critical to investigate the cellular and molecular adaption of cardiac cells and tissues relevant to cardiovascular adaption and disease. No device or cell culture platform is commercially available today to accomplish long term culture of cardiac cells *in-vitro* with accurate replication of realistic mechanical loading profiles. Efforts by other groups thus far have succeeded in replicating isolated mechanical loads. There is still a need for platforms where the culture conditions can be dynamically varied not only to replicate normal loading conditions, but also abnormal loading conditions. These platforms are necessary to study the molecular pathophysiology of cardiovascular diseases and in the discovery of drugs, treatment options and cardiac cell regeneration strategies.

CHAPTER 3

THE **µCCCM SYSTEM**

3.1. INTRODUCTION

Understanding the molecular basis of manifestations of cardiovascular disease requires multiscale and multilevel approaches and an appreciation of the developmental mechanisms that regulate cardiac morphogenesis and remodeling. Because cardiomyocyte cell death is the major cause of cardiac pathology leading to heart failure, many efforts are underway to restore cardiac tissue structure and function through regenerative approaches.⁶⁹ Unfortunately, unlike most cells in the body, cardiomyocytes stop differentiation and have limited proliferative potential after birth in higher vertebrates.¹⁰¹ To accommodate, scar tissue replaces the damaged cardiac tissue. Scar tissue increases the stiffness of the heart tissue and cause the inability to regenerate the same contractile forces as the normal undamaged cardiac tissue does. Therefore, cardiac tissue engineering plays a significant role in the process to find better treatment of heart disease due to the loss of cardiomyocytes. However, replicating all aspects of the mechanical loading and unloading environment for the *in-vitro* cardiac cultured cells is a challenging task as discussed in chapter 2. It is because the myocardium experiences passive stretching and pressure build-up during filling (preload) and actively generates mechanical force during ejection (contraction) against variable afterload. Cells in cardiac tissue are under constant physical stimulation and rely on conversion of these cues into

intracellular signals to control cell phenotype and muscle mass during mechanical conditions. Therefore, to study the molecular pathophysiology of cardiovascular diseases, in the discovery of drugs, treatment options, and cardiac cell regeneration strategies, *in-vitro* cardiac tissue must be cultured in the *in-vivo* like environment.

The need for platforms where the culture conditions can mimic the physiologically mechanical condition and can be dynamically varied to normal and abnormal environments necessitates engineers to design different cell culture models. With a primary goal of replicating such *in vivo* mechanical loading conditions for *in-vitro* cardiomyocytes and to enable cardiac tissue generation, a microfluidic cardiac cell culture model (μ CCCM) was developed.¹¹¹ The first generation of the cardiac cell culture model was built in 2008 in order to mimic cyclic mechanical strains and pressures experienced by cells during the cardiac cycle. With this model, cardiac cells undergo cyclic stretch and contraction, pulsatile pressure, as well as fluid loaded and ejected.

3.2. THE µCCCM

The μ CCCM system consists of a peristaltic pump, cell culture chamber, pulsatile actuated collapsible valve, and a tunable resistance in a series, along with accessories including tubing, an oil chamber, a pressure generator, and a digital manometer. (Fig. 3.1)



Figure 3.1: Assembled μ CCCM for cell culture experiment. The tunable valve and collapsible valve were placed downstream of the cell culture platform to create the resistance and pulsatile pressure inside the cell chamber. Cell culture chamber (pink color) was clamped between two fixtures of the cell culture platform. The μ CCCM system has a closed circulating fluid network.

Cells were placed in culture on a thin PDMS membrane attached at the bottom of the cell culture chamber inside the platform. Continuous circulation of culture medium is maintained using a peristaltic pump. Downstream the chamber is a collapsible valve actuated in a pulsatile fashion using a pressure generator. Closure of this collapsible valve leads to pressure build up in the chamber, which in turn also leads to stretching of the thin membrane as well as the cells on this membrane. This stretching phase mimics the diastolic loading phase in the ventricle. To ensure uniformity, a post is placed beneath the thin membrane such that, during stretch, the portion of the membrane on which cells are cultured experiences uniform strain and the edges experience larger non-uniform strain (Fig. 3.2). Lubricating oil fills in the chamber beneath the cell culture area to create friction-free sliding of the membrane on the post. Further, to influence outflow

resistance, a tunable homeostasis valve is placed downstream of the collapsible valve to mimic afterload. Fluid transport and subsequent shear stress can be controlled by varying the pump flow rate. Pressure buildup and strain can be controlled via a combination of factors, including the thickness of the membrane, fluid flow rate, and operation of both valves



Fluid loading induced pressure

Figure 3.2: Setup design for equi-baxial strain. A significant deformation at the edges of the membrane occurs when the pressure is applied, but the area of the membrane rested on the post has the same radial and circumferential strain.

3.3. FABRICATION AND ASSEMBLY OF THE µCCCM

3.3.1. Assembly for Housing the Cell Culture Platform and the µCCCM components

The assembly for housing the cell culture platform was fabricated in the Rapid Prototyping Facility at the University of Louisville using Computer Numerical Control (CNC) Milling Machine. The designs were laid out using Solidworks 3D layout software prior to machining the assembly using CNC milling. Acrylic was used for construction. (Fig. 3.3)



Figure 3.3: Schematic representation of the top and bottom fixtures of the platform for housing the cell culture chamber. [A] The top fixture has the fluid inlet and outlet accesses; [B] The bottom part of the platform has two rectangular holes at the center.

The cell culture chamber (~1cm diameter) and oil chamber were made from polydimethyl siloxane (PDMS) (Dow Corning, ratio 1:10 of the curing agent and the base) using standard soft-lithography techniques. The collapsible valve was created mainly via thin elastic ARGYLE Penrose tubing. More detail information for these fabrications will be seen in the published article.¹¹¹

3.3.2. Assembly of the µCCCM

First, an acrylic sheet was placed in the rectangular hole on the bottom piece of the platform, followed by the oil chamber (Fig.3.4). Then, the cell culture chamber, with 18G needle inserted, was aligned on top of the oil chamber. The top piece of the platform was then laid on top of the cell chamber. The platforms were tightened with four screws. Finally, low viscosity oil was injected into the oil chamber through needles.

A 3-stop Pharmed BPT tube (1.3 mm ID, Cole-Parmer, Vernon Hills, IL) was connected from a 50 mL medium container to the inlet of the device via a peristaltic pump (Ismatex, ISM 596D, Vancouver, MA). The collapsible valve was connected from the outlet of the device to the medium container. The tunable valve was placed downstream of the collapsible valve (Fig.3.1.). Finally, the pressure sensor was connected to the needle, which was connected to the cell chamber. A pulsatile pressure generator was connected to the bottom T of the collapsible valve.



Figure 3.4: Assembly of the cell culture and oil chambers between the platforms.

3.4. OPERATION OF THE µCCCM

Once assembled as in Fig. 3.1, the peristaltic pump was started gradually from a low flow rate to the desired flow rate. After 30 min running, the pressure in the pneumatic pressure generator source was applied and the tunable valve was adjusted until the pressure reached the desirable values. Variable parameters, such as the frequency of the membrane stretching as well as the percentage of systolic phase per one cycle, were determined based on the requirement of each experiment. The frequency of the stretching was controlled through the % systolic and the frequency controls on the

pressure generator source. The pressure inside the cell chamber was varied by the corroboration between the pressure applied on the collapsible valve and the adjustment of the tunable valve. The stretching level of the membrane was determined by the thickness of the membrane, which were measured and standardized appropriately and the pressure applied on the membrane. And the shear stress on the cells was controlled by the velocity of the fluid loading and the dimension of the cell culture chamber.

3.5. APPLICATIONS

3.5.1. Pressure profiles

The device was assembled and the pressure build-up within the chamber was generated for the following clinically relevant experimental conditions – normal, heart failure, hypertension, hypotension, tachycardia, and bradycardia. To accomplish pressure monitoring within the chamber, a high-fidelity pressure catheter (Millar Instruments, Boston, MA) was inserted through a hemostatic valve and syringe needle such that the pressure sensing element resided in the center of the chamber. The chamber pressure waveforms were analyzed by using a Hemodynamic Evaluation and Assessment Research Tool program developed in Matlab (MathWorks, Natick). The different waveforms for various physical heart conditions were therefore replicated and recorded by either increasing or decreasing the pressure in the pressure generator and by adjusting the tunable valve (Fig. 3.5). These results confirmed that the μ CCCM enabled to regenerate various clinically relevant physiologic conditions of the heart.



Figure 3.5: Pressure waveforms that simulate various physiologic conditions in the μ CCCM. These conditions include both normal and dysfunctional myocardium, such as heart failure, hypertension, hypotension, bradycardia, and tachycardia.

3.5.2. Cell studies for the proof-of concept

 H_9C_2 cells were cultured within the μ CCCM system to demonstrate the proof-of-concept. H_9C_2 cells were cultured in static condition (control) and within the μ CCCM under pulsatile pressure and stretch, representing normal physiological loading (peak pressures of 120 mm of Hg, strain of 20% and a frequency of 80 bpm with 50% systolic to diastolic, flow rate of 8.4ml/min) for 24 h at 37°C and 5% CO₂. More detail of cell culturing is available on the published article.¹¹¹

The results showed that cells not only survived physiological loads but also showed the positive effects of physiological loading. Cells cultured in static condition (control) attained a fibroblast like morphology (Fig. 3.6a), whereas cells cultured in the μ CCCM were more rectangular, and presented a postage stamp-like morphology (Fig. 3.6b). The size of the cells cultured within the μ CCCM exposed to pressure was larger than those cultures in static condition.

Staining with Phaloidin showed a low intensity fluorescent color and random orientation of f-actin in controls in comparison to aligned f-actin in cells cultured with pulsatile pressure and stretch (Fig.3.6c and d). This indicated that the contraction-stretching of the cells promotes the increasing % of f-actin and also an increase in the length of the sarcomere, and helps to align the cells in one direction. The increase in the length of the sarcomere is the result of the increase in contraction of the cell under pulsatile stretch. The alignment of the cells demonstrated that mechanical loading spontaneously rearranged the orientation of the cells.

P-phospholamban was detected in cells cultured within the μ CCCM, however, the expression of this protein was very low in cells cultured in static condition, as shown is Figure 3.6e, in comparison to the cells cultured in μ CCCM (Fig. 3.6). Phospholamban is the integral membrane protein. To respond to the contraction of the cells, phospholamban is phosphorylated. With cAMP, this p-phospholamban promotes the influx of Ca²⁺ into the cells to bind to the contractile unit, causing the cells to contract.^{112, 113} Therefore, indirectly, the increasing of activation of p-phospholamban, which was reflected by the intensive green color on the loading sample, in comparison of the color on the control sample on the Fig. 3.5.e and f, will be indicative of cell contraction.



Figure 3.6: Physiological loading promoted the alignment of f-actin and increased phosphorylated phospholamban activity in H_9C_2 cells. Cells were under a static condition (control) and normal physiological loading for 24 hrs. Notice the directional alignment of f-actin stress fibers and increased p-phospholamban activity in the loading condition. (a, b) Phase contrast images; (c, d) Staining with TRITC-conjugated Phaloidin

for detection of f-actin; (e, f) Immunofluorescence staining for detection of pphospholamban activity; (g, h) Merged images of F-actin and p-phospholamban.

The proof-of-concept demonstrations using the μ CCCM system for cardiac culture were accomplished, confirming that this system has the ability for the design and study of various conditions with different cell types associated with CVD. These studies can be cardiomyocyte regeneration using mechanical loading and stem cells, adult cardiomyocyte regeneration using controlled mechanical loads, study of cardiac and aortic endothelial cells under conditions of continuous and pulsatile flow ^{114, 115} and finally, evaluation of drugs and other treatment options using cardiac cells maintained under various disease conditions.

3.6. CONCLUSION AND LIMITATIONS

Microfluidics based systems have been used to create cardiomyocyte actuators and pumps as well as cell models.^{102, 116-121} The μ CCCM was the first system, to our knowledge, that was developed to replicate the mechanical loading conditions observed in the heart, which includes the fluid flow, pulsatile stretch, and pressure. The μ CCCM allowed dynamic studies accomplished via the direct manipulation of flow rate, valve operation, membrane thickness and the height of the cell culture chamber. We envisioned that this system would provide time varying mechanical cues for differentiation of stem/progenitor cells into adult cardiomyocytes and would also provide mechanical conditioning to generate sufficient contractile forces and integrate within native cardiac tissue to augment cardiac function. However, after re-examining carefully

the working principles of this system, we recognized that the pressure-volume relationships seen this in vitro system did not accurate replicate in vivo left ventricle PV relations. First, *in-vivo*, the stretch of nature cardiac tissue is mainly due to the fluid loading during the loading phase, while the stretch of the PDMS membrane in the μ CCCM is based on the pressure generated inside the cell chamber during the loading phase. Second, the stretch and contract of cardiomyocytes are in 3D directions, which include circumferential and radical stretch. With the post, this μ CCCM system creates the 2D biaxial stretching. In addition, in this model, the cells were seeded on a rigid 2D surface membrane which potentially constrained cell shortening and does not reflect the physiological condition of the *in-vivo* tissue. The summaries of similarities and differences between the left ventricle and the μ CCCM system are listed on the table 3.1. To overcome these shortcomings, the second generation of the cardiac cell culture model (CCCM) was designed and developed. In this new system, cells were cultured on a soft matrix attached to the top of a thin PDMS membrane in a cell culture chamber. With each cycle, cells cultured within the CCCM underwent passive stretch, isovolumic contraction and pressure buildup, ejection and relaxation. Thus, the second generation of cardiac cell culture model system is essentially a left ventricle mimic that can be dynamically tuned to go from static unloaded state (as seen in very early development), to pulsatile pressure and cyclic stretch conditions seen in the adult heart.

