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Criticality alarm system design guide with accompanying alarm system development for the Radiochemical Processing Laboratory in Richland, Washington

Bryce Greenfield

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Bryce Greenfield  
Graduate

Chemical and Nuclear Engineering  
Department

This thesis is approved, and it is acceptable in quality  
and form for publication.

*Approved by the Thesis Committee:*

*R. L. Bush*

Chairperson

*D. J. Coughlin*

Dr. Gary Coughlin

*Adam Hecht*

Dr. Adam Hecht

*Timothy Hahn*

Dr. Timothy Hahn

**CRITICALITY ALARM SYSTEM DESIGN GUIDE WITH  
ACCOMPANYING ALARM SYSTEM DEVELOPMENT FOR  
THE RADIOCHEMICAL PROCESSING LABORATORY IN  
RICHLAND, WASHINGTON**

**BY**

**BRYCE GREENFIELD**

**ASSOCIATE OF SCIENCE - COMPUTER SCIENCE  
WHATCOM TECHNICAL COLLEGE  
2004**

**BACHELOR OF SCIENCE - NUCLEAR ENGINEERING  
UNIVERSITY OF NEW MEXICO  
2007**

**THESIS**

Submitted in Partial Fulfillment of the  
Requirements for the Degree of

**Master of Science  
Nuclear Engineering**

The University of New Mexico  
Albuquerque, New Mexico

**December, 2009**

## Acknowledgements

I would like to thank Dr. Robert Busch. Your tireless effort and dedication is inspiring. The countless hours you have spent correcting my assignments and instructing me is truly appreciated. My work has been well received here at PNNL, and I feel that the credit is due to your patience and commitment to delivering a quality education to your students.

To all of my committee members, I would like to extend a heartfelt thank you for all that you have done. Through both undergrad and graduate levels Dr. Gary Cooper and Dr. Taro Ueki contributed so much to my education. The rigor of your classes may not have been entirely appreciated at the time, but is now more appreciated than you could know. Unfortunately I had finished my coursework before Dr. Adam Hecht arrived at UNM. However, from the very inception of this thesis writing process, he has offered his help and guidance, which was extremely valuable.

To all of those individuals at PNNL who have given me assistance over the last three years, thank you. With no exception, every staff member that I have encountered has been more than willing to lend a hand. Andrew Prichard deserves special mention. From the moment I arrived at the lab, he has painstakingly mentored me and taken the time to not just answer my questions, but to make me understand those answers. His never wavering patience and endless amounts of knowledge make him the ideal mentor.

And finally to my wife, Robin, words can not convey the heartfelt appreciation and love I have for you. Without your support I would be lost.

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**Bryce Greenfield**

**B.S., Nuclear Engineering, University of New Mexico, 2007  
M.S., Nuclear Engineering, University of New Mexico, 2009**

**ABSTRACT**

A detailed instructional manual was created to guide criticality safety engineers through the process of designing a criticality alarm system (CAS) for Department of Energy (DOE) hazard class 1 and 2 facilities. Regulatory and technical requirements were both addressed. A list of design tasks and technical subtasks was compiled and analyzed to provide concise direction for how to complete the analysis.

An example of the application of the design methodology, the Criticality Alarm System developed for the Radiochemical Processing Laboratory (RPL) of Richland, Washington is also included. The analysis for RPL utilized the Monte Carlo code MCNP5 for establishing detector coverage in the facility. Based on the design methodology, significant improvements to the existing CAS were made that increase the reliability, transparency, and coverage of the system.

## Table of Contents

<b>Acknowledgements .....</b>	<b>iii</b>
<b>ABSTRACT .....</b>	<b>v</b>
<b>List of Figures.....</b>	<b>vii</b>
<b>List of Tables .....</b>	<b>viii</b>
<b>Chapter 1 – Introduction .....</b>	<b>1</b>
Minimum Accident of Concern.....	2
Objective.....	3
Overview of Chapters.....	4
<b>Chapter 2 – Literature Review .....</b>	<b>6</b>
<b>Chapter 3 – Design Process Overview .....</b>	<b>14</b>
Design Methodology .....	16
<b>Chapter 4 – Application of Guideline Methodology .....</b>	<b>49</b>
<b>Chapter 5 – Conclusion .....</b>	<b>94</b>
Summary .....	94
Future Work .....	94
Enhancements .....	95
<b>Definitions.....</b>	<b>97</b>
<b>Appendix A: RPL Building Schematics with Accident and Detector Locations .....</b>	<b>99</b>
<b>Appendix B: CAS Component Descriptions.....</b>	<b>102</b>
Technical Description of the Comparator Panel .....	102
Technical Description of the Radiation Detectors .....	102
<b>Appendix C: Material Definitions for Codes.....</b>	<b>106</b>
<b>Appendix D: Schedule of Deliverables.....</b>	<b>115</b>
<b>Appendix E: Assumptions Used in the CAS Design of RPL.....</b>	<b>116</b>
Modeling Assumptions.....	116
Translation notes .....	118
<b>Appendix F: MCNP5 Input Decks .....</b>	<b>119</b>
<b>References .....</b>	<b>235</b>

## List of Figures

Figure 1. Design process flow sheet .....	24
Figure 2. UNCSR dose reduction factors for various shield thicknesses .....	29
Figure 3. UNCSR sample slide rule for U(93.2)O <sub>2</sub> -(NO <sub>3</sub> ) <sub>2</sub> @ H/X=500 .....	30
Figure 4. Experimental setup for the NIST Sphere Benchmarks.....	55
Figure 5. 0.02 rad arcs for the outlying MAC's in the basement of RPL.....	61
Figure 6. 0.02 rad arcs for the outlying MAC's in the first floor of RPL.....	62
Figure 7. RPL Basement shown with modeled accident locations and the existing detector placement.....	64
Figure 8. RPL First floor shown with modeled accident locations and the existing detector placement.....	65
Figure 9. RPL Second floor layout .....	66
Figure 10. Standard concrete material definition of 2.3g/cc density. ....	70
Figure 11. Graph of the total cross-section of <sup>113</sup> Cd.....	78
Figure 12. Neutron energy spectrum for the spontaneous fission of <sup>252</sup> Cf .....	80
Figure 13. Neutron energy spectrum grouped into 4eV and 20 MeV energy bins for the spontaneous fission of <sup>252</sup> Cf plotted on a log scale .....	81
Figure 14. Existing calibration spectrum .....	82
Figure 15. Average neutron energy spectrum during the Minimum Accident of Concern grouped into 4eV and 20 MeV energy bins .....	83
Figure 16. Existing NCD calibration setup.....	84
Figure 17. Revised NCD calibration setup with the added HDPE .....	86
Figure 18. Modified calibration spectrum grouped into 4eV and 20 MeV energy bins..	87
Figure 19. RPL Basement showing accident locations and NCD locations .....	99
Figure 20. RPL First Floor showing accident locations and NCD locations.....	100
Figure 21. RPL Second Floor showing accident locations, no NCD are located on this floor .....	101

## List of Tables

Table 1. Experimental normalized fission rates for $^{235}\text{U}$ and $^{239}\text{Pu}$ .....	56
Table 2. MCNP5 Computational results with comparison to experimental results.....	57
Table 3. Plutonium minimum accident scenario data.....	58
Table 4. $^{252}\text{Cf}$ calibration source information .....	73
Table 5. Detector counts for each MAC location in RPL.....	76
Table 6. As modeled MAC locations in RPL .....	77
Table 7. Corresponding Data Used in the Histograms .....	88
Table 8. Comparison of deterministic transport results to standard Monte Carlo results	89
Table 9. Detector counts for preliminary sensitivity analysis for maximum loading within the facility .....	91

## **Chapter 1 – Introduction**

There are a variety of hazards facing those who work with fissile material; the most severe of those hazards is a runaway chain reaction known as a criticality accident. A criticality accident can release enormous amounts of radiation that may injure or kill those who are near it. Great care is taken to minimize the chance of a criticality accident occurring, but the possibility cannot be totally eliminated. Therefore it is this minimal possibility that must be accepted and planned for.

One way to lessen the potential impact of an accident event is to install a Criticality Alarm System. The purpose of a CAS is to promptly detect a criticality accident and immediately issue an audible evacuation warning to personnel. It has been shown that rapid evacuation away from criticality accidents can considerably reduce the dose received by personnel (McLaughlin et al., 2000). Getting people out quickly can decrease injury and save lives. This is the motivation to design and implement detection systems in facilities where accidents could occur. Federal standards exist that establish the performance requirements of these systems and discuss their applicability. But nowhere, be it federal or private, is there a standard on how to design them. Currently, there exists no consolidated body of work that addresses how to design a CAS. Because these alarm systems have the potential to save lives, it is of the utmost importance that they be rigorously designed. It is the focus of this thesis to provide an instructional guide for the design of a robust CAS that will perform its functions with the highest reliability.

All non-reactor facilities that handle greater than or equal to:

- 700g of  $^{235}\text{U}$
- 500g of  $^{233}\text{U}$
- 450g of  $^{239}\text{Pu}$
- 450g of any combination of these three isotopes

are required by the Department of Energy to install and operate a criticality alarm system (U.S. DOE, 2005). For the specific performance and detector coverage requirements expected of a CAS, DOE Order 420.1B defers to ANSI/ANS-8.3-1997 Criticality Alarm Systems. ANSI/ANS 8.3.1997 is the primary standard used to judge the acceptability of a CAS design.

A CAS is generally comprised of 3 main components as described in Appendix B: a comparator panel, alarms, and radiation detectors. Selection and placement of the detectors is the most difficult part of a CAS design. The detectors must operate with a high degree of reliability and require infrequent servicing or repair. The detectors, as well as the system in general, also need to minimize the potential for false alarms. The final and most important requirement of the detectors is that they must respond immediately to the Minimum Accident of Concern (MAC).

## **Minimum Accident of Concern**

The Minimum Accident of Concern represents the smallest accident in terms of fission yield and dose rate that the Criticality Alarm System must detect. ANSI/ANS-8.3-1997 defines the MAC as one that delivers “the equivalent of an absorbed dose rate in free air of 0.2 Gy/min (20 rad/min) at 2 meters from the reacting material.” The design

engineer must determine what likely scenarios, specific to the facility, would meet this definition. The engineer must determine the forms of the reacting materials, configuration, concentration, and quantities involved in an accident that will reach the MAC dose rates. Establishing the appropriate MAC for the targeted facility is not trivial and requires considerable effort.

The MAC represents the most difficult accident scenario that the CAS must detect. Therefore, the MAC is used extensively during the design phase to prove or disprove adequate detector coverage in the facility. ANSI/ANS 8.3.1997 establishes what adequate coverage is by requiring that no single channel may cause an alarm or fault. This means that at least two detectors will alarm for every MAC regardless of the accident location. Proving the CAS meets the coverage requirements of ANSI/ANS 8.3.1997 is the ultimate goal of the design engineer and is the benchmark for an effective Criticality Alarm System.

## **Objective**

The purpose of this thesis is to provide a thorough guide to CAS design. Each step of the design process is discussed in detail to show why the step is needed and how to best complete it. Estimates for the time commitment of each step are included, as well as potential pitfalls that may be encountered. A complete CAS design for the Radioisotope Production Laboratory of Richland, Washington is included in this thesis to provide clear illustrations of what is being explained. The included CAS design provides corresponding examples for each topic discussed in the Design Process Overview section.

A Criticality Alarm System designed based on this methodology will meet and exceed all current regulatory requirements.

## **Overview of Chapters**

Chapter 2 provides a synopsis of the major federal requirements and standards that apply to CAS design. Each specific document is briefly summarized and discussed. After reading this chapter, the reader should have an understanding of the relevant regulations that drive the implementation and design requirements of a CAS. A general sense of how the regulations affect the system design is discussed. A more detailed analysis of the ANSI/ANS-8.3-1997 standard on Criticality Accident Alarm Systems completes the chapter.

