# MULTISCALE DYNAMIC MONTE CARLO / CONTINUUM MODELING OF DRYING AND CURING IN SOL-GEL SILICA FILMS 

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# ABSTRACT OF DISSERTATION 

Xin Li

The Graduate School
University of Kentucky
2008

# MULTISCALE DYNAMIC MONTE CARLO / CONTINUUM MODELING OF DRYING AND CURING IN SOL-GEL SILICA FILMS 

## ABSTRACT OF DISSERTATION

A dissertation submitted in partial fulfillment of the requirements for the degree of Doctor of Philosophy in the College of Engineering at the University of Kentucky

By<br>Xin Li<br>Lexington, Kentucky

Director: Dr. Stephen E. Rankin, Associate Professor of Chemical Engineering Lexington, Kentucky

2008

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ABSTRACT OF DISSERTATION

## MULTISCALE DYNAMIC MONTE CARLO / CONTINUUM MODELING OF DRYING AND CURING IN SOL-GEL SILICA FILMS

Modeling the competition between drying and curing processes in polymerizing films is of great importance to many existing and developing materials synthesis processes. These processes involve multiple length and time scales ranging from molecular to macroscopic, and are challenging to fully model in situations where the polymerization is non-ideal, such as sol-gel silica thin film formation. A comprehensive model of sol-gel silica film formation should link macroscopic flow and drying (controlled by process parameters) to film microstructure (which dictates the properties of the films).

This dissertation describes a multiscale model in which dynamic Monte Carlo (DMC) polymerization simulations are coupled to a continuum model of drying. Unlike statistical methods, DMC simulations track the entire molecular structure distribution to allow the calculation not only of molecular weight but also of cycle ranks and topological indices related to molecular size and shape. The entire DMC simulation (containing $10^{6}$ monomers) is treated as a particle of sol whose position and composition are tracked in the continuum mass transport model of drying. The validity of the multiscale model is verified by the good agreement of the conversion evolution of DMC and continuum simulations for ideal polycondensation and first shell substitution effect (FSSE) cases.

Because our model allows cyclic and cage-like siloxanes to form, it is better able to predict the silica gelation conversion than other reported kinetic models. By studying the competition between molecular growth and cyclization, and the competition between mass transfer (drying) and reaction (gelation) on the drying process of the sol-gel silica film, we observe that cyclization delays gelation, shrinks the molecular size, increases the likelihood of skin formation, and leads to a molecular structure gradient inside the film. We also find that compared with a model with only 3-membered rings, the molecular structure is more complicated and the structure gradients in the films are larger with 4membered rings. We expect that our simulation will allow better prediction of the formation of structure gradients in sol-gel derived ceramics and other nonideal multifunctional polycondensation products, and that this will help in developing
procedures to reduce coating defects.
KEYWORDS: Multiscale modeling, sol-gel silica films, dynamic Monte Carlo, polycondensation, cyclization

# MULTISCALE DYNAMIC MONTE CARLO / CONTINUUM MODELING OF DRYING AND CURING IN SOL-GEL SILICA FILMS 

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# DISSERTATION 

Xin Li

The Graduate School

University of Kentucky
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at the University of Kentucky


#### Abstract

By Xin Li Lexington, Kentucky Director: Dr. Stephen E. Rankin, Associate Professor of Chemical Engineering Lexington, Kentucky

2008


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$$
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## Chapter 1

## Sol-Gel Silica Chemistry for Multiscale Modeling of Drying and Curing

### 1.1 Motivation

Sol-gel silica films are of growing interest as engineered materials for a variety of applications ${ }^{[1,}{ }^{2]}$, e.g. sensor concentrators ${ }^{[3-9]}$, optical materials ${ }^{[10-15]}$, electrical insulators ${ }^{[16]}$, drug-delivery carriers ${ }^{[17]}$, and solar energy applications ${ }^{[18]}$. In sol-gel film processing, a continuous liquid phase displaces air at the substrate through a wetting process and undergoes a process of drying and polycondensation to form a stable porous film ${ }^{[19]}$. The sol-gel film forming process itself is the link between the structure and properties of the liquid precursor sol and the microstructure of the corresponding deposited film ${ }^{[20]}$. Tradeoffs between evaporation, diffusion, reaction and self-assembly have been hypothesized or shown to play significant roles in the synthesis of these films ${ }^{[19,20]}$. Evaporation is extremely important in forming well-defined microstructures in the sol-gel process. However, the process is not fully understood and the effect of process parameters is not entirely known. As a result, coating procedures are often developed by trial and error rather than by design. Modeling is a useful tool to better predict the formation of sol-gel silica films and to investigate the effects of process parameters. However, the sol-gel film formation process necessitates simultaneously modeling multiple length and time scales ranging from molecular to macroscopic. Macroscopic parameters control the formation of the film; diffusion and mass transport occur over micron or greater lengths scales, and define the concentration fields within which polymerization and self-assembly occur. These processes are best modeled with continuum methods and described by deterministic PDEs. At the same time, polymerization and (if surfactants are added) self-assembly processes occur which control the film properties such as film microstructure at the molecular level. However, the continuum assumption breaks down at such a small length scale and a molecular modeling technique should be applied ${ }^{[21]}$. Therefore, a multiscale model should be used to link these different length and time scale together. This multiscale model links
molecular-level structure to macroscopic parameters, and can be used to better control the film deposition, film uniformity, coating microstructure and final film thickness. In this chapter, the chemistry of sol-gel silica precursors will be reviewed as a prelude to the subsequent chapters regarding a multiscale model of sol-gel film formation, and the remainder of the dissertation will be outlined.

### 1.2 Sol-gel chemistry

In order to model sol-gel silica film formation, we first need to understand sol-gel chemistry. During the sol-gel process, a liquid sol is transformed into a liquid-filled solid gel phase. Inorganic or metal organic precursors which are dissolved in aqueous or organic solvents are subjected to a series of hydrolysis and condensation reactions to form the sol ${ }^{[19,20]}$. With further polycondensation reactions, the sol may be transformed into an extended three-dimensional network structure, which is a gel ${ }^{[20,22]}$. We focus our research on the reactions that occur in acid-catalyzed silicon alkoxide solution (especially using tetraethyoxysilane (TEOS) as example). This type of solution is commonly used when preparing thin films because these conditions favor slow curing and uniform films. The functional group-level reactions of silane precursors are as follows: Hydrolysis:

$$
\begin{equation*}
\equiv \mathrm{Si}-\mathrm{OR}+\mathrm{H}_{2} \mathrm{O} \stackrel{K_{h}}{\longleftrightarrow} \equiv \mathrm{Si}-\mathrm{OH}+\mathrm{R}-\mathrm{OH} \tag{1.1}
\end{equation*}
$$

Water-producing condensation;

$$
\begin{equation*}
\equiv \mathrm{Si}-\mathrm{OH}+\mathrm{HO}-\mathrm{Si} \equiv \rightarrow \equiv \mathrm{Si}-\mathrm{O}-\mathrm{Si} \equiv+\mathrm{H}_{2} \mathrm{O} \tag{1.2}
\end{equation*}
$$

Alcohol-producing condensation:
$\equiv \mathrm{Si}-\mathrm{OR}+\mathrm{HO}-\mathrm{Si} \equiv \rightarrow \equiv \mathrm{Si}-\mathrm{O}-\mathrm{Si} \equiv+\mathrm{R}-\mathrm{OH}$
Assuming that reactivity depends on the state of hydrolysis and condensation of a site (in other words, on the identity of the three ligands that are not explicitly shown in Eq. (1.1)-(1.3)) and assuming that all the reactions are irreversible, there are 15 different silica species and a total of 165 reactions ( 10 hydrolysis reactions, 55 water-producing condensation and 100 alcohol-producing condensation reactions) ${ }^{[23]}$ when only nearest neighbor ligands are considered. In order to model this complicated system, some assumptions and simplifications are needed. On the basis of previous research on acidcatalyzed silica sol-gel polymerization, there are three necessary modeling features that
can be used to create a simplified but accurate model: hydrolysis pseudoequilibrium, a First Shell Substitution Effect (FSSE) for condensation reactions and extensive cyclization to form primarily tetrasiloxane rings. In the following sections, we will give more details about these three modeling features and some assumptions.

### 1.2.1 Hydrolysis Pseudoequilibrium

Experiments have shown that under acid-catalyzed conditions, hydrolysis reactions of alkoxysilanes are much quicker than condensation reactions ${ }^{[24]}$, and that the hydrolysis reaction can nearly reach equilibrium while condensation has proceeded to a negligible extent ${ }^{[25,26]}$. Prior to the onset of significant condensation, hydrolysis is considered to be in a pseudoequilibrium state ${ }^{[27]}$. Rankin et al. ${ }^{[28]}$ have quantitatively demonstrated that this assumption can be made when hydrolysis rate coefficients are at least an order of magnitude greater than condensation rate coefficients. They also found similarities in the hydrolysis pseudoequilibrium behavior of methyl-substituted ethoxysilanes and found that all hydrolysis equilibrium coefficients are near $15 \pm 6^{[29]}$. Therefore, because of the difference in time scales for hydrolysis and condensation, "hydrolysis pseudoequilibrium is not only appropriate but also demanded if unique rate coefficients are to be determined" ${ }^{[28]}$. When it is at pseudoequilibrium, hydrolysis doesn't affect the development of polymer structure with respect to conversion. Only condensation reactions determine the evolution of polymer structure. This pseudoequilibrium condition allows one to characterize hydrolysis using only the average hydrolysis extent $\chi^{[28]}:$

$$
\begin{equation*}
\chi=\frac{[\mathrm{SiOH}]}{[\mathrm{SiOH}]+[\mathrm{SiOR}]} . \tag{1.4}
\end{equation*}
$$

Because hydrolysis equilibrium coefficients are all similar regardless of substitution, it is possible to regard $\chi$ as a constant for all silicon sites ${ }^{[29]}$. Also, if the amount of water is sufficient (for ethoxysilanes one mole of water per mole of silicon), $\chi$ can be regarded as constant with respect to time as well ${ }^{[30]}$.

### 1.2.2 First Shell Substitution Effect (FSSE)

Assink and Kay ${ }^{[24]}$ presented the functional group kinetics of alkoxysilanes, in which only three reactions are considered:

$$
\begin{align*}
& \mathrm{Si}-\mathrm{OR}+\mathrm{H}_{2} \mathrm{O} \rightarrow \mathrm{Si}-\mathrm{OH}+\mathrm{R}-\mathrm{OH} \text { (Hydrolysis) }  \tag{1.5}\\
& \mathrm{Si}-\mathrm{OH}+\mathrm{Si}-\mathrm{OH} \rightarrow \mathrm{Si}-\mathrm{O}-\mathrm{Si}+\mathrm{H}_{2} \mathrm{O} \text { (Water-producing condensation) }  \tag{1.6}\\
& \mathrm{Si}-\mathrm{OR}+\mathrm{Si}-\mathrm{OH} \rightarrow \mathrm{Si}-\mathrm{O}-\mathrm{Si}+\mathrm{R}-\mathrm{OH} \text { (Alcohol-producing condensation) } \tag{1.7}
\end{align*}
$$

This kinetic scheme assumes that the reactivities of functional groups are independent (notice that the other ligands attached to each site are not depicted in Eqs. (1.5)-(1.7)), which means the connectivity of the silica site doesn't change the reactivity of the reacted functional group. In other words, each reaction in Eqs. (1.5)-(1.7) has a single unique rate coefficient that does not change with respect to conversion. This is one of the assumptions made in an 'ideal' polycondensation model. Another ideal assumption is that there are no cyclization reactions ${ }^{[31]}$. We refer to the scheme satisfying these ideal assumptions as the ideal polycondensation case, which will be discussed in more detail in Chapters 2 and 3.

While the equal reactivity assumption mentioned above captures the basic reactions that can occur during sol-gel ceramic synthesis, many researchers have found that a strong, negative first shell substitution effect (FSSE) exists for condensation ${ }^{[30,32-34]}$. A substitution effect is a departure from ideal polycondensation ${ }^{[35]}$. It means the reactivity of a site is changed by substitution of the ligands attached to that site. For a FSSE, only the four nearest neighbor functional groups affect the reactivity of the silicon site for subsequent hydrolysis and condensation steps ${ }^{[23,35,36]}$. According to the experimental observations of reactivity of sol-gel silica oligomers and of bulk NMR trends, FSSE should be considered as part of a sol-gel silica polymerization model.

### 1.2.3 Bimolecular Site-level Condensation

Pouxviel and Boilot ${ }^{[32]}$ first proposed that reactions of silanes should be considered to be between sites (a silicon atom and its neighboring ligands) and not between molecules. With the premise of hydrolysis pseudoequilibrium and FSSE, there are still 155 condensation reactions left to be considered (if degree of hydrolysis of the reacting sites is assumed to affect condensation). By making the reasonable assumption that water-
producing condensation reactions dominate over alcohol-producing condensation reactions ${ }^{[24,37]}, 100$ alcohol-producing condensation reactions can be neglected. After this simplifying assumption, 55 water-producing condensation reactions remain in the model. Fortunately, the problem can be further simplified according to the studies that have been done by Sanchez ${ }^{[30]}$ and Rankin ${ }^{[27]}$. Since $\chi$ is almost a constant for all silicon sites after hydrolysis pseudoequilibrium is reached, the degree of hydrolysis has little observable effect on the condensation rate coefficients ${ }^{[30]}$. Therefore, the condensation rate coefficients can be isolated and defined only by the degrees of condensation of the two reacting sites that are involved ${ }^{[30]}$. Thus, only 5 species and 10 bimolecular site-level condensation reactions need to be considered in our modeling. The set of bimolecular condensation reactions among silicon sites can be simplified to ${ }^{[38]}$ :

$$
\begin{equation*}
Q_{i}+Q_{j} \xrightarrow{k_{i j}} Q_{i+1}+Q_{j+1}+H_{2} O \quad i, j=0,1,2,3 \tag{1.8}
\end{equation*}
$$

where $Q_{i}$ represents a tetrafunctional silicon site with $i$ siloxane bonds. For these reactions, the rate expressions are ${ }^{[38]}$ :

$$
R_{i j}^{b i m o l}= \begin{cases}\chi^{2}(f-i)(f-j) k_{i j}\left[Q_{i}\right]\left[Q_{j}\right], & i \neq j  \tag{1.9}\\ \frac{1}{2} \chi^{2}(f-i)(f-j) k_{i j}\left[Q_{i}\right]\left[Q_{j}\right], & i=j\end{cases}
$$

where $k_{i j}$ is the rate constant of bimolecular polycondensation (defined as reactivity per unit of silanol concentration), and $f$ is the functionality of the monomer (which is equal to 4 here). The site concentrations without superscripts are given by:

$$
\begin{equation*}
\left[Q_{i}\right] \equiv \sum_{j=1}^{f-i}\left[Q_{i}^{j}\right] \tag{1.10}
\end{equation*}
$$

where the subscript $i$ represents the number of siloxane bonds, superscript $j$ represents the number of hydroxyl group, and $\left[Q_{i}^{j}\right]$ is the concentration of $Q_{i}^{j}$. If we set

$$
\begin{equation*}
k_{i j}^{*} \equiv k_{i j} \cdot \chi^{2}, \tag{1.11}
\end{equation*}
$$

the rate expressions are re-expressed as:

$$
R_{i j}^{b i m o l}= \begin{cases}k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i \neq j  \tag{1.12}\\ \frac{1}{2} k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i=j\end{cases}
$$

The rate coefficients are set according to the experimental trend (negative FSSE), letting the values drop by an order of magnitude down the diagonal and decrease by $10 \%$
across each row ${ }^{[27,38,39]}$. These numbers are not exactly the experimentally observed values, but they capture the trend of a substitution reaction which preferentially occurs by inversion at the less sterically crowded site.

$$
K^{*}=k_{00}^{*}\left[\begin{array}{cccc}
1.0 & 0.9 & 0.81 & 0.729 \\
& 0.1 & 0.09 & 0.081 \\
& & 0.01 & 0.009 \\
& & & 0.001
\end{array}\right]
$$

### 1.2.4 Cyclization

All of the discussion above centered on bimolecular reactions where reacting sites are treated as independent. This type of modeling was typical in the sol-gel field up until the mid-90s. However, if cyclization (intramolecular reaction) is omitted, the maximum value of gel conversion that can be predicted with an FSSE kinetic model is about $50 \%$ for a tetrafunctional monomer, which can only be reached if very weakly branched structures are formed ${ }^{[27,31]}$. However, researchers have verified that siloxane cyclization is a nonrandom, preferred reaction ${ }^{[40-42]}$ that delays the gel conversion of tetraalkoxysilanes to about $82 \%{ }^{[43-45]}$. This is not the only evidence for the importance of cyclization; 3- and 4-membered rings (meaning that they contain 3 or 4 silicon sites) are found by different analytical techniques, most notably and clearly ${ }^{29}$ Si $\mathrm{NMR}^{[27, ~ 40-42, ~ 44, ~ 46-~}$ ${ }^{56]}$. Researchers have also presented several likely reasons for the importance of cyclization in siloxane-based systems. West and coworkers ${ }^{[40]}$ proposed on the basis of computational chemistry that cycle formation reactions are energetically favored over chain extension. Tang et al. ${ }^{[41]}$ suggested that ring formation is favored because of the high flexibility of siloxane chains. Both Sanchez et al. ${ }^{[42]}$ and Ng et al. ${ }^{[52]}$ presented kinetic results that favor cyclization during sol-gel silica polymerization. Ng et al. ${ }^{[52]}$ also pointed out that structure stabilization or changes in functional group reactivity (in the same molecule) can help to promote cyclization. Hence, we know that cyclization is very important at the molecular scale in the sol-gel coating process so that it should not be neglected at all. Models without cyclization may be able to match a selected set of data (such as ${ }^{29}$ Si NMR site concentrations) but the data will be fit with incorrect parameters and the models are likely to give incorrect predictions of other, more global properties (such as the point at which a gel forms). Therefore, cyclization should be taken into
account in the sol-gel polymerization process modeling. The details about implementation of cyclization in dynamic Monte Carlo modeling will be given in Chapters 4 and 5.

### 1.3 Dissertation Outline

This dissertation is organized as follows:
Chapter 2. Simulation Methods: There are two parts to this chapter corresponding to the elements that are brought together in the multiscale approach used here. The first part is about the molecular simulation technique - dynamic Monte Carlo (DMC). The second part is about the continuum method - finite difference method (FDM) as it is applied to the modeling of drying coating solutions. In both parts, after a review of other methods, a description of the simulation method algorithm will be given, and an example of the ideal polycondensation case is given for the DMC method.

Chapter 3. Multiscale Modeling of Ideal Polycondensation and FSSE: In this chapter, two relatively simple cases are used to show ways to couple molecular and continuum processes together. This type of coupling of modeling strategies is new in that it involves a polymerization process that occurs throughout the entire continuum domain rather than at a boundary. The validity of our multiscale model can be verified by the modeling the evolution of conversion in each of these two cases. Although these cases exclude cyclization, they can also show competition between drying and gelation, predict different drying / gelation phenomena, and predict the occurrence of gradients of concentration and gelation in the films. In extreme cases, gelation gradients can lead to the formation of a gel skin near the top surface of the film, which is thought to be a site for nucleation of defects in films such as wrinkles and cracks.

Chapter 4. Multiscale Modeling of Unlimited 3-membered Ring Cyclization: This chapter describes the addition of cyclization reactions to our multiscale model, but only cyclization reactions allowing the formation of 3-membered rings. This multiscale model is the first one coupling unlimited cyclization in polycondensation with continuum mass transfer process. It is also the first model that can predict the structure gradient throughout drying sol-gel films, as hypothesized in earlier work with closed dynamic Monte Carlo simulations.

Chapter 5. Multiscale Modeling of Unlimited 4-membered Ring Cyclization: This chapter presents the first dynamic Monte Carlo model that can simulate unlimited 4membered ring cyclization. This is important because 4-membered rings are the dominant cyclic structural units in real sol-gel silicates. Compared with 3-membered ring cyclization, the number of potential rings in the 4-membered rings cyclization is greater and the molecular structure of the products is more complicated with a dimensionless cyclization tendency $\kappa \geq 5$ (a physically reasonable value for sol-gel polymerization). At the same process conditions ( $B i, D a$ and $\kappa$ ), films with 4-membered ring cyclization gel more quickly, have more number-average cycle rank per molecule, and display more extreme structure gradient than films with only 3-membered rings. The inclusion of 4membered rings in this chapter represents a significant advance in our ability to quantitatively model sol-gel polymerization in thin films.

Chapter 6. Conclusions: A summary of the whole dissertation is presented along with a brief discussion about future opportunities presented by the work that has been done so far.

Chapters 3, 4 and 5 are under revision as journal manuscripts and will be submitted for peer-reviewed publications soon.

## Chapter 2

## Introduction to Molecular and Continuum Simulation Methods

### 2.1 Molecular Modeling Technique - Dynamic Monte Carlo (DMC) Method

### 2.1.1 Introduction

The Monte Carlo (MC) method is a stochastic simulation technique ${ }^{[57]}$. Using random numbers and probability, the Monte Carlo method allows one to study problems that are difficult or impossible to solve deterministically or are encountered during the evolution of a finite population ${ }^{[58]}$. In Monte Carlo simulations, integration is approximated through a random event selection process which is repeated many times to create multiple realizations of a sequence of events. Each time one event is randomly selected, it represents a step in one possible configuration and solution to the problem. Together, these configurations give a range of possible solutions, some of which are more probable and some less probable. When repeated for many configurations ( 10,000 or more), the average solution will give an approximate answer to the problem ${ }^{[58,59]}$. Accuracy of this answer can be improved by simulating more realizations of the sequence of events or, in the case of population balance modeling, by using a larger population ${ }^{[58,60]}$. For Monte Carlo method, the finite size of the population is the primary source of error ${ }^{[58]}$ and it restricts the maximum simulated length scale ${ }^{[38,61]}$.

In statistical physics, Monte Carlo methods are often used to sample the configurations of a system that contribute most to the average properties of that system. For instance, in molecular simulations at equilibrium, a Monte Carlo method favors configurations with a high probability of being found according to the Boltzmann distribution, rather than calculating average properties by enumerating all possible configurations of the system of many particles. Similarly, in a Markov chain process (a sequence of events described by transition probabilities) such as polymerization, Monte Carlo simulations are used to sample only the chain structures that are likely to be realized by the kinetic scheme,
rather than needing to enumerate and solve kinetic equations for all possible polymer structures.