<u>**Table 3.1:**</u> Summary of similarities and differences (*in italic*) between the left ventricle and the μ CCCM system

Aspects	Left Ventricle	The µCCCM system
Working principles	- "Filling" phase: fluid in, no fluid out, <i>no pressure buildup</i> .	- "Stretching" phase: fluid in, no fluid out, low <i>pressure buildup</i> .
	- Isovolumic contraction phase: pressure inside is compressed, <i>no fluid in nor out.</i>	- Contracting phase: pressure inside is released, <i>fluid in and out</i> .
	- Ejecting phase: cavity pressure exceeds aortic pressure, <i>pressure peaks and then begins to decline.</i>	- Ejecting phase: the releasing of the collapsible valve- <i>pressure inside released and goes down</i> .
	- Isovolumic relaxation phase: muscle relaxes and pressure decreases prior to the next filling cycle.	- Relaxing: similar to ejecting phase
Circulation network	- One way valves at the entrance and outlet of the ventricle	- Only one collapsible valve downstream of the chamber, and the fluid continuously loaded to the cell chamber.
Stretching	- 3 dimensional strains	- Biaxial stretch
Cell cultured	- Soft tissue	- Hard surface

CHAPTER 4 THE SECOND GENERATION CCCM SYSTEM

4.1. COMPONENTS OF THE SECOND GENERATION CCCM SYSTEM

The Second Generation CCCM system consists of a fluidic flow pathway, an air pathway, a cell culture platform station, and a control system (Fig. 4.1).¹²²

The fluid flow network includes a medium reservoir, a peristaltic pump, a fluid compliance, an upstream one-way valve, a cell culture platform station, a downstream one-way valve, and a tunable pressure relief valve in a series (Fig.4.1). From the medium reservoir, via the assistance of the pump, the fluid flows through the upstream one-way valve into the cell culture chamber and exits the cell culture chamber. The fluid then passes through the downstream one-way valve and the tunable valve and then returns back to the reservoir before being recycled within this flow loop via the peristaltic pump. A bypass with a spring valve was installed at the downstream pathway to prevent the chamber pressure from exceeding the pressure range set up for each case of studies.

While the fluid network is a closed pathway, the air network is a partially closed pathway. The air network includes the cell culture platform station, an air-compliance, a pneumatic valve, and a pneumatic pressure driver (Fig. 4.1). Air from the driver enters

the cell culture platform station and passes through the air compliance and the pneumatic valve before returning to the pneumatic pressure driver. This air network is a partial closed network because the pneumatic valve is a three-way valve. One of its three ports releases air to the outside when needed.



Figure 4.1: A schematic image of the second generation CCCM system. [A] 2 pathways are described: fluid pathway and air pressure pathway. [B] Picture of the CCCM system

where (a) the peristaltic pump, (b) upstream one-way valve, (c) the CCCM platform with cell culture chamber (arrow) and (d) the downstream one- way valve.

The cell culture platform station includes a cell culture chamber, an oil chamber, and the housing station (Fig. 4.2). The cell culture and oil chambers are placed on top of each other and in between the top and bottom plates of the housing station. Cells are cultured on a thin flexible PDMS membrane, which forms the base of the cell culture chamber and is thus sandwiched between the cell culture and oil chambers. This cell culture membrane deforms as fluid is loaded and unloaded to the chamber, applying cyclic stretch and relaxation to the cells. Underneath of the oil chamber is a post membrane. Therefore, the cell culture system is a chamber-membrane-chamber-membrane stack (Fig. 4.2.C). The oil chamber transfers the displacement between the cell culture membrane and the post membrane (Fig. 4.2.E). The post membrane prevents the cell culture membrane from moving beyond its original position when the pneumatic pressure is applied on the other side of the post membrane (Fig. 4.2F). Finally, the housing station has top and bottom plates to sandwich the cell culture and oil chambers and to install the fluid and air networks. The top plate of the housing station has an inlet and outlet ports for fluid loaded and unloaded to the cell culture chamber while the bottom plate has the inlet and outlet ports for the air from the air pathway in and out of the station.



Figure 4.2: Scheme of the CCCM cell culture platform station. [A]: the housing station has (a) top plate with fluid inlet (solid arrow) and outlet (breakdown arrow) and (b) bottom plate with air inlet (solid arrow) and outlet (breakdown arrow). [B]: the assembled CCCM chambers. The assembled CCCM is sandwiched between plates of the station. [C]: the components of the assembled CCCM chambers: (i) cell culture chamber, (i) a flexible membrane where the cells are seeded (blue), (iii) oil chamber, and (iv) the post membrane. The assembled CCCM system is a chamber-membrane-chamber-membrane stack. [D] Side view of the CCCM cell culture station: (i) top plate with fluid inlet (solid arrow) and outlet (breakdown arrow); (ii) cell culture chamber; (iii) cell membrane (orange); (iv) oil chamber made by 3 components (top, middle, and bottom)and filled with oil, and (v) the post membrane (black color) bottom plate with air

inlet and outlet. [E] The scheme of membrane deformed when fluid is loaded to the cell chamber. This case, oil in the oil chamber transfers the displacement between the cell culture membrane and the post membrane, pushing the post membrane down (breakdown bar). [F] Cell membrane goes back to its original position when the pneumatic pressure is applied on the other side of the post membrane. Due to the block from the bottom component of the oil chamber, the post membrane cannot move up further than its original position, preventing the cell culture membrane from moving beyond its original position.

Fluid flows into the cell chamber, deforming the membrane downward. The pressure driver provides cyclic pressure on the other side of the post membrane, pushing the deformed polymer membrane back to its original position. Releasing this pressure stretches down the cell culture membrane during the fluid loading phase (Fig. 4.3). The frequency of this pressure as well as the percentage of loaded and unloaded time per each cycle is controlled by the program set in the pressure driver.



Figure 4.3: Scheme of the PDMS membrane deflection under the influence of fluid and pneumatic pressure loading and unloading. [1, lower left] PDMS membrane in the phase

where no fluid filled into the cell culture chamber, the membrane has a horizontal position with no stretch. [2, lower right] the membrane deforms downward when fluid flows into the chamber from above (arrows down), [3, upper right] the membrane is pushed back to its original horizontal position when outside pressure applied to the inferior side of the post membrane, pushing the cell membrane up (arrows up); and [4, upper left] after ejection occurs the membrane is returned to its original position and one cycle of stretching-relaxing is completed.

The volume of the fluid loaded to the cell chamber is controlled by the peristaltic pump. Cyclic pressure inside the cell culture chamber is generated via the tunable pressure release valve and the pneumatic pressure inserted on the other side of the post membrane. The frequency and the air pressure loaded and unloaded to the station are controlled by the pressure generator. Finally, a pressure sensor connected to the cell culture chamber is monitored via real-time LabView program; and the pressure waveform inside the cell culture is hence recorded (Fig.4.4).


Figure 4.4: Image of the CCCM system connected to the LabView control system via pressure sensor.

4.2. DESIGN AND FABRICATION OF DIFFERENT COMPONENTS OF THE CCCM SYSTEM

4.2.1. Design the Top and Bottom Plates of Cell Culture Housing Station

The cell culture station was made in the Rapid Prototyping Facility at the University of Louisville using the Computer Numerical Control (CNC) Milling Machine. The designs were laid out using SolidWorks software prior to machining the assembly using CNC milling. Acrylic was the material used for construction.

This station consists of the top and bottom rectangular plates (10.5 cm x 9.0 cm x 1.3 cm) (Fig. 4.5). Two channels in the top plate serve as the entry and exit ports for fluid loading and unloading to the cell culture chamber. The distance between two inner ends of these channels is 0.6cm. The bottom plate of the platform has a circular hole (d =1.6 cm, h = 1.0 cm) at the center and 2 horizontal passages from the center hole to the outside

edges (l = 4.6 cm, d = 0.4 cm), creating the inlet and outlet air channels. Finally, 4 holes were drilled at 4 corners of these components for screw insertion.



Figure 4.5: Schematic of the top and bottom plates of the station for housing the cell culture chamber. [A] the top plate of the platform with entry and exit ports for fluid loading and unloading; and [B] the bottom plate of the platform with a circular hole at the center and two horizontal passages for pneumatic pressure pathway.

4.2.2. Fabrication of the thin PDMS membrane

The thin PDMS membrane was made from Sylgard[®]184 polydimethyl siloxane (PDMS) (Dow Corning, Midland, MI) using standard soft-lithography techniques. First of all, a mixture of silicon elastomeric base with its curing agent (ratio 10:1) was well mixed, followed by a 15 minute vacuum to remove air bubbles created during the mixing

process. To make a thin PDMS membrane less than 400µm thick, spinning method was used and the thickness of the membrane was determined by the spinning speed and time (Fig. 4.6). The degassed PDMS mixture was poured on a non-oxidized silicon wafer (0.525 mm thick, 100 mm diameter, Silicon Valley Microelectronics, Inc. Santa Clara, CA) and spun at a desire speed for 30 sec on a Headway Spinner (Brewer Science, Inc., Rolla, MO). The PDMS coated wafer was then baked at 90°C in an oven (Fisher Isotemp, Florence, KY) for at least 1 h. Once the PDMS was cured, the wafer was removed from the incubator. This method was used to make the post membrane.



Figure 4.6: Graph of PDMS membrane thickness (μ m) versus spinning speed (rpm). The spinning time is 30 sec. The membrane thickness as a function of spinning speed can be estimated using the equation y= 130728 x^{-1.05.}

For the PDMS membrane thicker than 400μ m, gasket method was used. Basically, the degased PDMS was poured to a square gasket (13.0 cm x 13.0 cm outside and 12.0 cm x

12.0 cm inside) sitting on a square glass (13.0 cm x 13.0 cm). The thickness of the gasket determines the membrane thickness. A thin transparent plastic sheet was then slowly placed on top of the PDMS mixture followed by another square glass. The whole setup was clamped tightly with paper clips and was put in the 90°C oven (Fisher Isotemp, Florence, KY) for being cured overnight to form a thin PDMS sheet (Fig. 4.7.). This method was applied to create the PDMS membrane at the bottom of cell culture chamber.



Figure 4.7: Fabrication steps of making a thin PDMS membrane via the gasket method.

4.2.3. Cell culture chamber and medium reservoir

For the cell culture chamber, the degassed PDMS mixture (10:1 ratio) was poured in a mold until it reached 1.0 cm high. After being cured at 90°C in the oven, the molded PDMS was removed from the container and a square piece of PDMS (3.0 cm x 3.0 cm x 1.0 cm) was cut (Fig. 4.8). A hole (d = 1.4 cm) was punched at the center of this PDMS piece using a cork borer. Finally, a thin PDMS cell membrane, which was previously made, was placed at the bottom of this PDMS to form the cell culture chamber.

To provide medium for cells cultured before placing them to the CCCM system, a medium reservoir was also created. A hollow PDMS square piece (2.5 cm x 2.5 cm outside and 2.0 cm x 2.0 cm inside) was cut from the molded PDMS (Fig.4.8). This reservoir was then placed on top of the cell culture chamber before sterilization.



Figure 4.8: Fabrication steps involved in construction of the cell chamber and the medium reservoir.

To measure the pressure inside the cell culture chamber, an accessible pressure chamber was created. The molded PDMS slack was cut (3cm x3 cm) and a center hole was punched, similar to the cell culture chamber. A horizontal channel was then created from the center hole to the edge via an 18 gauge blunt syringe needle (SmallParts, NE181PL-C). Finally, a 24 gauge blunt syringe needle (SmallParts) was inserted to this horizontal channel, served as a connecting port for the pressure sensor (Fig. 4.9.).



Figure 4.9: Schematic representation of fabrication steps involved in construction of the assessable pressure chamber.

4.2.4. Oil chamber

The oil chamber was built in a mechanical shop Facility at the University of Louisville. Three square acrylic pieces were cut and a circular hole was grilled at the center of each piece. The dimensions of each squares acrylic pieces were in the table 4.1 below. The edges of these pieces were smoothed before these pieces were glued together respectively to form the oil chamber. (Fig. 4.10, left)

Components	Thickness	Sauara dimonsions	Hole diameter
Components	THICKNESS	Square unitensions	more utallieter
_		-	
Ton component (i)	0.2 orm	$4.0 \text{ on } \times 4.0 \text{ on}$	1.2 om
Top component (1)	0.5 Cm	4.0 CIII X 4.0 CIII	1.5 CIII
Middle common ant (ii)	1.0 am	10 on $x 10$ on	25 and
Middle component (II)	1.0 Cm	4.0 CIII X 4.0 CIII	2.5 CIII
Dattam ageneration of (iii)	0.2	10 area v 10 area	2.0 area
Bottom component (III)	0.5 cm	4.0 cm x 4.0 cm	2.0 cm
· · · · ·			

Table 4.1: Dimensions of each component of the oil chamber



Figure 4.10: Schematic images of the oil chamber. [A] The oil chamber (top) and the post membrane (bottom). [B] Side view of the oil chamber: top component (i), middle component (ii), bottom component (iii) and the post membrane (black). Oil chamber is filled with oil. PDMS cell culture membrane (dark blue) is placed directly on the top of the component (i).

4.2.5. Fabrication of the post membrane

A thin 400 μ m PDMS (4.0 cm x 4.0 cm) previously made on a silicon wafer was peeled off. This thin PDMS membrane and a circular glass (d = 2.5 cm, t = 0.25 cm) were exposed to 10% oxygen plasma for 30 sec in a reactive ion etcher system (RIE March Instruments) with 150 mmTorr and 150 mmHg. The membrane and circular glass were then bonded together centrically and irreversibly to form the post membrane (Fig.4.11.). Finally, the subject was heated at 115°C on a hotplate (Standard Model 1100 Hotplate, Brewer Science, Inc., Rolla, MO) for 10 min to enhance the quality of bonding.



Waver coated with PDMS

Figure 4.11: Schematic representation of fabrication steps involved in construction of the post membrane.