Chapter 3 begins by giving a conceptual overview of what goes into the design of a CAS. A design process flow sheet is provided to illustrate how different design criteria affect the project. Following the process overview is the Design Methodology. An outline of tasks to be completed is presented as well as a technically-oriented subtask listing. The flow sheet and task outline form the foundation of how the remainder of the document is organized.

Chapter 4 uses a CAS developed for the Radioisotope Production Laboratory(RPL) in Richland, Washington to illustrate how to apply the methodology presented in Chapter 3. The task and technical subtask layout described in the previous chapter is applied to the RPL CAS. Results are given and evaluated for the MAC, coverage requirements, spectrum analysis, sensitivity analysis, and validation benchmarks. MCNP5 inputs (the facility model, validation benchmarks, spectrum

analysis, MAC, and sensitivity analysis) are provided in Appendix D for the different RPL specific models discussed.

The conclusion portion of the thesis draws all the sections together by highlighting and summarizing the major points. The improvements made to the RPL CAS are also listed with some discussion on their potential impacts on the facility with respect to safety and operations. The potential for future work in this area is also evaluated.

## **Chapter 2 – Literature Review**

There are a multitude of documents that regulate the design and performance of a CAS. The final compliance memo for a CAS must not only reference the applicable regulations but include an actual copy of them in an appendix. This is done because the rules change over time. It is crucial to have a hard copy of what the rules were at the time the analysis was performed. Doing so helps avoid liability for future design conditions and performance requirement alterations as well as providing documentation for future system analyses and upgrades.

To begin evaluating the regulations the engineer needs to recognize that different facility classifications require different sets of regulations. The largest difference in regulations is whether or not the facility contains a reactor. The rules are significantly different for reactor and non-reactor facilities. This analysis focuses on CAS systems for non-reactor facilities. An important note, some of the standards discussed apply to all types of facilities; however it is just as crucial to justify why the standard is not applicable as it is to show why it is. Below is list of the documents that should be pulled and checked for relevance for non-reactor facilities.

- 1) DOE 420.1B *Facility Safety* (USDOE, 1997)
- 2) ANSI/ANS-8.1-1998 *Nuclear Criticality Safety in Operations with Fissionable Material Outside of Reactors*
- 3) ANSI/ANS-8.3-1997 *Criticality Accident Alarm Systems*
- 4) ANSI/ANS-8.10-1983 *Criteria for Nuclear Criticality Safety Controls in Operations with Shielding and Confinement*
- 5) ANSI/ANS-8.15-1981 *Nuclear Criticality Control with Special Actinide Elements*
- 6) ANSI/ANS-8.19-2005 *Procedures for Nuclear Criticality Safety*

These are the federal regulations and standards related to Nuclear Criticality Safety and Criticality Accident Alarm Systems. There will also be company specific procedures for how to comply with these documents. If the final compliance report does not apply to both federal and company specific procedure, it will not be accepted. The language used in the final reports will vary from company to company so the format of the report itself will not be discussed. The analysis performed for a Pacific Northwest National Laboratory facility had to comply with the following internal documents:

- 1) *MEA001 Nuclear Criticality Safety Basis Memo Evaluation, Documentation and Approval*
- 2) *NQA1 Quality Control*
- 3) *MA250 Criticality Safety Manual*
- 4) *MA500 Nuclear Material Control and Accountability Plan*
- 5) *Radiochemical Processing Laboratory Documented Safety Analysis*
- 6) *Radiochemical Processing Laboratory Technical Safety Review*
- 7) *Criticality Safety Specification 1*
- 8) *Criticality Safety Specification 2*
- 9) *Criticality Safety Specification 3*

Each of the documents listed above has the possibility of impacting the design, implementation, and final compliance report. The need to thoroughly analyze each document for applicability and to make a detailed list of notes while doing so to keep track of them all is vital to the successful completion of the analysis. Because the second list of requirements is company specific, they will not be discussed in detail. Most of the company specific documents are controlled and not available for public release. Topics that are typically universal regardless of the company, like quality control and method

validation, will be discussed to illustrate how related to these topics tasks can be conducted.

Throughout the range of ANSI/ANS documents, the same definitions are used for the terms shall, should, and may. These terms are defined throughout the standards as follows: *The word "shall" is used to denote a requirement, the word "should" to denote a recommendation, and the word "may" to denote permission, neither a requirement nor a recommendation. To conform with this standard, all operations shall be performed in accordance with its requirements but not necessarily with its recommendations* (ANSI/ANS 8.3, 1997). To avoid misinterpreting what has been said, it is important to keep in mind how these words are defined when reading the standards.

To establish facility and program safety requirements for the DOE, a good starting point for all of these regulations and standards is the Department of Energy Order 420.1B Facility Safety. This document is the fundamental regulatory driver for a CAS in a federal facility. DOE 420.1B then breaks down what is required from a CAS, but it generally does not list the requirements. What Order 420.1B does is reference the documents that specifically list the technical requirements, which are typically ANSI/ANS standards. Order 420.1B is structured this way, no doubt, because the ANSI/ANS standards are periodically reanalyzed and updated. There are some key sections of Order 420.1B that must be read and understood:

- 4.1.1 Nuclear Safety
- 4.3 Nuclear Criticality Safety
- 4.3.3 Specific Requirements

It should be noticed that Order 420.1B augments many sections of the different ANSI/ANS standards. Why it is important to note these modifications is discussed further in Design Process Overview Task II. There is a section in Order 420.4.3.3e part 4 that addresses what is known as quasistatic criticality accidents. Quasistatic accidents are tremendously challenging to detect and are not addressed within this Thesis. Order 420.1B then directs the user to ANSI/ANS-8.1-1998, which is the overarching criticality safety standard. All other criticality related standards address implementing the general philosophy contained in ANSI/ANS-8.1-1998.

### **1) ANSI/ANS-8.1-1998 – Nuclear Criticality Safety in Operations with Fissionable Material Outside Reactors:**

*Scope – This standard is applicable to operations with fissionable materials outside nuclear reactors, except for the assembly of these materials under controlled conditions, such as in critical experiments. Generalized basic criteria are presented and limits are specified for some single fissionable units of simple shape containing U-233, U-235, or Pu-239, but not for multiunit arrays. Requirements are stated for establishing the validity and areas of applicability of any calculational method used in assessing nuclear criticality safety. This standard does not include the details of administrative controls, the design of processes or equipment, the description of instrumentation for process control, nor detailed criteria to be met in transporting fissionable materials.*

This standard lays out the general methodology and techniques for how work with fissionable materials should be carried out. It thoroughly discusses what an acceptable analysis would be for meeting safety requirements, and then it discusses what must happen if this analysis is based on computer simulations. This standard also discusses how computer systems must be validated using established experimental benchmarks to ensure that the code is performing as claimed.

## 2) ANSI/ANS-8.3-1997 – Criticality Accident Alarm System

*Scope – This standard is applicable to all operations involving fissionable materials in which inadvertent criticality can occur and cause personnel to receive unacceptable exposure to radiation. This standard is not applicable to detection of criticality events where no excessive exposure to personnel is credible, nor to nuclear reactors or critical experiments. This standard does not include details of administrative actions or of emergency response actions that occur after alarm activation.*

This standard contains a range of vital information. There is so much useful material in this standard that to discuss it all would be to almost reproduce it in its entirety. The most important parts with regard to design impact are the description of the coverage requirement, false alarm tolerance, detector failure, and the minimum accident of concern. Each of these parameters should be understood because each can impact the physical layout of the system. A brief discussion on the interplay among these parameters is useful to illustrate how one can affect another, and to show how important this standard is to CAS design.

The coverage requirement is the number of detectors that must alarm for the MAC. To meet the coverage requirement, the engineer would like the threshold (trip) setting for the detectors to be as low as possible, but if set too low, then there is a greater risk of false alarms. If the CAS is designed to meet only the minimum detector coverage requirement, then a fault at any one node takes the entire system out of compliance, thereby stopping work in the facility. However, the more detectors required for the system, then the greater the cost of installation and operation becomes. The most important piece of information this standard supplies is the general definition of the MAC.

The minimum accident of concern can be thought of conceptually as the worst case scenario for what a criticality safety engineer must design for. ANSI/ANS-8.3-1997

defines the minimum accident of concern as “the smallest event in terms of yield and dose that a criticality alarm system must detect.” It then goes on to define the MAC even further as “to deliver the equivalent of an absorbed dose rate in free air of 0.2 Gy/min (20 rad/min) at 2 meters from the reacting material.” For the system to be accepted in a DOE facility, CAS must be able to detect the MAC.

The purpose of the MAC definition is to give a clear lower limit of what must be detected, while still giving the criticality engineer some freedom with how to design the system. The standard does this by listing a minimum dose rate and by not listing how this dose rate is detected. From a practical sense not defining what the dose results from, neutrons, gammas, etc., lets the engineer decide what particles the system should detect. Having some freedom here allows the alarm system to be tailored to the individual facility.

### **3) ANSI/ANS-8.10-1983 – Criteria for Criticality Safety Controls in Operations with Shielding and Confinement:**

*Scope – This standard is applicable to operations outside of nuclear reactors with U-235 U-233, Pu-239, and other fissile and fissionable materials in which shielding and confinement are provided for protection of personnel and the public, except the assembly of these materials under controlled conditions, such as in critical experiments. Criteria are provided that may be used for criticality control under these conditions. The standard does not include the details of administrative procedures for control (which are considered to be management prerogatives) nor details regarding the design of processes and equipment or descriptions of instrumentation for process control.*

This standard outlines a possible exception to requiring a CAS in a facility that is over the mass limit cutoff but has large amounts of shielding. This obviously warrants some attention because nothing makes project managers angrier than spending thousands

of dollars on completely unnecessary work. Without going into great detail, the standard's basis for omission of a CAS deals with sufficient shielding requirements, remote operation, and personnel restrictions.

#### **4) ANSI/ANS-8.19-2005 – Administrative Practices for Nuclear Criticality Safety:**

*Scope – This standard provides criteria for the administration of a nuclear criticality safety program for outside-of-reactor operations in which there exists a potential for nuclear criticality accidents.*

*Responsibilities of management, supervision, and the nuclear criticality safety staff are addressed. Objectives and characteristics of operating and emergency procedures are included.*

This addresses the administration of a criticality safety program. Like the other standards mentioned in this section, it references many of the other criticality focused ANSI/ANS standards including ANSI/ANS-8.3-1997 Criticality Accident Alarm Systems. This standard is more focused on how programs are implemented and documented. Because the CAS design will have to be administered adherent to this standard, it should be reviewed during the CAS design process.

#### **5) ANSI/ANS-6.1-1991 – Neutron and Gamma-ray Fluence-to-Dose Factors:**

*Scope – This standard presents data recommended for computing the biologically relevant dosimetric quantity in neutron and gamma-ray radiation fields. Specifically, this standard is intended to for use by shield designers to calculate effective dose equivalent per unit fluence for neutron energies from 1eV to 14 MeV and for gamma-ray energies from 0.01 to 12 MeV. Establishing maximum permissible exposure limits is outside the scope of this standard.*

This is used convert gamma-ray fluence to dose in free air. The previous analysis of the RPL used this standard in conjunction with the MAC to find the smallest, and therefore most limiting, neutron fluence resultant from a criticality accident. It should be

noted at the time of this analysis, ANSI/ANS-6.1-1991 could not be used because the standards' status had been changed from Active to Historic. The status was changed to Historic because the standard was not reevaluated within the 10 year time frame designated by ANSI/ANS. The criticality safety engineer should be cautious about using it until the status is updated.