Monte Carlo simulations have been purposely used to capture the effects of fluctuations in small systems such as micro-fluidic reactors. As early as 1976, Gillespie ${ }^{[62]}$ proposed that the Monte Carlo method can be used for simulation of chemical kinetics in finite populations of molecules. He suggested that the Monte Carlo method is able to handle systems in which many chemical species participate in many highly coupled and highly nonlinear chemical reactions, and it takes full account of fluctuations and correlations near chemical instabilities ${ }^{[62]}$. Vlachos ${ }^{[63]}$ compared the instabilities in homogeneous non-isothermal reactors (CSTR), using deterministic and Monte Carlo methods. He suggested that the Monte Carlo method is uniquely suited to examine thermal fluctuations and finite size effects near critical points ${ }^{[63]}$.

In the last two decades, many researchers have found that Monte Carlo simulations are very good choices to model the sol-gel silica formation process and other network polycondensation reactions. Šomvársky and Dušek ${ }^{[61,64]}$ described a MC method for simulation of structure evolution in branched polymer systems and discussed the system size effect on network formation. They also discussed the disadvantages of other methods (e.g. cascade theory, recursive theory and percolation techniques) in the simulation of polymer network formation ${ }^{[61]}$. In contrast to the other statistically derived methods, the MC method can capture the complete reaction history for a finite set of monomers ${ }^{[61]}$. In particular, the additional network information such as molecular weight distribution and cycle rank distribution can be recorded during the simulation ${ }^{[64]}$, so MC simulations can provide more accurate results than other network polymer models such as a kinetic-recursive model ${ }^{[31,39,61]}$. The disadvantage of statistical approaches is that they derive average structural characteristics by assuming random assembly of some sort of building blocks. Even if a non-random kinetic feature such as a first-shell substitution effect (a dependence of condensation rate on prior condensation reactions) is included, correlations may be lost because the sites are essentially "cut up" and reassembled when properties like average molecular weight are computed, for example by a recursive approach. Hendrickson et $\mathrm{al}^{[35]}$ studied substitution effects in four-functional sol-gel precursors using a MC technique. They compared their results with analytical results to
confirm the accuracy of the MC method, and verified again that network properties can be calculated directly from the investigation of the network connectivity ${ }^{[35]}$, which is one advantage of MC method we just mentioned. Furthermore, the MC method has the flexibility to handle larger cycles and cages that are thought to play a significant role in the structure of sol-gel silica ${ }^{[43]}$. Hendrickson ${ }^{[65]}$, Kasehegen ${ }^{[39]}$, $\mathrm{Ng}^{[43]}$ and Rankin ${ }^{[27,38,}$ ${ }^{66]}$ et al. have shown how to use the Monte Carlo method to deal with cyclization reactions in sol-gel silica polycondensation, although they each treated cyclization somewhat differently. Compared with molecular dynamics simulations ${ }^{[67-69]}$ which are computationally intensive and have limitations in the accessible length and time scales, dynamic Monte Carlo simulations can simulate much larger systems and much longer times, and they are computationally efficient because each MC step is a reaction event ${ }^{[70]}$. A possible criticism of the MC approach is that kinetic parameters for the rates of bimolecular and cyclization reactions must be input into the simulation. However, these coefficients could hypothetically be derived from first-principles ab initio or molecular dynamics calculations based on transition state theory.

### 2.1.2 DMC Algorithm

Classical random branching theory (RBT) i.e. Flory-Stockmayer theory ${ }^{[71-73]}$ can provide an adequate prediction of the average properties of network polycondensation systems which satisfy the following 'ideal' assumptions ${ }^{[31,43]}$ : first, all of the functional groups have equal and independent reactivities; second, no cyclization reactions are allowed in the system. Here we use this ideal case as the example to illustrate the details of the DMC algorithm, and to verify the accuracy of the present implementation of the DMC method by comparing our simulation results with analytical results of RBT. Based on sol-gel chemistry discussed in Chapter 1 but not considering cyclization, we need to consider 10 condensation reactions among four differently connected silicon sites. This is a first-shell substitution effect (FSSE) model but it becomes ideal by setting all the rate constants equal to one another.

At the beginning of the simulation or the synthesis process, we have pure TEOS, so all the molecules are monomers (designated as $Q_{0}$ where the subscript indicates the number of siloxane bonds attached to a site). $R_{i j}(i$ from 0 to $3, j$ from $i$ to 3$)$ is used to denote the
reaction rate for one of the 10 condensation reactions between species $Q_{i}$ and $Q_{j}$. Although these rates are actually the product of the concentrations of the participants and a rate constant $k$, in the simulation, we calculate the reaction rates as the products of the populations of silicon sites and the rate constants, because we are only concerned with the relative reaction rates (for now - the concentration only becomes important when calculating the time evolution of the system, which will be discussed when needed in future chapters). In other words, we use are integral populations $\left\{Q_{i}\right\}$ to calculate $R_{i j}$, and not concentrations $\left[Q_{i}\right]^{[35, ~ 61]}$.

### 2.1.2.1 Data Structures

In the Monte Carlo simulation, we need to record a variety of information about the progress of the polycondensation process, such as the populations of silicon atoms with differing connectivities, molecular tags, the sizes of molecules, the molecule membership of the silicon atoms, and so on. The information contained in the data structures is updated after each step (reaction) for later interrogation. The data structures allow specific species to be selected randomly from the entire population when species of a particular type are needed to take part in a reaction.

The data structures used in the algorithm are as follows:

1) Silicon sites arrays: we use two one-dimensional arrays to store the information about silicon sites ( $Q$ species). One records the numbers of each type of $Q$ species $\left(Q_{i}\right)$, while the other is used to index the silicon sites. Each element of the latter array is a data structure, in which the information about molecular tag and membership is stored. The details are provided below.
2) Molecular tags ${ }^{[35]}$ : this array is used to identify the molecules. An integer tag is assigned to each molecule. In the beginning, all of the monomers have different molecular tags because they are unconnected to one another. In the bimolecular reaction, the product molecule is tagged with the tag of larger reactant molecule. All of the monomers (sites) on the same molecule have the same integer tag.
3) Membership: we keep track of molecule membership using four pointers to the four neighbors connected to each silicon site, indexed by silicon site number. The pointers are set to NULL for monomers. When a reaction occurs, a bond is formed between two sites,
and for each reactant site, one pointer to its new neighbor (the other reacting site) is added.
4) Size array ${ }^{[35]}$ : we use this array to record the sizes of molecules in the system. In the beginning, the sizes of monomers are all set to 1 . Using molecular tags as indices, in the bimolecular reaction, the length of the larger molecule is updated to be the sum of the sizes of the two reactants, while the length of the smaller one is set to zero.
5) Size distribution array: a linked list is used to keep track of the molecular weight distribution in the simulation. Each element of the linked list contains the information of molecular size, the number of molecules having this size and the pointer to the next member in the size distribution array.
6) Conversion: in the DMC simulation, because conversion is the fraction of functional groups that have condensed, it can be calculated as follows ${ }^{[35]}$ :

$$
\begin{equation*}
\alpha=\frac{\text { mol of condensed functional groups }}{\text { total mol of functional groups }}=\frac{[\mathrm{Si}-\mathrm{OSi}]}{4[\mathrm{Si}]}=\frac{2 \times S_{t}}{4 \times N} \text {, } \tag{2.1}
\end{equation*}
$$

where $S_{t}$ is the total number of DMC steps, and $N$ is the total number of monomers.
7) Gel point: In DMC simulations, the gel point can be estimated by the divergence of the weight-average degree of polymerization $\left(D P_{w}\right)^{[38]}$. $D P_{w}$ can be calculated directly from the molecular weight distribution as ${ }^{[38,64]}$ :

$$
\begin{equation*}
D P_{w}=\frac{1}{N} \sum_{i=1}^{N_{m o l}} L(i)^{2}, \tag{2.2}
\end{equation*}
$$

where $L(i)$ is the size of the molecules in the population, and $N$ is the total number of sites. A better way to find the value of gel conversion is to plot the reduced weight averaged degree of polymerization $\left(r D P_{w}\right)$ against conversion ${ }^{[38,74]} . r D P_{w}$ can be calculated by removing the largest molecule from the molecular weight distribution in the DMC simulation and recalculating $D P_{w}{ }^{[64]}$ :

$$
\begin{equation*}
r D P_{w}=\frac{\sum_{i=1}^{N_{m o l}} L(i)^{2}-\left(L_{\max }\right)^{2}}{N-L_{\max }}, \tag{2.3}
\end{equation*}
$$

where $L_{\text {max }}$ is the size of the largest molecule in the population. Below the gel point, $r D P_{w}=D P_{w}$; but $r D P_{w}$ drops sharply at gelation ${ }^{[64]}$. Therefore the value of conversion at gelation can be determined by the position of the peak in $r D P_{w}$.

### 2.1.2.2 Monte Carlo Reaction Selection

Monte Carlo reaction selection is used to make sure that reactions compete properly according to their relative rates. In Monte Carlo simulation, the rates are normalized into a set of probabilities $P_{i j}$ which (for bimolecular reactions only) are given by ${ }^{[35,39]}$ :

$$
\begin{equation*}
P_{i j}=\frac{R_{i j}}{\sum_{i=0}^{3} \sum_{j \geq i}^{3} R_{i j}} . \tag{2.4}
\end{equation*}
$$

A random number $r$ is used to choose a reaction. In our program, it is calculated based on a pseudo-random number generator - the ANSI C $\operatorname{rand}()$ function:

$$
\begin{equation*}
r=1.0 \times \operatorname{rand}() / R A N D \_M A X . \tag{2.5}
\end{equation*}
$$

In order to produce floating point numbers uniformly distributed over the interval $(0,1)$, we recalculate Eq. (2.5) if $r$ is equal to 0 or 1 . After a number is picked, the summation of probabilities is started in the sequence $\mathrm{P}_{00}, \mathrm{P}_{01}, \mathrm{P}_{02}$, etc. until the partial sum exceeds the random number. That is, if $\operatorname{sum}\left(i_{1}, j_{1}\right)<r \leq \operatorname{sum}\left(i_{2}, j_{2}\right)$, we choose the $i_{1} j_{1}$-th reaction. As a simple example shown in Figure 2.1, if $\mathrm{P}=\{0.3,0.13,0.27,0.3\}$, and the random number is equal to 0.61 , then reaction 3 is chosen. Finally, after the reaction is selected, it is executed. For bimolecular reactions, this means that two sites to react are chosen from the populations of all sites with the appropriate connectivities for the chosen reaction. The chosen sites are joined, and arrays are adjusted to reflect the change in state of the system. At the next step, the reaction rates and probabilities are updated and a new reaction is selected. The reaction rates and reaction probabilities are respectively stored as $4 \times 4$ matrices.

### 2.1.2.3 Flow Sheet

A flow sheet of the algorithm is given in Figure 2.2. At each DMC step, one siloxane bond is added to the population of monomers. This is an advantage of this algorithm in comparison with other Monte Carlo algorithms based on randomly selecting reactions and deciding whether to accept them based on acceptance probabilities. Our approach is sometimes called the "continuous time Monte Carlo" method because it is based not on discretizing time intervals but on discretizing reaction events. Because no bond additions attempts are rejected, this approach is very efficient, as we mentioned before. We begin


Figure 2.1 An example of Monte Carlo reaction selection


Figure 2.2 Flow sheet of the DMC algorithm
with $N$ monomers, initialize the data structures, and then we start the reaction steps. At each reaction step, we can calculate the reaction rates based on the current population of reactive species, and then obtain the probabilities according to all of the rates ${ }^{[39]}$. One reaction is selected by a random number and reactive sites are also chosen by two random numbers. Then the reaction is executed and the data structures are updated accordingly. The whole process for each reaction step is repeated until a stopping criterion is met (which is chosen to be after the gel point - for instance, once $D P_{w}$ reaches a value greater than $10 \%$ of the total number of monomers, finite size effects become important and so the simulation is stopped).

### 2.1.3 Random Branching Theory (RBT)

Based on the RBT, conversion at gelation can be expressed as ${ }^{[71]}$

$$
\begin{equation*}
\alpha_{g}=\frac{1}{(f-1)} . \tag{2.6}
\end{equation*}
$$

where $f$ is the functionality. For the acid-catalyzed TEOS system $f=4$, so we could infer that gelation is expected to occur when the conversion reaches $1 / 3$ in the ideal case. In addition, $D P_{w}$ can be predicted in the ideal case to be ${ }^{[64,75]}$ :

$$
\begin{equation*}
D P_{w}=\frac{1+\alpha}{1-(f-1) \alpha}=\frac{1+\alpha}{1-3 \alpha} . \tag{2.7}
\end{equation*}
$$

If we keep track of the number of silicon species with differing connectivity $i\left(Q_{i}\right)$, it is expected to be a function of the siloxane bond conversion $\alpha$. In the ideal case, the analytical solutions for the fractions of different $Q_{i}$ species as functions of conversion can be derived based on the assumption of equal reactivity, from which it follows that (1- $\alpha$ ) is the probability that any of the ligands attached to a site has not polymerized. Combinatorial considerations lead to the following expressions ${ }^{[75]}$ :

$$
\begin{align*}
& f\left(Q_{0}\right)=(1-\alpha)^{4},  \tag{2.8}\\
& f\left(Q_{1}\right)=4 \alpha(1-\alpha)^{3},  \tag{2.9}\\
& f\left(Q_{2}\right)=6 \alpha^{2}(1-\alpha)^{2},  \tag{2.10}\\
& f\left(Q_{3}\right)=4 \alpha^{3}(1-\alpha) . \tag{2.11}
\end{align*}
$$

### 2.1.4 Results and Discussion

In our DMC test simulations discussed here, we use $1.0 \mathrm{E}+05$ monomers. The accuracy of the DMC method can be verified by comparing the simulation results with analytical results based on RBT. Figure 2.3 shows the number fractions of different $Q_{i}$ species as a function of conversion. The DMC results (points) are very consistent with the analytical equations above (curves). Figure 2.4 presents the comparison of weightaverage degree of polymerization for DMC simulations and RBT. It is clear that the tendency of the $D P_{w}$ of DMC is correct until the gel conversion is approached. We can also find that above the gel point the deviation between simulation and analytical solution grows rapidly. This is a finite-size effect ${ }^{[64]}$ and it is normal for MC simulations. Because of the finite size of the population of polymers, a deviation is expected to happen late in reaction, but usually it does not begin until $D P_{w}$ is at least $1 \%$ of the total number of monomers, and usually is not severe until it is $10 \%$ of the total number of monomers. Based on Figures 2.3 and 2.4, DMC method is proven to be accurate to simulate the solgel polycondensation process.

As we mentioned above, a plot of reduced weight averaged degree of polymerization $\left(r D P_{w}\right)$ against conversion can also used to find the value of gel conversion. Figure 2.5 shows an example of using the peak in a plot of $r D P_{w}$ against conversion to estimate the gel conversion. For this case, we estimate the gel conversion to be about 0.336 , which is almost the same as the analytical solution.

### 2.2 Continuum Modeling Method - Finite Difference Method (FDM)

### 2.2.1 Introduction

As discussed in Chapter 1, modeling sol-gel film formation requires a multiscale approach that combines the granular, molecular description of polymerization given by the DMC method with a continuum model of the drying process. Researchers have shown that the finite difference method (FDM) can correctly model the drying process of polymer films. Blandin et al. ${ }^{[76]}$ presented a film drying model based on FDM, which gives results in good agreement with experimental data, thus validating the model. Vrentas et al. ${ }^{[77]}$ proposed using FDM to solve a set of equations which describe heat and mass transfer and film shrinkage in the drying of polymer films. Alsoy and Duda ${ }^{[78]}$


Figure 2.3 Comparison of DMC results with RBT analytical results for the ideal case:
$Q_{i} / N$ vs. conversion


Figure 2.4 Comparison of DMC results with RBT analytical results for the ideal case: $D P_{w}$ vs. conversion


Figure $2.5 r D P_{w}$ vs. conversion for the ideal case.
The peak in the plot is used to estimate gel conversion: $\alpha \approx 0.336$
applied their model, which is based on the model of Vrentas ${ }^{[77]}$ and solved by the finite difference approximation, to the well characterized polyvinylacetate (PVAC)-toluene system. Two sets of data available for the drying of polystyrene (PS)-toluene and PVACtoluene systems verify the validity of the model ${ }^{[78]}$. Kuznetsov et al. ${ }^{[79]}$ utilized FDM to solve their model which describes the effect of evaporation on the free surface profile and solute concentration distribution. Lou and coworkers ${ }^{[80]}$ demonstrated that a model solved by FDM can provide satisfactory long-term predictions of film formation.

The purpose of the work described in this dissertation is to develop a relatively simple, but sufficiently accurate method to model the moving boundary drying process in the solgel silica films. As will be discussed in later chapters, this model is to be coupled with the DMC model to give a comprehensive, multiscale approach. Compared with other methods that have been used to model the drying process of polymer solutions such as integral approach ${ }^{[81]}$ and finite element method ${ }^{[82-85]}$, FDM is easy and intuitive to implement, which is advantageous for developing multiscale methodology. In the following section, the FDM algorithm is briefly introduced. More details about our drying model (including the continuum equations) to be solved using FDM will be shown in Chapter 3.

### 2.2.2 FDM Algorithm

The FDM is a simple and efficient method for solving ordinary differential equations (ODEs) and partial differential equations (PDEs) in domains with simple boundaries. The method is based on substituting of derivatives in the differential equations by finite difference approximations ${ }^{[86]}$. These basic approximations are based on the definition of the derivative,

$$
\begin{equation*}
D_{+} f(x) \equiv \lim _{h \rightarrow 0} \frac{f(x+h)-f(x)}{h} \tag{2.12}
\end{equation*}
$$

provided that the limit exists. We just delete the limit operation in order to obtain a finite-difference approximation to $D_{+} f(x)$. The result is known as the first forward difference,

$$
\begin{equation*}
D_{+} f(x) \approx \frac{f(x+h)-f(x)}{h} \tag{2.13}
\end{equation*}
$$

or,

$$
\begin{equation*}
D_{+} f(x) \approx \frac{f_{i+1}-f_{i}}{h}=\frac{f_{i+1}-f_{i}}{x_{i+1}-x_{i}} \tag{2.14}
\end{equation*}
$$

where $x_{i+1}=x_{i}+h$ and the subscripts here denote different points in the grid defining the FDM modeling domain.

If $h$ is sufficiently small and $f \in C^{2}$ in a neighborhood of $x=x_{i}$, the accuracy of the first forward difference can be obtained using a Taylor series about the point $x_{i}$

$$
\begin{equation*}
f_{i+1}=f_{i}+f_{i}^{\prime} \cdot h+\frac{f_{i}^{\prime \prime}}{2} \cdot h^{2}+\ldots \tag{2.15}
\end{equation*}
$$

Substituting (2.15) into (2.14), we have

$$
\begin{equation*}
\frac{f_{i+1}-f_{i}}{h}=\frac{1}{h}\left[\left(f_{i}+f_{i}^{\prime} \cdot h+\frac{f_{i}^{\prime \prime}}{2} \cdot h^{2}+\ldots\right)-f_{i}\right]=f_{i}^{\prime}+\frac{f_{i}^{\prime \prime}}{2} \cdot h+\ldots \tag{2.16}
\end{equation*}
$$

So the leading error of Eq. (2.16) is $\frac{f_{i}^{\prime \prime}}{2} \cdot h$ and the approximation is first order accurate with respect to the step size $h$.

There are two other approximations: backward-difference approximation and centereddifference approximation. Using the same procedure we can see that backwarddifference approximation is also of first order accuracy, while the centered-difference approximation is of second order accuracy with respect to the step size $h$. Therefore, the centered-difference approximation is more accurate, and it is the approximation that we will use in our continuum modeling.

Backward-difference approximation: $\quad D_{-} f(h)=\frac{f_{i}-f_{i-1}}{h}=f_{i}^{\prime}+O(h)$
Centered-difference approximation: $\quad D_{0} f(h)=\frac{f_{i+1}-f_{i-1}}{2 h}=f_{i}^{\prime}+O\left(h^{2}\right)$
The approximation of higher order derivatives by the finite difference method can also be obtained using the similar approach. For example, the centered-difference approximation of a second order derivative can be derived as follows:

$$
\begin{aligned}
D_{0}^{2} f(h)=D_{+} D_{-} f(h) & =D_{+}\left(\frac{f_{i}-f_{i-1}}{h}\right) \\
& =\frac{1}{h}\left(D_{+} f_{i}-D_{+} f_{i-1}\right)
\end{aligned}
$$

$$
\begin{align*}
& =\frac{1}{h}\left(\frac{f_{i+1}-f_{i}}{h}-\frac{f_{i}-f_{i-1}}{h}\right) \\
& =\frac{1}{h^{2}}\left(f_{i+1}-2 f_{i}+f_{i-1}\right) \\
& =f_{i}^{\prime \prime}+O\left(h^{2}\right) \tag{2.19}
\end{align*}
$$

### 2.2.2.1 Discretization (grid)

The FDM requires that the domain is discretized to form a grid. At each grid point each term in the differential equation is replaced by a difference formula which may include the values of function at that point and its neighboring grid points. By substituting the difference formula into the equation, a difference equation is obtained. The grid is formed by the partition of the domain consisting of $M \times N$ points, and the grid points are indicated in Figure 2.6. In our cases, we use a uniform spacing for the computational mesh, using $j$ index as time and $i$ index as position.

### 2.2.2.2 Explicit Scheme

The PDEs are transformed to finite difference equations after the finite difference approximations replace the derivatives. These finite difference equations can be solved either by explicit or implicit method. In the explicit scheme, the modeled variable values at a new time can be directly calculated from the previous ones. Therefore in this approach, the PDE can be solved directly using the boundary conditions. In contrast, an iterative process is used to calculate modeled variable values at a new time in an implicit scheme. A trial solution is input as a first guess to the equations, and a new solution is calculated and used as new input in each iteration until the values converge to within a specified tolerance ${ }^{[87]}$. Because of their iterative nature, implicit schemes are usually more numerically intensive than explicit methods, although the increased accuracy they provide is required for some problems. It is clear that an explicit scheme is much easier to implement and debug than the implicit scheme. Therefore, we will use explicit FDM in our continuum modeling because our one-dimensional drying model is amenable to a simplified approach.


Figure 2.6 Example of finite difference discretization of a domain into a grid.