4.3. ASSEMBLY OF THE WHOLE CCCM SYSTEM

4.3.1. Assembly of the cell culture platform

The cell culture platform was assembled in a sandwich style. In general, the post membrane, oil chamber, cell culture chamber, and pressure chamber were stacked on top of each other respectively and clamped between two fixtures of the apparatus. In detail, first of all, the oil chamber was firmly laid on the top of the post membrane to form a unit; and oil was used to fill this oil chamber. Secondly, after the reservoir on the top of cell chamber was removed, the accessible pressure chamber was placed on top of the cell culture chamber to form cell chamber unit. This unit was then placed centrically on top of the oil chamber without creating air bubble inside the oil chamber. Thirdly, these stacked membranes-chambers were placed on top of the bottom component followed by the top fixture. Finally, screws were used to tighten the components. (Fig. 4.12)



4.3.2. Connection of the cell culture platform to the CCCM system

The assembled cardiac culture platform was then connected to the flow loop and cyclic pressure network as shown on Fig. 4.2. First, a 50 mL tube served as the medium reservoir to supply fluid to the cell chamber and to receive fluid flowing back from the cell culture chamber via a peristaltic pump, ensuring a continuous supply. Fluid compliance and a one-way valve were connected to the upstream of the fluid flow

network. A one-way downstream valve, tunable valve, and a by-pass pathway with a pressure gate valve were installed at the down-stream of this flow loop. Flexible, autoclave compatible polymeric tubing was used to establish connections within the flow loop (Fig.4.13). Second, the pressure sensor was attached to the cell culture chamber via the needle port of the pressure chamber. Third, the air compliance was attached to the apparatus.

This whole set up was then moved to the incubator before the pneumatic pathway was connected to the platform. Once in the incubator, the air compliance was connected to downstream of the pneumatic pathway, while upstream of the airway was hooded to a pulsatile pneumatic pump (lb Engineering GbR). Finally, the pressure sensor was connected to the computer; and the pressure inside the cell culture chamber was transferred digitally to the LabView Program on the computer.



Figure 4.13: Picture of the CCCM experimental setup.

4.4. WORKING PRINCIPLES OF THE CCCM SYSTEM

The working cycle of the CCCM mimics the working cycle of the left ventricle (Fig. 4.14). In the filling phase, fluid flow is introduced continuously into the CCCM cell culture chamber via the peristaltic pump. Fluid fills the cell culture chamber causing the PDMS membrane to stretch passively. The stretching of the membrane maintains the pressure inside the cell culture chamber as low as the base pressure should be. This stretching phase mimics the left ventricular diastolic filling. During the isovolumic contracting phase, air pressure generated by the pulsatile pneumatic pump (the frequency and pressure are programed based on each specific experiment) is applied to the reverse side of the post membrane, pushing the PDMS cell membrane back to its original position. Pressure is thus built up rapidly within the cell culture chamber, causing the upstream one-way valve to close. Because of this valve closure, the fluid from the peristaltic pump begins to be stored in the fluid compliance. However, the cell chamber pressure at this point is not high enough to overcome the downstream resistance, therefore, no fluid is loaded or unloaded to the chamber. This phase is similar to the isometric contracting phase inside the left ventricle. For the ejecting phase, the pressure inside the cell chamber increasing until it exceeds the set value of the resistance to open the downstream valve and then the accumulated fluid loaded in the cell culture is ejected. Finally, the pressure applied to the reverse side of the membrane is released, causing the CCCM to undergo isovolumic relaxation before another cycle begins. This phase mimics the isometric relaxing phase of the left ventricle.



Figure 4.14: A working cycle of the CCCM system and the pressure-volume loop occurred in left ventricle of the heart. [A] Schematic working principles of the CCCM system, including stretching phase (fluid loading causes the membrane stretched down), contracting phase (pneumatic pressure applied to the other side of the membrane brings the membrane back to the original position and elevates the chamber pressure), ejecting phase (chamber pressure overcomes the downstream resistance to eject the fluid out of the chamber), and the relaxing phase (no fluid in or out). X: valve is closed; \blacklozenge : fluid direction. [B] Pressure-Volume loop seen in the left ventricle: (a) diastolic filling phase, (b) isovolumic contraction phase, (c) ejecting phase, and (d) isovolumic relaxation phase.

Additionally, a programmable pressure generator is used to supply periodic pulses of pressurized air to the reverse side of the polymeric membrane on which cells are cultured to mimic ventricular contraction. Finally two tunable compliance elements, a fluidic compliance integrated prior to the upstream one-way valve, and air compliance element integrated at the end of the pressure generator flow path, are used to modulate pressure waveforms within the cell culture chamber. Therefore, with the pulsatile pneumatic

pump, the frequency of the stretching-contracting of the PDMS cell culture membrane is controlled; and the cylclic pressure inside the cell culture membrane is also generated, similar to the cyclic pressure seen in the left ventricle.

4.5. OPERATION OF THE CCCM SYSTEM

The assembly of the CCCM system was performed inside the cell culture hood. Once the CCCM platform station and the fluid network were assembled as in Fig. 4.13, the whole set up system was moved into the cell incubator. Then, the peristaltic pump began to run, followed by the connection of the air network to the pressure generator, which had been on. Along with the controlling from the pressure generator, the downstream tunable valve was adjusted until the pressure reached the desirable values. Variable parameters, such as the frequency of the membrane stretching as well as the percentage of systolic phase per one cycle, were determined based on the requirement of each experiment. The frequency of the stretching was controlled through the systolic time and the frequency control on the pressure generator source. The pressure inside the cell chamber was varied depending on the pressure applied on the post membrane and the adjustment of the tunable valve. At the end of the experiment, peristaltic pump was turned off first followed by the pressure generator. Finally, the cell chamber was removed from the platform.

4.6. CONCLUSION

Recognizing the limitations of the 1^{st} generation μ CCCM model, the second generation CCCM system was created to more accurately reproduce the mechanical loading and

unloading conditions observed in the heart. This system is capable of accurately mimicking preload and afterload experienced in the healthy and failing heart. The CCCM allows for dynamic studies, accomplished via direct manipulation of flow rate, valve operation, membrane thickness and the height of the cell culture chamber. When working with different types of cardiac cells or different physiological heart conditions, it is important to ensure that the type of mechanical loads delivered such as the stress, stretching, frequency of stretching, and the shear stress can be dynamically controlled. The following chapter therefore focusses on the characterization of this CCCM system.

CHAPTER 5

CHARACTERIZATION OF THE CCCM SYSTEM

5.1. YOUNG'S MODULUS OF THE THIN PDMS MEMBRANE

5.1.1. Introduction of PDMS

Polydimethyl siloxane (PDMS) is a common silicon rubber used for various applications such as mechanical interconnective layers between 2 wafers, mechanical-chemical sensors, microvalves in fluid applications, and biomedical applications.¹²³⁻¹²⁵ PDMS Sylgard 184 from Dow Corning Corporation (Midland, MI) is one of the two most common silicone products. It contains a base polymer and curing agent. Cross-linking reaction is the main reaction for the curing of PDMS; and this curing process is enhanced via heating process.¹²⁶ Therefore, the PDMS rigidity can be controlled by the ratio between its base and cross-linking agent, the heating temperature and the time of baking.

PDMS is a substrate widely used for cell behavior studies due to several advantages. PDMS is biocompatible, transparent, gas permeable, autoclavable, and elastic. This silicone is also physically and chemically stable.¹²⁷ It has a high flexibility and compressibility, suitable to use for making a thin stretchable membrane in the CCCM system. The fabrication of PDMS membrane is straight forward, less time consumed, and cost effective, making it suitable for replication.¹²⁵ PDMS is also hydrophobic; and yet, via oxygen plasma treatment, it becomes hydrophilic for a few minutes before going back to its original hydrophobic state.¹²⁶ This special chemical characteristic of PDMS helps different PDMS layers bond to themselves and therefore creating a watertight seal between layers of the CCCM culture chamber when the PDMS becomes hydrophobic.

In this project, Young's modulus and strain value of the thin PDMS sheet used in the CCCM system were determined. Due to the fact that this thin PDMS membrane is an elastomer and has the ability to hold a large amount of strain, true stress σ^* and true strain ϵ^* were determined from the engineering stress σ and strain ϵ of the PDMS membrane. Young's modulus E of the thin PDMS membrane under the tensile force was obtained by the following equations: ^{127, 128}

$$\sigma = \frac{F}{A_0} \text{ and } \varepsilon = \frac{\Delta L}{L_0}$$
(1)
$$\sigma^* = \sigma(1+\varepsilon) \text{ and } \varepsilon^* = \ln(1+\varepsilon)$$
(2)
$$E = \frac{\sigma^*}{\varepsilon^*}$$
(3)

where F is the tensile force applied onto the membrane, A_0 is the original cross-sectional area, ΔL is the elongation of the membrane after stretched, and L_0 is the original length of the membrane.

5.1.2. Tensile test

The RSA III Rheumatics System Analyzer was used for the PDMS tensile tests. First, the fabricating method for the thin PDMS sheet was described from section 4.2. The ratio of mixing between the base and curing agent was 10:1. The curing temperature was set at 90°C and the baking time was from 12 h or overnight. After cured, this thin PDMS

sheet was cut into strips (0.5 inch x 4.0 inches) and vertically mounted in the way that one end of the strip was attached to a fixed fixture while the other end was clamped to a movable fixture of the RSA Analyzer (Fig. 5.1). Zero force was initialized and the tension force was applied. The membrane was pulled slowly with the rate of 0.5 mm/s until it reached a 50% displacement (2 inches). Three different thicknesses of PDMS membranes (250 μ m, 400 μ m, and 500 μ m) were used. At least five different PDMS pieces molded on different days with the same thickness were made for this tensile test. The excel program was used to determine the stress, strain, and Young's modulus of the PDMS.



Figure 5.1: Experimental setup image for the strain and Young's Modulus measurement of PDMS membranes. Left: The PDMS strip (arrow) was installed between 2 fixtures of the RSA Analyzer. Right: Sketch of the displacement of a thin PDMS strip.

5.1.3. Results and Discussion

The mechanical properties and Young's modulus of different PDMS thicknesses were determined. Young's modulus of the PDMS depends greatly on the stress-strain curve, mixing ratio and strain rate.¹²⁷ For consistency, the mixing ratio of 10:1 (base: curing agent) was carried throughout this project. Tensile tests on the PDMS membrane were conducted. During the testing process, the elongation of the strips and the tensile forces were recorded automatically by the system. By loading the dimensions of the PDMS strip to the system, the engineering stress and the engineering strain were obtained. Since the PDMS is an elastomer and has a capacity to hold a large amount of strain, the true stress and true strain derived from engineering strain were used to calculate the elastic modulus of the PDMS (Fig. 5.2.) The results shows that with the PDMS thickness from 250 µm to 500 µm, Young's modulus and stress-strain relationship were not significantly different among each membrane thickness. The Young's modulus of the thin PDMS membrane was calculated using the equation (3) in the section 5.1.1, which was around 1.0 ± 0.17 MPa. The graph of stress vs strain and Young's modulus value agree with the results obtained from other research groups.¹²⁶⁻¹²⁸ These results were helpful to assist the fabrication of various membranes with different thicknesses for cardiac culture. Amongst these three membrane thicknesses, membrane with the thickness of 500 µm was used for cardiac tissue cultured in the CCCM system later.



Figure 5.2: Graphs of stress versus strain of thin PDMS sheets

5.2. PRESSURE GENERATED INSIDE THE CCCM CELL CHAMBER

A synergistic relationship exists between the pump flow rate, membrane thickness, downstream resistances and the magnitude of pressure pulses within the CCCM. All these parameters need to be set precisely to ensure proper filling and ejection of fluid from the cell culture chamber and mechanical stresses. The pressure waveform generated from the CCCM cell culture chamber was determined by the pressure input from the pulsatile pneumatic pump, frequency, flow, percentage between the stretching and contracting phases of each cycle as well as the downstream resistance. These variable parameters were determined and adjusted based on the requirement of each experiment. The frequency of the stretching was controlled by the frequency set up on the pressure generator. The pressure inside the cell chamber was mainly varied by the cyclic pressure applied on the post membrane and the adjustment of the tunable valve. For the proof of concept, the profile of pressure wave forms for different human heart conditions (normal, hypertension, hypotension, heart failure, bradycardia, and tachycardia)¹¹¹ seen in the left ventricle of human heart were generated inside the cell culture chamber of the CCCM system. (Table 5.1 and Fig.5.3.) This accomplishment indicates that this CCCM system can be a benefit for *in-vitro* cardiomyocyte studies under the effect of physiological mechanical relevance of different heart conditions.

Table 5.1: Hemodynamic parameters corresponding to the left ventricular mechanical loading during various clinical conditions were replicated using the CCCM system. These parameters include heart rate, systole as percent of the cardiac cycle, end systolic pressure, and end diastolic pressure of the left ventricle were applied to the CCCM system to obtain the pressure waveforms in the following figure 5.3 below. LV (left ventricle).

Conditions	Heart Rate (bpm)	Systolic Fraction (%)	LV systolic pressure (mmHg)	LV end diastolic pressure (mmHg)
Normal	75	40	125	9
Hypertension	75	40	183	6
Hypotension	75	40	95	6
Heart Failure	75	40	100	27
Tachycardia	200	50	120	4
Bradycardia	46	40	124	8



Figure 5.3: Pressure vs time plots representing the changes in pressure within the CCCM cell culture chamber for different human heart conditions. The parameter of the pressure and frequency were determined based on different conditions seen in the left ventricle of the human heart.

5.3. STRAIN OF THE PDMS CELL CULTURE MEMBRANE

As the cell type changed from H9C2 cells to embryonic chick ventricular cardiomyocytes as the primary cell line for characterization of the CCCM chamber, we set the CCCM strain to replicate the strain of the *in-vivo* chick embryonic left ventricle cardiomyocytes at stage of 36; which is reported to range from 0.10 to 0.20. ^{129, 130} For *in-vitro* CCCM culturing, strains of 8-15% were applied.

When fluid was induced to the cell culture chamber, PDMS experienced both radial and circumferential stretches (Fig. 5.4). These stretches of the PDMS membrane were also conveyed to the cells seeded on that membrane. Both strains were determined via the simulation from the ANSYS software program as well as via experimental membrane deflecting movies obtain from a Ultra Sound system.