Based on the facility description, the judgment can be made as to which ANSI/ANS standards are applicable. As stated previously, it is important to make clear arguments why or why not each standard is specifically applicable to the design. These arguments will be included in the final report and checked over by quality control engineers. Of all the ANSI/ANS standards, the most applicable is obviously 8.3-1997 Criticality Accident Alarm Systems. This document will likely guide the majority of the technical design and warrant a good deal of attention.

## **Chapter 3 – Design Process Overview**

Below is a brief overview of what goes into a complete CAS design. Each of the following steps is discussed in greater detail in the Methodology section. Throughout the design phase, frequent reviews of completed work and of the progress being made are advisable. In such a long process there are innumerable chances for mistakes to be made. If mistakes are made early on and go unnoticed, they can render the finished product useless. It is strongly recommended to have senior criticality safety engineers or other peers periodically review completed work. To provide an itemized summary of what lays ahead, the rather sprawling job of CAS design has been condensed into seven major tasks, which are:

- I. Become familiar with the facility where the CAS will be installed;**
- II. Obtain, read, and summarize all of the pertinent standards and guidelines; then compare company specific requirements to others, so that the most likely scenarios for the Minimum Accident of Concern can be found;**
- III. Outline a schedule of deliverables;**
- IV. Evaluate and choose a computer simulation package to perform the analysis based on validation benchmarks that clearly demonstrate the code chosen will perform as expected;**
- V. Design and model the criticality alarm system for the facility;**
- VI. Show the calibration method follows simple and concise methodology for setting the minimum detector trip points; and**
- VII. Assemble the final report;**

The tasks are roughly in chronological order. Lengthy projects such as this, more often than not, require tasks to be juggled simultaneously or to be moved around to meet deadlines. This project will likely be no different. The list above was constructed to help the novice engineer move from the beginning of the project to the end with organization and traceability.

## **Design Methodology**

This section focuses on how to carry out the design of the CAS. Each task from the outline listed at the beginning of this Chapter is thoroughly described. The approach to each task, as well as any corresponding potential issues, is examined. Task VI contains the majority of the technical design, and it includes a numbered list of specific technical subtasks. This numbered list is then revisited in the Application of Design Methodology Chapter where the same numbering is applied to the RPL Criticality Alarm System analysis.

### **I. Become familiar with the facility where the CAS will be installed**

#### **Initial Phase**

Begin by conducting walk downs of the targeted facility. Take general notes of the layout and the construction materials of the building. If a current CAS exists, make thorough notes about it; pay especially close attention to the detectors and their current locations. New CAS system installation and validation is very expensive so there is strong motivation to utilize existing components.

While in the facility, talk to people to get a sense of what day-to-day operations are like. The engineer needs to develop a sense for what typically occurs in the facility because it will help avoid incorrect assumptions during the modeling phase. Some questions to ask personnel are:

- How often are renovations performed?
- What fissile material movements occur?
- Where are operations with fissile material conducted?

- Do people and/or laboratories move around?
- Are there any neutronically significant materials present?

**II. Obtain, read, and summarize all of the pertinent standards and guidelines; then compare company specific requirements to others, so that the most likely scenarios for the Minimum Accident of Concern can be found;**

After the walk downs are completed, the engineer should have a better understanding of the operations and environment that the CAS design must accommodate. Using this knowledge, pull all of the references listed in the literature review section. Do not worry initially about whether or not they are specifically applicable.

- Spend the time to read them.
- Most are not terribly long.
- Pay close attention to the scope of each document.
- Obtain hard copies of all the references because they are often required in the final CAS design report.
- Make a summary of each document including:
  - Scope/applicability –specify any direct requirements for the facility.
  - Technical limits.

Repeat this process for the company specific regulations. Depending on the size of the company, it may or may not have a document clerk or department. If so, these personnel can be tasked to find and assemble all the applicable documents. Also, some companies maintain libraries that will have most if not all of the documents required. For example, the Hanford Technical Library at PNNL employs fulltime librarians that can be tasked with locating project specific documentation.

After all of the standards and guidelines have been assembled and summarized, it is time to select the most limiting accident scenarios to be modeled. It was found that inserting the summarized lists into a spreadsheet was very useful. The determination of which requirements represent the most limiting accident scenario is not always clear. For example, one standard may define a dose rate where another may define fluence. Unless the difference in magnitude for each situation is considerable, it can be difficult to discern what the most limiting parameter is. Therefore, it is recommended to perform some quick calculations to verify any conjecture.

Once an accurate assessment of the most likely minimum accident scenarios has been made, the assessment must be checked by experienced criticality safety engineers. PNNL requires that the limiting design conditions be peer reviewed, and there is a very explicit list of who can review what types of work. If for some reason, quality assurance is not required at this level, the engineer should seek it out independently. To reiterate, these limiting cases drive the analysis, so if they are incomplete, the design can be incomplete. An example of a final limiting case assessment is shown in Design Methodology Minimum Accident of Concern subtask.

### **III. Outline a schedule of deliverables**

The management responsible for the project may provide a time frame or they may ask the engineer for an assessment of the expected duration of the project. It is generally beneficial for all those involved to have the person(s) with the most applicable experience construct the time line. It is much more difficult to make an accurate judgment of how long a task will take if the individual has never performed it before.

The schedule is also highly dependent on the size of the facility that the CAS is being designed for. The length of time to complete the design phase seems to roughly scale with facility size. There are several factors that drive this relationship. The larger the facility is, the longer it will take to model. The larger the model, the longer it will take to QA. The number of potential accident locations increases with building size, which adds to both the computational time and the analysis phase. For reference, the RPL building description is given in Chapter 4 as well as schematics for each floor in Appendix A. It took approximately four months to perform the analysis and write the final report. The time it will take to draft the report depends on company requirements and individual writing speed. The final Basis Memo for PNNL was written, reviewed, and re-written in about 80 hours. More on the report is discussed later in this section.

There are a few key factors that can reduce the CAS design time. Most time saving factors are human-based. For example computer code writing skills, general criticality safety knowledge, and regulatory knowledge can all aid the design engineer in completing tasks more quickly. For all the duration times listed from this point on, it is assumed that the user has the skills of an average entry-level engineer.

#### **IV. Evaluate and choose a computer simulation package to perform the analysis based on validation benchmarks that clearly demonstrate the code chosen will perform as expected**

ANSI/ANS-8.1-1998 requires that any code used for criticality analysis be validated prior to its use. This part of the process is really several tasks combined: choosing a code, evaluating the codes usability, and validating the codes accuracy relative to the specific situation being modeled. The goal in this step is to choose a computer simulation

package that can show detector coverage and to perform sufficient analysis of the code package chosen, to prove that it does operate as assumed. Meeting this goal is the focus of this section, and it is highly recommended that this goal be met before the design phase is undertaken.

There are some common sense reasons for performing the tasks mentioned above, but there is also a regulation that clearly invokes the need to do them as well. DOE Order 420 mandates that all facilities categorized hazard level 1 or 2 must implement a quality assurance program to oversee and ensure the legitimacy of the work being performed. So throughout the design process all of the work performed, must be checked in accordance with the facility specific QA program. At PNNL, as it should be elsewhere, the code package used to perform ANY analysis most certainly falls into QA space.

A brief word of caution, ANY code used to perform analysis on the system that will be included in any way in the final report must be validated and put through QA. Hopefully it is obvious then that it would be wise for the engineer to pick as few codes as possible to simplify this requirement. It should also be noted that many companies maintain a list of approved code packages that are specific down to the version and release dates. If the code the engineer would like to use is not on this list, it can not be used.

Once the code has been selected, if not already familiar with it, spend a few days learning the basics. It is important to do this because the validation phase is somewhat time consuming and requires a working knowledge of the code to complete. Naturally, it is a good use of time to ensure that the work can be completed in a timely manner with the selected code package. It is just common sense to not waste time validating software

that will never be used. After getting acquainted with how the code works, it is time to proceed with the validation phase. Note, that validation is required for every project, and must be included in the final report regardless of whether similar work has been previously performed.

Computer code validation is accomplished by modeling known, well documented, and very similar real world experiments. Then the results of the simulation are compared to actual real world experiment data. The code is deemed acceptable when it is shown to model similar situations with a prerequisite accuracy. The accuracy varies from company to company. The most important part of the validation process is the selection of relevant benchmarks.

The term, “relevant benchmark” is used in reference to established experiments that are well documented and reviewed and that clearly demonstrate the phenomena being investigated. To put it simply, if modeling fission in  $^{235}\text{U}$ , then find a  $^{235}\text{U}$  benchmark to compare it to. But this is indeed too simple an explanation. Depending on the situation it is also usually important to match the energy spectrum, chemical state of the material, geometry, and in some cases the magnitude of the fluence. The closer the benchmark physically resembles the system being investigated, the easier it will be to argue that the results obtained from the model are indeed acceptable. Luckily there exists a collection of benchmarks that fulfill these requirements.

In the last 50 years there has been a wide variety of criticality experiments conducted all over the world. These experiments were used to gain an understanding of a range of phenomena. Since these experiments were conducted, an organization has been formed to find and assemble them into a readily accessible database. Currently that

organization is the Nuclear Energy Agency (NEA) and their database is known as The International Handbook of Evaluated Criticality Safety Benchmark Experiments (IHECSBE) (NEA, 2008). The NEA has focused on compiling and checking the validity of the experiments and then issuing very high quality detailed reports about there findings. Many evaluated experiments also include computer input and output files for the experiment. The IHECSBE database is a widely acceptable source for validation benchmarks and offers a large variety of experiments.

## **V. Design and model the criticality alarm system for the facility;**

As a certain professor of mine always used to say, “Here lies the meat and potatoes of your work.” Contained in this section are guidelines on how to complete the more technical aspects of this project. Below is an outline of the design phase of the project. Each number represents a subtask of the design process.

- 1) Find the MAC including fluence and spectrum**
- 2) Identify potential locations for detector placement**
- 3) Model the facility**
  - a. Assumptions/omissions/simplifications
  - b. Dimensions
  - c. Materials Used in Computational Models
  - d. Detectors
  - e. Source
  - f. Tallies
  - g. Accident Locations
- 4) Find count rates of the criticality detectors for known conditions**
- 5) Model the Calibration/Counting Setup to find the Detector Cell Tally Efficiencies**
- 6) Adjust the value for the detector minimum trip setting**
- 7) Verify that adequate coverage has been obtained at the new minimum trip setting**
- 8) Modify the Calibration Procedure**

- 9) Apply Variance Reduction as needed**
- 10) Perform sensitivity analysis on the final CAS design**

Each numbered item is discussed in greater detail below. Chapter 4 describes these steps when applied to the design of the RPL criticality alarm system. Figure 1, a design process flow sheet, is included to illustrate how each piece of Task 5 is used to establish detector coverage. Each box colored in grey represents the output of the different subtasks.