### 2.3 Summary

This chapter presented a general overview of the simulation methods used in this dissertation: the DMC method for molecular simulation and FDM for continuum modeling. DMC simulation is a very good choice to model the sol-gel silica polycondensation because it can capture the complete reaction history for a finite set of monomers, it has the flexibility to handle new types of reactions associated with the formation of large polycyclic species and cages, and it can simulate much larger systems and much longer times than competing molecular approaches such as molecular dynamics. The accuracy of DMC as we have implemented it can be verified by the good agreement between simulation results and analytical results (based on RBT) for the ideal polycondensation case. The FDM is an easy and intuitive numerical method to model the drying process of sol-gel silica films. Because we use a one dimensional model to develop the multiscale approach, FDM should provide adequate numerical accuracy and precision for the purposes of this dissertation. There are many examples to show that FDM can correctly model the drying process of polymer films. More details about our continuum modeling using explicit FDM will be shown in Chapter 3, including the balance equations, approach to nondimensionalizing the equations, boundary conditions, and coupling to the DMC simulation.

## Chapter 3

## Multiscale Modeling of Ideal Polycondensation and Polycondensation with First Shell Substitution Effect (FSSE) in Drying Thin Films

### 3.1 Introduction

Modeling silica curing in drying films is important for overcoming challenges in controlling the thickness, cracking and homogeneity of the films. Until now, most models of sol-gel polymerization or drying polymer films have provided useful insights into the essence of the physical phenomena, but they only focused on selected length and time scales. For example, kinetic models of the gelation behavior of silica polymerization have been developed using recursive statistical techniques or Monte Carlo simulation ${ }^{[31,38,39,75]}$. These modeling approaches are necessary to link rates of polymerization of individual monomers to molecular weight distributions and gelation of branched polymers. On the other hand, drying has been approached using continuum models and solved with an integral approach ${ }^{[81]}$, finite element method ${ }^{[82-84]}$ or finite difference method ${ }^{[76-78,80]}$. However, during the formation of sol-gel coatings, both polymerization and drying occur simultaneously, so the process involves multiple length and time scales ranging from molecular to macroscopic.

Unlike other processes where multiscale models have previously been applied, the solgel polycondensation occurs throughout the thickness of the film where solvent transport is occurring. Therefore, it is not possible to regard the polymerization reaction as occurring in a place spatially separate from the place where the coating flow occurs. At the molecular level, polymerization and (if surfactants are added) self-assembly process occur which control the film properties such as film microstructure. At the same time, the formation of the film is controlled by macroscopic parameters. Diffusion and mass transport occur over micron or greater length scales, and define the concentration fields within which polymerization and self-assembly occur. Therefore, we are challenged in this process to develop a methodology to link different length and time scales together throughout the entire simulated domain.

In this chapter we present a multiscale model which captures the evolution of both macroscopic and molecular phenomena of this sol-gel silica film formation process. The process of diffusion and mass transport can be adequately modeled by treating the film as a continuum. The macroscopic conservation equations for mass are expressed by a set of partial differential equations for species concentration with initial and boundary conditions. Based on finite difference method, the continuous domain is discretized and these PDEs are solved numerically. However, at the molecular length scale, the continuum hypothesis is no longer valid and the molecular phenomena cannot be described by deterministic PDEs ${ }^{[21]}$. At such a small length scale, the kinetics of sol-gel polymerization is best modeled by dynamic Monte Carlo (DMC) simulation. This approach is necessary because of the nonideal nature of silane polymerization (which precludes the use of random branching theory ${ }^{[71-73]}$ and even throws into question the validity of statistical techniques such as the kinetic-recursive method ${ }^{[31,39]}$ ). DMC simulations can simulate much longer times and much larger ensembles than molecular dynamics simulations ${ }^{[38,70]}$ can and have the potential flexibility of handling larger cycles and cages that are thought to play a significant role in the structure of sol-gel silica ${ }^{[38,43}$, ${ }^{66]}$. The inclusion of these cyclization reactions will be the subjects of the next two chapters, but here we focus on the coupled DMC / continuum model.

We will begin by describing the model integrating the DMC method and continuum model, as well as the physical assumptions and the simulation procedure. We first briefly review DMC simulation, since we have discussed sol-gel silica chemistry in Chapter 1 and presented the DMC algorithm in Chapter 2. Details are given about how to calculate the time interval in the DMC model. In the continuum model, the entire DMC simulation (containing $\sim 10^{6}$ monomers) is treated as a particle of sol whose position and composition are tracked using diffusion / evaporation finite difference calculations. Linking the two models is accomplished by tracking the positions of sol particles during drying. In the third section, two specific cases are considered - ideal polymerization and polymerization with a first shell substitution effect (FSSE). The effects of concentration gradients during drying are captured by simulating swarms of particles starting from different positions in the film. By varying process parameters, we observe their effects on the competition between drying and gelation, predict different drying / gelation
phenomena, and predict the occurrence of gradients of concentration and gelation in the films which can lead to the formation of a gel skin near the top surface of the film.

### 3.2 DMC Model

The DMC model is solved based on the following assumptions: only a first shell substitution effect for condensation is considered, hydrolysis is assumed to be at pseudoequilibrium, alcohol-producing condensation is neglected and no cyclization is allowed. With this set of assumptions, a finite set of N monomers $\left(\mathrm{N} \sim 2.5 \times 10^{6}\right)$ is polymerized in a manner consistent with the kinetics described in Chapter 1 by a DMC approach. The set of bimolecular condensation reactions is as follows:

$$
\begin{equation*}
Q_{i}+Q_{j} \xrightarrow{k_{i j}^{*}} Q_{i+1}+Q_{j+1}+\mathrm{H}_{2} \mathrm{O} \tag{3.1}
\end{equation*}
$$

where $Q_{i}$ represents a tetrafunctional silicon site with $i$ siloxane bonds (where $i$ represents the number of linkages to other silicon atoms), and both $i$ and $j$ can vary between 0 and $3^{[38]}$. Assuming that hydrolysis reaches quasi-equilibrium with constant $\chi$, the rate of reaction (3.1) can be expressed as:

$$
R_{i j}^{b i m o l}= \begin{cases}k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i \neq j  \tag{3.2}\\ \frac{1}{2} k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i=j\end{cases}
$$

where $\left[Q_{i}\right]$ represents the concentration of silicon sites $Q_{i}^{[39]}$.
In the simulation, each monomer unit is indexed as a separate entity. At each DMC step, one siloxane bond is added and the conversion $(\alpha)$ is increased by a small constant value $\Delta \alpha$, as given by:

$$
\begin{equation*}
\Delta \alpha=\frac{2}{4 \times N}=\frac{1}{2 N}=2.0 \times 10^{-7} \tag{3.3}
\end{equation*}
$$

where $N$ is the total number of sites.
At each step, the probabilities $P_{i j}$ of selecting each type of condensation reaction are evaluated by calculating the rates of the reactions, and one reaction is chosen to occur. After selecting a reaction, the particular sites joining in the reaction are randomly chosen from the subset of sites fitting to the required characteristics - in this case, that the sites have the correct connectivities chosen for the reaction. After the sites are chosen, they
are joined with one siloxane bond and all information is updated. DMC steps are repeated until a stopping criterion is met.

One thing that needs to be emphasized here is the calculation of the time interval ${ }^{[62,70]}$ during each bond addition, which is given by:

$$
\begin{equation*}
\Delta t=\frac{N}{C_{S i} \sum R_{i j}} \cdot \ln \left(\frac{1}{r}\right), \tag{3.4}
\end{equation*}
$$

where $N$ is the total number of sites, $r$ is a random number chosen from $(0,1)$, and $R_{i j}$ is the rate described by Eq. (3.2) but based on the populations of silicon sites $Q_{i}$ in the DMC model, rather than the concentrations $\left[Q_{i}\right]^{[35]}$. In this equation, $C_{S i}$ is the total silicon site concentration which comes from the continuum model at the time that the reaction is selected. This concentration serves as one link that allows us to synchronize our DMC model and the continuum model in this multiscale process. We will give more details in the following description of the continuum model.

One of the important results we need to obtain from the DMC simulation is the gel point. We know that a gel is a sample-spanning polymer network. In theory we can use an infinite molecular weight polymer to represent the gel ${ }^{[31]}$. In the DMC simulation, the gel point can be estimated by the point at which $D P_{w}$ diverges, or could be better determined using the peak of $r D P_{w}{ }^{[38,39]} . D P_{w}$ is the weight-averaged degree of polymerization, and $r D P_{w}$ is the reduced weight-averaged degree of polymerization, which is calculated by removing the largest molecule (the gel) from the population and recalculating $D P_{w}$.

Here, we will simulate two cases with the DMC model - an ideal polymerization case and a FSSE case. In the ideal polymerization case, the functional groups will react randomly and independently, which means that all the rate constants are equal to each other and no cyclization exists. In the FSSE case, we consider non-ideal polymerization effects, but still exclude cyclization. The rate coefficients of the FSSE case are set to drop by $10 \%$ across each row and to decrease by $90 \%$ down the diagonal, which resembles the experimental substitution effect ${ }^{[38]}$. In other words, $k_{01}^{*}=0.9 k_{00}^{*}$, $k_{02}^{*}=0.81 k_{00}^{*}$, etc. while $k_{11}^{*}=0.1 k_{00}^{*}, k_{22}^{*}=0.01 k_{00}^{*}$, etc. In fact, the ideal case represents a particular case of a FSSE model in which the set of connectivity-dependent rate coefficients are all set equal to one another.

### 3.3 Continuum Drying Model

### 3.3.1 Model Assumptions and Description

The continuum model for the formation of sol-gel thin-film coatings is described by macroscopic conservation equations for mass. It is a simplified one-dimensional model corresponding to a rapidly deposited film that begins drying and curing after the coating process is complete. Via evaporation, solvent is removed continuously at the top liquid / vapor interface. In addition to this evaporation, the diffusion of solvent within the film and the chemical reactions of dissolved species need to be included in this model. A schematic diagram of the sol-gel film drying process is given in Figure 3.1.

To facilitate the modeling, the following major assumptions are used here:

1) The film is extremely thin as compared with the surface area so that concentration variation is assumed to occur only in the thickness direction.
2) The concentrations of species are uniform throughout the film at the beginning of the drying process.
3) The solid substrate supporting the thin film is taken to be impermeable.
4) At the surface of the coating the vapor is in equilibrium with the coating, and the pressure in the gas phase is effectively uniform.
5) The evaporation rate of the solvent from the surface is proportional to the difference in gas-phase mole fraction of solvent between the vapor just above the surface of the film and the bulk gas.
6) The process is isothermal, i.e. heat transfer effects are not considered here.
7) The diffusion coefficients of solvent and sol are assumed to be constant and equal, and the cross-term diffusion coefficients are set to zero.
8) Hydrolysis is assumed to achieve quasi-equilibrium before the drying process is started and hydrolysis extent $\chi=1$.
9) Alcohol has already evaporated before the drying process is started and there is excess water in the solution. That means we can consider just water as the solvent.
10) The film thickness changes are assumed to be dominated by solvent evaporation so that volume changes due to reactions can be ignored.

## Solvent Evaporation



Figure 3.1 1-D drying sol-gel silica film schematic diagram
The z direction is defined to be perpendicular to the drying film. The initial thickness of the film is $H_{0}$, and during the drying process, the instantaneous thickness is $H(t)$. The entire DMC simulation (containing millions of monomers) is treated as a particle of sol whose position and composition are tracked using a diffusion / evaporation finite difference calculation.

### 3.3.2 Governing Equations

The governing equations for solvent and solute are as follows:

$$
\begin{align*}
& \frac{\partial C_{1}}{\partial t}-D_{1} \frac{\partial^{2} C_{1}}{\partial z^{2}}=0  \tag{3.5}\\
& \frac{\partial C_{2}}{\partial t}-D_{2} \frac{\partial^{2} C_{2}}{\partial z^{2}}=0  \tag{3.6}\\
& \frac{\partial Q_{i}^{C}}{\partial t}-D_{Q_{i}^{C}} \frac{\partial^{2} Q_{i}^{C}}{\partial z^{2}}=R_{Q_{i}^{C}}(i=0,1,2,3 \text { and } 4) \tag{3.7}
\end{align*}
$$

where $C_{1}$ is the concentration of solvent, $C_{2}$ is the total silicon concentration, $Q_{i}^{C}$ is the concentration of a tetrafunctional silicon site with $i$ siloxane bonds in the continuum model. $R_{Q_{i}^{c}}$ is the net rate for creation of each type of site through reaction.

$$
\begin{equation*}
R_{Q_{i}^{c}}=\sum_{j=0}^{3} R_{(i-1) j}-\sum_{j=0}^{3} R_{i j}(i=0,1,2,3 \text { and } 4) \tag{3.8}
\end{equation*}
$$

where $R_{i j}$ is the bimolecular reaction rate between sites $Q_{i}$ and $Q_{j}$ given by Eq. (3.2).
Initial conditions in this formulation are as follows:

$$
\begin{equation*}
C_{1}(0, z)=C_{1,0} ; C_{2}(0, z)=C_{2,0} ; Q_{i}^{C}(0, z)=Q_{i, 0}^{C}(i=0,1,2,3 \text { and } 4) . \tag{3.9}
\end{equation*}
$$

Consistent with the description of the film model described above, the boundary conditions are given by:

$$
\begin{align*}
& \text { At substrate }(z=0): D_{i} \frac{\partial C_{i}}{\partial z}=0 \quad(i=1,2)  \tag{3.10}\\
& \qquad D_{Q_{i}^{C}} \frac{\partial Q_{i}^{C}}{\partial z}=0 \quad(i=0,1,2,3 \text { and } 4) \tag{3.11}
\end{align*}
$$

At free surface $(z=H(t)):-D_{1} \frac{\partial C_{1}}{\partial z}-C_{1} \frac{d H(t)}{d t}=k_{g}\left(y_{1}^{s}-y_{1}^{\infty}\right)$

$$
\frac{\partial C_{2}}{\partial z}=-\frac{\hat{V}_{1}}{\hat{V}_{2}} \frac{\partial C_{1}}{\partial z}
$$

$$
\begin{equation*}
\frac{\partial Q_{i}^{C}}{\partial z}=\frac{Q_{i}^{C}}{C_{2}} \frac{\partial C_{2}}{\partial z} \tag{3.14}
\end{equation*}
$$

The effect of boundary motion due to solvent evaporation is taken into account using the term $\frac{d H(t)}{d t}{ }^{[88]}$. In Eq. (3.12), $k_{g}$ is the mass transfer coefficient of solvent in the vapor
phase (in units of $\mathrm{mol} /\left(\mathrm{cm}^{2} \cdot \mathrm{~s}\right)$ ), $y_{1}^{s}$ is the molar fraction of solvent at the surface in the gas phase (which is calculated based on Raoult's law), and $y_{1}^{\infty}$ is the molar fraction of solvent far away in the gas, which is set to zero here. Eq. (3.13) was derived from the relation $C_{1} \hat{V}_{1}+C_{2} \hat{V}_{2}=1$, where $\hat{V}_{i}$ is the molar volume, and $\hat{V}_{2}=\frac{1-C_{1,0} \hat{V}_{1}}{C_{2,0}}$. Eq. (3.14) is obtained by realizing that the probability that a Si atom in the solute mixture is associated with a $Q_{i}^{C}$ site is given by $\frac{Q_{i}^{C}}{C_{2}}$. Using this relationship, the diffusion term for $Q_{i}^{C}$ can also be substituted into Eq. (3.7) as follows:

$$
\begin{align*}
& D_{Q_{i}^{C}} \frac{\partial^{2} Q_{i}^{C}}{\partial z^{2}}=\frac{Q_{i}^{C}}{C_{2}} D_{2} \frac{\partial^{2} C_{2}}{\partial z^{2}},  \tag{3.15}\\
& \frac{\partial Q_{i}^{C}}{\partial t}-\frac{Q_{i}^{C}}{C_{2}} D_{2} \frac{\partial^{2} C_{2}}{\partial z^{2}}=R_{Q_{i}^{c}} . \tag{3.16}
\end{align*}
$$

Because only solvent is assumed to evaporate, the rate of change of film thickness, also known as the surface velocity $v^{s}$, can be calculated according to the following expression:

$$
\begin{equation*}
\frac{d H(t)}{d t}=v^{s}=-\hat{V}_{1} k_{g}\left(y_{1}^{s}-y_{1}^{\infty}\right), \tag{3.17}
\end{equation*}
$$

If we just consider ideal polymerization, the model can be simplified because the condensation rate constants are all equal. Therefore we can use independent functional group kinetics ${ }^{[36]}$, in which the hydrolyzed functional group $(\mathrm{SiOH})$ is the only species that participates in the reaction. If we use $C_{3}$ to denote the concentration of $(\mathrm{SiOH})$, then based on the fact that one Si atom is associated with $4(1-\alpha)(\mathrm{SiOH})$ functional groups where $\alpha=$ the siloxane bond conversion, we write the conservation equation, initial and boundary conditions for $C_{3}$ as follows:

$$
\begin{equation*}
\frac{\partial C_{3}}{\partial t}-4(1-\alpha) D_{2} \frac{\partial^{2} C_{2}}{\partial z^{2}}=-k_{00} C_{3}^{2} \tag{3.18}
\end{equation*}
$$

Initial conditions: $\quad C_{3}(0, z)=C_{3,0}=4 C_{2,0}$
Boundary conditions:

$$
\begin{equation*}
\text { At substrate }(z=0): \quad D_{3} \frac{\partial C_{3}}{\partial z}=0 \tag{3.20}
\end{equation*}
$$

At free surface $(z=H(t)): \frac{\partial C_{3}}{\partial z}=-4(1-\alpha) \frac{\hat{V}_{1}}{\hat{V}_{2}} \frac{\partial C_{1}}{\partial z}$

### 3.3.3 Dimensionless Variables and Simulation Procedure

The following dimensionless variables are defined to solve the transport equations numerically:

$$
\begin{equation*}
\eta=z / H(t), h=H(t) / H_{0}, c_{i}=C_{i} / C_{0}, q_{i}=Q_{i}^{C} / C_{0}, \tau=\frac{D_{1}}{H_{0}{ }^{2}} t \tag{3.22}
\end{equation*}
$$

Using the dimensionless variable $\eta$, the region in which diffusion occurs is always from $\eta=0$ to $\eta=1$. In other words, the physical moving domain is mapped onto a fixed domain, and we do not need to modify the spatial grid during the simulation. Meanwhile, a pseudoconvective term is produced by this Landau transformation ${ }^{[89]}$ in the diffusion equation ${ }^{[88]}$. For example, the dimensionless form of the equation for the solvent now is

$$
\begin{equation*}
\frac{\partial c_{1}}{\partial \tau}-\frac{\eta}{h} \cdot \frac{d h}{d \tau} \cdot \frac{\partial c_{1}}{\partial \eta}-\frac{1}{h^{2}} \frac{\partial^{2} c_{1}}{\partial \eta^{2}}=0 \tag{3.23}
\end{equation*}
$$

We can see that this pseudoconvective term is proportional to the free surface velocity $\frac{d h}{d \tau}$.

This set of dimensionless equations is numerically solved using the explicit centered finite difference method (FDM). We discretize the whole domain into a number of thin slices; each one with a fixed thickness $\Delta \eta$. For the solution, the time interval $\Delta t$ is equal to the time interval between reactions estimated from the DMC simulation. At each finite difference step, we use the concentrations, film thickness, surface velocity, and Robin boundary condition at the surface from the previous time step to complete the calculation.

### 3.3.4 Tracking the Sol Particle

As we mentioned before, the entire DMC simulation is treated as a particle of sol whose position and composition are tracked in the continuum model, which provides an important link between the parts of our multiscale model. We perform the tracking using linear interpolation. Similar to the film thickness calculation, the change of particle position can be expressed as follows:

$$
\begin{equation*}
\frac{d H_{p}(t)}{d t}=\left.\hat{V}_{1} \cdot D_{1} \frac{\partial C_{1}}{\partial z}\right|_{H_{p}} \tag{3.24}
\end{equation*}
$$

From the value of particle position of the previous step on the calculation, we can determine the finite difference slice where the particle is located. Then we are able to estimate the approximate value of concentration gradient in that interval (between slice ( $m-1$ ) and slice $m$ ) and continue to calculate the composition and position of the particle (expressed in dimensionless form):

$$
\begin{align*}
& \frac{\partial c_{i}}{\partial \eta} \approx \frac{c_{i, m}-c_{i,(m-1)}}{\Delta \eta}, \frac{\partial q_{i}}{\partial \eta} \approx \frac{q_{i, m}-q_{i,(m-1)}}{\Delta \eta},  \tag{3.25}\\
& c p_{i}=c_{i, m}-\frac{\partial c_{i}}{\partial \eta} \cdot\left(m \cdot \Delta \eta-h_{p}\right), c q_{i}=q_{i, m}-\frac{\partial q_{i}}{\partial \eta} \cdot\left(m \cdot \Delta \eta-h_{p}\right),  \tag{3.26}\\
& h_{p}(t+1)=h_{p}(t)+d \tau \cdot \frac{1}{h^{2}} \cdot \frac{\partial c_{1}}{\partial \eta} \cdot C_{0} \hat{V}_{1}, \tag{3.27}
\end{align*}
$$

where $c p_{i}(i=1,2$ or 3$)$ is the dimensionless concentration of solvent, total silicon sites or $(\mathrm{SiOH})$ group at the particle position, $c q_{i}$ is the dimensionless concentration of silicon sites with $i$ siloxane bonds at the particle position. Using the calculated information of this tracked particle, we can then determine the conversion and total silicon site concentration in the continuum model. This total silicon site concentration is then supplied to the DMC routine to choose the next reaction and calculate the time interval of the next DMC step, as discussed earlier. The equations we use to calculate conversion and overall silicon concentration from the integrated concentrations for the two polymerization cases are presented below:

Ideal case: $\quad \alpha=1-\frac{c p_{3}}{4 \cdot c p_{2}}, \quad C_{S i}=c p_{2} * C_{0}$
FSSE case: $\quad a=c q_{1}+2 \cdot c q_{2}+3 \cdot c q_{3}+4 \cdot c q_{4}($ reacted $[\mathrm{SiOH}])$

$$
\begin{align*}
& b=4 \cdot c q_{0}+3 \cdot c q_{1}+2 \cdot c q_{2}+c q_{3}(\text { remaining }[\mathrm{SiOH}])  \tag{3.30}\\
& C_{S i}=c p_{2} * C_{0}=(a+b) * C_{0} / 4  \tag{3.31}\\
& \alpha=1-\frac{b}{4 \cdot c p_{2}}=\frac{a}{4 \cdot c p_{2}}=\frac{a}{a+b}
\end{align*}
$$

Using these expressions, we can compare the conversions and site distributions (for the FSSE case) with those obtained from the DMC model to validate the implementation of this multiscale model. Note that the DMC model still contains a significant amount of information about the polymer structure distribution that is not available from a continuum kinetics approach.