Figure 5.4: Scheme for the stretches of the circular membrane

5.3.1. Membrane Deflection Strain measurement via ANSYS program

The following formulas were used for calculation:

• Mooney- Rivlin strain energy (5 parameters) for hyper-elastic material (PDMS)

$$\Psi = C_{10}(T_1 - 3) + C_{01}(T_2 - 3) + C_{11}(T_1 - 3)(T_2 - 3) + C_{20}(T_1 - 3)^2 + C_{02}(T_2 - 3)^2 + (1/d)(J - 1)^2$$
(4)

 $C_{10}, C_{01}, C_{20}, C_{11}, C_{02}$ = material constants

d = material incompressibility parameter

 T_1, T_2, T_3 = invariants of the right Cauchy-Green deformation tensor

• Volume:

$$V = \frac{1}{6}\pi h(3R^2 + h^2)$$
 (5)

V: volume; R: radius; and h: height

• Radial strain ϵ_r :

$$\epsilon_{\rm r} = \frac{{\rm R}_{\rm f} - {\rm R}_{\rm i}}{{\rm R}_{\rm i}} \tag{6}$$

R_f and R_i: final and initial radius of the membrane (Fig. 5.5)

• Circumferential strain ϵ_c (Green strain equation):

$$\epsilon_{\rm c} = 0.5(\lambda_{\rm c}^2 - 1) \tag{7a}$$
$$\lambda_{\rm c} = (2\pi r_{\rm f})/(2\pi r_{\rm i}) \tag{7b}$$

 $\lambda_{c:}$ circumferential stretching ratio; r_f and r_i : final and initial radius at horizontal position

Instead of using fluid flow model to create the membrane deformed, different pressure scales were applied. In this perspective, it was assumed that for a small amount of fluid loaded to the cell chamber, the shape of the extending PDMS was similar to the semi-sphere. In this case, 44μ l fluid was applied for 1.3cm diameter membrane. This value

was selected based on the condition of the experiment for the embryonic chick ventricle cell culture that was performed later in chapter 6. From equation 5, the maximum deflection (or height) was estimated. This maximum deflection value (h = 0.33mm) was used as a reference for the deflection profile of the cell membrane generated by the finite element analysis (FEA).

Finite element software ANSYS 14.5 (Southpointe, PA) was utilized to generate the membrane deflecting profile as a function of applied pressures. The PDMS membrane was modeled using SHELL 281 with 2D, axi-symmetric boundary condition. For this simulation, it was assumed that PDMS membrane was hyper-elastic material; therefore, Mooney-Rivlin strain energy was used to declare the physical properties of PDMS membrane,¹²² and large deflection mode was turned on. The thickness of the membrane was 500 μ m and a Poisson's ratio was 0.49. The membrane was assigned with fixed boundary conditions at the edges, and the pressure was applied evenly on the top of the membrane. For each run, a certain pressure value was applied to the membrane until the maximum deflection of the membrane (h ~ 0.33mm) was obtained. Once the displacement profile (Fig. 5.6) was obtained, the radial and circumferential strains of the membrane were determined (Fig. 5.7). The radial strain from the center to the edge was estimated using Eq. 6 and 7, where R_f and R_i are the initial and final radius.



Figure 5.5: Schematic demonstration for radial strain (left) and circumferential strain (right) measurements for a thin PDMS circular membrane.



Displacement (mm)

Figure 5.6: The sketch of PDMS membrane deflection (d = 13.0 mm, t = 0.5 mm) using SHELL 281. The maximal displacement of this membrane was 0.33 mm at the center.



Figure 5.7: Plots of displacement and strain of the circular PDMS membrane. [A] Plot of the PDMS membrane displacement from ANSYS and [B] Estimation of radial strain (▲) and circumferential strain (■) on the thin polymeric membrane at the bottom of the cell culture chamber as a function of radial position.

5.3.2. Strain measurement via real set-up experiment

Besides using Finite Element Analysis (FEA) to estimate the membrane deflection and strain ¹²², we used high resolution ultrasound Imaging (Vevo-2100, Visual Sonics Inc, Toronto, Canada) to examine the membrane displacement of the real set-up system. A MS-400 probe (30 MHz) was used for recording the cyclic movement of the membrane (Fig.5.8.).



[B]



Figure 5.8: Images of experimental set up for taking real-time video of the PDMS membrane deflections using the Ultra Sound system. [A] Image of the Vevo2100 high frequency ultrasound system used for the PDMS strain measurement. [B] Experimental set-up for the strain measurement with [1] probe and [2] CCCM platform where the CCCM culture chamber was installed.

Three different experiments were set up with three different 500 μ m thick PDMS membranes. The flow rate was set at 44 μ l/cycle, the cyclic pressure was from 0mmHg as

the base to its peak of 10mmHg, and the frequency was set at 2.0 Hz with 40% diastolic phase. To ensure that CCCM system worked correctly and the membrane deflection was in the right range for each membrane, manual ejections of different fluid volumes (25 μ l and 50 μ l) were performed besides the real set-up experiment (Fig. 5.9.).



Figure 5.9: Ultrasound images of PDMS membrane deflection at 0, 25, and 50 μ l fluid loading along with the real set-up experiement. From these images, the level of membrane stretch from the experiment is located between 25 μ l and 50 μ l injections.

For each ultrasound movie, the deflecting movement of the PDMS membrane was converted to single moving slides (30 slides /sec). The base slide and the maximum deflecting slides were selected for each measurement (Fig.5.10.). Using an *ad hoc* program developed in MATLAB (Mathworks, Natick, MA), reference points and displacement points along the membranes from the base line and the maximum deflecting slides were created evenly along the membrane to determine the R_i and R_f . The deflection profile was then created to calculate the strains, and the radial, as well as the

circumferential strain of these membranes, were therefore calculated using the equations (6) and (7a-b).

5.3.3. Conclusion

In addition to the pressure stimulation, stretch levels in cardiac cells play a critical role ensuring cell phenotype and function. In the CCCM system, cardiac cells were attached and grown on a soft matrix which is laid on the thin PDMS membrane. Therefore, the % strain of the PDMS membrane represents the stretch level of the cells growing on it. With two different methods for strain measurement, the strain profile for the PDMS membranes was found to match the strain experienced by cardiomyocytes within the native ventricle. These results confirm that the PDMS membrane could replicate *in-vivo* stretch experienced in the heart.



Figure 5.10: Results of the PDMS membrane deflection. [A] Slide of base line where no fluid was loaded to the system. [B] Slide of the maximum PDMS membrane deflection. The vertical lines were created to divide the membrane in even distances between 2 edges. [C] Image of reference points on the base line (green color) and displacement points along with the deflecting curve (blue color). [D] Graphs of circumferential strain (left) and radial strain (right) of the 500µm PDMS membrane.

5.4. SHEAR STRESS MODELING

The dimension of the cell culture well is similar to the dimension of the previous μ CCCM model. The height of the later model is 0.5cm higher than the height of the well in the μ CCCM model. Therefore, a design guideline published in the prior work (for the μ CCCM system¹¹¹) was applied to ensure that the depth of the cell culture wells was >0.5 cm, resulting in low shear recirculation at the bottom of the wells. This work was performed by Vahidreza Parichehreh, the co-author of the previously published manuscript.¹¹¹ Below is the detail copy of method and results from the previous work for shear stress modeling in the μ CCCM system.

5.4.1. Method

Finite element software ANSYS Academic Teaching Advanced 12.0, FLOTRON module, was used to determine the wall shears stress as a function of channel height and flow rate. A 2D simulation was applied and environment was verified for steady incompressible flows. For the simulation, it was assumed that no-slip boundary conditions for the channel and groove walls, and that the participating fluid has the same physical properties of water with the density of 1000 kg.m⁻³ and the dynamic viscosity of 10 Pa.s. The inlet fluid flow rate was set at 8.6 mL/min and zero pressure was applied to the outlet. The fluid domain was meshed using 2D quadrilateral element, FLUID141, to model steady state fluid. A segregated sequential solver algorithm was used; that is, the matrix system derived from the finite element discretization of the governing equation for each degree of freedom was solved separately. The mesh was refined through mesh sensitivity analyses: at each simulation, the elements showing high velocity gradients

were refined, until reaching convergence of sensitive measures of the predicted quantities.

5.4.2. Results

Four wells with different depth (0.25, 2.00, 4.00, and 8.00 mm) were used; and a velocity of ~ 0.024 m/s (corresponding to 8.6 mL/min) at the inlet of the wells was applied in all the experiments. The shear stress (τ) was determined using the equation ¹³¹

$$\tau = \mu \frac{du}{dy}$$

where τ is the shear stress(dynes/cm²), μ is viscosity coefficient (kg/(m.s)), u is the fluid velocity (m/s). The viscosity (μ) of water at 1atm and 20° C is 1.0 x 10-³ kg /(m.s).¹³¹

5.4.3. Discussion

The flow velocity simulation (Fig.5.11.) showed that for the wells with depth of 2.00, 4.00, and 8.00 mm, with the flow rate of 8.6 mL/min, the flow velocity was nearly 0.00 m/s at the bottom of the well whose height is higher than 0.25mm. Indeed, the result from ANSYS shows that the shear stress was 0.00 dynes/cm² to approximately 200 μ m above the bottom of the wells with the height higher than 8.0 mm. The second generation CCCM system has the same diameter of cell chamber and same dimensions of fluid inlet and outlet; but the height of the chamber is about 10.00 mm. With this height, definitely, fluid flow will not create a significant shear stress, affirming that cell cultured in the second generation CCCM won't expose to the shear stress. In addition, this characterization confirmed that this system can be able to manipulate the shear stress based on the height of the cell chamber and the velocity of the fluid.



Figure 5.11: Flow velocity simulation for the cell culture chamber of the μ CCCM. Note that the flow velocity are almost 0.00 m/s at the bottom of the wells except the 0.25mm deep well, meaning fluid movement does not touch the bottom of these wells; therefore, shear stress is negligible at the bottom region where cells are cultured.

5.5. CONCLUSION

Overall, the characterization of mechanical properties of thin PDMS membrane and pressure, strain, and shear stress affirmed strongly that the CCCM can be used to replicate the *in vivo* heart function. This replication can be accomplished through a combination of different variables such as membrane thickness, the height of the cell

chamber and adjustment of tunable components, including the tunable valve, the peristaltic pump, and the pressure generator.

CHAPTER 6

USING THE CCCM SYSTEM FOR CARDIOMYOCYTES STUDIES

6.1. BUILDING THE EXTRACELLULAR MATRIX FOR CARDIAC CELL CULTURE

6.1.1 Introduction

The development of scaffolds that mimic the *in-vivo* extra cellular matrix (ECM) is crucial for the engineering tissue remodeling/regeneration. The ECM provides a microenvironment for cells to grow, proliferate, and migrate. The biochemical, structural, and mechanical properties of scaffolds play a significant role in regulating cell adhesion to ECM and to neighboring cells, which in turn affect cell morphogenesis and differentiation.¹³²⁻¹³⁷ It is true especially in the case of *in-vitro* cardiomyocyte studies, the beating rate, force of contraction, and cytoskeleton structure of cardiac myocytes which depend greatly on the ECM.^{132, 133, 138, 139} Therefore, cardiac cells need to be seeded and grow on a soft cell culture matrix, similar to the *in-vivo* heart tissue. In this study, collagen matrix was used. Based on the paper published,^{16, 140} the cell culture matrix used for cardiac tissue was determined via the morphology and spreading of cells similar to the *in-vivo* physiology. Therefore, the concentration of the collagen used for constructing matrix was 0.667g/ml collagen.^{16, 140}

In addition, to ensure that the collagen ECM was not rapidly digested by the cardiomyocytes during the experiment, crosslinking with glutaraldehyde was applied to the matrix. Glutaraldehyde is a cross-linking agent that is commonly used for collagen-based biomaterial.^{141, 142} Finally, for the cell to attach and grow on the cross-linked collagen ECM, a gelatin solution containing fibronectin was also added to the matrix prior to the cells seeded.

6.1.2. Fabrication of the ECM

First, the sterilized PDMS cell culture chamber was treated with oxygen plasma to create a hydrophilic surface (March RIE, 200 mmTorr, 200 mmHg, 10% oxygen, 30 seconds). Then, a 300 μ L of the collagen type I solution (0.67 mg/mL) was promptly added to the cell culture chamber and allowed to be cured at 37°C for 3-4 h. Second, a 400 μ L of 0.5% (w/v) glutaraldehyde solution was gently added on the surface of the cured collagen matrix and maintained for 1 h at room temperature (RT). After 1 h, the matrix was washed with deionized (DI) water three times, followed by a 4N sodium hydroxide solution twice (30 min/each). Finally, DI water was used again for the final wash (three times). The cell chamber was filled with DI water and stored at 4 °C for later use. 48 h before cells were seeded, a 400 μ L solution composed of 10% gelatin attachment factor (1X, Gibco, S- 006-100) and 50 μ g/mL of fibronectin (BD Biosciences, 356008) was added to the chamber. A one-time washing with 1X PBS or fresh culture medium was performed before the cells were seeded.


Figure 6.1: Image of the collagen matrix with cardiac cells after 4 day cultured in the CCCM system.

6.2. CULTURING CARDIOMYOCYTES IN THE CCCM SYSTEM

6.2.1. Primary embryonic chick ventricular cardiomyocytes

Embryonic chick cardiac cells are commonly used to study the complex processes leading to normal or abnormal heart development. Chick embryonic heart development is quite similar to that of the human heart. Fertile chick eggs are relatively easy to obtain and less expensive than rodent models. Finally, it is possible to observe the embryonic heart at the earliest stage of its embryogenesis and to isolate embryonic cardiomyocytes for *in-vitro* culture.^{15, 79, 143}

During the embryonic period, cardiomyocytes have a high proliferation rate and differentiation.¹⁶ The synthesis of DNA from the embryonic cardiomyocytes reaches its peak during the cardiac morphogenesis. During this developmental window, mechanical hemodynamic loading and unloading play a crucial role in regulating the cardiomyocyte

morphogenesis, architecture, and contractile functions and stimulating different molecular signal pathways. On the other hand, in response to these mechanical stimulations, embryonic cardiomyocytes themselves regulate their proliferation and differentiation rate. Therefore, any changes in mechanical hemodynamic loading and unloading system affect the development of cardiomyocyte tissues and their contractive functions greatly.