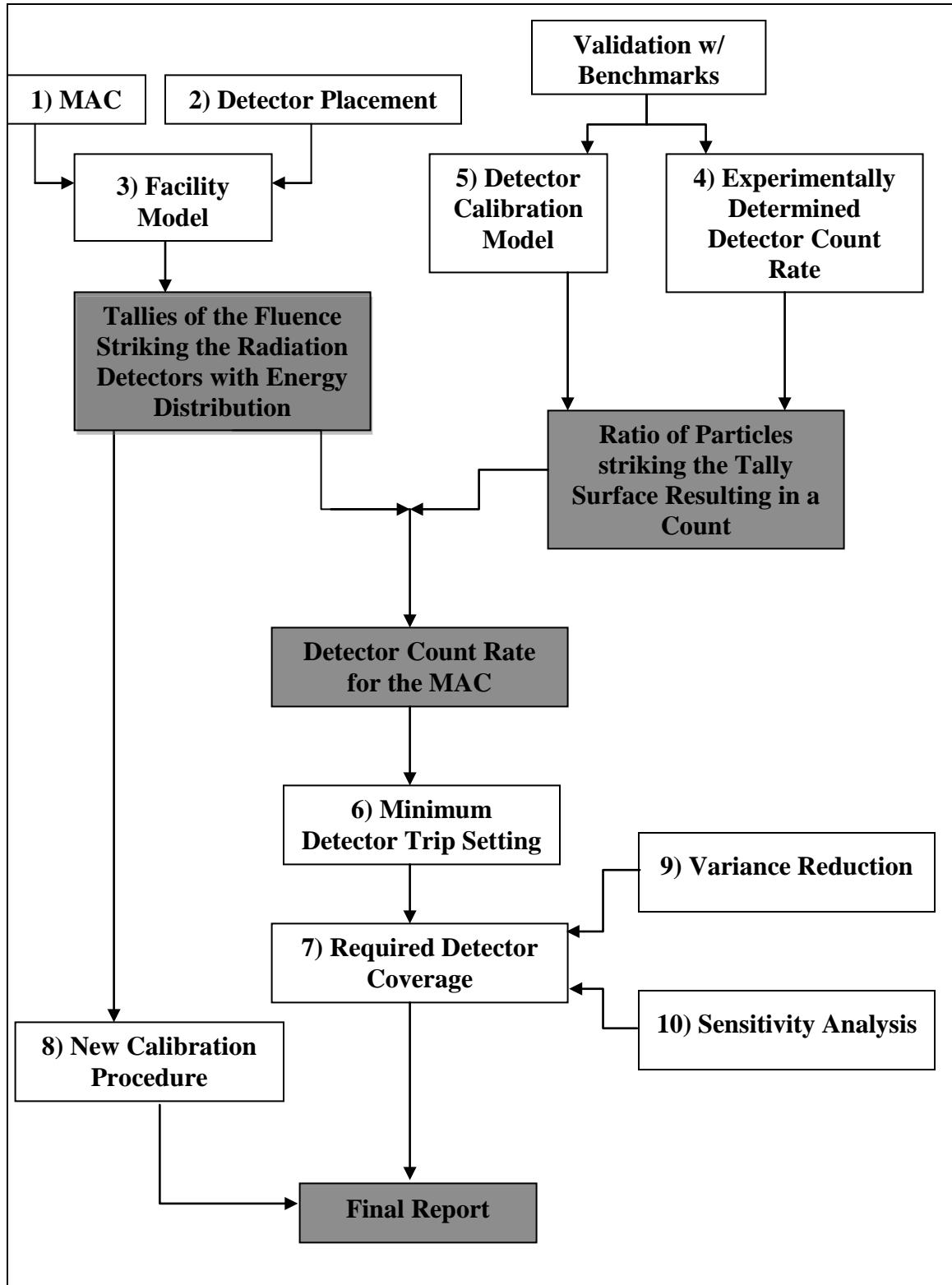


Figure 1. Design process flow sheet

### **Subtask 1 - Find the MAC – Fluence and spectrum**

What the engineer seeks here is the determination of which accident is the most difficult accident to detect. The justification for the need to do this was discussed previously in Design Methodology Task II. How to actually make the determination is the focus of this section.

To find the MAC, start with the definition listed in ANSI/ANS-8.3-1997. Then pick the most probable physical scenarios that are most likely to reach the ANSI/ANS-8.3-1997 dose limit with the smallest number of detectable particles. So if the system employs gamma detectors, then look for the accident condition that maximizes the number of neutrons that contribute to the absorbed dose rate and vice a versa for a neutron detection system. Of course, it is not reasonable to model every conceivable accident scenario to be able to say with absolute certainty what the right answer is. What is reasonable is to pick a handful of the most likely candidates and model those.

To make a guess of what the likely accident scenarios are, it is very useful to remember the shielding properties of both gamma rays and neutrons. Low Z materials shield neutrons the best: increasing density, high Z materials shield gamma rays the best. It is clear that maximizing this discrepancy will likely generate the most limiting accident condition for the respective particles.

If both Uranium and Plutonium are present in the facility, then fission from each isotope should be looked at to determine which is more difficult to detect. Several accident conditions were analyzed for both Plutonium and Uranium including bare metal spheres, metal shielded cask type scenarios, and water reflected sources. Eventually it

was determined for the neutron detection system in RPL that optimally moderated Plutonium and water solutions yielded the fewest neutrons for the required dose rate. Of course Plutonium and water mixtures are not very physically meaningful for chemical reasons, but that is not as important as establishing an absolute lowest bounding accident condition.

Computer models should be made for the most likely accident scenarios: one complete set using  $^{235}\text{U}$  sources, and one complete set using  $^{239}\text{Pu}$  sources. For the accident scenarios, the dose rate in free air from neutrons and photons must be found. Finding this dose rate per neutron and per photon is necessary to determine the corresponding minimum fluence for the accident. The smallest fluence found then identifies the most difficult accident to detect for the ANSI/ANS-8.3-1997 MAC definition.

An advantage of using MCNP5 is absorbed dose can be tallied directly by using the F6 Tally, which is discussed further in the 2) f. Tallies subtask. MCNP5 makes a track length estimate in a designated cell for the absorbed dose there. The dose conversion equation listed as a footnote can be used to convert the result of a standard F6 tally to a final neutron fission source term.<sup>1</sup> KENO can not directly tally absorbed dose at a location. To find dose with KENO, the fluence must first be found with the code and then converted to dose by using published fluence to dose factors. One such standard is ANSI/ANS-6.1-1991 Neutron and Gamma-ray Fluence to Dose Factors. Be aware that currently the status of this standard has been changed to “Historical,” because it has not been reevaluated in the mandatory ten year review period.

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<sup>1</sup> **F6 Result (MeV/g)\*1.00e6 (eV/MeV)\*1.60218e-12 (erg/eV)\*0.01 (g-rad/erg)\*v(neutrons/fission)**

The result of the most limiting fluence found from the MAC absorbed dose analysis will be used as the source weighting factor in the facility model. This weighting factor will therefore scale the results of the simulations to the correct MAC.

### **Subtask 2 - Identify potential locations for detector placement**

Before the facility can be modeled in subtask 3, a preliminary number and location of the criticality detectors must be found. As stated in ANSI/ANS-8.3-1997, there must be at least two detectors that will alarm for every MAC. It is up to the user if a greater degree of coverage is desired. This initial detector placement should be viewed as a starting point, and not as the complete effort for detector placement. It should be noted that for the project, each detector represents a significant installation and maintenance cost. From a fiscal standpoint then, the engineer should optimize the design to use the fewest number of detectors to meet the coverage needs. To simply install dozens of detectors throughout the facility would be very expensive. Also, every detector must be periodically recalibrated and serviced, which adds cost over the lifetime of the system.

It was found that the fastest and simplest method for determining detector placement was to use the Updated Nuclear Criticality Slide Rule (UNCSR) (Hopper & Broadhead, 1998). The UNCSR can be used to estimate dose resultant from a user specified fission yield. This reference allows the user to select the fission yield and then see the corresponding dose from neutrons, gamma rays, and the total at a distance. The UNCSR also provides dose reduction factors as a function of shielding thickness. This allows the yield to be adjusted for different thicknesses of interceding materials.

Preliminary placement of the detectors needed in the facility can be made by inserting the yield from the MAC into the UNCSR. Then using engineering judgment, sufficient accident locations should be chosen for a good estimate of the coverage. For each accident location chosen, the UNCSR can be used to find the absorbed dose in rads, at a distance. It is recommended that floor by floor drawings of the facility are obtained and the appropriate scaling factors established.

To begin placing the detectors, the user must pick a threshold value of dose that represents a detectable fluence for the system. There are a number of ways to reach an estimation of the detection threshold. For both neutron and gamma ray-based systems, the average energy from fission can be used to calculate fluence as a function of absorbed dose in free air. Equation 1 shows the relationship between absorbed dose and fluence.

$$\text{Dose in Air} = \Phi * E_{\text{avg}} / \rho_{\text{air}} \quad (1)$$

In Equation 1,  $\Phi$  is the fluence in # of particles per MAC,  $E_{\text{avg}}$  is the average particle energy from fission, and  $\rho_{\text{air}}$  is the density of air. Equation 1 does not contain time values or rates because the dose is assumed to be entirely from prompt fission. The values found with Equation 1 have to be corrected for the amount of intervening shielding. The UNCSR provides tables that make it easy to approximate the reduction caused by shielding. Figure 2 shows a table of dose reduction factors for prompt fission, which is included in the UNCSR.