### 3.4 Results and Discussion

In our modeling, we focus on the effects of two important dimensionless parameters, $B i$ and $D a$ (Eq. (3.33)) to understand how process parameters affect the drying process of the sol-gel silica films. $B i$ is the Biot number, which is the ratio of external mass transfer resistance to the internal diffusion resistance, and can be thought of as a dimensionless mass transfer time. $D a$ is the Damköhler number, which is the ratio of reaction rate to diffusion rate, and can be thought of as a dimensionless reaction time. In the FSSE case, we have different rate coefficients, but we use the first reaction rate coefficient $k_{00}^{*}$ as the reference to define the Damköhler number. For a negative FSSE (considered here) $k_{00}^{*}$ is the largest rate coefficient.

$$
\begin{equation*}
B i=\frac{k_{g} H_{0} \hat{V}_{1}}{D_{1}}, \quad D a=\frac{k_{00}^{*} C_{0} H_{0}{ }^{2}}{D_{1}} . \tag{3.33}
\end{equation*}
$$

The ratio of initial concentration used in our work is $C_{1,0}: C_{2,0}=4: 1$, and the molar volume of the solvent is arbitrarily set to 0.1 .

### 3.4.1 Solvent Concentration Profile

Figures 3.2 and 3.3 display the time-dependent solvent concentration profiles in the films which are calculated by the continuum model for the ideal case and FSSE case respectively. The red curve shows the change of the tracked sol particle position for the two examples selected for display. As expected, the film thickness, solvent concentration and particle position all drop as the gel film dries. This suggests that the transport equations are being correctly handled. Simplified cases of the transport with boundary conditions amenable to symbolic solutions (for instance, drying without reaction and with constant rate of evaporation at the free surface) were also tested to confirm the accuracy of our numerical method.


Figure 3.2 Solvent concentration profile for the ideal case:

$$
B i=1013.25, D a=2, H_{0}=0.1, H p_{0}=0.9 H_{0}
$$



Figure 3.3 Solvent concentration profile for the FSSE case:

$$
B i=506.625, D a=40, H_{0}=1.0, H p_{0}=0.8 H_{0}
$$

### 3.4.2 Conversion and Site Distribution

Since we can calculate the conversion and site distributions (for the FSSE case) as functions of time with continuum equations in addition to the DMC model, the validity of this multiscale model was tested by comparing the continuum results to the DMC results, as presented as examples in Figures 3.4 to 3.6. In both cases, the results are terminated when a gel forms (see below). The ability to validate the DMC approach is one of the strengths of developing the multiscale model for relatively simple polymerization kinetics. In both cases, the conversions calculated by both methods agree exactly, as shown in Figures 3.4 and 3.5. In addition, the site distributions calculated by both methods for the FSSE case achieve good agreement, as shown in Figure 3.6. The good agreement found between the continuum kinetics and the DMC results prove the validity of our model. In addition, this set of figures shows that, as expected, because the rate coefficients drop in the FSSE case, the rate of the condensation reactions decreases significantly compared with the ideal case, and because of the structure of the resulting polymers, the gelation occurs at a larger conversion and therefore at a much later time.

### 3.4.3 Three Types of Drying and Gelation Phenomena

There are three main types of qualitative drying and gelation phenomena in the drying process of a sol-gel film, as originally defined by Cairncross et al ${ }^{[36]}$ : drying before gelation, gelation before drying and literal skinning. The competition between drying and gelation determines the phenomenon type, and this competition is dictated by the values of Biot number and Damköhler number. We define these three types of phenomena by comparing the values of gel time with drying time, according to the definitions of Cairncross et $\mathrm{al}^{[36]}$. The gel time is the time when the DMC simulation of the sol particle reaches the gel point (see below). The drying time is calculated by integrating the solvent content throughout the coating and finding the point at which only $1 \%$ solvent content is left ${ }^{[36]}$. The definitions of these three types of phenomena are presented below:

- drying before gelation: $d r y{ }_{-} t<g e l_{-} t b$,
- gelation before drying: gel_tb<10\% $\cdot d r y_{-} t$,


Figure 3.4 Conversion predicted by DMC and continuum model for the ideal case:

$$
B i=1013.25, D a=2.0, H p_{0}=0.9 H_{0}
$$



Figure 3.5 Conversion predicted by DMC and continuum model for the FSSE case:

$$
B i=506.625, D a=40, H p_{0}=0.8 H_{0}
$$



Figure 3.6 Site distributions predicted by DMC and continuum model for the FSSE case:

$$
B i=506.625, D a=40, H p_{0}=0.8 H_{0}
$$

- literal skinning: $\frac{g e l_{-} t b-g e l_{-} t s}{d r y_{-} t} \geq 0.1$,
where $d r y_{-} t$ denotes the drying time, gel_tb is the gel time at the base of the coating, and gel_ts is the gel time at the coating surface. The gel time varies throughout the film because of concentration gradients due to the solvent evaporation, which are illustrated in Figures 3.2 and 3.3.

Figure 3.7 displays the DMC-generated values of $D P_{w}$ as a function of time for tracked particles starting from different positions in the film for one particular set of conditions ( Bi and Da ). It is obvious that $D P_{w}$ increases much more quickly at the film surface than inside the film, and that means there is a time lag of gelation between the film surface and base. At any point in the film, gelation is defined by the point where $D P_{w}$ appears to diverge.

The effects of process parameters $B i$ and $D a$ on the gelation and drying time for the ideal and FSSE cases are illustrated with examples in Figures 3.8 and 3.9. Figure 3.8 shows the effect of varying $D a$ number with constant $B i$ which is equal to 1013.25 in ideal case. In this case, the drying time remains constant and gel time drops considerably as $D a$ increases. At this high $B i$, drying before gelation, literal skinning and gelation before drying appears in turn with increasing reaction rates, which means that the type of phenomenon depend only on $D a$ when the value of $B i$ is high.

Figure 3.9 shows another representative result: the gelation and drying times at various $B i$ values for the FSSE case. With constant $D a=4.0$, the gelation is always faster than drying. At low $B i(B i<=10)$, the difference of the gel time between the coating surface and base is so small that we conclude that the coating gels uniformly. However, the gel time lag between surface and base increases with increasing $B i$, and literal skinning is predicted to occur when $B i$ is equal to or larger than 300 for the FSSE polycondensation case.

### 3.4.4 Gelation Regime Map

The competition between drying and gelation as a function of the values of $B i$ and $D a$ can be most clearly visualized using gelation regime maps ${ }^{[36]}$. Figures 3.10 and 3.11 are the results found by multiscale DMC / finite difference modeling for the ideal and FSSE


Figure 3.7 DP $P_{w}$ as a function of time for tracked particle starting at different positions in the film for the ideal literal skinning case: $B i=1013.25, D a=0.4$


Figure 3.8 Gelation and drying time as a function of $D a$ for the ideal case: $B i=1013.25$.
The phenomena depend only on $D a$


Figure 3.9 Gelation and drying time as a function of $B i$ for the FSSE case: $D a=4.0$. When $B i \geq 300$, literal skinning occurs


Figure 3.10 Gelation regime map for the ideal polycondensation case.
Points are the average values of five repeated calculations.
Dashed lines are the approximate boundaries of each region.


Figure 3.11 Gelation regime map for the FSSE polycondensation case.
Points are the average values of five repeated calculations.
Dashed lines are the approximate boundaries of each region.
cases, respectively. The lines are the approximate boundaries between regions (as defined above) and the points are the conditions related to each phenomenon ${ }^{[36]}$, which are the average values of five repeated simulations. At low $D a$, the coating dries before it gels and at high $D a$, the gelation reaction rates are much quicker than the drying rate. With high $B i$, literal skinning occurs between the regions of "drying before gelation" and "gelation before drying". The maps are similar for the ideal and FSSE cases, except that with FSSE, all three regions are shifted towards higher $D a$. These results are consistent with the findings of Cairncross et al. ${ }^{[36]}$, but they used an approximate kinetic-recursive model with reduced accuracy for FSSE modeling and which is not capable of correctly modeling the high degree of cyclization found in real sol-gel polymerization (to be discussed in Chapter 4 and 5).

### 3.4.5 Relationship between Gel Time and Initial Particle Position

To gain more insight into the effects of the FSSE on film uniformity, we further investigate the relationship between gel time and initial particle position for the three types of phenomena, as shown in Figures 3.12 and 3.13. Representative points from the gelation regime maps are shown. According to the maps, we can observe all three types of phenomena by setting $B i$ to a high value and varying $D a$. In order to compare these three types phenomena easily, all of the gel time values are normalized by the one at the surface. With fixed $B i$, gel times are, of course, longest when "drying before gelation" is found and smallest when "gelation before drying" is found. The gel time gradient is much more severe when "gelation before drying" is observed than with "drying before gelation". This suggests that, when the coating dries completely as a liquid (drying before gelation) the gel time lag is small and defects are not likely to appear due to formation of a gel layer at the film surface, and when the coating gels before it is dry, the difference of gel time is more visible and likely to induce defects. Regardless of the rate of drying, drying before gelation is best achieved by reducing the rate of condensation relative to the rate of diffusion of solvent. In sol-gel systems, this is best accomplished by working near the minimum condensation rate which occurs at a pH of $\sim 2$. Gel times for the FSSE case simulations are longer than those of ideal case, proving again that gelation is delayed compared with the ideal case, as we mentioned earlier. Also, the gradients in


Figure 3.12 Normalized gel time as a function of initial particle position of the sol for the ideal case. Points are the average values of five repeated calculations. The gel time is normalized by the value at the surface. $B i=1013.25$. Drying before gelation, $D a=0.06$, gel_ts $=0.505689$; Literal skinning, $D a=0.4$, gel_ts $=0.076512$;

Gelation before drying, $D a=2.0$, gel_ts $=0.015567$


Figure 3.13 Normalized gel time as a function of initial particle position of the sol for the FSSE case. Points are the average values of five repeated calculations.
The gel time is normalized by the value at the surface. $B i=506.625$. Drying before gelation, $D a=0.4$, gel_ts $=47.9099$; Literal skinning, $D a=4.0$, gel_ts $=4.96508$;

Gelation before drying, $D a=40.0$, gel_ts $=0.514136$
gel time are more severe than those found in the ideal case, suggesting that nonideal polymerization may worsen the formation of coating defects in sol-gel systems.

### 3.5 Summary

The proposed multiscale model for the drying process of sol-gel coatings couples molecular to macroscopic phenomena by combining dynamic Monte Carlo simulations and the finite difference method. For the cases studied here, continuum equations can be formulated for the overall extent of reaction, and the results agree well with the multiscale DMC / FDM model, which demonstrates the validity of the multiscale model. In the continuum model, the entire DMC simulation is treated as a particle of sol whose position and composition are tracked using a diffusion / evaporation finite difference calculation. Therefore, the total silicon concentration, which is provided by the continuum model, serves as one "handshake" with the DMC model. The second "handshake" between the models is the time interval from the DMC simulation, which is used as the time interval for the continuum model. By simulating swarms of particles starting from different positions in the film and varying process parameters, we observe their effects on the competition between drying and gelation, predict different drying / gelation phenomena, and predict the occurrence of gradients of concentration and gelation in the films which can lead to the formation of a gel skin near the top surface of the film.

This multiscale model is our first step to understand the drying process of sol-gel coating. Further efforts are needed to improve the realism of the polymerization model, the most important and obvious of which is to add the cyclization in the model and see its effects on gelation regime maps and structural gradients. We expect that the results of our simulation will allow better prediction of the formation of structure gradients in solgel derived ceramics and other nonideal multifunctional polycondensation products, and that this will help in developing coating procedures to reduce coating defects.

## Chapter 4

## Multiscale Modeling with Unlimited 3-membered Ring Cyclization

### 4.1 Introduction

The coating process of sol-gel films involves multiple length and time scales ranging from molecular to macroscopic. At the molecular scale, polymerization and (with surfactant templates) self-assembly processes occur which control the film properties such as film microstructure. At the same time, macroscopic parameters control the formation of the film; diffusion and mass transport occur over micron or greater length scale, and define the concentration fields within which polymerization and self-assembly occur. Therefore, a multiscale model should be used to link these different length and time scale together. In our previous chapter, we developed a multiscale model to describe the competition between polymerization reaction and mass transfer, but we didn't include cyclization in our model. However, experiments have shown that three- and fourmembered rings exist early in alkoxysilane polymerization processes and give rise to a gel conversion as large as $82 \%^{[27,41,43,47,66]}$. Researchers have also presented several probable reasons for the occurrence of cyclization. West and coworkers ${ }^{[40]}$ presented quantum chemical calculations indicating that cycles are energetically favored over chains extension. Tang et al. ${ }^{[41]}$ proposed that ring formation is easy because of the flexibility of siloxane chains, and as a unimolecular reaction, cyclization is favored by a low concentration of monomer. Both Sanchez et al. ${ }^{[42]}$ and Ng et al. ${ }^{[52]}$ presented evidence that kinetic trends may favor cyclization of silanes. Ng et al. ${ }^{[52]}$ also proposed that stabilization of rings toward solvent attack or changes in functional group reactivity favor cyclization. Hence, cyclization is very important at the molecular scale of sol-gel drying process so that it can't be neglected at all. Models without cyclization may be able to match the kinetics of polymerization but they may not be able to correctly model large-scale (gel) structures, may include wrong parameters and may give incorrect prediction of the effects of process parameters. Therefore, a better multiscale model for silica should also include cyclization in the polymerization process.

Some researchers have already tried to include the cyclization effect in their models of sol-gel polymerization, but they often include simplifications that limit their fidelity. For instance, Vainrub et al. ${ }^{[44]}$ didn't directly simulate cyclization in their kinetic model. Instead, they used rate coefficients whose values decreased as a function of time to mimic the kinetic effect of cyclization. Hendrickson et al. ${ }^{[65]}$ also simulated cyclization during stepwise polymerization. They assumed that each monomer was a stationary hard sphere, and reactions were only allowed to happen when two randomly chosen monomers were within a sphere of radius $r_{h}$ which was centered on one of the reactants. While they admitted that this method had shortcoming that real diffusion of monomers was not modeled, this approach did capture the effect of cyclization on delaying gelation to some extent. Kasehagen et al. ${ }^{[39]}$ limited their simulation of cyclization to include only cyclization of trimers and linear tetramers. Rankin et al. ${ }^{[27]}$ also used this kinetics of forming single rings as a first step to model the cyclization effect in polymerizing silane solutions. Ng et al. ${ }^{[43]}$ treated cyclic or even cagelike intermediates as f-functional random branching "monomeric" units (i.e. new precursors). These cyclic (cagelike) intermediates were assumed to form in the early stage of reactions from monomers by cyclization, but after they were formed, they could only connect with each other until forming a gel. Highly cyclized cages were shown to give a gelation conversion close to the experimental value. Rankin et al. ${ }^{[38]}$ first presented a model with extensive cyclization to form polycyclic structures made up of three-membered rings. They applied the dynamic Monte Carlo (DMC) simulation technique which has advantages over statistical approaches due to full accounting of the reaction history, molecular structure and weight distributions, membership in cyclic and polycyclic species, and so on. Similar to the work of Rankin et al, here we add unlimited cyclization to form only threemembered rings in our multiscale model of sol-gel silica drying films. This is our first step to investigate how extensive cyclization affects the sol-gel process in a drying film. More details will be given below.

### 4.2 DMC Model

In this chapter, we will describe our DMC modeling approach and give details about new approaches used to track the effects of cyclization, e.g. calculating the Wiener index, a topological index related to molecular size.

### 4.2.1 Bimolecular Condensation

Experiments have shown that under acid-catalyzed conditions, the hydrolysis reaction of alkoxysilanes reaches pseudoequilibrium ${ }^{[28]}$. This often results in a constant average extent of hydrolysis $\chi$, which is defined as:

$$
\begin{equation*}
\chi=\frac{[\mathrm{SiOH}]}{[\mathrm{SiOH}]+[\mathrm{SiOR}]} . \tag{4.1}
\end{equation*}
$$

By assuming that water-producing condensation dominates over alcohol-producing condensation ${ }^{[37]}$, and based on the fact that a strong, negative first shell substitution effect (FSSE) exists in the condensation reactions ${ }^{[30]}$, the set of bimolecular condensation reactions among silicon sites can be written as ${ }^{[38]}$ :

$$
\begin{equation*}
Q_{i}+Q_{j} \xrightarrow{k_{i j}} Q_{i+1}+Q_{j+1}+\mathrm{H}_{2} \mathrm{O}, \quad i, j=0,1,2,3 \tag{4.2}
\end{equation*}
$$

where $Q_{i}$ represents a tetrafunctional silicon site with $i$ siloxane bonds. With these assumptions, the bimolecular rate expressions are given by ${ }^{[38]}$ :

$$
R_{i j}^{\text {bimol }}= \begin{cases}k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i \neq j  \tag{4.3}\\ \frac{1}{2} k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i=j\end{cases}
$$

Where $k_{i j}^{*}=\chi^{2} k_{i j}$ and $f=$ the functionality of the monomer $(f=4$ for tetrafunctional silane precursors). The matrix of rate coefficients is set to mimic the experimental trend observed for alkoxysilanes under acidic conditions ${ }^{[39]}$ :

$$
K^{*}=k_{00}^{*}\left[\begin{array}{cccc}
1.0 & 0.9 & 0.81 & 0.729 \\
& 0.1 & 0.09 & 0.081 \\
& & 0.01 & 0.009 \\
& & & 0.001
\end{array}\right]
$$

### 4.2.2 Three-membered Ring Cyclization

After some reaction steps, oligomers of size large enough to form rings will have formed. Cyclization reactions can then occur when two sites chosen to react are in the same molecule. This results in a new ring within an existing molecule. According to the approach of Rankin et al. ${ }^{[38]}$, we use bond blocks ${ }^{n} B_{i j}$ to calculate the cyclization rates. Here the superscript $n$ represents the number of bonds between two sites, and subscripts $i$ and $j$ represent the connectivities of the ends (i.e. the number of siloxane bonds attached to each end). For example, a linear trimer has one ${ }^{2} B_{11}$ bond block, while a linear tetramer has two ${ }^{2} B_{12}$ blocks and one ${ }^{3} B_{11}$ block. As the first step in our multiscale model with cyclization, we just consider the formation of three-membered rings. Therefore we just need to pay attention to two-bond blocks. In this case, the rate of cyclization reactions is calculated by analogy with any isolated ring closure reaction as ${ }^{[38]}$ :

$$
\begin{equation*}
{ }^{3} R_{i j}^{c y c}=(f-i)(f-j) k_{3 c(i, j)}^{*}\left[{ }^{2} B_{i j}\right], i \& j=1,2,3 . \tag{4.4}
\end{equation*}
$$

In order to have the concentrations of these two-bond blocks, the number of ${ }^{2} B_{i j}$ of each type needs to be updated after each reaction step, by adding the new bond blocks created by the reaction and modifying the old ones that have changed. Figure 4.1 shows an example of a new ring formed in an existing molecule. From this example, we can see that after each cyclization reaction, only the first- and second- shell neighbors of the reacting sites are involved in changes of ${ }^{2} B_{i j}$ blocks. Therefore, updating the list of ${ }^{2} B_{i j}$ sites is accomplished with a set of subroutines that enumerate all first and second shell neighbors of a pair of reacting sites and test for changes, not considering neighbors outside the second shell, thus avoiding over-counting of new blocks.

We assume that the substitution effect for cyclization reactions follows the same trend as for bimolecular reactions, since it still involves nucleophilic displacement between sites of varying connectivity:

$$
K_{3 c}^{*}=k_{3 c(1,1)}^{*}\left[\begin{array}{ccc}
1.0 & 0.9 & 0.81 \\
& 0.1 & 0.09 \\
& & 0.01
\end{array}\right] .
$$



Figure 4.1 Example of updating information about 2-bond blocks.
Circles represent silicon sites, and lines represent siloxane bonds. The shaded circles are members of a new ring. When a new bond is formed between site L and R in a cyclization reaction, two new 2-bond blocks need to be added, which are 2-L-R and 3-RL. In addition, three existing 2-bond blocks need to be modified, 1-2-L, 4-M-L and 4-MR , because the connectivity of L and R is changed from 2 to 3 . Plus, because of ring closure, the L-M-R block needs to be deleted.

To characterize the cyclization tendency, the dimensionless parameter $\kappa$ is used as defined by Rankin et al. ${ }^{[38]}$ :

$$
\begin{equation*}
\kappa \equiv \frac{k_{3 c(1,1)}^{*}}{k_{11}^{*}[S i]_{0}} . \tag{4.5}
\end{equation*}
$$

### 4.2.3 Wiener Index

In our multiscale model, we record a new type of information (relative to prior DMC studies) which can be used to characterize molecular size and shape - the Wiener index. The Wiener index is a topological index that has been shown to be proportional to zeroshear viscosity, and thus to relate molecular structure and rheology ${ }^{[90]}$. It is defined as follows ${ }^{[91]}$ :

$$
\begin{equation*}
W=\frac{1}{2} \sum_{i, j} d_{i j}=\sum_{i \leq j} d_{i j} \tag{4.6}
\end{equation*}
$$

where $d_{i j}$ is the topological distance (i.e. number of bonds along the shortest path connected by bonds) between sites $i$ and $j$ in the molecule. Because the Wiener index takes into account the distribution of topological distances between sites in a molecule, it can be used as a measure of molecular compactness. It can also be used in quantitative structure activity/property relationship (QSAR/QSPR) modeling in chemistry ${ }^{[92,}{ }^{93]}$, for example, by using Wiener index in QSPR to model the boiling temperature, molar heat capacity, standard Gibbs energy of formation, vaporization enthalpy, refractive index, and density of alkanes ${ }^{[93]}$.

If the molecules are linear, the Wiener index can be easily calculated according to the following expression ${ }^{[91,94]}$ :

$$
\begin{equation*}
W_{l i n}=\frac{1}{6} m\left(m^{2}-1\right), \tag{4.7}
\end{equation*}
$$

where $m$ is the degree of polymerization. However, calculations of the Wiener index of arbitrarily branched and cyclic molecules are much more complicated. Here we present a new algorithm to calculate the Wiener index during dynamic Monte Carlo simulation of polycondensation. In our model, the sites are silicon atoms, and the bonds are not single bonds but $\mathrm{Si}-\mathrm{O}-\mathrm{Si}$ bonds. At first, the Wiener index for all monomers is 0 . After each reaction (bimolecular or cyclization reaction), we calculate the Wiener index of the
product based on the known indices of the reactant molecule(s) and the distances from the reacting sites to all other sites.