Chick embryonic heart development can be divided into 46 stages, called Hamburger Hamilton (HH) stages.^{79, 144} These stages are used rather than only using days of incubation due to variations in maturational rate that occur in response to changes in ambient environmental factors. The first myocardial differentiations are detected on stage HH7 when the formation of the endocardial heart tube begins. On HH 8, the process of heart tube fusion starts, and is completed on HH 11. Heart beat begins on this 11th HH stage. During stages between the 13 to the 18, the heart tube transforms to the C shape loop then to the S-shape loop to form atria and ventricles. HH 18-22, the primary ventricular channels can be observed. HH 21-34, valve development, vasculature, atrial and ventricular septations are gradually formed, along with other cardiac components, such as the cardiac conduction system, atrial-ventricular (AV) nodes or cardiac neural crest. Ventricular septation is completed around HH 34. HH 36 (or day 10 gestation), the Purkinje fiber network begins to form and the atrial-ventricle valve is completely formed to separate the atria from the ventricle. HH 40-41 is the hatching stage. Besides the HH stage, the stages of embryonic heart development can also be named based the incubation day. The chick hatches on approximately the 21st day of incubation. Primary

cardiac morphogenesis occurs between day 2 to day 10 of a 21-day gestation. Day 10 is corresponding with HH36, where the ventricles are completely separated. Therefore, we selected 10th day embryonic chick ventricles for cell isolation in our CCCM experiments.

Embryonic cardiac development depends on the integration of the environmental conditions, biomechanical forces, molecular programming, and adaptive remodeling. Cyclic mechanical stimulation inside the heart induces myocardial hyperplasia. In addition, in the early period of cardiac morphology, the function of chick embryonic cells, including the adaption of the contractile function, is greatly affected by mechanical loading conditions. Mechanical stimulation thus affects the formation of the shape, as well as the growth of heart chambers. Indeed, applying mechanical stimulation during different stages of the embryonic period will greatly affect the function of the heart tissue, which includes cell proliferation, contraction, frequency, and the duration of contraction. Heart cells start beating synchronically and strongly, similar to the *in-vivo* nature, reached the peak *in-vitro* on culture day 12.¹⁶ Therefore, the heart embryonic tissue increased active contractile force from culture day 7 to day 12. Also, culture day 12 has the highest proliferation. However, the contractile response to the β -adrenergic stimulation was less than culture day 9. Under these studies, 3 different developing stages were standardized for mechanical stimulation: from culture day 4 to 6 (before the cells increase the contraction force), from culture day 9-11 (before the proliferation goes down), and at culture day 13-15 (the transition between embryonic and fetal stages).

6.2.2. Embryonic chick cardiomyocyte isolation and culturing

6.2.2.1. Embryonic Chick Cardiomyocyte Isolation and seeding

Fertile White Leghorn chicken eggs (Utah) were incubated in a forced-draft, constanthumidity incubator until day 10 of the gestation (HH: stage 36). Ventricles were collected and enzymatically digested using 2 mg/mL of collagenase type II, followed by 0.05% trypsin-EDTA solution (Invitrogen, Carlsbad, CA). The cell solution was then filtered and isolated cells were collected. An 1 h pre-plate for the isolated cells at 37°C was performed in 10 mL of cell culture medium (DMEM high glucose, 10% Fetal Bovine Serum, 1% embryonic chick extract, and 1% antibiotic), followed by a 5 min centrifuge at 1000rpm. Cell pellet was then re-suspended in a new 10 mL of cell culture medium and were cultured on a gyratory shaker (60-70 rotations/min) for 18 h to re-aggregate viable cardiomyocyte clusters. The following day, the whole cells, clusters, and medium were collected and spun at 1000rpm for 5 min. Old medium was discarded and 1ml of warmed fresh medium was added. Cell clusters were counted and cell viability was checked with Trypan blue staining. For each cell culture chamber prepared from the session 6.1.2, approximate 500µl of $3.0-3.5 \times 10^4$ cell clusters were seeded and cultured in a static condition at 37 °C, 5% CO₂ for 3 h before filling the reservoir with warmed fresh culture medium. A static culture condition at 37°C and 5% CO₂ was maintained for 24 h to obtain 100% confluence. On the following day, the sample was subject to mechanical loading within the CCCM, or maintained under static conditions as a control.

6.2.2.2. Culturing cardiac cells under the influence of mechanical stimulation within the CCCM

Day 10 embryonic chick cardiomyocytes experience *in-vivo* peak pressures of ~10–15 mmHg and radial and circumferential strains of ~10–20%.¹³⁰ Since the cardiac cell tissue is thinner and weaker than the *in-vivo* cardiac tissue, a peak systolic pressure of 10 -12 mmHg and a strain of 8-15% were chosen for the whole experiment. To culture cardiomyocytes under these conditions, a 500 μ m thick membrane was selected and a flow rate of ~2.6 ml/min was used to attain a filling volume of 44 μ l per cycle.

Following 24 h of culturing under static conditions to achieve 100% confluence, the cell culture chamber with cells was transferred to the CCCM system and the system was assembled as described in the section 4.3. The whole set-up CCCM system was then moved into the cell culture incubator and was ready for mechanical stimulation for 4 days at 37 °C and 5% CO₂. The static pressure inside the cell culture chamber was reported before the peristaltic pump was turned on. The flow rate was set at ~2.6 ml/min (~ 44 μ l/cycle). The downstream one-way valve and the pressure from the generator were adjusted to obtain cyclic pressures of 0-10 mmHg at a frequency of 2.0 Hz. Pressure waveforms were checked in a period during 4 day stimulation. For comparison, the control samples were culture under a static condition in the same culture incubator with the same amount of fresh culture medium. After 4 days, the cell culture chamber was removed from the CCCM platform and then maintained under a static condition for ~3 h prior to analysis.

During the CCCM stimulation, the instantaneous pressure generated inside the cell chamber was obtained using a high fidelity pressure transducer and LabView software. Based on the percentage of systolic versus diastolic timing set on the pressure generator, along with the pressure waveform and fluid volume loaded to the chamber, the pressurevolume loop for a single working cycle of the CCCM was obtained (Fig. 6.2.).



Figure 6.2: Plot of pressure vs time and pressure-volume loop obtained within the CCCM system. The changes in pressure within the CCCM cell culture chamber and pressure–volume loop correlating changes in pressure with changes in volume within the CCCM chamber was determined. The parameters of the pressure and fluid volume were set up based on the parameters from the left ventricle of the embryonic chick heart. Similar to the pressure-volume loop seen in the left ventricle of the heart, this pressure-volume loop represents the (a) filling phase, where the pressure was low but the volume increased, (b) the isovolumic contracting phase, where the pressure increases significantly but the fluid volume was maintained the same during this phase, (c) the

ejection phase, where the fluid was ejected out of the chamber, and (d) the isovolumic relaxing phase where the pressure drop significantly with no change in the fluid volume.

After 4 days in the mechanical stimulations, the tissues were removed from the system, followed by tissue analysis. Observed under the microscope, the stimulated construct has more cardiac islands on the surface and looked more crowded and rougher, while the control has a flatter surface with larger sized cells (Fig.6.3.).



Figure 6.3: Phase contrast images of *in-vitro* embryonic chick cardiac cells cultured under the static and CCCM stimulated conditions. Left: embryonic chick cardiac cells cultured under the static condition as a control. Right: embryonic chick cardiac cells cultured under mechanical stimulations generated within the CCCM system. Compared to the control cardiac tissue, the conditioned cells appeared to have higher cellular density.

6.2.3. Conclusion

The CCCM system is able to mimic the mechanical conditions which occur in the left ventricle. Primary chick embryonic left ventricle cardiomyocytes are able to grow well under the influence of cyclic mechanical stimulation generated within the CCCM system. Further analysis between the stimulated and the static cultured groups will be described below, included tissue alignment, beating rate, maturation, proliferation, and gene expression.

6.3. CARDIAC TISSUE ALIGNMENT AND PROLIFERATION

6.3.1. Introduction

Cardiomyocytes continuously experience the stress and the change in length during the heart cycle, due to the blood loading and unloading. Cardiac tissues are elongated during diastolic phase and shortened during the systolic phase of a heart. These hemodynamic stress and tissue strain affects cell proliferation and cytoskeletal remodeling.⁸⁴ Indeed, in response to the strain and stress, cardiomyocytes have the ability to remodel cell shape by adding the sarcomere in series or filaments in parallel respectively to maintain cardiac function.¹⁴⁵ In addition, cardiomyocytes during embryogenesis have a high proliferation. Staining nucleus with Bromodeoxyuridine (BrdU) along with DAPPI is a common method to check the cell proliferation.

 $Proliferation = \frac{\text{total BrdU nucleus}}{\text{total DAPPI nucleus}} 100\%$

6.3.2. Methods and materials

Immunofluorescence staining was used to evaluate the cell alignment and proliferation. To examine the cell alignment, the constructs were stained with F-actin and α -actinin. Before staining, the samples were fixed with 4% paraformaldehyde (PFA) at room temperature (RT) for 20 min, followed by a washing with 1X phosphate buffered saline (PBS) solution. A 0.1% Triton solution was then added to the constructs for 30 min, RT. A solution of 0.5% BSA in 1X PBS was used as a blocking solution. For F-actin staining, the samples were incubated with TRITC-conjugated Phaloidin (1:100; Millipore, Billerica, MA) in the blocking solution for 1 h at RT. For α -actinin, primary antibody cardiac α-actinin EA53 IgG1(1:400, Abcam, Ab7817) and second antibody antimouse (1:600, 488 green, Invitrogen, A21121) in 1% BSA/1X PBS solution were applied individually to the tissue for 1 h, RT, alternated with a washing buffer (0.05%)Tween-20/1X PBS) 1 h in between. DAPPI (1:100, Millipore, 90229) was also applied to stain the nucleus at the end. Finally, the tissue constructs were mounted with anti-fade solution (Invitrogen, San Jose, CA), and imaged using a Nikon A1 confocal microscopy system (Nikon Instruments, 284 Melville, NY).

To examine cell proliferation, Bromodeoxyuridine (BrdU) incorporation during DNA synthesis was utilized. Basically, 48 h prior to the tissues being fixed with PFA, 20 μ M of BrdU (Sigma) was added to the cell culture medium both for the control and the stimulated tissues. After being removed from the present culture environment, the tissues were fixed with 4% PFA solution for 20 min at RT and permeablized with 0.1% Triton solution for 30 min at RT. A one hour washing with 1X PBS solution was performed

before the HCl solution (1N) was added directly to the tissue on ice for 10 min. A 1N HCl solution was then replaced by 2N HCl solution. After sitting at RT for 10 min, the tissues in the 2N HCl solution were incubated at 37°C for an additional 20 min. A one hour washing with 1X TBE buffer (10X TBE, Mediatech Inc., Manassas, VA, 46-011-CM) at RT was performed before the tissues were blocked with a blocking solution (1% BSA + 0.1% glycine in 1X PBS) for 1 h at RT. The tissues were then incubated with the primary antibody Anti-BrdU (1:100, Abcam, ab1893) in the blocking solution for 24 h at RT. After 1 h washing with the washing buffer, the tissue was incubated with secondary antibodies, anti-sheep (1:400, red, Abcam, Ab6743) in the blocking buffer for 1 h at RT, followed by another 1 h washing. DAPI (1:100, Millipore, 90229) was then added to stain the nucleus at the end. Finally, the tissue constructs were mounted with anti-fade solution (Invitrogen, San Jose, CA) and imaged using a Nikon A1 confocal microscopy system (Nikon Instruments, 284 Melville, NY).

6.3.3. Results

Specimens were stained with F-actin and cardiac alpha-actinin antibodies, and then examined under the confocal microscopy with 60X magnification. Compared to the control group, embryonic chick heart cells in the CCCM tissue samples were more aligned and oriented (Fig.6.4.). The parallel orientation showed up obviously in the CCCM construct stained with F-actin. The cell arrangement of the control sample appeared to be random.



Figure.6.4: Immunofluorescence images of cardiomyocyte tissue cultured in the CCCM system and in the static condition. (A) Images of the cell skeleton structure with f-actin (green). The stimulated tissue cultured in the CCCM system gave more parallel arrangement compared to the random arrangement of the control tissues cultured under the static condition (B) Images of cell alignment with α -sarcomeric actinin (red). The picture of the CCCM construct shows *in-vivo* like matured tissues with stripped and closer connection between cell-to-cell connections. The blue color is the nucleus stained with DAPPI.

To determine the cell proliferation, BrdU, the marker stained for nuclei that have synthesized new DNA during the BrdU treatment period, was used. Different locations of the constructs were observed under 60X magnification of the confocal microscope (Fig.6.5.). The dividing cells had nuclei that showed both blue and red colors overlapping each other, while the undivided cells showed only blue nuclei. Red nuclei without blue were the dead cells. The cell proliferation rate was determined by the ratio between the dividing cells to the total of living cells. Six different experimental sets were done for data statistical analysis.

[A]











The sample size was N = 6 with two tailed significance was set at ** $p \le 0.05$, meaning a strong chance of having statistical significance between these 2 groups.

6.3.4. Discussions and conclusions

The alignment of cardiomyocytes and the cell proliferation were evaluated via immunefluorescence microscopy. Cardiomyocytes were subjected to mechanical stimulation. Cell alignment expresses more in mature cells. Therefore, cardiomyocyte maturation was observed under the immunofluorescence images via Phaloidin and sarcomeric α -actinin. The result shows that the contraction-stretching of the cells promotes the increasing of Factin and helps to align the cells. Cell alignments demonstrated that mechanical loading spontaneously rearranged the cytoskeletal orientation of the cells. In addition, from BrdU staining, a higher proliferation rate was observed on the CCCM tissues rather than on the control ones. This result suggests that applying mechanical stimulations on the embryonic cardiac tissue is necessary to promote the cell alignment and proliferation rate of the cardiomyocytes.