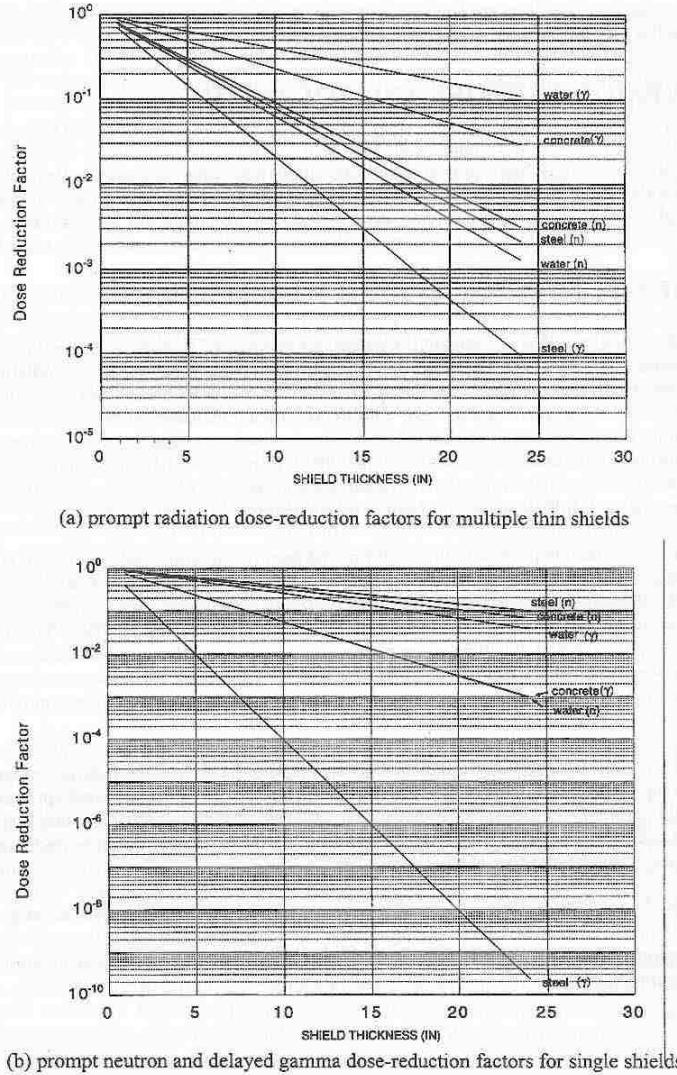


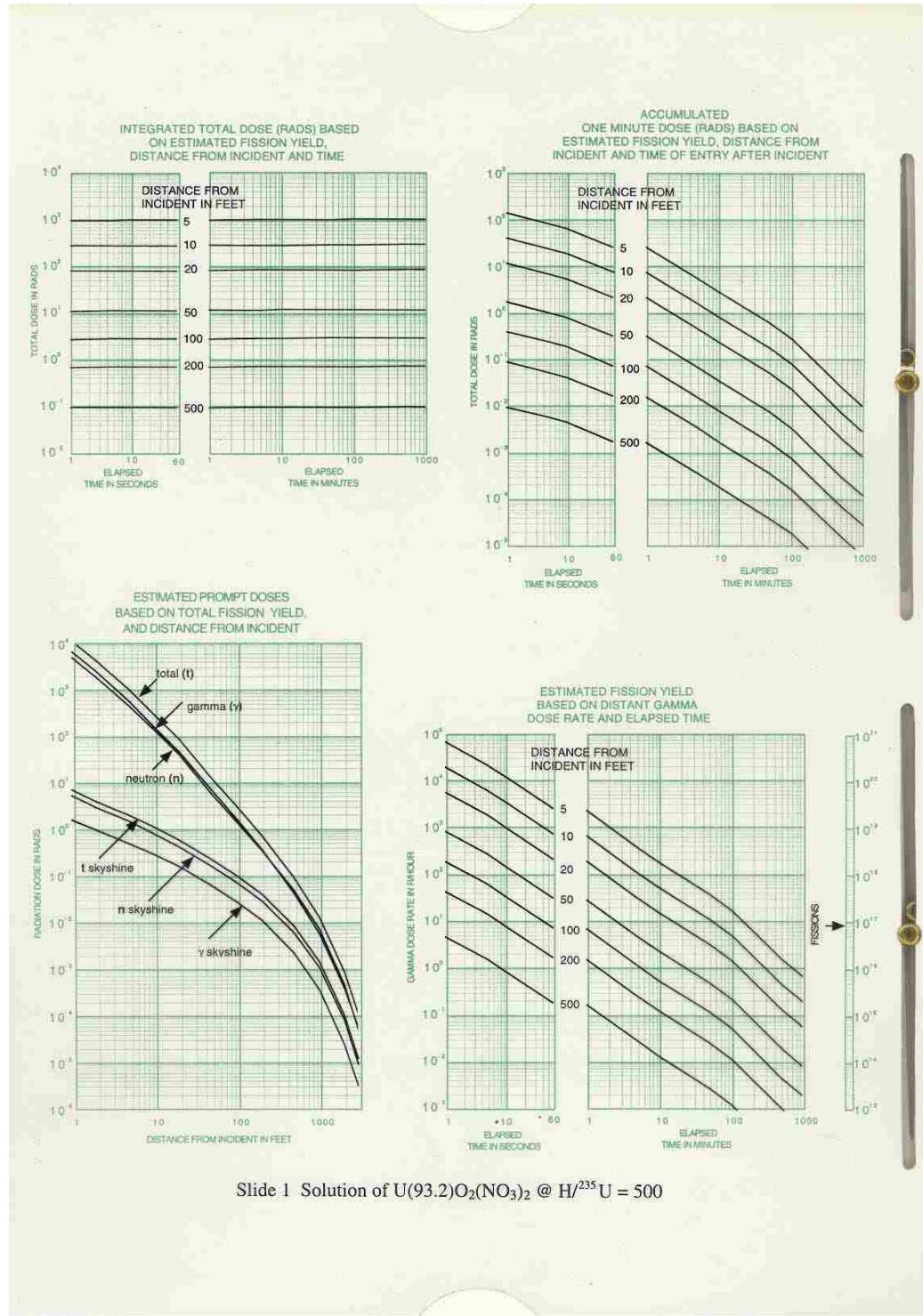
Figure 1 Dose reduction factors for various shield thicknesses

NUREG/CR-6504,  
Vol. 2

6

**Figure 2. UNCSR dose reduction factors for various shield thicknesses**

Once the dose threshold value is found and corrected for shielding, the corresponding distance for the MAC can be established with the slide rule. Figure 3 is an example of a slide rule provided in the UNCSR.



Slide 1 Solution of  $\text{U}(93.2)\text{O}_2(\text{NO}_3)_2$  @  $\text{H}/^{235}\text{U} = 500$

**Figure 3.** UNCSR sample slide rule for  $\text{U}(93.2)\text{O}_2\text{-}(\text{NO}_3)_2$  @  $\text{H}/\text{X}=500$

Using facility drawings, plot an arc of that distance value on the drawing(s) for each accident location. Areas with the most overlapping arcs will logically see the greatest number of accidents and are therefore the optimal locations to place detectors.

If the facility has multiple stories, then the process is repeated for each floor. Once a detector layout is found for each floor, then the facility as whole can be examined. Keep in mind that particles will travel through floors and ceilings. The UNCSR can be used to find the neutron fluence reduction rates through the floors and ceilings for the MAC. Do not spend an extensive amount of time trying to get a perfect detector arrangement here because the computer simulations will provide more accurate guidance. Examples of how the arcs can be drawn are included in the corresponding subtask in Chapter 4.

### **Subtask 3 - Modeling the facility**

#### a. Assumptions/omissions/simplifications

Assumptions, if any, must be clearly documented because they will need to be included as an appendix to the final report. The QA engineer will check the validity of the claims made to ensure that they all result in increased model conservatism. The guiding principle for making assumptions is that they are allowable so long as they increase the amount of conservatism, not decrease it. An example assumption could be to not model the dirt surrounding the building to save computational time. This is an example of an acceptable assumption because it only results in decreasing the number of particles that could be reflected back into the facility from the MAC. Therefore the same guiding principle still holds of being able to detect the worst case possible. An

unacceptable assumption goes in the other direction and could then potentially invalidate the CAS. An example of an incorrect assumption is to avoid modeling the contents of offices located in the facility to save modeling time. This assumption is not conservative because taking material out of the interior of the model decreases the amount of absorption taking place. Removing a loss term inside of the facility artificially “increases” the source of the MAC, which is not conservative.

#### b. Dimensions

There is no substitute for good structural drawings, preferably digital CAD files. Not much needs to be said on the model geometry if it is mostly complete. Model everything that affects the particles being detected, e.g., concrete for neutrons and metals for gammas. If dimensions must be estimated, then always error on overestimating the size of bodies located within the facility and in the opposite direction for bodies located outside of it. In some instances, it may be useful to make hand drawn sketches of the facility. If this is done and the sketches are used as reference material for the model, then they must be included in the Appendices of the final report. This is a generally accepted practice.

#### c. Materials Used in Computational Models

Modeling the materials contained within the facility can be done with a mixture of facility inspections and published material definitions. It is very useful to physically inspect walls, ceilings, offices etc. to determine their contents. Walk-downs should be conducted to determine what amount and type of material is located in the facility.

Generally, it will be unreasonable and unnecessary to model the interiors of every office or laboratory space. It would take too much time to include this level of detail in most facility models. But as mentioned before, the interior fill material must be included to preserve conservatism. The size of the facility, the computational resources, and the time available to perform the CAS analysis should all be considered in how the interior material will be accounted for. The sensitivity analysis conducted on the final design will show how the addition and subtraction of material in the model affects the outcome and ultimately the applicability of the design.

#### d. Detectors

If at all possible the detectors should be modeled to resemble the actual detectors to be installed in the facility. Geometrically accurate detector models may not be usable when the facilities get sufficiently large because computational times grow considerably. For larger facilities it can become necessary to run trillions of particles to get acceptable statistics at the detector surfaces. This number of particles can correspond to very long run times, sometimes weeks or more. Depending on project requirements and company resources, it may become necessary to look at ways of reducing the time required to run the respective codes. Methods for decreasing run times are first discussed in the tally subtask below and then again in more detail in the variance reduction subtask.

Once the computational model of the detector has been made, it must be held constant for every input. However the detectors are modeled in the facility is how they must be modeled in the calibration setup, and likewise for any other model that includes them. Keeping the modeled detectors unchanged is vital to the validity of the method

being applied for finding the minimum trip settings and ultimately the detector coverage verification. Why keeping the detectors unchanged is so important will be discussed further in Chapter 4.

#### e. Source

Getting the correct source in the facility model is very important and can also be very difficult. Whatever situation that was found to be the MAC in the specific facility is the foundation of the source term for the facility model. The resultant minimum fluence found in the MAC is used as the source weighting factor in the model. MCNP5 provides a multitude of methods for modeling different sources. MCNP5 contains fission spectrums for several isotopes as well as a range of distribution functions (X5 Monte Carlo Team, 2003).

It is important to check the computer modeled source distributions for accuracy. The simulated source used in the computational model should mimic what occurs in the real world MAC. It should be understood that modeling a time dependent criticality event is extremely difficult and is beyond the needs of this project. An acceptable substitute is to make an approximate match of both the energy spectrum and fluence of the criticality accident to the simulated source. To verify that this has been done, it is recommend to use the program Vised, which is the visualization tool provided by RSICC with MCNP5. Vised has proven invaluable for catching the numerous source distribution errors made along the way. It is highly recommended to spend some time becoming familiar with the array of uses Vised has to offer. More specifically, time should be spent learning how to check source distributions using the particle tracking features. Vised will

“run” a user designated number of particles through the model using what has been defined as the source. Vised will then produce a picture that will show a variety of useful information about what occurred with the source particles, making it very easy to see errors.

#### f. Tallies

The tallies chosen for the model will yield the results that are used to determine whether or not a detector has alarmed. The tallies can also be used in clever ways to decrease computational run time. MCNP5 provides eight basic tallies for recording particle information but for this project only four of them are of any use (X5 Monte Carlo Team, 2003). The tallies of interest for this design are the F1, F2, F4, and F6. Correspondingly they are surface current, surface flux, track length estimate of cell flux, and the track length estimate of energy deposition. Equations 2, 3, and 4 show, respectively, the F1, F2, and F4 tally equations. The F6 tally equation is merely the F4 cell flux tally multiplied by a heating function.

$$F1 = \int_{E_i} dE \int_{t_j} dt \int_{\Omega_k} d\hat{\Omega} \int dA |\hat{\Omega} \cdot \hat{n}| v n(\vec{r}, \hat{\Omega}, E, t) \quad (2)$$

$$F2 = \frac{1}{A} \int_{E_i} dE \int_{t_j} dt \int dA \phi(\vec{r}, E, t) \quad (3)$$

$$F4 = \frac{1}{V} \int_{E_i} dE \int_{t_j} dt \int dV \phi(\vec{r}, E, t) \quad (4)$$

The units are important to note for the output of each tally. In their standard modes, the F1 tally has units of number of particles, the F2 and F4 tallies both have units of particles/cm<sup>2</sup>, while the F6 tally has units of MeV/gram. MCNP5 will attempt to calculate the corresponding areas, volumes, or masses for each tally but is prone to error (X5 Monte Carlo Team, 2003). It is recommended that the user supply any and all of the aforementioned parameters by using the tally modification cards available in MCNP5.

The F4 tally was found to be the most reliable for tallying fluence. It should be noted that the method MCNP5 uses to calculate the F2 surface flux contains a large angle cosine approximation, which was found for this investigation, to report larger fluence values than did the F4 tally. The surface flux approximation used in the F2 tally for large angle approximation is given in Equation 5 (X5 Monte Carlo Team, 2003). The parameters in Equation 5 are W for the particle weight,  $\delta$  for surface thickness, A as the surface area, n for the unit normal vector, and  $\Omega$  as the particle position vector. Therefore, to be conservative, the decision was made to only use the F4 tally for the detectors in the building and calibration models.

$$\bar{\phi}_S = \lim_{\delta \rightarrow 0} \frac{W \cdot \delta}{A \delta |\Omega \cdot n|} \quad (5)$$

The F6 tally worked very well for the MAC determination because it was very easy to show the conversion from MeV/gram to the absorbed dose value listed in ANSI/ANS-8.3-1997. The F1 current tally can be used to find amounts of reflection provided by different pieces of the facility. This information can then be used to greatly speed up the computational time by creating ALBEDO boundary conditions or modified

cell importance. Run times may be decreased by up to 40 percent using these techniques. This significant decrease in run time is mostly attributed to limiting the amount of time spent on tracking particles in the sand surrounding the facility. Another way to decrease the time spent tracking particles in sand is to change the composition from pure Silicon Dioxide to include a small fraction of Boron. So many collisions can occur in the surrounding sand that a small amount of Boron makes large contributions to absorption. The discussion on tallies and variance reduction more specific to the needs of this project is continued in the Variance Reduction subtask below.