For bimolecular polycondensation, we assume that the reaction occurs between two molecules of sizes $m$ and $n$, to produce a new molecule of size $(m+n)$. Because the adjacency matrix has not changed in either of the blocks taken from the old molecules, the distance matrix also will not have changed in each of those blocks from what it was in the old molecule (Figure 4.2). Therefore, we only need to calculate the distance submatrix for the new $m \times n$ section of the distance matrix. The Wiener index of the new molecule therefore is composed of three parts:

$$
\begin{equation*}
W=W_{A}+W_{B}+W_{\text {new }}, \tag{4.8}
\end{equation*}
$$

where $W_{A}$ and $W_{B}$ are the Wiener indices of the reactant molecules $A$ and $B$, and $W_{\text {new }}$ is the index calculated using only the new $m \times n$ submatrix.

Noting that any new pathway between a site in submolecule $A$ and a site in submolecule $B$ must pass through the new bond between them, the new distance can be expressed in terms of its distance to the sites at new bond. For example, in Figure 4.3,

$$
\begin{equation*}
d_{i j}=d_{i R}+d_{L j}-1 \tag{4.9}
\end{equation*}
$$

When this expression is inserted into the definition of the Wiener index of the new submatrix, the calculation becomes simple:

$$
\begin{align*}
W_{\text {new }} & =\sum_{i=1}^{m} \sum_{j=1}^{n} d_{i j}=\sum_{i=1}^{m} \sum_{j=1}^{n}\left(d_{i R}+d_{L j}-1\right)  \tag{4.10}\\
& =n \sum_{i=1}^{m} d_{i R}+m \sum_{j=1}^{n} d_{L j}-m n
\end{align*}
$$

In our model, the whole submolecule $A$ is traversed starting from site $L$ to calculate the distance from each site in submolecule $A$ to site $R$. A similar procedure is done for submolecule $B$. The advantage of this approach is that the calculation of the Wiener index for the new molecule scales linearly with $(m+n)$. Competing algorithms based on brute-force calculation of the distance matrix ${ }^{[95,96]}$ would scale much more poorly with molecule size.

The Wiener indices of linear molecules with the same degrees of polymerization as the actual simulated molecules are also tracked in our model for comparison purpose, and the new piece of the Wiener index due to a bimolecular reaction is given by:


Figure 4.2 Schematic diagram of distance matrix of the product of oligomers $A$ and $B$.


Figure 4.3 Schematic diagram of a bimolecular reaction product. Circles represent silicon sites, lines represent siloxane bonds, and dashed circles represent reactant submolecules $A$ and $B$.

$$
\begin{align*}
W_{\text {nev,lin }} & =W_{(m+n), \text { lin }}-\left(W_{m, \text { lin }}+W_{n, \text { lin }}\right)  \tag{4.11}\\
& =\frac{1}{6}(m+n)\left[(m+n)^{2}-1\right]-\left[\frac{1}{6} m\left(m^{2}-1\right)+\frac{1}{6} n\left(n^{2}-1\right)\right] \\
& =\frac{1}{2} m n(m+n)
\end{align*}
$$

When updating the Wiener index due to a cyclization reaction, we separate the whole molecule into three parts: left part, middle part and right part (Figure 4.4). The distance from each site in the left part (size $m$ ) to each site in right part (size $n$ ) is decreased by 1 after cyclization, because of forming a three-membered ring. At the same time, the distance from each site in the middle part to each site in left and right part doesn't change. Therefore the calculation of $W_{\text {new }}$ is very simple if we know the sizes of the left and right parts:

$$
\begin{equation*}
W_{\text {new }}=-m n . \tag{4.12}
\end{equation*}
$$

Then Wiener index of the product after cyclization is:

$$
\begin{equation*}
W=W+W_{\text {new }}=W-m n \tag{4.13}
\end{equation*}
$$

For example, in Figure 4.4, the left part has 4 nodes, the middle part has 2 nodes and the right part has 3 nodes. After the cyclization reaction, the Wiener index decreases by 12 . In our program, we traverse the left and right part to count the number of nodes (size) of each part.

The number-average Wiener index $\left(W_{n}\right)$ is calculated as follows:

$$
\begin{equation*}
W_{n}=\frac{1}{N_{m o l}} \sum_{i=1}^{N_{m o l}} W_{i} \tag{4.14}
\end{equation*}
$$

where $N_{\text {mol }}$ is the number of molecules, $W_{i}$ is the Wiener index of molecule $i$.

### 4.2.4 Cycle Rank

Cycle rank is the number of bonds (edges) that would need to be cut from a molecule to eliminate all cycles and form a spanning tree ${ }^{[64,97,98]}$. For example, the cycle rank is 2 for the molecule shown in Figure 4.5. It is an important measure of the number of independent cycles in the system ${ }^{[38,64]}$. At the beginning of simulation, the cycle rank for all monomers is 0 . In our model, number-average and weight-average cycle rank of the whole population are tracked.


Figure 4.4 Schematic diagram of a cyclization reaction product.
Circles represent silicon sites, lines represent siloxane bonds,
and dashed circles identify different parts of the molecule: left, middle and right.


Figure 4.5 Example of a molecule with cycle rank 2: showing the bonds that would have to be broken to form a molecule without any cycles.

$$
\begin{equation*}
C r_{n}=\frac{1}{N_{m o l}} \sum_{i=1}^{N_{m o l}} C r_{i}, \quad C r_{w}=\frac{1}{N} \sum_{i=1}^{N_{m o l}}\left(C r_{i} \cdot D P_{i}\right), \tag{4.15}
\end{equation*}
$$

where $C r_{i}$ is the cycle rank of molecule $i, D P_{i}$ is the degree of polymerization of molecule $i$, and $N$ is the total number of sites (monomers).

### 4.2.5 Ring Involvement

Ring involvement can be quantified by the average number of independent rings in which a randomly chosen site is involved ${ }^{[38]}$. Ring involvement provides additional insight into the local network structure because it ranges from 0 (no rings) to almost 3 ( $100 \%$ cages for 3 -membered rings).

Ring involvement is 0 at the beginning of simulation. Since one new independent ring is formed after each cyclization reaction, and each ring has three sites, ring involvement (I) is increased by

$$
\begin{equation*}
\Delta I=\frac{3}{N} \tag{4.16}
\end{equation*}
$$

### 4.2.6 DMC Algorithm

The dynamic Monte Carlo simulation starts with a finite set of $N$ (which is equal to $10^{6}$ in our model) monomers. The data structures are almost the same compared with our description of the ideal case in Chapter 2. However, we add arrays to store information about the distribution of cycle ranks, Wiener indices and the populations of two-bond blocks. In addition, to allow fast selection of sites for cyclization, we maintain six linked lists of specific two-bond blocks differentiated by end-site connectivities. The simulation procedures are the same as other DMC simulations of polycondensation ${ }^{[38,39]}$. At each MC step, a new siloxane bond is formed, and the conversion is increased by a small constant value (which is $5 \times 10^{-7}$ in our model). The time increment is given by ${ }^{[70]}$ :

$$
\begin{equation*}
\Delta t=\frac{\ln (1 / r)}{\left(N / C_{S i}\right) \sum\left(R_{i j}^{\text {bimol }}+{ }^{3} R_{i j}^{\text {cyc }}\right)}, \tag{4.17}
\end{equation*}
$$

where $N$ is the total number of sites, $r$ is a random number selected from $(0,1)$, and $R_{i j}^{\text {bimol }}$ and ${ }^{3} R_{i j}^{\text {cyc }}$ are the rates described by Eq. (4.3) and (4.4). $C_{S i}$ is the total silicon site
concentration which comes from the continuum model results (see below). Based on the three-membered cyclization reaction rates, Monte Carlo reaction selection is performed in each step to choose the type of reaction to occur. The probability of choosing each reaction is set equal to its rate over the sum of the rates of all possible reactions. If cyclization is chosen, we randomly select one two-bond block from the corresponding linked list. For bimolecular reactions, the reactants are randomly selected from a list containing all sites grouped according to connectivity. Then we update all the data structures including the two-bond block information, molecular weight, Wiener index, cycle rank, and so on. The expressions for the increments of all variables after a DMC step except for conversion and time are shown in Table 4.1. (The derivations of these expressions are shown in the Appendix A.)

Using DMC simulation, we are able to keep track of lists of specific two-bond blocks and then use these to calculate the cyclization rate. This is a significant advantage of the DMC method compared with statistical models. When nonrandom polymerization occurs with extensive cyclization, ${ }^{2} B_{i j}$ populations cannot be correctly predicted by statistical means. Also with the DMC method, we can obtain gel point information, molecular weight distribution, Wiener index, and so on, which are related to film microstructure.

### 4.3 Continuum Drying Model

### 4.3.1 Model Description

The continuum model for the formation of a sol-gel silica coating is described by macroscopic mass conservation equations. The coating is described here with a simplified one-dimensional model. Solvent is removed via evaporation continuously at the top liquid / vapor interface. In addition to evaporation, the diffusion process of solvent within the film should be taken into account in this model. The assumptions made in the model are the same as in our previous chapter. The entire DMC simulation (containing $\sim 10^{6}$ monomers) is treated as a particle of sol whose position and composition are tracked in the continuum model.

Table 4.1 Expressions for incremental changes in variables after each DMC step

| Bimolecular reaction between molecule $i$ and $j$ <br> $\left(N_{m o l}\right.$ is decreased by 1) | Cyclization reaction <br> $\left(N_{\text {mol }}\right.$ remains same $)$ |
| :---: | :---: |
| $\Delta D P_{n}=\frac{D P_{n}^{2}}{N}$ | No changes |
| $\Delta D P_{w}=\frac{2 \cdot D P_{i} \cdot D P_{j}}{N}$ | No changes |
| $\Delta C r_{n}=\frac{C r_{n} \cdot D P_{n}}{N}$ | $\Delta C r_{n}=\frac{D P_{n}}{N}$ |
| $\Delta C r_{w}=\frac{\left(C r_{i} \cdot D P_{j}+C r_{j} \cdot D P_{i}\right)}{N}$ | $\Delta C r_{w}=\frac{D P_{i}}{N}$ |
| $\Delta W_{n}=\frac{D P_{n}}{N}\left(W_{n}+W_{\text {new }}\right)$ | $\Delta W_{n}=\frac{W_{\text {new }} \cdot D P_{n}}{N}$ |
| $\Delta W_{n, l i n}=\frac{D P_{n}}{N}\left(W_{n, l i n}+W_{\text {nev,lin }}\right)$ | $\Delta I=\frac{3}{N}$ |
| No changes |  |
|  |  |

### 4.3.2 Governing Equations

Since the validity of our multiscale model without cyclization has been verified in Chapter 3, we can simplify the continuum model to just consider the solvent and total silica, without including equations for each $Q_{i}$ reactant species.
Therefore, the governing equations are as follows:

$$
\begin{align*}
& \frac{\partial C_{1}}{\partial t}-D_{1} \frac{\partial^{2} C_{1}}{\partial z^{2}}=0  \tag{4.18}\\
& \frac{\partial C_{2}}{\partial t}-D_{2} \frac{\partial^{2} C_{2}}{\partial z^{2}}=0 \tag{4.19}
\end{align*}
$$

where $C_{1}$ is the concentration of solvent, $C_{2}$ is the total silicon concentration.
The initial conditions are:

$$
\begin{equation*}
C_{1}(0, z)=C_{1,0} ; C_{2}(0, z)=C_{2,0} ; \tag{4.20}
\end{equation*}
$$

and the boundary conditions are:
At the substrate $(z=0): \quad D_{i} \frac{\partial C_{i}}{\partial z}=0 \quad(i=1,2) ;$
At the free surface $(z=H(t)):-D_{1} \frac{\partial C_{1}}{\partial z}-C_{1} \frac{d H(t)}{d t}=k_{g}\left(y_{1}^{s}-y_{1}^{\infty}\right)$

$$
\begin{equation*}
\frac{\partial C_{2}}{\partial z}=-\frac{\hat{V}_{1}}{\hat{V}_{2}} \frac{\partial C_{1}}{\partial z} \tag{4.22}
\end{equation*}
$$

where $k_{g}$ is the mass transfer coefficient of solvent (in units of $\mathrm{mol} /\left(\mathrm{cm}^{2} \cdot s\right)$ ), $y_{1}^{s}$ is the molar fraction of solvent at the surface in the gas phase (which is calculated based on Raoult's law), and $y_{1}^{\infty}$ is the molar fraction of solvent far away in the gas, which is set to zero in this paper. As we mentioned in Chapter $3, \hat{V}_{2}=\frac{1-C_{1,0} \hat{V}_{1}}{C_{2,0}}$, where $\hat{V}_{i}$ is the molar volume of component $i$. Assuming that only solvent evaporates, the rate of change of film thickness, or surface velocity, can be calculated according to the following expression:

$$
\begin{equation*}
\frac{d H(t)}{d t}=v^{s}=-\hat{V}_{1} k_{g}\left(y_{1}^{s}-y_{1}^{\infty}\right), \tag{4.24}
\end{equation*}
$$

### 4.3.3 Dimensionless Variables and Simulation Procedure

The following dimensionless variables are utilized to solve the governing equations numerically:

$$
\begin{equation*}
\eta=z / H(t), h=H(t) / H_{0}, c_{i}=C_{i} / C_{0}, \quad \tau=\frac{D_{1}}{H^{2}} t . \tag{4.25}
\end{equation*}
$$

Using the dimensionless variable $\eta$, the new region is always from $\eta=0$ to $\eta=1$, that is, the physically moving domain is mapped onto a fixed domain, and we do not need to modify the spatial grid during the simulation. The solvent transport equation in dimensionless form was given in Chapter 3.

This set of dimensionless equations is numerically solved using an explicit centered finite difference method. We discretize the whole domain into a number of thin slices, each one with a fixed thickness $\Delta \eta$. The time interval $\Delta t$ comes from the DMC simulation, as given by Eq. (4.17) for each DMC step. At the surface, the mole fraction of solvent in solution is $x m=\frac{c_{1}^{s}}{c_{1}^{s}+c_{2}^{s}}, c_{i}^{s}$ is the dimensionless concentration at the surface of the solution. Therefore we can calculate the mole fraction of solvent at the surface in the gas phase using Raoult's law, $y_{1}^{s}=\frac{P_{1} \cdot x m}{P_{t}}$, where $P_{1}$ is the solvent vapor pressure and $P_{t}$ is the total pressure. At each finite difference step, we use the concentrations, film thickness, surface velocity, and Robin boundary conditions at the surface from the previous time step to complete the calculation. Also, the entire DMC simulation is treated as a particle of sol whose position and composition are tracked in the continuum model. We use linear interpolation to perform the tracking of the particle and to obtain the total silicon site concentration, which is used as an input for the calculation of time intervals in the DMC model, as mentioned above. The procedure for tracking particles is the same as that described in Chapter 3.

### 4.3.4 Parameters

Two important dimensionless parameters, Biot number (Bi) and Damköhler number $(D a)$ are used to summarize how process parameters affect the drying process of the solgel film. We use the monomer condensation rate coefficient $k_{00}^{*}$ as the reference to
define the Damköhler number because it represens the fastest reaction rate in a sol-gel solution.

$$
\begin{equation*}
B i=\frac{k_{g} H_{0} \hat{V}_{1}}{D_{1}}, \quad D a=\frac{k_{00}^{*} C_{0} H_{0}{ }^{2}}{D_{1}} \tag{4.26}
\end{equation*}
$$

The variations of $B i$ and $D a$ values correspond to using different values of the parameters in their definition.

The values of parameters $D_{1}, \hat{V}_{1}, k_{g}$, and so on are set to arbitrary values in the model, because these values are not easy to obtain and they may change during drying and gelation; in addition, the dimensionless form of our model makes it insensitive to specific values of parameters, and allows us to focus on the competition between the drying and gelation process, and how this competition affect the coating structure. Still, it should be possible to relate a good model to real process parameters; in the future it should be possible to use structure-property relationships based on the Wiener index to even handle changing transport coefficients during coating. For now, we use constant values in our program, which are given by $C_{1,0}: C_{2,0}=4: 1, C_{2,0}=1.0 \mathrm{~mol} / L, \hat{V}_{1}=0.1 \mathrm{~cm}^{3} / \mathrm{mol}$, and $D_{1}=D_{2}$.

### 4.4 Results and Discussion

### 4.4.1 Conversion at Gelation

One method to estimate the value of gel conversion is based on a plot of weightaverage degree of polymerization $\left(D P_{w}\right)$ as a function of conversion. The divergence of the curve indicates gelation. In Figure 4.6, DMC results are presented for polycondensation of tetrafunctional monomers to establish the effect of cyclization. Because of the limitation of the Monte Carlo method - namely, the finite size of the population - a deviation of $D P_{w}$ from the bulk value is expected to happen when $D P_{w}$ is larger than $1 \%$ of the total number of monomers, and usually is severe when it is $10 \%$ of the total number of monomers ${ }^{[64]}$. Therefore in Figure 4.6, the upper range of $D P_{w}$ is $1.00 \mathrm{E}+04$ even though $N=1.00 \mathrm{E}+06$. The ideal polycondensation case means the rate coefficients are set equal to one another, and no cyclization is allowed. This case can be


Figure 4.6 Weight-average degree of polymerization as a function of conversion for varying $\kappa$ in DMC simulations of sol-gel polycondensation: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$.
modeled by random branching theory (RBT), and the analytical gel conversion is $\frac{1}{f-1}^{[71]}$, where $f$ is the number of polymerizable groups per monomer, which for silicon sites is $f=4$. In Figure 4.6, the gel conversion founded by DMC simulation of the ideal case is about 0.33 , consistent with the prediction of RBT. The case plotted for $\kappa=0$ is a situation in which only the negative the first shell substitution effect (FSSE) described above is allowed but which still excludes cyclization reactions. The estimated gel conversion of the FSSE case is about 0.45 , which agrees with the results obtained by Kasehagen et al ${ }^{[39]}$. After adding unlimited cyclization in our multiscale model ( $\kappa>0$ ), the gel conversion increases as the cyclization tendency $\kappa$ increases, and for large $\kappa$ the gelation conversion can be even larger than $82 \%$, which is the experimental value. It is very clear from Figure 4.6 that cyclization delays the gelation. The results are consistent with what Rankin et al ${ }^{[38]}$ observed with their polycondensation model without drying. The difference is that here drying is being simulated, and the results discussed are just for one particular sol particle as it traverses through the film.

### 4.4.2 Wiener Index

Wiener index can be used as a measure of molecular compactness. Figure 4.7 shows the scaled Wiener index $\left(W_{n} / W_{n, \text { lin }}\right)$ as a function of conversion for varying $\kappa$ in DMC simulations. All the curves start from 1 and decrease with increasing conversion. That means the molecules are becoming more compact than linear molecules of comparable degree of polymerization would be. This is due to branching and cyclization (for $\kappa \neq 0$ ). Since a negative FSSE results in polymers that are more linear than in the ideal polycondensation case, the scaled index is larger for $\operatorname{FSSE}(\kappa=0)$ and small values of $\kappa$ compared with ideal polycondensation. For a very large value of $\kappa$, e.g. $\kappa=50$, three regions are shown: first, the scaled index decreases and the value is even smaller than the ideal case. This indicates that cyclization can shrink the molecular size so much that it can offset or even override the effects of negative FSSE for molecular growth. After the stage where $W$ decreases (forming precursors), a plateau is reached. Growth of the molecules becomes more important and the molecules maintain the same compactness while growing. Finally, gelation is reached and the molecules become much more


Figure 4.7 Evolution of $W_{n} / W_{n, l i n}$ as a function of conversion for varying $\kappa$ in DMC simulations of sol-gel polycondensation: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$.
compact than comparable linear chains would be. Figure 4.7 also clearly shows that gelation is delayed by cyclization. Because the Wiener index can be used in quantitative structure property relationship in chemistry, we may apply it to obtain the parameters we need in the future, such as diffusion coefficient, to improve our model. For now we consider the Wiener index results to be an indication that viscosity rise would be delayed by cyclization, in addition to a $D P_{w}$ divergence.

### 4.4.3 Cycle Rank

Figure 4.8 shows the number-average cycle rank as a function of $D P_{w}$ with $B i=1000$, $D a=60$, and $H p_{0}=0.8 H_{0}$. The curves in the figure start flat, then increase quickly, especially for large $\kappa$, and finally reach a plateau. These curves show the competition between molecular growth and cyclization (which leads to molecular shrinkage). The set of curves can be divided into three stages. The first is a growth stage, in which molecular growth dominates over cyclization. Cyclization is very low ( $\kappa>10$ ), or even nonexistent at this stage for $\kappa \leq 2$. For our model, this stage occurs for $D P_{w} \leq 5$. The second stage is a cyclization stage, in which cyclization increases much quicker, and growth is comparably low, especially for $\kappa \geq 5$. The third stage is a gelation stage, in which, growth dominates over cyclization again until the sol-gel transition begins.

### 4.4.4 Ring Involvement

Calculated values of ring involvement as a function of conversion with varying $\kappa$ in DMC simulations are shown in Figure 4.9. The numbers in the legend are the values of $\kappa$. This figure shows that ring involvement increases with increasing conversion for all cases. With larger value of $\kappa$, the value of ring involvement at the gel point is higher. At high gel conversion cases, for example, when $\kappa=50$, ring involvement is nearly 3 at the gel point. Thus, multiple rings per silicon site are formed before gelation, that is, cage-like intermediates are formed before gelation.

### 4.4.5 Gelation Regime Map

Two important dimensionless parameters $B i$ and $D a$ are used in our multiscale model to show the competition between mass transfer (drying) and reaction (gelation) in the drying process of sol-gel films. The results can be summarized clearly with a gelation


Figure 4.8 Number-average cycle rank as a function of $D P_{w}$ with varying cyclization tendency $\kappa$ in DMC simulations of sol-gel polycondensation:

$$
B i=1000, D a=60, H p_{0}=0.8 H_{0}
$$



Figure 4.9 Ring involvement as a function of conversion with varying cyclization tendency $\kappa$ in DMC simulations of sol-gel polycondensation: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$. Circles represent gel points.
regime map, as we did for the ideal and FSSE cases in Chapter 3. Before investigating the gelation map of cyclization, we first determine a suitable value of $\kappa$ to be used. As shown in the results so far, a higher gel conversion is correlated with a greater amount of cyclization and the formation of ring- and cage- like species prior to gelation. We are interested in exploring situations where the structure gradient across the film is most severe, and this can be quantified by the difference in gel conversion between the surface of the film and the base. This difference is used as the standard to determine $\kappa$. Figure 4.10 shows gel conversion difference between the surface and base with respect to $\kappa$ for $B i=1000$ and $D a=60$. The average values are based on five repeated calculations and the maximum and minimum values are obtained according to the standard deviations. For the range of $\kappa$ from 1 to 10 , the gel conversion difference between the surface and base is largest when $\kappa=5$. Thus, $\kappa$ is set to 5 in our following results.