6.4. CARDIAC TISSUE MATURATION

6.4.1 Beat rate

Beat rates (BR) of the conditioned and control constructs were obtained after being removed from the CCCM for 3 hours. Two different time frames of the CCCM stimulations (4 and 7 days in the CCCM system) were performed. At least 10 different experiments on different dates were performed. The BR of the stimulated samples was almost 1.5 times higher than the BR of control samples (Fig.6.6). In addition, the BR of the stimulated samples cultured in the CCCM system for 7 days yielded a little higher than the BR of samples with 4 days stimulation, whereas the controls of both groups are the same. This indicates that mechanical stimulations are important to maintain and enhance the BR of the cardiac tissue.



Figure 6.6: Graph of the beat rate (beats per min) between the control and the stimulated groups. 2 different periods of mechanical stimulations (4 days and 7 days) were performed along with their controls cultured under a static condition. Number of samples was N=10. Two tailed significance was statically set at **p \leq 0.005.

6.4.2. Electrical Pacing

Electrical pacing of stimulated constructs and unstimulated controls was accomplished to identify changes in electrical properties in response to mechanical conditioning in the CCCM. Platinum wire electrodes (d=0.5mm, Alfa Aesar, Ward Hill, MA, 43288) were embedded vertically into the tissue-collagen gel matrix and connected to an electrical pacing system (Isolated Programmable Stimulator, Colbourn Instruments, 02142-1) (Fig. 6.7).



Figure 6.7: Electrical Pacing Setup System. [A] The image of the real pacing experiment, which was set on the stage of the microscope before pacing the tissue. [B] Diagram of the electrical stimulating, which was programed on the electrical pacing system.

The maximum pacing tissue beat rate was recorded while varying the threshold voltage. To find the maximum pacing rate, the voltage was increased from the lower to the higher voltage until the BR reached to 2:1 phase (BR was half of the maximum BR). The threshold voltage was also determined. This voltage was the voltage at which the tissue started beating with the frequency of 2.0 Hz. The results show that the CCCM tissues reached their maximum BR of 245bpm, which is close to the BR of the *in-vivo* mature chick cardiac tissue (Fig. 6.8). In addition, the threshold voltage needed for the CCC tissues to reach the frequency of 2.0 Hz was lower than the threshold voltage inserted on the control samples. This result affirms that mechanical conditioning within the CCCM resulted in tissue maturation represented by more efficient cell-cell connections and higher maximal beat rates.



Figure 6.8: Pacing Electrical Stimulation Results. [A] The Maximum Pacing Beat Rate (bpm) between the non-stimulated (light blue) and the stimulated cardiac tissue group (red). [B] The Threshold Voltage (V) in corresponding to the maximum pacing beat rate for the non-stimulated and stimulated cardiac tissue groups. N= 6 with two-tailed significance set at ***P<0.05

6.4.3. Cell contractility

Movies of beating cardiomyocyte were recorded and analyzed to determine regional tissue strain during contraction. For an individual sample, 5 different locations on the movie were selected randomly for strain measurement. Lagrangian strain calculation for finitely small displacement was used as previously described by Bonet et al.¹⁴⁶ Briefly, if p_1 and p_2 are two nearby points defined on the first frame, and d_1 denotes the Euclidian distance between p_1 and p_2 at the first frame (i.e., reference frame), then d_j denotes the Euclidian distance between these two points at time frame j, then, the engineering strain S, at frame j, is defined as:

$$S_{i} = (d_{i} - d_{1})/d_{1}$$
 (8)

A custom algorithm was written to estimate the Lagrangian strain. First, the peak displacement was determined by tracking two points based on their appearance features through the image frames and calculating the displacement between the two points over the image frames. The maximum displacement was then selected as the reference frame. Then, five pairs of points on the first (reference) frame were determined and their tracked pairs on the selected frame with maximum displacement. The Lagrangian strain for each pair of points was estimated using equation (8). Finally, the mean Lagrangian strain was calculated as expressed a % shortening.

The results show that without the electrical pacing, the percentage shortening of the CCCM stimulated tissues was about $4.49 \pm 0.88\%$, whereas controls were only at $2.73 \pm 1.8\%$ (Fig. 6.9). The unpaired t-test shows no statistical significance between the shortening length of the control and the CCCM samples. However, when electrical pacing was applied, the shortening of the CCCM stimulated tissues increased to $5.52 \pm 0.88\%$, whereas the shortening of the un-stimulated tissue only went up to $2.96 \pm 1.79\%$. The statistical results showed significant difference with *p<0.05. These results suggest that, the mechanical stimulation enhances the shortening of the cardiac tissue, and this contractility increases further with the association of the electrical pacing applied on the tissue.



Figure 6.9: Graph of cardiomyocyte shortening with and without electrical stimulation: control (black) and the CCCM stimulated (clear) samples evaluated with and without electrical pacing. N=6 with two-tailed significance set at P<0.05

6.5. CARDIAC TISSUE RESPONSE TO β-ADRENERGIC STIMULATION

6.5.1. Introduction

Isoproterenol (ISO) is a β -Adrenergic Agonist which binds to G-protein coupled β -Adrenergic receptors (β -AR). The coupling of ISO/ β -AR activates adenylyl cyclase (AC). These activated AC catalyze the conversion of Adenosine triphosphate (ATP) into cyclic adenosine monophosphate (cAMP), followed by the activation of protein kinase A (PKA). After activated, PKA is able to phosphorylate L-type Ca²⁺ channel and phospholamban (PLB); as a result, increase the Ca²⁺ influx into the cytosol and enhance the activity of sarcoplasmic reticulum Ca²⁺ pump SERCA2a to transport Ca²⁺ from the cytosol into the sarcoplasmic reticulum (SR). Un-phosphorylated PLB inhibits the activity of the SERCA2a pump. Phosphorylating of β -AR via PKA prevents the coupling between ISO and β -AR and reduces the sensitization of β -AR to the agonist.⁵⁴ In summary, ISO and β -AR play a significant role in the intracellular mediate signal transduction pathway by enhancing the Ca²⁺ influx into SR and the transportation of Ca²⁺ from the cytosol into the SR, therefore, contributes to regulate the heart function via contractility and frequency.

ISO affects the chick embryonic ventricle development as early as day 4th (out of a total of 21 days of gestation before hatching) via the increase of contracting force of cardiac tissue. In contrast to the mature heart, ISO does not affect the early embryonic heart until the expression and coupling of functional β -AR. In addition to the positive chronotropic and inotropic effects of ISO stimulation, ISO treatment also has a toxic effect on developing and mature cardiomyocytes and can trigger cell death in cardiomyocytes from a wide range of species.¹⁴⁷⁻¹⁴⁹ In adult hearts, ISO continues to enhance the rate of tension development and beat rate (BR) of the tissues.¹⁵⁰ Our hypothesis that, if mechanical stimulation enhances the maturation of the cardiac tissue, in comparison to the control tissue group, the contractility and the BR of the stimulated tissue group must be increased in response to the ISO administration.

6.5.2. Material and Methods

Embryonic chick cardiac left ventricle cells at day 10 were isolated, seeded, and experimented as mentioned in the previous sections. After being cultured for 4 days with mechanical stimulation within the CCCM system, cardiac tissues were removed from the system and incubated in a static condition at 37°C for another 3 hours before applying ISO to the tissue. After 3 h, samples were brought to a microscope for analysis. Different

concentrations of ISO (0.5µM, 1µM, 5µM, 10µM, and 50µM) (Sigma Aldrich, I6504) in warmed fresh medium were applied respectively to the tissues. An electrical hot plate was used to keep the temperature of the tissues and medium at 37°C. BR before and after administrations were reported; and contractile movies were made within 5 minutes of each ISO administration. Then, a brief washing with warmed fresh culture medium was performed before adding a new higher dose of ISO to the tissue. Contractile movies were analyzed using MATLAB software (MathWorks, Naticks, MA) to determine the percentage shortening for tissue contractility.

6.5.3. Results

The effect of ISO on the BR and contraction of the constructs cultured in the mechanically active CCCM system and in static conditions were observed. The BRs before and after each ISO application were recorded. The BR of the tissue before the 0.5μ M ISO solution added to the tissue was used as the referent BR to determine the percentage change in BR under the effect of ISO administrations (Fig.6.10). The results show that the BR of the CCCM group increased in response to increasing doses of ISO to a maximal response at 10μ M ISO, then declined. In contrast, the BR of the control group decreased in response to increasing doses of ISO above 0.5μ M. This result indicated that the ISO produced a toxic response in static (unconditioned) chick cardiomyocytes. However the CCCM stimulated group had positive chronotropic responses to ISO, consistent with CM maturation.



Figure 6.10: Plot represents the percentage change in beat rate of the cardiac tissue under the effects of Isoproterenol. While the control group showed cellular toxicity with increasing ISO concentration, the beat rate of the stimulated group increased and reached its peak at 10μ M ISO. The horizontal line is the base line corresponding to the referent beat rate recorded before the ISO applications. Five experiments were performed.

Cardiac contractility with and without ISO was also examined. Movies of each ISO application were made and maximum contraction was chosen to determine tissue shortening. Shortening was calculated as described in the section 6.4.3. With ISO applications contractility of the stimulated tissues significantly increased versus the unstimulated group, to $7.55 \pm 0.78\%$ versus $4.52 \pm 0.43\%$, respectively (Fig. 6.11). In response to ISO, contractility increased 67% in the conditioned group versus 36% in the

unconditioned group. These results suggest that mechanical stimulation may have accelerated CM maturation as measured by reduced toxicity and increased BR and shortening in response to ISO stimulation.



Figure 6.11: Changes in the cardiomyocyte contraction with and without the influence of ISO: controls (black) and CCCM stimulated (clear) constructs. Measurements were made at 3 different locations on each sample. N= 6 different paired experimental sets. Two tailed significance was set at *** $p \le 0.001$.

6.5.4. Discussion

Catecholamine affects mechanical performance of the heart tissues through the activation of β -AR; and the cardiovascular function is controlled primarily on this adrenergic signaling pathway.⁵²⁻⁵⁴ Under normal physiological conditions, catecholamine induces positive inotropic and lusitropic responses in the heart tissue through β 1-AR-activated pathway. Once stimulation of β 1-ARs via ISO binding occurs, cAMP accumulation

rapidly increases which indirectly promotes the phosphorylation of PLB, and enhances the cardiac contractility. Out of their subtypes, subtype β 1-ARs exhibits dominantly when cardiomyocytes become more mature under normal physiological condition.^{53, 56} This dominant β 1-ARs, therefore, induces positive inotropy and lusitropy via heart rate and contractility. Under the abnormal physiological condition of the heart, or failing heart, β 1-ARs decreases, but β 2-ARs increases, causing cardiomyocyte death.⁵⁶

After adding the ISO to the tissue, the CCCM conditioned constructs yielded a higher percentage of contraction compared to the control ones; and the BR of the conditioned tissue kept increasing until a 10 μ M ISO solution (2.5mg/ml) was added. However, for the controls, the concentration of ISO higher than 10 μ M created negative inotrope and reduced BR on the cardiac tissue, and finally the cardiac tissue stopped beating This result is similar to the result found in the early studies from Serverin,¹⁵¹ indicating that these CM undergo cell damage and death if a higher concentration of ISO is applied. These results state that, compared to the static cultured control group, the CCCM stimulated construct has a higher response to the β -AR, and at the same time, has a higher resistance against the cellular toxic effect of ISO, hence, is less likely to undergo cell damage and death. Higher response and higher resistance may be the result of higher cell-cell connection, more maturity, or more population. In conclusion, mechanical stimulations of embryonic CM in the CCCM resulted in a more mature ISO response, consistent with the maturation of β 1-adrenergic signaling.

6.6. SELECTED CARDIOMYOCYTE GENE AND PROTEIN EXPRESSIONS IN RESPONSE TO MECHANICAL CONDITIONING

6.6.1. Introduction

From previous results, embryonic chick cardiac tissues cultured in this CCCM system showed a higher proliferation rate, better alignment, and more maturation via BR and contractility. This section focusses on the effect of mechanical stimulation on proteins that play a critical role in the beating rate and contractility of the heart tissue. Along with the 2D constructs (CCCM stimulated and the control ones), ventricle tissues at day 16, cell suspension from day 16th (same day harvesting the 2D constructs), and 3D engineered cardiac tissues (ECT) harvested at culture day 5 (equivalent to day 16 chick ventricular cells) were also collected for selected gene expression and protein synthesis analysis.

As markers of CM maturation and function, sarcoplasmic reticulum calcium ATPase2a (SERCA2a), phospholamban (PLN), Troponin T (TnT), and Alpha and Beta-Myosin Heavy Chain (α -, β -MHC), and total protein were analyzed in control and conditions tissues.

SERCA2a and PLB are essential proteins that regulate calcium cycling inside the cardiomyocytes. These genes are involved in regulating the contraction-relaxation of the heart muscle. Un-phosphorylated PLB binds to SERCA2a, prevents Ca^{2+} binding to SERCA2a, and acts as an endogenous inhibitor of SERCA2a. Phosphorylated PLB (pPLB) releases this inhibitory effect, making the affinity site to Ca^{2+} on SERCA2a more

apparent. This activated SERCA2a then transports calcium against the gradient from cytoplasm back to sarcoplasmic reticulum (SR).⁵⁸ As the result, the rate of calcium ions influx back to the SR increases, promoting the muscle relaxation prior to the next cycle of calcium release and myofiber contraction. Therefore, SERCA2a has a central role in regulating Ca^{2+} cycling between the SR and myofibers and a direct impact on CM contractility. The regulation of SERCA2a activities plays a critical factor in the contractile function and heart disease.^{152 32}

TnT is the protein binding with tropomyosin and involved in the regulation of thin filament function and the interaction between the thin and thick filament during myofiber shortening.⁵⁰ Abnormalities of this TnT gene are associated with sudden death in cardiac patients. Myosin heavy chain (MHC) is the major sarcomeric protein expressed in heart tissue during development and adulthood and regulates mechanical performance of the heart, especially muscle contractility.⁶⁴⁻⁶⁶ Alpha and Beta MHC are the two important isoforms of the MHC found in the heart tissue. β -MHC isoform is expressed mainly during embryogenesis or heart diseases. α -MHC isoform exists dominantly in the adult heart tissue and inhibits the expression of β -MHC. The ratio of α -MHC to β -MHC expression is also seen in species with rapid or slow beating rates⁶⁷

6.6.2. Methods

6.6.2.1. Cell suspensions and 3D ECT constructs

Cell suspension from ventricular cardiomyocyte tissues from day 16 were also isolated using GentleMACSTM Dissociator (MACS Miltenyi Biotec, Auburn, CA), pre-plated, and

rotated before being collected for cDNA and proteins. At the same time, ventricular tissues from day 16 were also collected for cDNA and proteins.