#### **Subtask 4 - Find count rates of the criticality detectors for known conditions**

A bridge must be made between what is tallied in the model to what is counted in reality. The first step in establishing this link is to find a count rate for the detectors in a known configuration that can be modeled in subtask 4 with the same code packaged used for the analysis. The quantity sought in this task will be used in conjunction with the Detector Cell Tally Efficiency to ultimately determine what count rate the minimum trip setting will be.

One possible source of well-documented count rate data would be any existing calibration procedures or operations for the detectors in question. If the calibration procedure has already been developed, then there will be extensive records for count rates as a function of source activity. If this is the case, then acquire all the data regarding the calibration setup that would be needed for modeling it in the designated code package and proceed to subtask 5. If the calibration procedure does not exist then more discussion is needed.

The bulk of how the calibration procedure is developed and implemented is discussed in subtask 8 and hence out of the scope of this subtask. But to proceed with next task, modeling the calibration setup to find the DCTE, some preliminary work for the calibration must be conducted here. For reasons that will be discussed in subtasks 6 and 8, it is important to establish a set of 3 or 4 core detectors that will be used for finding the count rates in this subtask. This set of core detectors will be important for establishing the minimum trip setting and instating the calibration method in subtasks 6 and 8, respectively. Ensure that these core detectors are easily traceable and identifiable. Once this set of detectors has been established, find at least one set of count rates for each in a well defined counting setup. The better the counting setup is documented, the easier subtask 5 becomes.

### **Subtask 5 - Modeling the Calibration/Counting Setup to find the Detector Cell Tally Efficiencies**

The next piece of the puzzle is to find the detector cell tally efficiency (DCTE), which is basically the computational equivalent of the detector efficiency. The DCTE has the units of real world detector count rate divided by the number of simulated particles entering the modeled detector. The quantity being sought here is the fluence striking the modeled version of the detector in the same geometry that the experimental count rate was obtained in. The following provides a simple example of how the DCTE is applied.

Hypothetically, during the MAC runs in the facility, a detector recorded 1000 particles striking it. Using an exact replica of the facility detector in a model of a known counting setup, for a source of weight W, 750 strikes were recorded. The actual count

rate data obtained in the same setup as was modeled, with the same geometry and source used as weight W, was found to be 500 counts per second. Dividing the recorded count rate of 500 counts per second by 750 simulated strikes recorded yields a DCTE of 0.66. The DCTE can then be applied to the number of particles recorded in the MAC scenario to find an actual count rate. Multiplying the simulated 1000 particle strikes found in the facility model by the DCTE of 0.66, equates to a real world count rate of 666 counts for that detector for that MAC. This argument is valid because ANSI/ANS-8.3-1997 states that the MAC is assumed to happen in 1 millisecond, or essentially instantly.

The reason for the assumed duration of the MAC in ANSI/ANS-8.3-1997 is because modeling time dependent criticality is very challenging. Currently there is no widely accepted simulation package that will accurately depict a time dependent criticality event. The current solution for modeling a criticality accident is to simply eliminate the time dependence and assume a prompt yield, thereby ignoring the delayed contributions to the total yield. Experience with criticality accidents has shown that this prompt burst assumption is valid for all non-delayed critical excursions (McLaughlin et al., 2000). Order 420.1B does not require CAS be able to detect delayed critical accidents. Therefore, the source can be weighted by the number of particles resultant from the MAC and not the time dependent fluence.

The DCTE also provides a way to check the validity of the experimentally observed count rate and efficiency. The DCTE allows the computer simulated fluence at the detector location to be compared to the fluence recorded in the real world experiment. If the computational fluence striking the detector versus the recorded count rate is considerably different than the experimentally determined detector efficiency, then

something may be amiss. If necessary a simple solid angle approximation should identify which is wrong –the model or the experiment.

Because the DCTE is so important, the setup used to calibrate the nuclear criticality detectors needs to be modeled with greater precision than the building model. There will be activity data for whatever source is used to find the count rates or to calibrate the detectors. It is important for some, but not all sources, to very accurately decay correct their activities. For example, the neutron source  $^{252}\text{Cf}$ , has a half life of only 2.6 years so it is very important to correct for the change in activity over time. Make sure to use the same energy bin structure for the calibration model as was used for the tallies in the facility model. The same goes for the orientation and configuration of the detectors in each model. Finally, it is very important that the exact same tally be used for both the calibration and the facility models.

### **Subtask 6 - Adjust the value for the detector minimum trip setting**

In theory the minimum trip setting is desired to be as high as possible to avoid false alarms. In practice the engineer wants this value to be as low as possible to make the system design easier. It is advised to take a preliminary look at the count rates being recorded for the detectors in the facility model and the coverage requirements to make an initial trip setting approximation. Based on the radioactive material inventory in the specific facility, an assessment of the likelihood of a false alarm resulting from internal radioactive sources should be made.

With regard to false alarms, it is far more important to get the minimum trip setting as high as possible for gamma detection systems than it is for neutron detection

systems. This is because there are far more natural sources of gamma radiation that could potentially cause a false criticality alarm than there are for neutrons. However, with regard to minimum accident detection it is more important to get the trip setting as low as possible for the neutron based systems than it is for the gamma. Neutron-based systems are not really affected by cosmic radiation sources like their gamma counterparts but neutrons levels are typically lower during a MAC making them more difficult to detect. There is no hard and fast way to identify the minimum trip setting. Only a best guess with sufficient documentation can get a reasonable answer.

### **Subtask 7 - Verify that adequate coverage has been obtained at the new minimum trip setting**

The final steps in the design are focused on proving and optimizing the detector coverage of the facility. Enough data has been determined to evaluate the detector coverage in the facility. General intuition about detector and accident placement has already been discussed, so proceed with proving that the system detects the MAC everywhere in the facility. Once the coverage has been verified at the minimum trip setting by using the DCTE, then the analysis in regards to detector placement is completed. After the detector coverage has been shown, focus should be shifted to the spectrum incident on the detectors. All that remains is to modify the calibration procedure to better mimic the average spectrum observed at the detectors in the facility model during the MAC.

## **Subtask 8 - Modify the Calibration Procedure**

When the coverage has been thoroughly proven, it is time to take the spectrum incident on the tally surfaces of the facility and compare it to the calibration models' incident tally spectrum. It makes sense conceptually to calibrate the nuclear criticality detector to a similar spectrum of what it is expected to detect. There are a variety of ways the calibration source spectrum can be modified. The methods are somewhat different for neutrons and gammas.

For neutrons, low Z materials can be used to increase the ratio of thermal to fast neutrons, or conversely cadmium can be used to almost entirely eliminate neutrons below about 0.4eV. Reflection can be increased by placing materials behind the detectors, which increases the fluence hitting the detectors. Increasing the fluence hitting the detector may be crucial if significant portions of the fluence are lost when the spectrum is modified to better emulate what is seen in the facility.

Gammas require slightly different treatment than neutrons. Equation 6 gives the formula for the linear photon attenuation coefficient  $\mu$ .

$$\mu = \tau + \sigma + \kappa \quad (6)$$

Equation 6 contains the three main physical processes that remove or slow photons in a beam, which are  $\tau$  for the photoelectric effect,  $\sigma$  for the Compton Effect, and  $\kappa$  for pair production. Using these three parameters, materials can be found to modify the spectrum in a targeted way. Contributions from Rayleigh scattering and photonuclear effects can usually be ignored because they are small in comparison to the three processes in Equation 6. Gamma sources are generally cheaper and have a larger intensity than

neutron sources. So eliminating too much of the incident beam is not as significant a concern as it is for neutron sources.

### **Subtask 9 - Variance Reduction**

It should be readily apparent that even in small facilities the volume of the radiation detector is many orders of magnitude smaller than that of the facility. Computationally this presents a problem that is increasingly exacerbated as facility size grows. In stochastic codes, the statistics get ever worse as the detector to building volume ratio decreases. Getting usable statistics can become very arduous for large models. The run times necessary to produce tolerable variance can become unrealistic. The ensuing discussion addresses techniques for reducing computational run times by providing a few possible solutions.

It is extremely important to note that incorrectly applying variance reduction techniques can completely invalidate the results and worse still the errors can be very hard to catch. Each code package has a variety of options available for reducing variance in a problem. There are code specific options, such as invoking deterministic transport for Monte Carlo codes, and there are techniques based on engineering intuition like omitting the material surrounding the facility to decrease time tracking particles there.

The following is a brief list of other code specific variance reduction methods:

- Minimum Energy Cutoffs
- Importance/weight Cutoffs
- Weight windows
- Simplified Scattering treatments
- Source direction biasing

Each technique must be thoroughly analyzed before it is implemented. It should be noted that many organizations' quality control programs explicitly disallow some or all code-invoked variance reduction techniques. Next is a list of engineering-based simplifications that can significantly decrease run times:

- Reduction of MAC locations in the facility needed to show full coverage
- Modifying the numbers of particles being run according to ease of detection in a location
- Form arguments based on proving worst case scenarios to eliminate situations that are obviously easier, simpler, etc.

Each type of simplification has drawbacks and should be used with caution. If any method, be it code specific or engineering based, is used to reduce variance of computations, it must be well documented and peer reviewed.

### **Subtask 10 - Perform sensitivity analysis on the final CAS design**

Sensitivity analysis is the investigation of how different factors could affect the operations of the alarm system. For example, in the computer model, fill all of the rooms within the building with “paper” to see how the neutronics are affected. This is done to say that even in the almost totally inconceivable event of the building turning into a paper repository, the alarm system will still function properly. It might sound outlandish that this type of analysis would need to be performed, but knowing how tolerant the alarm system is to potential facility modification can add credibility to the design.

Sufficient sensitivity analysis should be conducted so that clear bounding limits can be included in the final design memo for what can, and cannot be done, to/in the facility and not interfere with the CAS. The data collected during facility inspections is

especially useful here. Much of what is investigated here will be based on what typically occurs in the facility. Depending on the facility, the following parameters could be important to investigate:

- Modifications and remodeling
- Movement of large amounts of various materials into and out of the facility
- The effect of fire suppression systems
- Changes to the material surrounding the facility

This analysis is done just as much to say what the CAS will not tolerate as it is to say what it will. Both are important for establishing the bounding operational tolerances that the system can endure.

## **VI. Show the calibration method follows simple and concise methodology for setting the minimum detector trip points**

After all the technical analysis is completed and reviewed, it is time to make the recommendations of how to perform detector calibration and movement. It is crucial to make recommendations and corresponding instructions as clear and concise as possible. First, it is a good engineering practice to not over complicate things. A saying from another professor applies in this instance, “keep it simple, stupid.” The more instructions there are, the greater the chance of error. Those who have to implement the recommendations should receive instructions that give abundant measurements to a single common reference point. They should see very few, if any, ambiguous words like around, near, or approximately. All dimensions should be given in one system: mks, cgs, etc.

The second reason to keep things clear and concise is for the regulators. One of the drivers for redoing the analysis of RPL was that the DOE found the minimum trip setting for the neutron detectors to be very poorly worded. What the DOE wanted was a clear minimum trip setting that was easy to confirm or refute. The old criterion was related in terms of absorbed dose per source particle referenced to a Plutonium-Beryllium source. The new definition is, “The neutron detectors in RPL are set to alarm at 600 counts per minute, which corresponds to an absorbed dose rate in free air of 80mrem/hr.” -a clear improvement.