In the gelation regime map, three types of qualitatively different phenomena were defined by Cairncross et al. ${ }^{[36]}$ for development of a drying regime map: drying before gelation, gelation before drying and literal skinning. Comparing Figure 4.11 with the gelation regime map of ideal and FSSE cases (see Chapter 3), the cyclization case has the same pattern of regions for three types of phenomena: at low $D a$, the film dries before it gels; at high $D a$, gelation happens before drying; and with high $B i$, literal skinning occurs between the "drying before gelation" region and the "gelation before drying" region. However, the literal skinning region is expanded extensively when cyclization is included in the DMC model. That means cyclization increases the occurrence of literal skinning.

Figure 4.12 shows an example of a structure gradient caused by literal skinning with cyclization. The figure presents number-average cycle rank calculated for conditions within the "literal skinning" region as a function of time for different initial particle positions. First, according to the gel points shown in the figure, we find that the film gels much faster at the surface than inside the film in this case. That means there is a time lag of gelation between the surface and base. This resembles the time lag seen with ideal and FSSE model, but in those cases, the structure across the film was uniform (the gel conversion was the same everywhere). In the present set of calculations with cyclization, Figure 4.12 shows that number-average cycle rank at the gel point inside the film is much larger than that at the surface. Similarly, Figure 4.13 also presents ring involvement at


Figure 4.10 Gel conversion difference between the film surface and base with respect to $\kappa$ in DMC simulations of sol-gel polycondensation: $B i=1000, D a=60$.


Figure 4.11 Gelation regime map with unlimited cyclization (3-membered ring) with $\kappa=5$ in drying sol-gel silica films.

Points are the average values of five repeated calculations.
Dashed lines are the approximate boundaries of each region.


Figure 4.12 Number-average cycle rank as a function of time with different initial particle positions for cyclization literal skinning case: $B i=1000, D a=60, \kappa=5$.


Figure 4.13 Ring involvement at the gel point as a function of initial particle positions for cyclization literal skinning case: $B i=1000, D a=60, \kappa=5$.
the gel point is smaller at the surface than inside the film. The extent of cyclization at gelation is significantly different - about $50 \%$ more cycles per site are found at the base than at the surface of the film. Therefore, there is a molecular structure gradient across the film.

### 4.4.6 Structure Gradient Map

The above sections showed that larger $\kappa$ values cause both an increase in gelation conversion and in the ring involvement. As noted earlier, a quantitative measure of the structural gradient in a film can be represented as the gel conversion difference between the film surface and base $\left(\Delta \alpha_{g e l}\right)$. By definition, the $\kappa$ value is inversely proportional to the silica concentration. We also know that gel conversion increases as $\kappa$ increases, so gel conversion is inversely related to the silica concentration as well. Due to solvent evaporation, the silica concentration at the surface increases more rapidly than inside the film, so the gel conversion is observed to be smaller at the surface than inside the film. Without cyclization, because the gel conversion is not dependent on the silica concentration, the gel conversions are the same throughout the whole film and the structure is uniform. Thus, the gelation conversion difference can be used to estimate just how much the tradeoff between reaction and transport results in a structure gradient across the film. Figure 4.14 presents a structure gradient map with $\kappa=5$. The regions of $B i$ and $D a$ with high values of $\Delta \alpha_{g e l}$ coincide with literal skinning region in the gelation regime map. And the largest $\Delta \alpha_{\text {gel }}$ value observed so far is about 0.1.

Figure 4.15 shows a graphical representation of some of the results of an example with $\Delta \alpha_{\text {gel }} \geq 0.1$. It is a contour plot of number-average cycle rank as functions of position and time with $B i=800, D a=80$ and $\kappa=5$. Because of the finite size limitation of Monte Carlo method, we stop our DMC simulation when the value of $D P_{w}$ is larger than $10 \%$ of the total number of the monomers. This leads to the rough boundary on the right hand side of Figure 4.15 , and represents times well after gelation has occurred, so the cycle rank at that point would presumably be "locked in" to the gel that has formed at that point. The calculated position of the film surface is also shown in the figure.


Figure 4.14 Structure gradient map for cyclization case with $\kappa=5$.
Points are the average values of five repeated calculations. Dashed lines are the approximate contours representing fixed values of $\Delta \alpha_{g e l}$ of each region.


Figure 4.15 Example of contour plot of number-average cycle rank as functions of position and time calculated with $B i=800, D a=80$, and $\kappa=5$. The film surface is labeled, and the contours end at times where $D P_{w}=10 \%$ of the total number of monomers
(leading to the rough boundary on some contours).

### 4.4.7 The Effect of Solvent Vapor Pressure

We also examine the effects of solvent vapor pressure in our model by using two different assumptions about solvent. One is the same as was used in previous calculations - assuming that there is excess water in the solution and that all alcohol has evaporated before the drying process starts, so water is the solvent. The second approach is to assume that alcohol is the solvent and that whatever water was added to the sol was completely consumed for hydrolysis (this may be true for methoxysilanes, for instance). The results of assuming water as solvent have been shown above. In the following, results of assuming alcohol as solvent are compared with those assuming water as solvent. The differences between these two cases come from the different value of solvent vapor pressure. Here, we use PE to denote the vapor pressure of ethanol and PW to denote the vapor pressure of water.

Figure 4.16 shows the gelation regime map calculated using ethanol as solvent and with $\kappa=5$. Compared with figure 4.11 , all three regions are moved to higher values of $D a$ when $B i$ is smaller than 100. However, with high $B i$ ( $B i>100$ ), the conditions related to each phenomenon are almost the same, while the literal skinning region is a little expanded for smaller Bi. Figure 4.17 shows structural gradient map using ethanol as solvent with $\kappa=5$. Compared with figure 4.14 , the region of $B i$ and $D a$ with largest value of $\Delta \alpha_{\text {gel }}(>0.1)$ is almost the same $(B i>500)$, while other regions are shifted to smaller values of $B i$ and $D a$.

Since solvent vapor pressure is a parameter related to the drying process, its value can affect the results only when drying process is the rate-limiting process, that is, when $B i$ is small. This explains why the differences of the results are shown only in the range with small Bi . With the solvent vapor pressure increasing (the ethanol vapor pressure is larger than water vapor pressure), the structural gradient is increased for the same values of Bi and Da . Since our other results (Figure 4.6 to Figure 4.9) are based on large value of Bi ( $B i=1000$ ), there are no major differences in these results due to the change in solvent vapor pressure. Therefore, we don't show the corresponding results of Figure 4.6 to Figure 4.9 with ethanol vapor pressure.


Figure 4.16 Gelation regime map with unlimited cyclization (3-membered ring) for $\kappa=5$ with PE. Points are the average values of five repeated calculations.

Dashed lines are the approximate boundaries of each region.


Figure 4.17 Structure gradient map for cyclization case for $\kappa=5$ with PE.
Points are the average values of five repeated calculations.
Dashed lines are the approximate contours of fixed $\Delta \alpha_{\text {gel }}$.

### 4.5 Summary

A multiscale model for the drying process of sol-gel films with unlimited cyclization has been presented. Two main linkages between components of our multiscale model were used: first, in the continuum model, the entire DMC simulation is treated as a particle of sol whose position and composition are tracked using a diffusion / evaporation finite difference calculation. Thus, the total silicon concentration, which is provided by the continuum model, serves as one input parameter in the DMC model. Second, the time interval used in the continuum model comes from the DMC simulation.

With assumptions of hydrolysis pseudoequilibrium and negative first shell substitution effect for bimolecular and cyclization reactions, our model can predict that the gel conversion increases with increasing cyclization tendency $\kappa$, and the gel conversion can be equal to or larger than the experimental value $(82 \%)$. In this paper, the Wiener index has been introduced as a measure of molecular compactness. An efficient way is described to update the Wiener index. The results clearly show that cyclization shrinks the molecular size.

Competition between molecular growth and cyclization can be represented by curves of number-average cycle rank as a function of weight-average degree of polymerization. Three stages are obtained based on the results: i) A growth stage in which molecular growth dominates over cyclization; ii) A cyclization stage where cyclization increases much quicker than the first stage, and growth is slow, especially for $\kappa \geq 5$; and iii) A gelation stage where growth dominates over cyclization again until the sol-gel transition begins.

The gelation regime map shows the effects of the competition between mass transfer (drying) and reaction (gelation) on the drying process of the sol-gel film. Compared with similar maps for the ideal and FSSE cases, the DMC model with unlimited 3-membered rings has the same tendency to generate three types of phenomena: drying before gelation, literal skinning and gelation before drying. The difference is that the literal skinning region is expanded with cyclization. In other words, cyclization increases the likelihood of literal skinning.

The relationship between ring involvement and conversion with different $\kappa$ and initial particle positions was investigated. The simulations showed that cage-like intermediates
form before gelation at high gel conversion cases (with large $\kappa$ ). With drying the maximum value of ring involvement inside the film is much larger in some cases than that at the surface, suggesting that cyclization can lead to a molecular structure gradient inside the film.

Although by now our model just considers forming 3-membered rings, it is the first model to couple unlimited cyclization in a DMC model of polycondensation with continuum mass transfer processes. It is the first model that can predict structure gradients across drying sol-gel films due to cyclization. The simulations that predict high values of gel conversion gradient between surface and base coincide with the literal skinning region in the gelation regime map.

This multiscale model is our first step to understand the drying process of sol-gel coating with unlimited 3 -membered rings cyclization. However, experiments have shown that 4-membered rings are the dominant structural unit ${ }^{[47,49,56]}$. Therefore a model with unlimited 4-membered rings should give better quantitative predictions. We present the results of this modeling in Chapter 5. And, because Wiener index can be used in quantitative structure property relationship in chemistry, we can apply it to obtain the parameters we need in the future, such as diffusion coefficient, to further improve our model.

## Chapter 5

## Multiscale Modeling with Unlimited 4-membered Ring Cyclization

### 5.1 Introduction

Sol-gel silica films and related polycondensation networks are of growing interest in industrial practice and as sources of novel materials ${ }^{[1]}$. In particular, there has been an explosive growth in the design of mesoporous and macroporous silica-based thin films in the last decade, which is based on the slow formation of a silica gel near ambient conditions in the presence of a structure-directing agent ${ }^{[1,99,100]}$. The coating process of forming sol-gel silica films couples polymerization and drying, i.e., it involves multiple length and time scales ranging from molecular to macroscopic. Therefore, a multiscale model is necessary to link different length and time scales together throughout the entire simulated domain.

At the molecular scale of the sol-gel silica polymerization process, cyclization occurs as a nonrandom, preferential reaction ${ }^{[40-42]}$ and delays gelation to a siloxane bond conversion of about $82 \%{ }^{[43-45]}$ (this value can be compared to a value of $33 \%$ expected for random, ideal polycondensation). Large concentrations of 3- and 4-membered rings containing species have also been found during sol-gel silica polymerization by different analytical techniques ${ }^{[27,40-42,44,46-56]}$. Therefore, cyclization should be taken into account in the polymerization process modeling. Rankin et al. ${ }^{[38]}$ were the first group to present a polymerization model with extensive cyclization to model the formation of polycyclic structures containing 3-membered rings. They used the concept of bond blocks (contiguous paths of discrete numbers of bonds that occur in the population of oligomers) to calculate cyclization reaction rates and applied the dynamic Monte Carlo (DMC) technique to the simulation of the polymerization process. In our previous chapter, we added unlimited 3-membered ring cyclization into our multiscale DMC / continuum model as our first step to investigate the effects of cyclization on the sol-gel silica film coating process. However, experiments show that 4-membered rings dominate over and are more stable structural units than 3-membered rings in real silicates ${ }^{[47-49,53,56]}$ A
polymerization model allowing the formation of 4-membered rings should give better qualitative and quantitative predictions than those allowing only intermolecular reactions (even with substitution effects) or only 3-membered rings. Based on our previous work with a model allowing unlimited formation of 3-membered rings, we will describe a new multiscale model with unlimited 4-membered ring formation. While it seems to be a simple extension of the 3-membered ring polymerization model, accounting for all possible types of 3-bond blocks and their evolution during polymerization introduced challenges that needed to be addressed. Most importantly, the new approach brings the prediction of cyclization into a physically reasonable concentration range for the first time.

In this chapter, we first briefly review DMC simulation of sol-gel silica kinetics ${ }^{[27,31,36,}$ ${ }^{38,39]}$ with a particular focus on our new algorithm for 4-membered rings cyclization. Then, the continuum model to which the DMC method is coupled is formulated based on macroscopic conservation equations for mass, and expressed by a set of partial differential equations for species concentrations with initial and boundary conditions. The entire DMC simulation is treated as a particle of sol whose position and composition are tracked in the continuum model. Linking the two models is accomplished by synchronizing time steps and concentrations between the continuum and DMC models while tracking the positions of sol particles during drying. After introducing the model, we present the results of simulations of small swarms of sol particles starting from different positions in the film. The effect of dimensionless cyclization tendency on the gel point, cycle rank and ring involvement are calculated and discussed. The multiscale modeling approach allows us to observe the competition between growth and cyclization, and between drying and gelation. We will compare the quantitative predictions of the new 4-membered ring calculations with those based only on 3-membered rings.

### 5.2 DMC Model

### 5.2.1 Bimolecular Condensation

With the simplification that hydrolysis is assumed to be at pseudoequilibrium, that only a first shell substitution effect for condensation needs to be considered and that
alcohol-producing condensation can be neglected, the bimolecular rate expressions are given (as in Chapters 3-4) by ${ }^{[38]}$ :

$$
R_{i j}^{b i m o l}= \begin{cases}k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i \neq j  \tag{5.1}\\ \frac{1}{2} k_{i j}^{*}(f-i)(f-j)\left[Q_{i}\right]\left[Q_{j}\right], & i=j\end{cases}
$$

### 5.2.2 Four-membered Ring Cyclization

A cyclization reaction occurs when the two sites chosen to react are in the same molecule. This intramolecular reaction causes a new ring to form. Usually in DMC simulations, if the sites chosen to react by a bimolecular reaction are members of the same molecule, they are not allowed to react. This prevents unrealistic random intramolecular reactions from occurring at a rate that does not take into account the bonding restrictions that favor certain sizes of rings. Similar to the previous chapter regarding 3-membered rings, we use bond blocks ${ }^{n} B_{i j}$ to explicitly calculate cyclization rates based on quasi-unimolecular reactions of these structural units. Here the superscript $n$ represents the number of siloxane ( $\mathrm{Si}-\mathrm{O}-\mathrm{Si}$ ) bonds linking one site to another, and the subscripts $i$ and $j$ represent the connectivities of the sites at the ends of the block (i.e. the numbers of siloxane bonds attached to each end). Since 4-membered rings are prevalent and more stable than 3-membered rings in real silicates, we model cyclization reactions to form only 4-membered rings. Therefore, we just need to pay attention to three-bond blocks. Based on this approach, the rates of cyclization reactions are calculated as ${ }^{[38]}$ :

$$
\begin{equation*}
{ }^{4} R_{i j}^{c y c}=(f-i)(f-j) k_{4 c(i, j)}^{*}\left[{ }^{3} B_{i j}\right], i \& j=1,2,3 . \tag{5.2}
\end{equation*}
$$

where $k_{4 c(i, j)}^{*}$ is the rate coefficient for a bond block terminated with $Q_{i}$ and $Q_{j}$ sites and [ ${ }^{3} B_{i j}$ ] is the concentration of 3-bond blocks. Assuming that the same substitution effect applies to ring closure even in the presence of the geometric restriction from the bond block, the following rate coefficients are used:

$$
K_{4 c}^{*}=k_{4 c(1,1)}^{*}\left[\begin{array}{ccc}
1.0 & 0.9 & 0.81 \\
& 0.1 & 0.09 \\
& & 0.01
\end{array}\right] .
$$

We use the same dimensionless parameter $\kappa$ as defined by Rankin et al. ${ }^{[38]}$ to represent the cyclization tendency of the system

$$
\begin{equation*}
\kappa \equiv \frac{k_{4 c(1,1)}^{*}}{k_{11}^{*}[S i]_{0}} . \tag{5.3}
\end{equation*}
$$

### 5.2.3 DMC Algorithm

The simulation procedures are the same as our previous model with 3-membered ring cyclization. The dynamic Monte Carlo simulation starts from a finite set of $N$ (which is equal to $10^{6}$ in our model) monomers. At each MC step, a new siloxane bond is formed, and the conversion is increased by a small constant value (which is $5 \times 10^{-7}$ here). The time interval is given by the expression originally derived by Gillespie ${ }^{[62,70]}$ :

$$
\begin{equation*}
\Delta t=\frac{\ln (1 / r)}{\left(N / C_{S i}\right) \sum\left(R_{i j}^{\text {bimol }}+{ }^{4} R_{i j}^{c y c}\right)} \tag{5.4}
\end{equation*}
$$

where $N$ is the total number of sites, $r$ is a random number selected from the interval ( 0 , 1), and $R_{i j}^{\text {bimol }}$ and ${ }^{4} R_{i j}^{c y c}$ are the rates given by Eq. (5.1) and (5.2). In this expression, $C_{S i}$ is the total silicon site concentration which comes from the continuum model results at the moment that the reaction is selected. This concentration serves as one link between the DMC model and the continuum model in this multiscale modeling strategy. The largest differences between the models with 3-membered and 4-membered rings are the algorithms for updating the Wiener index after a cyclization reaction and maintaining the lists of bond blocks (changing from two-bond blocks to three-bond blocks):

As described previously for modeling sol-gel polymerization with 3-membered rings (Chapter 4), the Wiener index is a topological index that can be directly related to molecular compactness and rheology of suspensions. Updating the Wiener index of a molecule after a bimolecular reaction was described in that chapter and we use the same procedure here. For updating the Wiener index of a molecule due to a 4-membered ring cyclization reaction, we separate the whole molecule into three parts: left part, middle part and right part (Figure 5.1). Because the new ring has four members (rather than three), the distance from each site in left part (of size $m$ ) to each site in right part (of size $n$ ) is decreased by 2 after cyclization. At the same time, the distance from each site in the middle part of the molecule to each site in the left and right parts remains unchanged.


Figure 5.1 Schematic diagram of the product of a cyclization reaction producing a 4membered ring. Circles represent silicon sites, lines represent siloxane bonds, and dashed circles represent different parts of the molecule used for calculations:
left, middle and right.

Therefore, if we know the sizes of the left and right parts, the calculation of the new part of the Wiener index, $W_{\text {new }}$, is very simple:

$$
\begin{equation*}
W_{\text {new }}=-2 \times m \times n . \tag{5.5}
\end{equation*}
$$

Therefore, Wiener index of the molecule after cyclization is:

$$
\begin{equation*}
W=W+W_{\text {new }}=W-2 m n . \tag{5.6}
\end{equation*}
$$

For example, in Figure 5.1, the left part has 3 nodes, the middle part has 4 nodes and the right part has 2 nodes. After the cyclization reaction, the Wiener index decreases 12. For a general molecular topology in our DMC program, we traverse both the left and right parts of a molecule to calculate the number of nodes (the size) of each part.

To maintain the necessary information about three-bond blocks, we use six linked lists to record all three-bond blocks capable of forming rings, sorted by the connectivities of their ends. In order to have the concentrations of these three-bond blocks, information about ${ }^{3} B_{i j}$ needs to be updated after each reaction step by adding newly created bond blocks created and modifying old ones changed by the reaction. Figure 5.2 shows an example. When a new bond is formed between site L and R in a cyclization reaction, six new 3-bond blocks need to be added, which are L-R-M $\mathrm{M}_{2}-6, \mathrm{R}-\mathrm{L}-1-2, \mathrm{R}-\mathrm{L}-\mathrm{M}_{1}-4,1-\mathrm{L}-\mathrm{R}-5$, 1-L-R-M $\mathrm{M}_{2}$ and $\mathrm{M}_{1}$-L-R-5. Also, three old 3-bond blocks need to be modified, L-1-2-3, L-$\mathrm{M}_{1}-\mathrm{M}_{2}-6$ and $\mathrm{R}-\mathrm{M}_{2}-\mathrm{M}_{1}-4$, because the connectivities of L and R are both changed from 2 to 3. Besides that, the 3-bond block $\mathrm{L}-\mathrm{M}_{1}-\mathrm{M}_{2}$-R that forms a cycle needs to be deleted.

Once the 4-membered cyclization reaction rates are calculated based on the concentration of all 3-bond blocks, Monte Carlo reaction selection can be performed at each step to choose one reaction to occur. As in all DMC methods, the probability of selecting a particular reaction type is proportional to its rate. If cyclization is chosen, we randomly select one three-bond block with the appropriate end connectivities from the corresponding linked list. Then we update all the data structures including the three-bond block information, molecular weight, Wiener index, cycle rank, and so on. We also track the number-average Wiener index $\left(W_{n}\right)$, number-average $\left(C R_{n}\right)$ and weight-average $\left(C R_{w}\right)$ cycle rank of the whole population. Please refer to Chapter 4 for more information about updating the data structures.


Figure 5.2 Schematic showing how information about 3-bond blocks is updated due to an intramoleculer reaction.
Circles represent silicon sites, and lines represent siloxane bonds.
The shaded circles are members of a new ring.

Using the DMC approach, we are able to explicitly track all information about threebond blocks formed and consumed in the course of polymerization, and then to use this information to calculate the cyclization rates. This is the advantage of the DMC method compared with statistical models, which assume that bond block populations can be derived from the populations of constituent sites. Even the hybrid Monte Carlo / spanning-tree model of Sarmoria and Miller used the Monte Carlo method just to sample the populations of bond blocks about a given site based on randomly joining sites according to the polymerization conversion ${ }^{[101]}$. This approach is likely to introduce systematic errors for highly non-random polymerization such as the polymerization we are modeling here. Another advantage of the DMC approach is that we can obtain structural parameters including the gel point, molecular weight distribution, Wiener index, etc., which are related to film microstructure and are not available from a continuum kinetic model.