To create 3D ECT constructs for PCR, the isolated embryonic cardiomyocyte clusters (~ 3.0×10^4 clusters) were also mixed with collagen solution (0.667mg/ml) and seeded in the TT-4001C Tissue TrainTM plates (Flexcell® International Corporation, HillSborough, NC) using Flexcell FX5X Tension system until the collagen solution was cured (about 1.5 h vacuumed, 37°C, 5% CO₂). Then the constructs were cultured under the static condition for 5 days prior to analysis for PCR.

6.6.2.2. Real time PCR (qPCR) for gene expression

Total RNA was extracted from the cardiac constructs, cell suspensions, or ventricles, using the Trizol isolation method. Briefly, the sample was homogenized in 1ml Trizol three times (7 sec/each) in ice. After RNA isolation, cDNA was then transcribed via the RNeasy mini kit (QIAGEN). The concentration of cDNA was measured using the NanoDrop 2000 spectrophotometer (Thermo Scientific, Waltham, MA). The real time PCR for each target gene was then performed in triplicate. The GAPDH primer was included as the housekeeping gene. SERCA2a, α and β MHC, TnT, and PLB were the interested genes chosen for these PCRs. For data analysis, the relative quantification of each target gene was normalized to GAPDH. The fold change of each interested gene was determined by $\Delta\Delta C_t$ where the calibrating sample is the control construct.

6.6.2.3. Western blotting for protein synthesis

The end of the experiment, total protein of each sample was collected using the Complete-Lysis M solution (Roche Diagnostics, Indianapolis, IN). The protein concentration was then determined, using the NanoDrop 2000 Spectrophotometer. The target proteins were separated using 10% SDS-PAGE and transferred to ImmobilonTM-FL membranes (Millipore Corporation, Bedford, MA). After being blocked with 5% non-fat milk, the membrane was probed with different primary antibodies including anti-SERCA2a (1:500) (LSBio, Seattle, WA), anti α -MHC (1:150) (Santa Cruz, Dallas, TX) and β -MHC (1:500) (Bioss, Woburn, MA), anti-Actinin (1:500) (Abcam, Cambridge, MA), anti TnT (1:1000) (Sigma, St. Louis, MS) and anti β -actin (1:3000) (Cell Signaling, Beverly, MA). The secondary antibody was Cy3[®]goat anti-Rabbit IgG (1:500) (Life TechnologiesTM, Grand Island, NY) and Cy5[®] goat anti-mouse IgG1 (1:500) (Abcam, Cambridge, MA). The labeled bands representing the target proteins were visualized via the Typhon 9400 system. NIH Image J software program was used for densitometry.

6.6.3. Results and discussions

6.6.3.1. Gene expression

Figure 6.12 and figure 6.13 show that compared to the level of gene expression in the embryonic chick ventricle, gene expression decreased progressively from cells suspension to 2D CCCM culture for all three genes: SERCA2a, α -MHC, and β -MHC. The gene expression on 2D constructs, both the controls and the CCCM stimulated samples, was much lower compared to the heart ventricles and cell suspension on day 16th, as was shown in a previous study.⁹³ When compared, the 2D constructs together,

gene expressions between the control and the CCCM group showed no significantly statistic increase or decrease. The p values were greater than 0.05. However, gene expressions of these genes were partially restored with the 3D ECT constructs especially with PLN, α -MHC, and β -MHC genes.



Figure 6.12: Plots of fold changes in gene expression with ventricular gene expression set as the control state. [A] SERCA 2a gene expressions, [B] PLN gene expression. All samples were collected on day 16^{th} (out of 21 days of gestation). N \ge 3 and p > 0.05.



Figure 6.13: Plots of fold changes in gene expression with ventricular gene expression set as the control state. [A] α -MHC gene expressions and [B] β -MHC gene expressions. All samples were collected on day 16th (out of 21 days of gestation). N \geq 3 and p > 0.05.

Figure 6.14 shows the total RNA synthesis obtained from 2D cardiac construct groups: the control and the stimulated ones. From the plot, the embryonic chick cardiac tissues stimulated yielded more RNA (1803 \pm 218 ng/µl) than the tissues cultured under the static condition (1186 \pm 102 ng/µl); which was about 1.5 time higher.



Figure 6.14: Total RNA obtained from 2D embryonic chick cardiac tissues. Total samples N = 3, **p < 0.05

6.6.3.2. Protein Synthesis

More than 10 samples in pair (controls vs the CCCM stimulated groups) were used to determine the total protein in each group. The total protein in the CCCD stimulated constructs significantly increased (97.15 \pm 4.97 mg) versus total protein in the 2D controls (71.52 \pm 4.14 mg) (Fig. 6.14)



Figure 6.15: Total proteins of the 2D cardiac tissue constructs. $N \ge 12$ two tailed significance was set at ** p < 0.005.

Five different CM proteins (SERCA2a, α - and β -MHC, α -Actinin, and TnT) were selected for the Western Blot (Fig. 6.16). Figure 6.17 and figure 6.18 show the target proteins collected from different conditions. Proteins SERCA2a, TnT, and β -MHC from the cell suspension were much lower than those in the ventricular tissues. Interestingly, the amount of α -Actinin protein almost doubled after cell isolation from ventricular tissue. As noted in the previous study, protein levels decreased in response to 2D culture. However, when mechanically conditioned in the CCCM system, protein levels were modestly increased, except for myosin heavy chain proteins.



Figure 6.16: Images of Western Blot bands of the interested proteins in the 2D control and CCCM stimulated groups



Figure 6.17: Graphs of SERCA2a, α - and β -MHC proteins normalized by β -Actin. [A] SERCA2a protein, [B] α -MHC protein, and [C] β -MHC protein. N \geq 3 and two tailed significance was set at *p < 0.05.



Figure 6.18: Graphs of TnT and α -Actinin proteins normalized by β -Actin. [A] TnT protein and [B] α -Actinin protein. N \geq 3. SEM was used for error bars; and two tailed significance was set at * p < 0.05 and **p<0.005.

6.6.4. Discussion

During cell isolation, cell-cell contacts are disrupted and extracellular matrix is destroyed, causing cells to lose the extra cellular network connections that influence many cellular functions, including calcium handling and contractility. Consistent with the

negative impact of cell isolation is the disruption of gene expression and protein synthesis of contractile relating proteins.⁹³ As a result, gene expression and protein synthesis of the Ca2+ regulating protein (SERCA2a) and contractile proteins (β-MHC) were lower in the cell suspension group than in the ventricle group. However, these results also demonstrate that transcriptional and translational processes still occur and that viable cardiomyocytes recover and mature in the CCCM. The protein α-MHC obtained from the cell suspension was higher than those in the ventricular tissues, but was not statistically significant. However, when these embryonic cardiac cells were cultured under 3D, gene expressions of α -MHC, β -MHC, and PLN were augmented, demonstrating that 3D culture is necessary for the cardiac tissue to fully regulate the transcriptional processes. These results are similar to the results done by L.Khait and R.K.Birla group with neonatal rat tissues.⁹³ 2D constructs are compacted, cells are laid on top of each other; therefore, limiting their ability to arrange their orientation and their potentials to create their own cellular matrix as well as to access their nutrients. 3D constructs allow cells more space to rearrange their orientation, create their own cellular matrix, and build up their connection among cells. Nutrients are easy to access. Therefore, when cells were cultured under 3D condition, their gene expressions are nearly restored to levels found in the 3D native ventricular tissues even though all these 3D ECT constructs in this experiment were cultured under the static condition.

In contrast to other CM associated proteins, the protein synthesis of α -Actinin protein doubled in the short time from ventricle tissue to cell suspension. The amount of Alphaactinin was also higher than those in the ventricular tissues. In cardiac cells, α -actinin protein is the cytoskeletal actin-binding protein to stabilize the contractile apparatus.^{42, 153, 154} Once the extra-cellular network was disrupted during the isolation, this protein synthesis may be augmented due to the greater need in order to maintain the integrity of cardiac function and stabilize the shape of the cells.

For 2D constructs, compared to the control unstimulated group, SERCA2a protein synthesis in the stimulated tissue increased. However, the result from gene expression showed no statistically significant change in the SERCA2a gene expression including the 3D ECT constructs. In the cardiac cells, the sarcoplasmic reticulum where Ca²⁺ is stored during the relaxing phase becomes functional only around birth and embryonic chick CM are known to have immature SR,¹⁵⁵ hence, it is understandable to show no significant difference in SERCA gene expression. Further, the level of PLN in the CCCM tissues was not significantly increased, compared to the static culture tissue, indicating that cells did not undergo negative regulation in response to mechanical stimulation within the CCCM system. In addition, the amount of total protein obtained from the conditioned group was higher than the control one. All these results affirm that mechanical stimulation during embryogenesis mainly enhanced proliferation rate rather than increase gene expression for SERCA. Understanding these biomechanical responses of the cardiac embryonic cells will be important for engineering myocardial tissue studies.

The two cardiac MHC isoforms reciprocally shift their expression depending on the developmental stage and physiological condition of the heart. Before birth, β -MHC is the main MHC isoform in the ventricle. After birth, β -MHC reduces dramatically but α -

MHC increases significantly and becomes the main MHC isoform. The reversal of these 2 MHC isoforms is seen under heart failure diseases or in an aging heart in which β -MHC is dominant. Our results showed no significant change of the α - and β -MHC gene expression and the protein synthesis within 2D construct groups. First, no increase in the β -MHC gene expression indicates that tissues undergoing mechanical treatment in the CCCM system may become more mature and are not overstressed, which was supported by the PLB gene expression level above. Second, this study was performed during the embryonic and fetal stage, five days before hatching, indicating that the α -MHC expression will not be dominant yet. Third, the expression of these isoforms is controlled by thyroid hormone T3.⁶⁴ Applying mechanical stimulation at an early stage of cardiac tissue development may not be enough to promote α - and β -MHC gene expression, as well as protein synthesis. In fact, the gene expressions and the reciprocity of these MHC isoforms are controlled by developmental stages and thyroid hormone T3. ^{64, 156} Therefore, for further maturation of the tissue, besides mechanical conditions, the thyroid hormone needs to be included to generate more MHC, especially when dealing with embryonic cardiac tissue engineering for tissue transplant.

6.7. CONCLUSION

We have demonstrated that early mechanical stimulation during embryogenesis is needed for tissue proliferation, maturation, responses to the β -adrenergic agonist, and protein synthesis. Mechanical stimulations also help to maintain the calcium regulation inside the cells. These results prove that CCCM system is a novel system to insert the *in-vitro* mechanical stimulation on cardiac tissue; therefore, holds significant promise for
generation of functional cardiac patches for replacement of injured cardiac tissue. 3-D cell culture in CCCM with incorporation of thyroid hormone and mechanical stimulation may be necessary for cardiac tissue engineering.

CHAPTER 7 CONCLUSION

7.1. SUMMARY

CVD continues to be a major global healthcare dilemma. Current treatment options, though beneficial, have significant limitations. In order to address these issues and provide new treatment options, a better understanding of the molecular pathophysiology of CVDs is necessary. Cellular level models provide the best platform for discovery based studies. However, current approaches for cardiac cell culture fail to accurately replicate the mechanical loading conditions seen *in-vivo* as a consequence of normal hemodynamic loading and unloading. Available techniques address mechanical loading on an individual basis, but to date, no system that accurately replicates the *in-vivo* mechanical loading environment exists. This has resulted in cell-level studies being conducted in environments with little or no physiological relevance.

The CCCM system was designed and developed to culture various cardiac cells in a physiologically relevant environment by replicating the mechanical loading conditions generated as a consequence of normal hemodynamic loading and unloading. Various variables like cyclic pressure, strain and shear can accurately be replicated in a pulsatile fashion similar to conditions experienced in the left ventricle of a heart. Characterization

studies show that mechanical loading profiles associated with normal and various disease conditions of the human heart, including heart failure, hypertension, hypotension, bradycardia and tachycardia can be accurately replicated over extended periods of time. Finally, proof-of-concept studies using primary chick embryonic ventricle cardiomyocytes confirms the ability of this system to generate *in-vivo* like mature cardiac tissue cultured within this platform in phenotype, function and gene expression.

Thus far, characterization and proof-of-concept demonstrations were accomplished using this CCCM system. Confirmation of the ability of the CCCM system to accurately mimic the *in-vivo* cardiac environment allows for the design and study of various conditions associated with CVD. These future studies are likely to include cardiomyocyte regeneration such as stem cells or adult cardiomyocyte regeneration using a mechanical loading environment, study of cardiac and aortic endothelial cells under conditions of continuous and pulsatile flow,^{114, 115} and finally evaluation of drugs and other treatment options using cardiac cells maintained under various disease conditions.

7.2. LIMITATIONS

The CCCM system, however, has some limitations, including its complexity, the absence of an authentic 3D cell culture, and lack of electrical and hormonal factors. First of all, due to the complication of the system (tubes, valves, and multiple layers), it is time consuming to set up one experiment which includes the cleaning, setting, and operating processes. These can easily create a high risk of cross-contaminations. Second, ECM was constructed before seeding the cells; once seeded, the cells attach well on the surface of the ECM. Generated tissues hence cannot be easily detached from the crosslinking collagen matrix, which can create a serious issue for tissue transplant or tissue regeneration. Thirdly, cardiomyocytes cultured in this system are in 2 dimensions on the top of the gel matrix, not inside the matrix, therefore lack of a 3D ECM model, which affects the development of the cardiac tissue including gene expression. Finally, beside physiological and mechanical aspects, *in-vivo* cardiomyocytes are influenced by electrical and hormonal stimulation. Mechanical, hormonal, and electrical aspects need to be incorporated simultaneously for cardiomyocyte culturing.