## **VII. Assemble the final report**

The structure of the final report is likely to vary greatly from institution to institution, so it is of no use to go into great detail about how to write it. Also the final report drafted for PNNL is classified as business sensitive, thereby prohibiting it from being used outside of the organization. Accordingly the time needed for writing the report is likely to fluctuate considerably. It took approximately 80 hours to draft, review, rewrite, review again, and finalize the report as a whole. For time estimating purposes it should be taken into consideration that the PNNL report requirements did not seem excessive. It should also be noted that the 80 hour time estimate was not all used at once, but rather over the duration of the project. The report drafted for PNNL contained several sections that were not affected by technical design changes so they could be written ahead of time. Writing report sections early on is highly recommended. The sooner the sections are written, the sooner they can be reviewed. Having fewer sections to go over in the final review will greatly expedite the final submission process. To give

a general sense of what may be included in the final design report, an outline is provided below.

*1) Introduction-State the purpose and scope of the evaluation*

*1.1) Review of Previous Methods*

*2) Description-Describe the process/system*

*3) Requirements Documentation*

*Indicate specific DOE Orders and Guides, ANS Standards, Code of Federal Regulations or other requirement documents that are uniquely applicable to the analysis*

*4) Methodology*

*4.1) Evaluation Methodology*

*When using computer codes, indicate what codes and cross section libraries were used and reference the applicable code configuration control information and the code documentation. Identify the type of computing platform.*

*4.2) Benchmark Evaluation and Bias Determination*

*List the benchmark experiments chosen and discuss their applicability to the problem. Show the calculation of the bias and the uncertainty in the bias. Describe how the bias is applied to the results of this evaluation.*

*5) Evaluation and Results*

*Provide a detailed description of any models used. Reference code generated drawings in an Appendix. State assumptions and simplifications made. Include all calculation results.*

*7) Design Features\changes\improvements*

*8) Summary and Conclusions*

*State the systems, processes or facilities that the analysis is applicable to and indicate any limitations on the evaluation.*

*9) References*

*List all original references. Avoid referencing documents that reference other documents.*

*Appendix Containing Materials and Compositions*

*List and reference all materials. Include atom densities.*

*Appendix Containing Sketches and Drawings*

*Include sketches of the actual process (hand-drawn sketches are generally acceptable and expected) and as-built or design drawings.*

*Appendix Containing Code Input Listings*

*Include input listings for all computer code runs.*

One final note on the report - a hard copy of all the references used along the way was required to be inserted as an Appendix. The definition of references at PNNL was not as expected, so it would be wise to get a clear description of what a reference is before even conducting the building walk downs.

## **Chapter 4 – Application of Guideline Methodology**

This set of tasks deals with the technical application of the CAS design methodology. The CAS designed for RPL is used as an example of the design methodology. Sample MCNP5 computer code inputs are listed in Appendix F for the RPL facility model, the detector calibration setup, the MAC evaluation, and the validation benchmarks. These inputs will help to guide the user through the modeling phase and ultimately the detector placement.

### **I. Familiarization with the facility where the CAS will be installed;**

Over the 6 month duration of this project, roughly a dozen facility inspections were conducted. These inspections provided a solid fundamental understanding of the facility and the operations conducted therein. To form a better understanding of how the system works, a test of the existing criticality alarm system in the building was observed. This is highly recommended because seeing the test put into perspective how the testing procedures were performed.

Until the test of the CAS was witnessed, it had not been readily apparent that the people carrying it out did not have very technical backgrounds. This observation is important because it brings up a very crucial point; the procedures must be written for those who have to read them. Rigorous technical analysis can be performed but if the conclusions drawn from it can not be communicated clearly to those who must enable them, then the analysis itself is trivialized.

The inspections of the facility repeatedly proved to be useful so it is highly recommended to conduct them frequently. Doing so can make many facets of the project go more efficiently.

**II. Obtain, read, and summarize all of the pertinent standards and guidelines; then compare company specific requirements to others, so that the most likely scenarios for the Minimum Accident of Concern can be found;**

After much debate three scenarios, with two different sources, were assumed to be the most likely limiting cases that would reach the MAC. The three cases contained either pure  $^{235}\text{U}$  or pure  $^{239}\text{Pu}$  in an optimally moderated water filled sphere as the source. The three cases were: a bare sphere, a water reflected sphere, and an iron reflected sphere. These three cases were chosen because they resemble some possible physically relevant accident scenarios in the facility. The bare and water reflected spheres were chosen to represent laboratory type accident scenarios. RPL is a radioisotope production facility where much bench top radiochemistry takes place. The iron reflected sphere was selected because it resembled an accident occurring in a shipping cask. A significant amount of material is moved in and out of the facility, including into and out of the High Level Radiochemistry Hot cells. Then all six permutations of these scenarios were modeled to find the most limiting fluence during the MAC. The result of the limiting plutonium accident runs with the final determination of the most limiting scenario is presented in this chapter under Subtask 1.

### **III. Outline a schedule of deliverables;**

Assembling the schedule of deliverables was taken care of by the project manager and is included in Appendix D. The project manager assembled a preliminary timeline, and then asked for feedback on whether the timeline was acceptable. It is very important that the timeline is carefully examined because it is the criticality safety engineer that is responsible for the majority of the work. Voice any concerns as soon as they are uncovered because it gives management more time to address any issues, which is in everyone's best interest for completing the project. The single largest use of time for this project was the development and quality analysis of the facility model. It should be noted that no results are acceptable for the facility model until after it has been put thru QA. This makes it a high priority to finish as soon as possible. Do not put off either job.

### **IV. Evaluate and choose a computer simulation package to perform the analysis based on validation benchmarks that clearly demonstrate the code chosen will perform as expected;**

The decision was made early on to use MCNP5 because it was felt that it had the capacity to perform the analysis, and it had been accepted by the Quality Assurance program at PNNL. To ensure that MCNP5 could perform as assumed, a series of benchmarks were modeled to prove that it was indeed an appropriate tool for the design. This task goes through the process of validation per the quality control requirements of PNNL.

MCNP5 was used extensively for modeling many aspects of this project. An MCNP5 model was created for each of the following;

- A thorough representation of RPL

- 6 different accident scenarios involving  $^{235}\text{U}$
- 6 different accident scenarios involving  $^{239}\text{Pu}$
- The current setup used for calibrating the  $\text{BF}_3$  Nuclear Criticality Detector(NCD) to a specified dose rate
- The recommended modified calibration setup
- 6 different scenarios for sensitivity analysis

It is necessary then to model a set of accepted, experimentally confirmed, benchmarks that resemble the models created above with the same code package. Modeling these benchmarks in the same code allows experimentally confirmed results to be compared to those received from simulation. Showing that the simulation correctly reproduces the published physically similar benchmark results therefore validates the use of this code for the work being performed.

The benchmarks selected to validate the models described above were all taken from the Nuclear Energy Agency International Handbook of Evaluated Criticality Safety Benchmark Experiments, September 2008 edition (IHECSBE). The benchmarks in the IHECSBE are an extensive set of criticality experiments that have been thoroughly peer reviewed and modeled in a variety of computer codes. The physical details of each experiment, as well as their inherent uncertainty, are listed for each benchmark. Experimental results are given with how they were obtained, detectors/type, location, etc. Then these experiments are reproduced using a common software simulation package. Results from the simulations are included in the write up of the benchmarks and generally an accompanying input file is also listed. Such an extensive degree of detail in these benchmarks allows the user to model the experimental results with a good deal of confidence.

Now it is necessary to discuss how these benchmarks are chosen and how they directly apply to this project. Much of the CAS analysis performed hinges on the overall ability of MCNP5 to correctly model criticality events. More specifically this code must accurately account for fission of  $^{235}\text{U}$ ,  $^{239}\text{Pu}$ , and  $^{252}\text{Cf}$  and the resulting myriad of interactions that the particles may undergo after fission. The following criteria should be used to judge the applicability of a benchmark to what is being modeled:

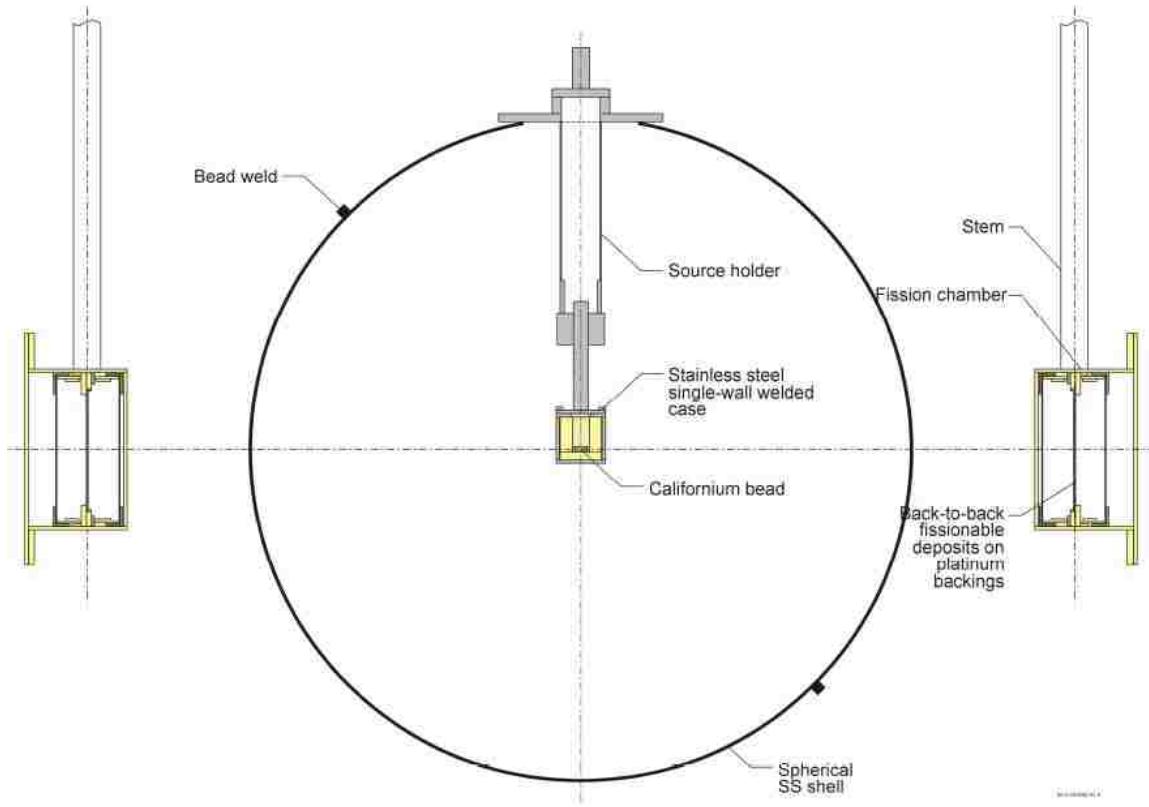
- Reflection
- Energy range of the particle(s) being investigated
- Geometry
- Magnitude of the fluence being investigated
- Material compositions

There is no way to assert that if x number of the above criteria are met then the benchmark is relevant. What can be said is that the more closely the benchmark resembles what is being investigated, the easier it will be to argue that it is relevant.

A set of evaluated benchmarks was selected from the fundamental physics section of the IHECSBE. This set of experiments is designated in the handbook as FUND-NIST-CF-MULT-FISSION-001 (Kim, 1995). These experiments were performed from 1989-1990 at the National Institute of Standards and Technology facility in Gaithersburg, Maryland. This research was performed using a spherical stainless steel container and fission chambers to investigate discrepancies in neutron transport being observed in subcritical assemblies. A lightly encapsulated  $^{252}\text{Cf}$  neutron source was placed at the center of the spherical shell of Stainless steel. Absolute fission rates of  $^{235}\text{U}$ ,  $^{239}\text{Pu}$ ,  $^{238}\text{U}$ , and  $^{237}\text{Np}$  deposits in fission chambers positioned outside the spherical container were measured. The measurements were performed for spherical containers of three different diameters;

3-in., 4-in. and 5-in., with and without water in the spherical container. So it is clear that these experiments thoroughly investigate fission in all of the isotopes used in the CAS models. To replicate the results of the benchmarks, MCNP must track particles through several materials before a normalized fission rate is calculated. It is asserted that if the model created in MCNP5 can accurately replicate these experimental results, then MCNP5 is valid for use in this analysis for the design of a CAS.