### 5.3 Continuum Drying Model

### 5.3.1 Model description

The 1D continuum transport model for the formation of sol-gel thin-film coatings is exactly the same as the one described in our previous multiscale modeling work (Chapter 4). It is developed from macroscopic conservation equations for mass. It is a simplified one-dimensional model corresponding to a rapidly deposited film that begins drying and curing after the coating process is complete. Via evaporation, solvent departs the film continuously at the top liquid / vapor interface. In addition to this evaporation, the diffusion of solvent within the film needs to be included in the model. Please refer to Chapter 4 for the assumptions and discussion of the modeling equations. Here, we assume that alcohol (ethanol) is the sole solvent.

### 5.3.2 Governing equations

Assuming only diffusion inside of the film, the governing equations are simply written as follows:

$$
\begin{equation*}
\frac{\partial C_{1}}{\partial t}-D_{1} \frac{\partial^{2} C_{1}}{\partial z^{2}}=0 \tag{5.7}
\end{equation*}
$$

$$
\begin{equation*}
\frac{\partial C_{2}}{\partial t}-D_{2} \frac{\partial^{2} C_{2}}{\partial z^{2}}=0 \tag{5.8}
\end{equation*}
$$

where $C_{1}$ is the concentration of solvent, $C_{2}$ is the total silicon concentration, and $D$ is the diffusion coefficient for each species.

Initial conditions in this formulation are as follows:

$$
\begin{equation*}
C_{1}(0, z)=C_{1,0} ; C_{2}(0, z)=C_{2,0} ; \tag{5.9}
\end{equation*}
$$

Consistent with the description of the film model described above, the boundary conditions are given by:

At the substrate $(z=0): \quad D_{i} \frac{\partial C_{i}}{\partial z}=0 \quad(i=1,2) ;$
At the free surface $(z=H(t)):-D_{1} \frac{\partial C_{1}}{\partial z}-C_{1} \frac{d H(t)}{d t}=k_{g}\left(y_{1}^{s}-y_{1}^{\infty}\right)$

$$
\begin{equation*}
\frac{\partial C_{2}}{\partial z}=-\frac{\hat{V}_{1}}{\hat{V}_{2}} \frac{\partial C_{1}}{\partial z} \tag{5.11}
\end{equation*}
$$

In Eq. (5.11), $k_{g}$ is the mass transfer coefficient of solvent in the vapor phase, $y_{1}^{s}$ is the molar fraction of solvent just above the film surface in the gas phase (which is calculated based on Raoult's law), and $y_{1}^{\infty}$ is the molar fraction of solvent in the gas phase far away from the film, which is set to zero here. The rate of change of film thickness, as known as the surface velocity $v^{s}$, can be calculated according to the following expression:

$$
\begin{equation*}
\frac{d H(t)}{d t}=v^{s}=-\hat{V}_{1} k_{g}\left(y_{1}^{s}-y_{1}^{\infty}\right), \tag{5.13}
\end{equation*}
$$

In Eq. (5.12), $\hat{V}_{2}=\frac{1-C_{1,0} \hat{V}_{1}}{C_{2,0}}$, where $\hat{V}_{i}$ is the molar volume of species $i$.

### 5.3.3 Dimensionless Variables and Simulation Procedure

The following dimensionless variables are defined to solve the transport equations numerically:

$$
\begin{equation*}
\eta=z / H(t), h=H(t) / H_{0}, c_{i}=C_{i} / C_{0}, \quad \tau=\frac{D_{1}}{H^{2}} t \tag{5.14}
\end{equation*}
$$

Using the dimensionless variable $\eta$, the region in which diffusion occurs is always from $\eta=0$ to $\eta=1$. In other words, the physical moving domain is mapped onto a fixed
domain, and we do not need to modify the spatial grid during the simulation. The parameters are the same as those in Chapter 4.

This set of dimensionless equations is numerically solved using explicit centered finite difference method. We discretize the whole domain into a number of thin slices; each one has a fixed thickness $\Delta \eta$. For the solution, the time interval $\Delta t$ is equal to the time interval between reactions estimated from the DMC simulation. At each finite difference step, we use the concentrations, film thickness, the surface velocity, and Robin boundary conditions at the surface from the previous time step to complete the calculation. The entire DMC simulation is treated as a particle of sol whose position and composition are tracked in the continuum model. We use linear interpolation to perform the tracking (see Chapter 3) and obtain total silicon site concentration, which is supplied to the DMC routine to choose the next reaction and calculate the time interval of the next DMC step, as discussed earlier.

### 5.4 Results and discussion

As in our previous chapter about forming 3-membered rings, we will present the results of the multiscale model with 4-membered rings in terms of conversion, numberaverage Wiener index, cycle rank, ring involvement, gelation regime map and structure gradient map. Some of these results will be compared with the results of a model allowing only 3 -membered rings.

### 5.4.1 Conversion at Gelation

Figure 5.3 shows the weight-average degree of polymerization $\left(D P_{w}\right)$ calculated by the model with 4-membered rings as a function of conversion for a specific set of drying conditions, for varying values of $\kappa$. The divergence of the curve indicates the onset of gelation. Similar with the results of the model with unlimited 3-membered rings, the gel conversion increases as cyclization tendency $\kappa$ increases. It is very obvious that cyclization delays gelation, and that for some values of $\kappa$, the gel conversion can be as large as or larger than the experimental value for tetraalkoxysilanes ( $82 \%$ ).

The gel conversions as a function of dimensionless cyclization tendency $\kappa$ for models with 3- or 4-membered rings are compared in Figure 5.4. There are no major differences of gel conversions between simulations with the two types of rings. The curves can still


Figure 5.3 Weight-average degree of polymerization from DMC model with unlimited 4membered rings as a function of conversion for varying $\kappa$ :

$$
B i=1000, D a=60 \text {, and } H p_{0}=0.8 H_{0} .
$$



Figure 5.4 Gel conversion as a function of cyclization tendency $\kappa$ with $B i=1000, D a=60$, and $H p_{0}=0.8 H_{0}$. All points are the average values from five repeated calculations.
be divided into several parts: when $\kappa \leq 0.5$ or $\kappa \geq 50$, gel conversions are almost constant with respect to $\kappa$ for both cases. When $1 \leq \kappa \leq 3.5$, gel conversions with 3membered rings are a little larger than with 4-membered rings. When $5 \leq \kappa \leq 20$, on the other hand, gel conversions of 4-membered rings cyclization are a little larger than those of 3-membered rings cyclization. This transition from the range of $\kappa$ giving almost no cyclization ( $\kappa \leq 0.5$ ) to the range of $\kappa$ giving cage-like precursor formation before gelation ( $\kappa \geq 50$ ) is sharper in the model with 4-membered rings. However, the assumptions behind the model with 4 -membered rings are more realistic. Experiments have shown that 3 -membered ring formation is reversible, at least in the case of methylmodified precursors ${ }^{[27]}$, which has not been accounted for in our model (but which would presumably cause lower conversions at gelation with 3-membered rings). Also, the experimental value of $\kappa$ is about twice as large for 4-membered rings (see below), which would favor the high conversions at gelation observed experimentally.

As we mentioned before, at each MC step, a new siloxane bond is formed, and the conversion is increased by a small constant value (which is $5 \times 10^{-7}$ in our model). So in fact, the gel conversion is determined by the total number of MC steps required to reach the gel point. We can divide the total MC steps into two parts:

$$
\begin{equation*}
S_{t}=S_{b}+S_{c}, \tag{5.15}
\end{equation*}
$$

where $S_{t}$ is the total number of MC steps at the gel point, $S_{b}$ is the number of bimolecular reactions steps and $S_{c}$ is the number of cyclization reactions.

At each bimolecular reaction step, the total number of molecules decreases by one, while at each cyclization reaction step, the total number of molecules remains the same. We keep track of the numbers of reaction steps for $\kappa=50$ and show the results in Table 5.1. This table shows that more bimolecular reactions occur in the 4-membered ring case than with 3-membered rings. This suggests that at gelation, the total number of molecules in the 4-membered ring system is smaller than in the 3-membered ring system. The net result (as we will discuss below) is a higher number-average cycle rank with 4membered rings, although the absolute number of rings per site in the simulation is less.

Table 5.1 Counts of total, bimolecular and cyclization reaction steps in DMC simulations with 3- or 4-membered rings. Here, $B i=1000, D a=60, H p_{0}=0.8 H_{0}$.

| $\kappa=50$ | 3-membered rings cyclization | 4-membered rings cyclization |
| :---: | :---: | :---: |
| $S_{b}$ | 909386 | 949028 |
| $S_{c}$ | 957013 | 919864 |
| $S_{t}$ | 1866399 | 1868892 |

### 5.4.2 Wiener Index

Molecular compactness can be measured by the Wiener index. Figure 5.5 shows the scaled Wiener index ( $W_{n} / W_{n, \text { lin }}$ ) as a function of conversion for varying $\kappa$ in DMC simulations. All the curves start from 1 and decrease with increasing conversion. That means the molecules are becoming more compact than linear molecules of comparable degree of polymerization would be. This is due to branching and cyclization (for $\kappa \neq 0$ ). Since a negative FSSE results in polymers that are more linear than in the ideal polycondensation case, the scaled index is larger at a given conversion for $\operatorname{FSSE}(\kappa=0)$ and cyclization (for $\kappa \neq 0$ ) compared with ideal polycondensation. Figure 5.5 also clearly shows that cyclization delays the gelation.

Compared with results of 3-membered ring case (Figure $5.5^{\prime}$ ), the only difference exists in the region where $\alpha<0.2$ with $\kappa=50$. In this region, the value of scaled index with $\kappa=50$ is identical to or larger than that of ideal case for 4-membered ring cyclization, while the opposite is observed for the 3-membered ring case - the value of scaled index with $\kappa=50$ is smaller than that of ideal case. This is because 3-bond blocks are formed later than 2-bond blocks, so 4-membered ring cyclization reactions start later and occur less in the beginning of the polycondensation process than for 3membered rings. For $\alpha<0.15$, it is also possible that the compaction effect of 4membered ring cyclization can offset the effects of negative FSSE for molecular growth. Therefore, the curve of $\kappa=50$ behaves like the ideal case for $\alpha<0.15$.

### 5.4.3 Cycle Rank

The cycle rank of an oligomer represents the number of independent cycles that must be closed in order to form that structure ${ }^{[38]}$. Figure 5.6 shows the number-average cycle rank for simulations with 4-membered rings and various $\kappa$ values as a function of $D P_{w}$. Compared with Figure 5.6', the curves have same tendencies as for simulations with 3membered rings and also show the competition between molecular growth and cyclization. Models with both types of cyclization can be divided into three stages: growth stage (I), cyclization stage (II) and gelation stage (III). When $\kappa$ is smaller than 2, the values of number-average cycle rank of models with both ring sizes are almost identical. However, with increasing $\kappa$ (especially when $\kappa \geq 5$ ), the number-average cycle


Figure 5.5 Evolution of $W_{n} / W_{n, \text { lin }}$ as a function of conversion for varying $\kappa$ in DMC simulations with 4-membered rings: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$.


Figure 5.5' Evolution of $W_{n} / W_{n, l i n}$ as a function of conversion for varying $\kappa$ in DMC simulations with 3-membered rings: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$.


Figure 5.6 Number-average cycle rank as a function of $D P_{w}$ with varying cyclization tendency $\kappa$ for a DMC model with 4-membered rings: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$.


Figure 5.6' Number-average cycle rank as a function of $D P_{w}$ with varying cyclization tendency $\kappa$ for a DMC model with 3-membered rings: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$.
ranks with 4-membered rings are larger than those found with 3-membered rings. For example, when $\kappa=50$, the number-average cycle rank of 4 -membered rings is about 18.6 at $D P_{w}=10000$ (just after gel point), while the corresponding value with 3membered rings is just about 10.8 . This means that, on average, each molecule in the model with 4-membered ring cyclization has at least 7 more independent cycles at the gel point than each molecule in the model with 3-membered ring cyclization. Naturally, this indicates that the molecular structure is more complicated in the case of 4-membered ring cyclization. This is because the variety and number of 3-bond blocks arrangements is much greater than for 2-bond blocks. The reason for this result will be discussed below.

At each bimolecular reaction step, the total number of molecules decreases by one and the total number of cycles does not change. Therefore, the increment of number-average cycle rank due to a bimolecular reaction step is:

$$
\begin{equation*}
\frac{\partial C r_{n}}{\partial N_{\text {mol }}} \cong \frac{\Delta C r_{n}}{\Delta N_{\text {mol }}}=-\Delta C r_{n}=-\frac{\sum_{i=1}^{N_{m o l}} C R_{i}}{N_{m o l}^{2}}=-\frac{C r_{n}}{N_{m o l}} \Rightarrow \Delta C r_{n}=\frac{C r_{n}}{N_{\text {mol }}}, \tag{5.16}
\end{equation*}
$$

where $C r_{n}$ is the number-average cycle rank and $N_{m o l}$ is the total number of molecules. At each cyclization reaction step, the total number of molecules remains the same and the total number of cycle rank is increased by one for the reactant molecule. Therefore, the incremental change in the number-average cycle rank due to a cyclization reaction is:

$$
\begin{equation*}
\Delta C r_{n}=\frac{1}{N_{m o l}}, \tag{5.17}
\end{equation*}
$$

Comparing Eq. (5.16) and Eq. (5.17), it is easy to see that when $C r_{n}$ is larger than 1 , $\Delta C r_{n}$ is larger for bimolecular reactions based on the same value of $N_{m o l}$. Also, for both reactions, $\Delta C r_{n}$ is larger with smaller $N_{\text {mol }}$. When $\kappa=50$, Table 5.1 shows that more bimolecular reactions occur in 4-membered ring cyclization, so $N_{\text {mol }}$ in the 4-membered ring cyclization is smaller than that in the 3 -membered ring case after some steps. Therefore, the $C r_{n}$ values with 4-membered rings are much larger than those with 3membered rings.

### 5.4.4 Ring Involvement

Another measure of the average level of cyclization in the population of oligomers is ring involvement ${ }^{[38]}$. It is defined as the average number of independent rings in which a silicon site is involved. Ring involvement is 0 in the beginning of simulation. Since one new independent ring is formed after each cyclization reaction, and each ring has four sites, ring involvement $(I)$ is increased by

$$
\begin{equation*}
\Delta I=\frac{4}{N} . \tag{5.18}
\end{equation*}
$$

Figure 5.7 shows the ring involvement of 4 -membered rings as a function of conversion with varying $\kappa$. The numbers in the legend are the values of $\kappa$. Comparing Figure 5.7 with Figure 5.7', the curves have same tendencies for simulations with 3-membered and 4-membered rings: ring involvement increases as conversion increases for all cases. With larger value of $\kappa$, the value of ring involvement at the gel point is higher. In cases corresponding to high gel conversion, for example, when $\kappa=50$, ring involvement approaches 4 before the gel point. Thus, multiple rings per silica site (representing the formation of cage-like intermediates) are formed before gelation. For $\kappa \geq 5$, the ring involvement of 4-membered rings cyclization is larger as that of 3-membered rings cyclization. Therefore, a silica site is involved in more independent rings with 4membered ring cyclization than in the 3 -membered case. This is consistent with the earlier observation that the molecular structure is more complicated in the 4-membered rings cyclization.

### 5.4.5 Gelation Regime Map

Two important dimensionless parameters $B i$ and $D a$ are used in our multiscale model to summarize the competition between mass transfer (drying) and reaction (gelation) in the drying process of the sol-gel silica film. In all of the discussion above, arbitrary values of $B i$ and $D a$ were used for all calculations, and the focus was on the effects of cyclization parameter. However, these results can be placed into context using gelation regime maps, as we did in our previous chapters. In the gelation regime map, there are three types of qualitative phenomena represented: drying before gelation, gelation before


Figure 5.7 Ring involvement as a function of conversion with varying cyclization tendency $\kappa$ for DMC simulations with 4-membered rings: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$. Circles represent gel points.


Figure 5.7' Ring involvement as a function of conversion with varying cyclization tendency $\kappa$ for DMC simulations with 3-membered rings: $B i=1000, D a=60, H p_{0}=0.8 H_{0}$. Circles represent gel points.
drying and literal skinning ${ }^{[36]}$. These are defined based on time to dry values and gelation times at the top and bottom of the film, and thus give a global picture of the state of the film predicted by the multiscale DMC / continuum model. Figure 5.8 shows the gelation regime map for simulations with unlimited 4-membered ring cyclization and with a fixed value of $\kappa=5$. For 4 -membered rings, this is very much an experimentally relevant value. For the cases where Ng and McCormick were able to estimate $k_{4 c(1,1)}$ and $k_{11}$ of acid-catalyzed tetraethyl orthosilicate sol-gel solutions, the average ratio of the two has a value of about $5.5 \mathrm{~mol} / \mathrm{L}^{[52]}$. Therefore, if an as-deposited sol has a concentration close to $[\mathrm{Si}]_{0}=1 \mathrm{~mol} / \mathrm{L}$, this gives a value for a realistic sol-gel silica solution of $\kappa \sim 5$. Also in terms of the modeling, this value is interesting to study because it represents the conditions with greatest sensitivity of gel conversion difference between film surface and base (and therefore gel structure) to concentration. Comparing Figure 5.8 with the gelation regime map of a multiscale model with 3-membered rings (Figure 5.8'), they are very similar and almost overlap, but the literal skinning region is subtly expanded in the 4-membered ring case.

As discussed above, one of the advantages of our multiscale model is that it allows us to probe the microstructural implications of macroscopic transport processes. One of the unique insights it offers is into structural gradients that can form as a result of concentration gradients present during literal skinning. An example of the effect of 4membered ring cyclization on literal skinning is shown in Figure 5.9. It shows numberaverage cycle rank as a function of time for different initial particle positions. The first thing that we can notice from this figure is that according to the gel points (circles) on the graph, the film gels much faster at the surface than inside the film. That means there is a time lag for gelation between the film surface and base. Such time lags are characteristic of literal skinning and are seen in all gelling / drying systems under the right conditions. However, a new feature is also revealed - the gel points on the curves indicate what extent of number-average cycle rank can be reached before gelation for different initial sol particle positions. Figure 5.9 clearly shows that the number-average cycle rank at the gel point inside the film is twice as large as it is at the film surface. Therefore, there is a molecular structure gradient inside the film. We compare this finding with the corresponding figure for a model with 3-membered rings in Figure 5.9’. It is clear that


Figure 5.8 Gelation regime map with unlimited 4-membered ring cyclization calculated with $\kappa=5$. Points are the average values from five repeated calculations. Dashed lines are the approximate boundaries of each region.


Figure 5.8' Gelation regime map with unlimited 3-membered ring cyclization calculated with $\kappa=5$. Points are the average values from five repeated calculations.

Dashed lines are the approximate boundaries of each region.


Figure 5.9 Number-average cycle rank as a function of time with different initial particle positions for 4-membered ring cyclization: $B i=1000, D a=60, \kappa=5$.

The circles represent gel points.


Figure 5.9' Number-average cycle rank as a function of time with different initial particle positions for 3-membered ring cyclization: $B i=1000, D a=60, \kappa=5$.

The circles represent gel points.
the values of number-average cycle rank at gel point in Figure 5.9 are larger than the values in Figure 5.9', and the gel times in Figure 5.9 are smaller than the gel times in Figure 5.9'. The gradient in number-average cycle rank is also smaller for the model with 3-membered rings; the interior of the film has only approximately $60 \%$ more rings per molecule in Figure 5.9'. Figure 5.10 and 5.10' also show that the gradient of ring involvement is larger for the 4 -membered ring case. Thus, at the same conditions ( $B i, D a$ and $\kappa$ ), compared with a model having 3-membered ring cyclization, the $\mathrm{DMC} /$ continuum model with 4-membered ring cyclization shows faster gelation, a large number-average cycle rank, and a larger gradient of structure across the film with literal skinning.

### 5.4.6 Structure Gradient Map

As discussed above, direct measures of cyclization such as ring involvement and cycle rank increase as the cyclization tendency increases. Also, the conversion at gelation increases in a way that is correlated with cyclization. Therefore, a measure of the structure gradient in a film is the difference in gel conversion between the surface and base. Figure 5.11 presents a structure gradient map for the multiscale model with 4 membered ring cyclization and $\kappa=5$, which is a contour plot of gel conversion difference vs. $B i$ and $D a$. The regions of $B i$ and $D a$ with high values of $\Delta \alpha_{g e l}$ coincide with the literal skinning region of the gelation regime map. Comparing Figure 5.11 with Figure 5.11' (the structure gradient map for 3-membered ring cyclization), all the regions in Figure 5.11 move to much smaller values of $B i$ and $D a$, especially for the large $\Delta \alpha_{g e l}$ value of 0.1 . Therefore, structure gradients occur more easily in the model with 4 membered rings than in the model with 3-membered rings. This suggests that in the real films, where 4-membered rings are the predominant species, drying under conditions of high $B i$ and $D a$ is likely to lead to structure gradients where the top of the film has a "skin" that gels quickly and has fewer cycles, while the interior of the film (near the base) is made up of cage-like precursors. The polymer network with fewer cycles is likely to be more elastic and tough, while a network made up weakly linked, rigid cages would be expected to be more brittle. This would be expected to exacerbate the problems encountered with defect formation due to skinning in sol-gel films. The best way to avoid this problem is most likely to push the conditions towards the "drying before


Figure 5.10 Ring involvement at the gel point as a function of initial particle positions for 4-membered ring cyclization literal skinning case: $B i=1000, D a=60, \kappa=5$.


Figure 5.10' Ring involvement at the gel point as a function of initial particle positions for 3-membered ring cyclization literal skinning case: $B i=1000, D a=60, \kappa=5$.


Figure 5.11 Structure gradient map for the 4 -membered ring cyclization case with $\kappa=5$.
Points are the average values of five repeated calculations.
Dashed lines are the approximate contours of constant $\Delta \alpha_{g e l}$.


Figure 5.11' Structure gradient map for the 3-membered ring cyclization case with $\kappa=5$.
Points are the average values of five repeated calculations.
Dashed lines are the approximate contours of constant $\Delta \alpha_{g e l}$.
gelation" regime, so that a uniform gel film without residual solvent forms.

### 5.5 Summary

The results of a multiscale model for the drying and curing process of sol-gel silica films with unlimited 4-membered ring cyclization are presented. Two main links between the parts of the multiscale model are as follows: first, in the continuum model, the entire DMC simulation is treated as a particle of sol whose position and composition are tracked using a diffusion / evaporation finite difference calculation. The importance of this particle tracking is that the continuum model provides the total silicon concentration for the DMC model, and this thus serves as a spatially distributed "handshake" between the DMC and continuum calculations. The second "handshake" between the models is the time interval for each bond addition in the DMC simulation, which is used as the time interval for the finite difference calculation.