7.3. FUTURE WORK

The CCCM system opens a wide opportunity to understanding the behavior of cardiac cells on molecular and cellular levels. It also provides an excellent tool to regenerate mature cardiac tissue for tissue transplant, which is our ultimate goal. From the previous chapters, cardiac tissues cultured in the CCCM system become more mature via higher beat rate, more alignment, and stronger contraction,. However, in this study, cardiac cells were cultured on the surface of a soft collagen matrix and under mechanical stimulations of a normal heart condition. For tissue regeneration or tissue transplant, it is necessary to generate the 3D tissue without collagen matrix attached. For molecular and cellular studies, understanding the impact of mechanical stimulation for different cardiovascular conditions on a heart tissue is crucial to provide a better treatment options for CVD. In addition, with electrical pacing, the beating rate and the contraction increase significantly. This electrical pacing for the *in-vitro* cardiac tissue can be considered as the sinoatrial node in the heart, which generates impulses to the cardiac tissue at the greatest

frequency.¹¹⁰ With these perspectives, the future works for this CCCM project might include:

1. Using higher vertebrate (mammalian) tissues with 3D cell culture

Embryonic chick cardiac cells have been commonly used in studies. However, tissues from higher mammal levels are more relevant to the human tissues. Also, cardiac tissue is more physiologically relevant to the *in-vivo* cardiac tissue if it is cultured within a 3D matrix. In addition, it is much better to use human iPS cell lines to study cardiac tissue behavior and regenerate tissues. Similar to the Flexcell system, 3D cell culture can be done in the cell culture chamber. In this case, the crosslinking matrix ring serves as an anchor for the cell to attach and keep the tissue from forming a ball. Primary testing results (not shown) proves that this technique can be used for cardiac culture under the mechanical stimulation in the CCCM system and warrants further investigation.

2. Studies the effects of mechanical stimulations from various heart conditions

Chapter 5 shows that this CCCM system is capable of replicating different pathological conditions. Molecular and cellular studies of cardiac tissue under pathological conditions can be specifically investigated.

3. Create a co-existing electrical and mechanical stimulation within the system.

Pilot studies with the CCCM system were conducted with simultaneous electrical and mechanical stimulation. The next step is to build a network for field electrical stimulation inside the cell chamber. When mechanical stimulations causing the tissue to go up and down, stretched and contracted, the electrical network must ensure that it won't create friction or tear the tissues apart.

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APPENDIX

LIST OF ABBREVIATIONS

A _o	Original cross-sectional area
AC	Adenyl cyclic
AR	Adrenergic Receptor
ATP	Adenosine triphosphate
BSA	Bovine Serum Albumin
BrdU	Bromodeoxyuridine
BR	Beat rate
cAMP	cyclic Adenosine Monophosphate
Ca ²⁺	Calcium ion
СВ	Cork Borer
CCCM	Cardiomyocyte Cell Culture Model
СМ	Cardiomyocytes
CNC	Computer Numerical Control
cm	centimeter
CVD	Cardiovascular disease
d	Diameter
DI water	De-ionized water

DMEM	Dulbecco's Modified Eagles's Medium
Е	Young's Modulus
ECM	Extra-cellular matrix
F	Tensile force
FBS	Fetal Bovine Serum
FEA	Finite Element Analysis
h	Height
HF	Heart Failure
НН	Hamburger Hamilton
ID	Inner diameter
ISO	Isoproterenol
1, L	Length
Lo	Original length of the membrane
LV	Left ventricle
LVAD	Left ventricle assistant device
L ₀	Length between two black dots at 0.0 mmHg
L _f	Length between two black dots after pressure is applied
MHC	Myosin Heavy Chain
mL	Milliliter
mm	Millimeter
Ν	Total number of the sample
OD	Outer diameter
PBS	Phosphate Buffer Saline

PDMS	Polydimethyl siloxane
PFA	Paraformaladehyde
РКА	Protein Kinase A
PLB, PLN	Phospholamban
pPLB, pPLN	Phosphorylated phospholamban
R	Radius
R _f	Final radius
R _i	Initial radius
RIE	Reactive Ion Etcher
rpm	revolution per minute
RT	Room Temperature
SERCA2a	Sarcoplasmic reticulum calcium ATPase 2a
SR	Sarcoplasmic reticulum
TnT	Troponin T
V	Volume
_	Engineering stress
0	Engineering suess
σ^*	True stress
3	Engineering strain
£*	True strain
ε _r	Radial strain
ε _c	Circumferential strain
λ_{c}	Circumferential stretch ratio
τ	

	Shear stress
μ	Viscosity
μCCCΜ	Microfluidic cardiac cell culture model
μL	Microliter

CURICULLUM VITAE

MAI-DUNG THI NGUYEN dmnguy01@gmail.com

The University of Louisville, KY
Pursuing a PhD in Mechanical Engineering focusing in Biomedical
Research
<u>Project:</u> The Second Generation of CCCM System for In-Vitro
Cardiac Tissue Engineering
Month for graduation: 08/2014
The University of Louisville, KY
MS in Mechanical Engineering/Biomedical Research
The University of Oklahoma, OK
BS in Chemical Engineering/ Biotechnology Option

Professional Experience:

05/2007- present	Graduate Research Assistant Mentor and co-mentors: Dr. G. Giridhan, Dr. P. Sethu, and Dr. B. Keller	
	 + Bioengineering Engineering Department, the University of Louisville, KY + Pediatric Cardiac Research Department, the University of Louisville, KY 	
	 + Design, fabricate, validate and operate systems for cardiovascular research. + Mentor and train middle school, high school, undergraduate and new coming graduate students. 	
08/2005- 05/2007	Research Technologist II Supervisor : Dr. B. Clark Biochemistry & Molecular Biology Department, the University of Louisville, KY <i>Study the effects of Bt</i> ₂ <i>cAMP on the expression of COUP-TF,</i> <i>STAR, and SF-1 in diabetic diseases.</i>	

08/2004- 08/2005	Research Technologist II Supervisors : Dr. P. Feldhoff and Dr. H. Lassiter. Pediatrics and Neonatology Department, the University of Louisville, KY <i>Study the regulation of C₂ and C₂ in stroked infant rat brain</i>
11/1999- 06/2003	Research Assistant
	Supervisor: Dr. L. Griffith
	Department of Neuroscience and Biochemistry, Brandeis University, MA
	Study the effect of eag Potassium Channel on Calcium/
	Calmodulin Dependent Protein Kinase II

Publications in Journals:

- Mai-Dung Nguyen, Joseph P. Tinney, et.al; *Cardiac Cell Culture Model as a Left Ventricle Mimic for Cardiac Tissue Generation*; Anal. Chem., August 16, 2013.
- Rosendo Estrada, Guruprasad A. Giridharan, Mai-Dung Nguyen, et.al, Endothelial Cell Culture Model for Replication of Physiological Profiles of Pressure, Flow, Stretch, and Shear Stress in Vitro, Anal. Chem., April 15 2011, 83 (8), pp 3170-7
- Rosendo Estrada, Guruprasad Giridharan, **Mai-Dung Nguyen**, et.al. *"Microfluidic Endothelial Cell Culture Model to Replicate Disturbed Flow Conditions Seen in Atherosclerosis Susceptible Regions"* Biomicrofluidics, 5, 032006, 2011
- Mai-Dung Nguyen, Guruprasad Giridharan, Rosendo Estrada, et al, "*Microfluidic Cardiac Cell Culture Model (μCCCM)*" Anal. Chem., 2010, 82
 (18), pp 7581–7587.
- William N. White, Ashok Raj, **Mai-Dung Nguyen**, et al, "*Clinical application of microfluidic leukocyte enrichment protocol in mild phenotype sickle cell disease (SCD)*." Biomed Microdevices (2009) 11:477-483
- Lori A. Devlin, **Mai-Dung Nguyen**, et. al. "*Effects of endotoxin administration and cerebral hypoxia-ischemia on complement activity and local transcriptional regulation in neonatal rats.*" Neuroscience Letters, Vol. 390, Issue 2, December 23, 2005, p. 109-113.

• Xiu Xia Sun, James J.L Hodge, Yi Zhou, **Mai-Dung Nguyen**, and Leslie C. Griffith., "*The eag Potassium Channel Binds and Locally Activates Calcium/ Calmodulin Dependent Protein Kinase II*." The Journal of Biological Chemistry, Vol. 279, No. 11, March 12, 2004, p. 10206-10214.

Selected Conference Proceedings:

- Mai-Dung Nguyen, Joseph P. Tinney, Fangping Yuan, Thomas Roussel, Guruprasad Giridharan, Bradley B. Keller, and Palaniappan Sethu, "Significant Mechanical and electrical stimulating effects on generation of 3D cardiac tissue via CCCM system.", Oral Presentation, September 27, BMES 2013, Seattle, WA
- **Mai-Dung Nguyen**, Joseph P. Tinney, Fangping Yuan, Thomas Roussel, Guruprasad Giridharan, Bradley B. Keller, and Palaniappan Sethu, "*An In-Vitro Model System for Generation of Mechanically Conditioned Cardiac Tissue Constructs*", Poster Presentation, April 12, MMB 2013, Marina De Rey, CA.
- **Mai-Dung Nguyen,** Joseph P. Tinney, Fangping Yuan, Bradley B. Keller, Guruprasad Giridharan, and Palaniappan Sethu, "*Cardiac Cell Culture Model for Cardiac Tissue Generation*." Oral Presentation, Oct. 25th, BMES 2012, Atlanta, GA
- Mai-Dung Nguyen, Kranthi K. Bhavanam, Awdhesh Kalia, Yongsheng Lian, and Palaniappan Sethu, "Microfluidic Cell Arrays for High-Throughput Culture." Poster Presentation, 2011 May 26th, 7th KIEC and 16th KY EPSCoR-Joint Conference, Louisville, KY
- **Mai-Dung Nguyen**, Guruprasad Giridharan, Rosendo Estrada, Sumanth D. Prabhu, and Palaniappan Sethu, "*Cardiac Cell Culture Model to Study Cardiomyocytes under Physiological Loads*." Poster Presentation, BMES 2010, October – The 2010 Annual Meeting of the Biomedical Engineering Society, Austin, TX
- Rosendo Estrada, Vahid Parichehreh, **Mai-Dung Nguyen**, and Palaniappan Sethu, *"Microfluidic Devices to Study the Effect of Atherogenic Flow Pattern on Cultured Endothelial Cells."* Poster Presentation, BMEMS 2010, October – The 2010 Annual Meeting of the Biomedical Engineering Society, Austin, TX
- Mai-Dung Nguyen, Guruprasad Giridharan, Sumanth D. Prabhu and Palaniappan Sethu, "Microfluidic Cardiac Circulation Model for Functional

Cardiomyocyte Studies ", Conf Proc IEEE Eng Med Biol Soc. 2009;1:1060-3, Minneapolis, MN

- **Mai-Dung Nguyen**, Guruprasad Giridharan, Palaniappan Sethu, "*Cardiomyocyte Acutuator for Microfluidics Platform Nozzle-Diffuser Pump*." Poster presentation, MicroTAS 2008, October- Twelfth International Conference on Miniaturized System for Chemistry and Life Science, San Diego, CA.
- William White, **Mai-Dung Nguyen**, and Palaniappan Sethu, "*Microfluidics* enumeration protocol for comprehensive profiling of nucleated cells in mild phenotype sickle cells disease (SCD)." Poster presentation, MicroTAS 2008, October- Twelfth International Conference on Miniaturized System for Chemistry and Life Science, San Diego, CA.
- Bobby L. Gibbons, Mai-Dung Nguyen, Guruprasad Giridharan, Mohammed Ishmahil, Sumant D. Prabhu and Palaniappan Sethu, "Microfluidic Platform to Study Cardiomyocyte Mechanotransduction", Research Louisville! 2008, Louisville, KY. (2nd Place, Interdisciplinary Research Category)

Invention Disclosures:

Palaniappan Sethu, Guruprasad Giridharan, Rosendo Estrada, **Mai-Dung Nguyen** and Sumanth D. Prabhu, "*Cardiac and Endothelial Cell Culture Models and Methods*."

Honors and Affiliations:

2010-present	Southern Regional Education Board (SREB) Doctoral Fellow Scholarship
2010-present	Member of Biomedical Engineering Society
2009-present	Member of the Society of Engineering Women
2008	Best Poster Award Team, University of Louisville, Engineering Expo
1999	Second Team Work Award with the Senior Design Project of Energy Retrofit
1998	Best Award for Laboratory Chemical Engineering Advanced Design

Other Achievements and Professional Conference Attendances:

05/2013	Receive a certificate for Graduate Teaching Academy.
10/2013	Attend "Institute on Teaching and Mentoring: Faculty Diversity", Arlington,
	VA.
10/2011	Attend "Institute on Teaching and Mentoring: Faculty Diversity", Atlanta, GA.
10/2010	Attend "Institute on Teaching and Mentoring: Faculty Diversity", Tampa, FL.

Outreach Activities:

10/2005-present	St. JOHN VIANNEY CHURCH, KY Teach Sunday Catechism
4/2/2011	LOUISVILLE SCIENCE CENTER, KY Participate the demo " <i>Heart on a chip</i> " Bioengineering Activities for Nanodays.
3/1/2011	UNIVERSITY of LOUISVILLE, KY Participate in the demo " <i>Cardiovascular Cell Culture Model</i> " Engineering Career Day
01/2007-11/2007	BAPTIST EAST HOSPITAL, KY Participate in <i>Pastoral Care Ministry</i>
10/1999-06/2003	St. WILLIAM CHURCH, MA Teach Sunday <i>Catechism</i>

References:

Provided upon request