By comparing with our previous model of drying sol-gel films with unlimited 3membered ring cyclization, this new model allowed us to comment on a more physically relevant type of cyclization. As in the previous model, the model with 4-membered rings showed that the gel conversion increases as dimensionless cyclization tendency $\kappa$ increases, and for reasonable values of $\kappa$, gel conversion meeting or exceeding the experimental value ( $82 \%$ ) was observed. Calculations of the topological Wiener index clearly showed that cyclization shrinks the molecular size, including in extreme cases the formation of cage-like precursors that remain compact until the gel point.

Competition between molecular growth and cyclization can be understood using plots of number-average cycle rank as a function of weight-average degree of polymerization. This allows us to make a fair comparison of different cases independent of the changes in gel time and conversion induced by cyclization. Three stages were identified based on the plots: a growth stage where cycle rank remains low, a cyclization stage where cycle rank increases rapidly and a gelation stage where cycle rank reaches a plateau and growth takes off. For $\kappa \geq 5$, on average, each molecule in the new model with 4-membered rings has more independent cycles than each molecule in the former model with 3membered rings, indicating that the molecular structure is more complicated in the 4 membered ring case.

The gelation regime map shows the competition between mass transfer (drying) and reaction (gelation) in the coating process of the sol-gel silica films. The gelation regime maps of models with 4-membered rings and with 3-membered rings were found to be very similar and almost overlapped; the only difference is that the literal skinning region of is a very slightly expanded with 4-membered rings.

The relationships between measures of cyclization (ring involvement and numberaveraged cycle rank) and conversion, time and initial particle position were investigated. The simulations showed that cage-like intermediates form before gelation when the gel conversion is high (with large $\kappa$ ). The number-average cycle rank and the ring involvement at gel conversion inside the film are much larger than those at the surface in many experimentally relevant conditions, so that there is a molecular structure gradient inside the film. The gradients in number-average cycle rank and ring involvement are smaller for the model with 3-membered rings, which also points out that the molecular structure is more complicated in the model with 4-membered ring cyclization. At the same conditions ( $B i, D a$ and $\kappa$ ), compared with the 3 -membered ring case, 4 -membered ring cyclization causes gels to form more quickly and produces gels with more rings per molecule.

The simulations predict that high values of gel conversion difference between the surface and base of a film coincide with the literal skinning region of the gelation regime map. They also show that the structure gradients in the films with 4 -membered rings are larger than those found in films with 3-membered rings. The formation of gel structure gradients would be expected to exacerbate defect formation due to literal skinning.

While its development has been complex, this multiscale model represents a first step to understanding the complete coating process of sol-gel silica. The inclusion of unlimited 4-membered ring cyclization will give more accurate and relevant predictions than our previous models. Still, this model still can be improved in several aspects. For example, transport properties were assumed to be constant during polymerization. The multiscale model provides the opportunity for more "handshaking" between the model components to improve this situation. One way of doing this it to utilize the Wiener index with diffusivity correlations to provide a more physically relevant self-consistent continuum / DMC result in the future. In addition, some limitations may need to be
added for the cyclization reactions, because realistic molecular structures need to be constrained by the actual bond angles and energies of the oligomers. Although 4membered rings are the dominant units, there are still some 3 -membered rings found in the experiments. Therefore, a more comprehensive model would combine 3- and 4membered ring cyclization and would include reversibility of cyclization. This, obviously, is a substantial challenge even with available computational resources, but these are challenges that can be overcome in future developments.

## Chapter 6

## Conclusions

Comprehensive modeling of the coating process of sol-gel silica films requires the consideration of multiple length and time scales ranging from molecular to macroscopic. The formation of the film is controlled by macroscopic parameters; diffusion and mass transport occur over micron or greater lengths scales, and define the concentration fields within which polymerization and (if surfactants are added) self-assembly occur. At the same time, polymerization and self-assembly processes occur which control the film properties such as film microstructure at the molecular level. Therefore, a multiscale model should be used to link these different length and time scale together.

The multiscale model described in this dissertation for the drying process of sol-gel coatings couples molecular to macroscopic phenomena by combining dynamic Monte Carlo (DMC) simulations with the finite difference method (FDM). DMC simulation is a very good choice to model the sol-gel silica polycondensation because it can capture the complete reaction history for a finite set of monomers, it has the flexibility to handle new types of reactions associated with the formation of large polycyclic species and cages, and it can simulate much larger systems and much longer times than competing molecular approaches such as molecular dynamics. The accuracy of DMC as we have implemented it can be verified by the good agreement between simulation results and analytical results (based on RBT) for the ideal polycondensation case. The FDM is an easy and intuitive numerical method to model the drying process of sol-gel silica films. Because we use a one dimensional model to develop the multiscale approach, FDM should provide adequate numerical accuracy and precision for the purposes of this dissertation. In our multiscale model, the entire DMC simulation (containing at least $10^{6}$ monomers) is treated as a particle of sol whose position and composition are tracked using a diffusion / evaporation finite difference calculation. Therefore, the total silicon concentration, which is provided by the continuum model, serves as one "handshake" with the DMC model. The second "handshake" between the models is the time interval from the DMC simulation, which is used as the time interval for the continuum model.

The validity of the multiscale model is verified by the good agreement of the conversion evolution of DMC and continuum simulations for ideal polycondensation and FSSE cases. With assumptions of hydrolysis pseudoequilibrium and negative FSSE for bimolecular and cyclization reactions, our multiscale model can predict that the gel conversion increases with increasing dimensionless cyclization tendency $\kappa$, and the gel conversion can be equal to or larger than the experimental value ( $82 \%$ ). Calculations of the topological Wiener index clearly showed that cyclization shrinks the molecular size, including in extreme cases the formation of cage-like precursors that remain compact until the gel point.

Curves of number-average cycle rank as a function of weight-average degree of polymerization represent the competition between molecular growth and cyclization. This allows us to make a fair comparison of different cases independent of the changes in gel time and conversion induced by cyclization. Three stages are obtained based on the results: i) A growth stage in which molecular growth dominates over cyclization. ii) A cyclization stage where cyclization increases much quicker than the first stage, and growth is slow, especially for $\kappa \geq 5$. iii) A gelation stage where growth dominates over cyclization again until the sol-gel transition begins. For $\kappa \geq 5$, on average, each molecule in the model with 4-membered rings has more independent cycles than each molecule in the model with 3-membered rings, indicating that the molecular structure is more complicated in the 4-membered ring case.

The gelation regime map shows the effects of the competition between mass transfer (drying) and reaction (gelation) on the drying process of the sol-gel silica film. Compared with similar maps for the ideal polycondensation and FSSE cases, the cyclization case has the same tendency to generate three types of phenomena: drying before gelation, literal skinning and gelation before drying. The difference is that the literal skinning region is expanded with cyclization. That means that cyclization increases the likelihood of literal skinning.

The relationships of ring involvement and conversion, number-average cycle rank and time with different $\kappa$ values, ring involvement and initial particle position were investigated. The simulations showed that cage-like intermediates form before gelation at high gel conversion cases (with large $\kappa$ ). With drying the maximum value of ring
involvement inside the film is much larger in some cases than that at the surface, suggesting that cyclization can lead to a molecular structure gradient inside the film.

The simulations predict that high values of gel conversion difference between the surface and base of a film coincide with the literal skinning region of the gelation regime map. They also show that the structure gradients in the films with 4-membered rings are larger than those found in films with 3-membered rings. The formation of gel structure gradients would be expected to exacerbate defect formation due to literal skinning.

The dissertation presents the first multiscale model of polymerization and drying in sol-gel films, and our model confirms the hypothesis that cyclization can lead to structure gradients. While our multiscale model is improved from just considering FSSE to including unlimited 3 -membered ring cyclization, further to including unlimited 4membered ring cyclization, it represents a first step to understanding the complete coating process of sol-gel silica. Still, this model can be improved in several aspects. For example, some limitations may need to be added for the cyclization reactions, because realistic molecular structures need to be constrained by the bond angles and energies. Although 4-membered rings are the dominant units, there are still some 3membered rings found in the experiments. Therefore, a more comprehensive model would combine 3 - and 4 -membered ring cyclization and would include reversibility of cyclization. In addition, transport properties were assumed to be constant during polymerization. The multiscale model provides the opportunity for more "handshaking" between the model components to improve this situation. For example, the Wiener index can be utilized with diffusivity correlations to provide a more physically relevant selfconsistent continuum / DMC result in the future. This, obviously, is a substantial challenge even with available computational resources, but these are challenges that can be overcome in future developments. The dissertation focuses on processing-structure relationships in the films. Using structure-property relationships to understand more about how the structure gradient influences the properties of the film is a logical extension of our work. Another important direction of future work is to expand our 1D model into two dimensions, using finite element method substituting finite difference method to establish a similar connection between the DMC simulations in 2D and the continuum calculations, as we have described in this dissertation for 1D calculations. We
expect that our simulation will allow better prediction of the formation of structure gradients in sol-gel derived ceramics and other nonideal multifunctional polycondensation products, and that this will help in developing coating procedures to reduce coating defects in the future.

## Appendix A

## Calculation of Number- and Weight-average Parameters

## A. 1 Definition

## A.1.1 Degree of Polymerization

- Number-average degree of polymerization: $D P_{n}=\frac{\sum_{i=1}^{N_{m o l}} D P_{i}}{N_{\text {mol }}}=\frac{N}{N_{\text {mol }}} \Rightarrow \frac{1}{N_{\text {mol }}}=\frac{D P_{n}}{N}$
- Weight-average degree of polymerization: $D P_{w}=\frac{\sum_{i=1}^{N_{\text {mol }}}\left(D P_{i}\right)^{2}}{\sum_{i=1}^{N_{\text {mol }}} D P_{i}}=\frac{\sum_{i=1}^{N_{\text {mol }}}\left(D P_{i}\right)^{2}}{N}$
$D P_{i}$ : size of molecule $i ; N$ : number of monomers; $\quad N_{m o l}$ : number of molecules


## A.1.2 Cycle Rank

- Number-average cycle rank: $C r_{n}=\frac{\sum_{i=1}^{N_{m o l}} C r_{i}}{N_{m o l}}=\sum_{i=1}^{N_{m o l}} C r_{i} \cdot \frac{D P_{n}}{N}$,
- Weight-average cycle rank: $C r_{w}=\frac{\sum_{i=1}^{N_{m a l}} C r_{i} \cdot D P_{i}}{\sum_{i=1}^{N_{m a l}} D P_{i}}=\frac{\sum_{i=1}^{N_{m o l}} C r_{i} \cdot D P_{i}}{N}$
$C r_{i}$ : cycle rank of molecule $i$


## A.1.3 Wiener Index

- Number-average Wiener index: $W_{n}=\sum_{i=1}^{N_{m o l}} W_{i} \cdot \frac{1}{N_{m o l}}$,
$W_{i}$. Wiener index of molecule $i$
- Wiener index for linear molecules: $W_{\text {lin }}=\frac{1}{6} m\left(m^{2}-1\right)$
$m$ : molecular size


## A. 2 Bimolecular Condensation Reactions

After each bimolecular reaction, the number of molecules is decreased by 1, i.e. $\Delta N_{\text {chains }}=-1$. Assuming the bimolecular reaction occurs between molecule $i$ (size m$)$ and $j$ (size n ):

## A.2.1 Degree of Polymerization

- Number-average degree of polymerization:

$$
\begin{align*}
& \because \frac{\partial D P_{n}}{\partial N_{\text {mol }}} \cong \frac{\Delta D P_{n}}{\Delta N_{\text {mol }}}=-\Delta D P_{n}, \text { and } \frac{\partial D P_{n}}{\partial N_{\text {mol }}}=\frac{\partial}{\partial N_{\text {mol }}}\left(\frac{\sum_{i=1}^{N_{m o l}} D P_{i}}{N_{m o l}}\right)=-\frac{N}{\left(N_{m o l}\right)^{2}}=-\frac{D P_{n}^{2}}{N} \\
& \therefore \Delta D P_{n}=\frac{D P_{n}^{2}}{N} \tag{A.7}
\end{align*}
$$

- Weight-average degree of polymerization:

$$
\begin{align*}
& \because D P_{w_{-} \text {before }}=\left(\cdots+D P_{i}^{2}+\cdots+D P_{j}^{2}+\cdots\right) / N, \\
& \\
& \quad D P_{w_{-} \text {affer }}=\left(\cdots+\left(D P_{i}+D P_{j}\right)^{2}+\cdots\right) / N=\left(\cdots+D P_{i}^{2}+2 \cdot D P_{i} \cdot D P_{j}+D P_{j}^{2}+\cdots\right) / N  \tag{A.8}\\
& \therefore \\
& \Delta D P_{w}=D P_{w_{-} \text {affer }}-D P_{w_{-} \text {before }}=2 \cdot D P_{i} \cdot D P_{j} / N
\end{align*}
$$

## A.2.2 Cycle Rank

- Number-average cycle rank:

$$
\begin{align*}
& \because \frac{\partial C r_{n}}{\partial N_{m o l}} \cong \frac{\Delta C r_{n}}{\Delta N_{m o l}}=-\Delta C r_{n}, \text { and } \frac{\partial C r_{n}}{\partial N_{m o l}}=-\frac{\sum_{i=1}^{N_{m o l}} C r_{i}}{\left(N_{m o l}\right)^{2}}=-\frac{C r_{n}}{N_{m o l}}=-\frac{C r_{n} \cdot D P_{n}}{N} \\
& \therefore \Delta C r_{n}=\frac{C r_{n} \cdot D P_{n}}{N} \tag{A.9}
\end{align*}
$$

- Weight-average cycle rank:

$$
\begin{aligned}
& \because C r_{w_{-} \text {before }}=\left(\cdots+C r_{i} \cdot D P_{i}+\cdots+C r_{j} \cdot D P_{j}+\cdots\right) / \mathrm{N} \\
& C r_{w_{-} \text {affer }}= \\
&\left(\cdots+\left(C r_{i}+C r_{j}\right) \cdot\left(D P_{i}+D P_{j}\right)+\cdots\right) / \mathrm{N}
\end{aligned}
$$

$$
\begin{align*}
&=\left(\cdots+C r_{i} \cdot D P_{i}+C r_{i} \cdot D P_{j}+C r_{j} \cdot D P_{i}+C r_{j} \cdot D P_{j}+\cdots\right) / \mathrm{N} \\
& \therefore \Delta C r_{w}=C r_{w_{-} \text {affer }}-C r_{w_{-} \text {before }}=\left(C r_{i} \cdot D P_{j}+C r_{j} \cdot D P_{i}\right) / \mathrm{N} \tag{A.10}
\end{align*}
$$

## A.2.3 Wiener Index

- Linear Wiener index increment:

$$
\begin{align*}
W_{\text {nev,lin }} & =W_{(m+n), \text { lin }}-\left(W_{m, \text { lin }}+W_{n, \text { lin }}\right) \\
& =\frac{1}{6}(m+n)\left[(m+n)^{2}-1\right]-\left[\frac{1}{6} m\left(m^{2}-1\right)+\frac{1}{6} n\left(n^{2}-1\right)\right] \\
& =\frac{1}{2} m n(m+n) \tag{A.11}
\end{align*}
$$

- Wiener index increment:

$$
\begin{equation*}
W_{\text {new }}=\sum_{i=1}^{M} \sum_{j=1}^{N} d_{i j}=\sum_{i=1}^{M} \sum_{j=1}^{N}\left(d_{i R}+d_{L j}-1\right)=n \sum_{i=1}^{M} d_{i R}+m \sum_{j=1}^{N} d_{L j}-m n \tag{A.12}
\end{equation*}
$$

- Number-average Wiener index:

$$
\begin{align*}
& \because \frac{\partial W_{n}}{\partial N_{\text {mol }}} \cong \frac{\Delta W_{n}}{\Delta N_{\text {mol }}}=-\Delta W_{n}, \text { and } \sum_{i=1}^{N_{\text {mol }}} d W_{i}=W_{\text {new }}, d N_{\text {mol }}=-1 \Rightarrow \sum_{i=1}^{N_{m o l}} \frac{d W_{i}}{d N_{\text {mol }}}=-W_{\text {new }} \\
& \quad \frac{\partial W_{n}}{\partial N_{\text {mol }}}=-\frac{\sum_{i=1}^{N_{\text {mol }}} W_{i}}{\left(N_{\text {mol }}\right)^{2}}+\frac{\sum_{i=1}^{N_{\text {mol }}} \frac{d W_{i}}{d N_{\text {mol }}}}{N_{\text {mol }}}=-\frac{W_{n}}{N_{\text {mol }}}-\frac{W_{\text {new }}}{N_{\text {mol }}} \\
& \therefore \Delta W_{n}=\frac{W_{n}}{N_{\text {mol }}}+\frac{W_{\text {new }}}{N_{\text {mol }}}=\frac{D P_{n}}{N}\left(W_{n}+W_{\text {new }}\right)  \tag{A.13}\\
& \text { Similarly, } \Delta W_{n, \text { lin }}=\frac{W_{n, \text { lin }}}{N_{\text {mol }}}+\frac{W_{\text {new,lin }}}{N_{\text {mol }}}=\frac{D P_{n}}{N}\left(W_{n, l i n}+W_{\text {new,lin }}\right) \tag{A.14}
\end{align*}
$$

## A. 3 Cyclization Reactions

After each cyclization reaction, $N_{m o l}, D P_{n}$, and $D P_{w}$ are not changed, one cycle rank is added for the reactant molecule $i$.

## A.3.1 Cycle Rank

- Number-average Cycle rank: $\Delta C r_{n}=\frac{D P_{n}}{N}$,
- Weight-average Cycle rank: $\Delta C r_{w}=D P_{i} / N$


## A.3.2 Wiener Index

- Number-average Wiener index: $\Delta W_{n}=\frac{W_{\text {new }}}{N_{\text {mol }}}=\frac{W_{\text {new }} \cdot D P_{n}}{N}$


## Appendix B

## Nomenclature

Bi: Biot number
${ }^{n} B_{i j}$ : n-bond block with ends connectivity $i, j$
${ }^{2} B_{i j}$ : 2-bond block with ends connectivity $i, j$
${ }^{3} B_{i j}$ : 3-bond block with ends connectivity $i, j$
$C$ : concentration
$C_{S i}$ : concentration of total silicon at the particle position
$c$ : dimensionless concentration
$c_{i}^{s}$ : dimensionless concentration at the surface of the solution
$c p_{i}$ : dimensionless concentration at particle position
$c q_{i}$ : dimensionless concentration of $Q_{i}$ species at particle position
$C r_{i}$ : the cycle rank of molecule $i$
$C r_{n}$ : the number-average cycle rank
$C r_{w}$ : the weight-average cycle rank
$D$ : diffusion coefficient
Da: Damköhler number
$d_{i j}$ : topological distance between sites $i$ and $j$ in the molecule
$D P_{w}$ : the weight-average degree of polymerization
$f$ : the number of functionality
$h$ : dimensionless thickness of the film at time $t$
$H(t)$ : the thickness of the film at time $t$
$H_{0}$ : the initial thickness of the film
$h_{p}$ : dimensionless particle position
$I$ : ring involvement
$k_{i j}$ : bimolecular rate constant polycondensation
$k_{3 c(i, j)}$ : rate coefficient of 3-membered ring cyclization
$k_{4 c(i, j)}$ : rate coefficient of 4-membered ring cyclization
$k_{g}$ : mass transfer coefficient of solvent
$L$ : the size of the molecules
$m$ : molecular size
$M W_{i}$ : molecular weight of molecule $i$
$n$ : molecular size
$N$ : the total numbers of sites/monomers considered in MC method
$N_{\text {mol }}$ : the total numbers of molecules in MC method
$P_{i j}$ : the probabilities of reaction rates
$P_{1}$ : the solvent vapor pressure
$P_{t}$ : the total pressure
$P E$ : vapor pressure of ethanol
$P W$ : vapor pressure of water
$Q_{i}$ : a tetrafunctional silicon site with $i$ siloxane bonds
$\left\{Q_{i}\right\}$ : the population of $Q_{i}$ species
[ $Q_{i}$ ]: the concentration of $Q_{i}$ species
$Q_{i}^{C}$ : the concentration of $Q_{i}$ species in the continuum model
$q_{i}$ : dimensionless concentration of $Q_{i}$ species in the continuum model
$r$ : the random number from $(0,1)$
$R_{i j}^{\text {bimol }}$ : bimolecular reaction
${ }^{2} R_{i j}^{c y c}: 3$-membered ring cyclization reaction
${ }^{3} R_{i j}^{c y c}: 4$-membered ring cyclization reaction
$S_{b}$ : the steps of bimolecular reactions
$S_{c}$ : the steps of cyclization reactions
$S_{t}$ : the total number of DMC steps
$t$ : time
$\Delta t$ : time interval calculated by MC method
$v^{s}$ : the free surface velocity
$\hat{V}$ : molar volume
$W$ : Wiener index
$W_{i}$ : Wiener index of molecule i
$W_{n}$ : number-average Wiener index
$W_{n, \text { lin }}$ : number-average Wiener index of linear molecule
$x m$ : the molar fraction of solvent in solution
$y_{1}^{s}$ : the molar fraction of solvent at the surface in the gas phase
$y_{1}^{\infty}$ : the molar fraction of solvent far away in the gas phase
$z$ : distance from the bottom
$\alpha$ : conversion
$\eta$ : dimensionless distance from the bottom
$\tau$ : dimensionless time
$\chi$ : hydrolysis extent
$\kappa$ : cyclization tendency
Subscripts:
With $C$ :
1: solvent
2: total silicon
3: $(\mathrm{SiOH})$ functional group
With $Q^{C} / q$ :
$i$ : number of siloxane bonds

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- Xin Li, Stephen E. Rankin. Multiscale modeling of coupled drying and nonideal polymerization in sol-gel silica films, AIChE 2006 Annual Meeting, San Francisco, CA, November 2006.


## Peer-viewed Publications:

1) Xin Li, Stephen E. Rankin. Multiscale Dynamic Monte Carlo / Continuum Modeling of Drying and Curing in Sol-gel Silica Films (in preparation).
2) Xin Li, Stephen E. Rankin. Multiscale Modeling of Coupled Drying and Curing of Sol-gel Silica Films with Unlimited Three-membered Ring Cyclization (in preparation).
3) Xin Li, Stephen E. Rankin. Multiscale Modeling of Coupled Drying and Curing of Sol-gel Silica Films with Unlimited Four-membered Ring Cyclization (in preparation).