It was selected to use 3-in., 4-in. and 5-in spheres filled with water and the same set repeated for the sphere filled with air. Absolute fission rates were obtained for all four isotopes listed above, but only the  $^{235}\text{U}$  and the  $^{239}\text{Pu}$  results are relevant to these models and hence the validation. Each case was modeled with the same version of MCNP5 used for the CAS analysis. A diagram of the general setup for the NIST experiments is shown in Figure 4.



**Figure 4. Experimental setup for the NIST Sphere Benchmarks**

The Spherical Stainless Steel Shell had a diameter of 3, 4, or 5 inches. The detectors remained in the same location for both the 3- and 4-inch Shells –distance from the source was unchanged. In the 5-inch experiments, to facilitate the increase in radius of the shell, the detectors had to be moved 0.75 inches outward. To keep the source at mid-plane with the fission chambers for each shell size, the source holder was either lengthened or shortened accordingly. For the water-filled experiments, the sphere shown above was completely filled with room temperature water. These are the only geometric parameters altered for the experiments.

Table 1 gives the experimental results for the normalized fission rates in barns, as well as the associated relative error. MCNP5 will output a variety of cross section values including single group effective fission cross-sections in barns. That cross-section value multiplied by the fluence striking the fission detector yields the benchmark designated Fission Rate in barns shown in Table 1. Further details on how the Fission Rate was calculated can be found in (Kim, 1995).

The implications of having data for both water-and air-filled spheres are important to note. It is imperative for proving validity that the code is able to accurately account for the scattering and fission of neutrons. Demonstrating that MCNP5 can track neutrons through a strong scattering medium such as water, for all the isotopes involved in this analysis proves the code will perform as needed. The air-filled sphere data is important because the spectrum of the neutrons is much harder than that of the water-filled experiments. Showing that MCNP5 can track and account for fission of both thermal and fast neutrons is crucial to the dependability of the CAS analysis.

**Table 1. Experimental normalized fission rates for  $^{235}\text{U}$  and  $^{239}\text{Pu}$**

<b>Isotope</b>	<b>Condition</b>	<b>Sphere</b>	<b>Fission Rate (barns)</b>	<b>Relative Error (%)</b>
<b>U-235</b>	dry	3-inch	1.278	1.6
	dry	4-inch	1.279	1.6
	dry	5-inch	No Results	
	wet	3-inch	19.6	1.7
	wet	4-inch	45.7	1.7
	wet	5-inch	72.2	1.7
<b>Pu-239</b>	dry	3-inch	1.916	1.5
	dry	4-inch	1.924	1.5
	dry	5-inch	No Results	
	wet	3-inch	36.7	1.5
	wet	4-inch	82.3	1.5
	wet	5-inch	125.5	1.5

Table 2 shows the results found from modeling the experiment in MCNP5 and the percent that this computational result differs from the experimental value.

**Table 2. MCNP5 Computational results with comparison to experimental results**

Isotope	Condition	Sphere	Fission Rate ( barns)	MCNP5 Results	Variance from Experimental (%)
<b>U-235</b>	dry	3-inch	1.278	1.280	0.186
	dry	4-inch	1.279	1.281	0.175
	wet	3-inch	19.6	20.237	3.250
	wet	4-inch	45.7	46.245	1.194
	wet	5-inch	72.2	72.536	0.465
<b>Pu-239</b>	dry	3-inch	1.916	1.850	-3.457
	dry	4-inch	1.924	1.847	-4.027
	wet	3-inch	36.7	37.339	1.742
	wet	4-inch	82.3	81.753	-0.664
	wet	5-inch	125.5	124.669	-0.662

The requirement at PNNL for dose modeling accuracy is only plus or minus 20 percent of the accepted values. Table 2 clearly shows that MCNP5 exceeds this requirement. Table 2 shows the largest variance is -4.027 percent in the  $^{239}\text{Pu}$  dry 4-inch sphere model. The results obtained with MCNP5 clearly show that MCNP5 can accurately model fission of  $^{235}\text{U}$ ,  $^{252}\text{Cf}$ , and  $^{239}\text{Pu}$ . It is also clear that MCNP5 models neutron transport through strong scattering media substantially well.

## V. Design and model the criticality alarm system for the facility;

### Subtask 1 - Finding the MAC including fluence and spectrum

Table 3 shows the results for the minimum accident scenarios that contained Plutonium. The Uranium accident scenarios were not included because the Plutonium accidents were found to generate fewer neutrons. These results were obtained using MCNP5 with F6 dose tallies. The inputs for all the Plutonium scenarios used to determine the MAC are listed in Appendix F. Looking at Table 3 it makes sense based on the shielding properties of neutrons that a water moderated system shields the most neutrons. Table 3 shows the minimum neutron fluence for RPL, which was found to be 3.94E15 (n/cm<sup>2</sup>-s) for the MAC. This fluence was the result of an optimally moderated bare Plutonium and water sphere. This scenario had the largest portion of gamma-rays contributing to the dose limit. For reference the RPL minimum accident of concern MCNP5 input file is included in Appendix F.

**Table 3. Plutonium minimum accident scenario data**

Accident Scenario for Optimally Moderated 1kg Pu-239 and H <sub>2</sub> O Spheres	Neutron Dose per Source Particle (MeV/g)	Photon Dose per Source Particle (MeV/g)	Total Source Neutrons Required to Reach the MAC
Unreflected	1.34E-08	8.92E-08	3.94E+15
Water Reflected	2.94E-10	8.84E-08	4.90E+15
Iron Reflected	3.86E-09	4.74E-09	5.06E+16

When tracking photons in MCNP5, the user must designate the appropriate cross-sections for both neutrons and for photons. Cross-sections must also be included for photonuclear effects if the physics card does not explicitly disable them. Correctly defining the cross-sections and the physics options are not trivial exercises. Using the

wrong libraries or incorrectly tracking the particles can result in much different answers. Chapter II of the MCNP5 manual goes into greater detail on this matter so refer to it for specific guidance (X-5 Monte Carlo Team, 2003).

It is important to remember that the F6 tally output is normalized to per starting particle. This means that the branching ratios of the fission events taking place are not represented in the tallied quantities. So they must be included to determine the Total Source Neutrons Required to Reach the MAC quantity listed in Table 3. For example, a non-kcode calculation, for californium-252 emulates the fission energy spectrum but it does not account for the average number of neutrons emitted per fission ( $\bar{n}_f$ ). Not including the correct branching information would result in source numbers that were at least a factor of  $\bar{n}_f$  too high, which could invalidate the calculated detector coverage.

Also it is important to remember that MCNP5 does not track delayed photons. It is essential to include the delayed photon contribution because it ultimately lowers the source term needed to reach the minimum dose level. Omitting the delayed fraction is then non-conservative and should be addressed. Depending on how much time is available, burn up calculations can be performed to determine the isotopics as a function of accident history. Then another MCNP5 input can be constructed that tracks only the resultant photon contribution from these delayed products. It was attempted to get this dose contribution for the delayed fraction but the total delayed contribution never amounted to more than roughly 3.5 percent of the total dose contribution. Several engineers felt that 3.5 percent was too small of a delayed fraction to guarantee conservatism. It was advised to assume a delayed dose contribution of 7 percent to be sure. It is unlikely that the delayed photon contribution is that high. Because there was

not great confidence in the numbers found with MCNP5, the decision was made to error on the side of conservatism.

### **Subtask 2 - Identify potential locations for detector placement**

An analysis of the detector placement in RPL was performed using the Criticality Slide Rule (UNCSR) and an assumed minimum detectable dose value. To find the minimum detectable dose value, assumptions had to be made for the following quantities:

1. Average neutron fission energy of 2.1MeV for  $^{239}\text{Pu}$
2. Average value of interceding shielding of 8 inches of concrete
3. Minimum detectable fluence of 1e5 neutrons

Assumption 1 was made because the only fissile material that the MAC contained for RPL was  $^{239}\text{Pu}$ . Assumption 2 was found by looking at the materials between the accident locations and the detectors. The actual shielding values are different for every MAC location but an average value was used to save time.

The final assumption for the minimum detectable fluence was not as straightforward as the first two. At this point in the analysis, detector count rates, efficiency, and spectral dependence were not known for the system. Not knowing these parameters for the detectors to be used in the facility made choosing the minimum detection value difficult. Because no alternative was found a typical value was assumed for a similar detector type found on the General Electric (GE) website for a Reuter-Stokes  $\text{BF}_3$  tube. The GE tube value had a lower detection threshold than the 1e5 fluence chosen for this system but the  $\text{BF}_3$  tubes that were available for this CAS were legacy tubes,

some over 40 years old. To compensate for the age, the decision was made to increase the GE minimum detection value by a factor of 100.

Using Equation 1 and the assumed parameters discussed above, the final equivalent minimum detectable dose was calculated to be 0.028 rad. The resulting dose reduction factor for 8 inches of concrete was 0.70. This yielded a final dose of 0.02 rad at a distance of 200ft. An arc was traced over facility drawings using the correctly scaled distance for each MAC. Figure 5 and Figure 6 show the arcs for the basement and first floors of RPL, respectively.



**Figure 5. 0.02 rad arcs for the outlying MAC's in the basement of RPL**



**Figure 6. 0.02 rad arcs for the outlying MAC's in the first floor of RPL**

The green arcs are the assumed minimum detectable distances for the specified parameters. The red dots are the MAC locations that correspond to the arcs. The highlighted areas represent the greatest number of arc unions on that floor. The most outlying MAC locations were chosen because they represent the most challenging detection locations. Comparing Figures 5 and 6 to Figures 7 and 8 shows how good of an approximation the Criticality Slide Rule provides. The actual detector locations for the basement are very near the highlighted areas. The first floor is slightly less accurate but the majority of the actual detector locations are within a small distance of highlighted

area. It can be concluded from Figures 5 and 6 that the assumed minimum detectable distance was slightly conservative, but still relatively accurate for predicting the detector coverage in the facility.

### **Subtask 3 - Modeling the facility**

#### a. Assumptions/omissions/simplifications

All of the assumptions made for the CAS design of RPL are given in Appendix E. One major assumption for the RPL facility model was to standardize the fill material for the different spaces in the building. As mentioned in the Design Methodology section to be conservative, the material located inside of the facility must be included in the model. The method used for the RPL project was to make fill approximations based on facility inspections. The following classifications were made based on the average contents of the spaces in RPL, *Empty Rooms*, *Full Office*, *Full Laboratory*, *Half Full Office* and *Half Full Laboratory*. The contents of each classification are given in subtask c. These fill definitions were used to characterize the spaces within the facility.

To make the application of these fill definitions easier, the items located in the requisite space, i.e., desks, glove boxes, bookshelves, are homogenized for material definition. What this means is that the volumes of the corresponding items are conserved, but the items do not retain their geometric shape. The corresponding number densities for each item desks, glove boxes, bookshelves, etc., are all found independently and then added together to make the final appropriate room fill definitions.

## b. Dimensions

Figures 7, 8, and 9 are floor layouts for RPL generated with the program Vised mentioned earlier. The red dots represent where each MAC was placed for the simulations. The green squares represent the existing detectors. Figure 9 shows the 2<sup>nd</sup> floor of RPL. There is only one laboratory on that level and the rest of the space in the northwest corner is taken up by offices. On the east side of that same figure is the top of High Level Radiochemistry Facility (HLRF). At that altitude HLRF is only open space and structural material.

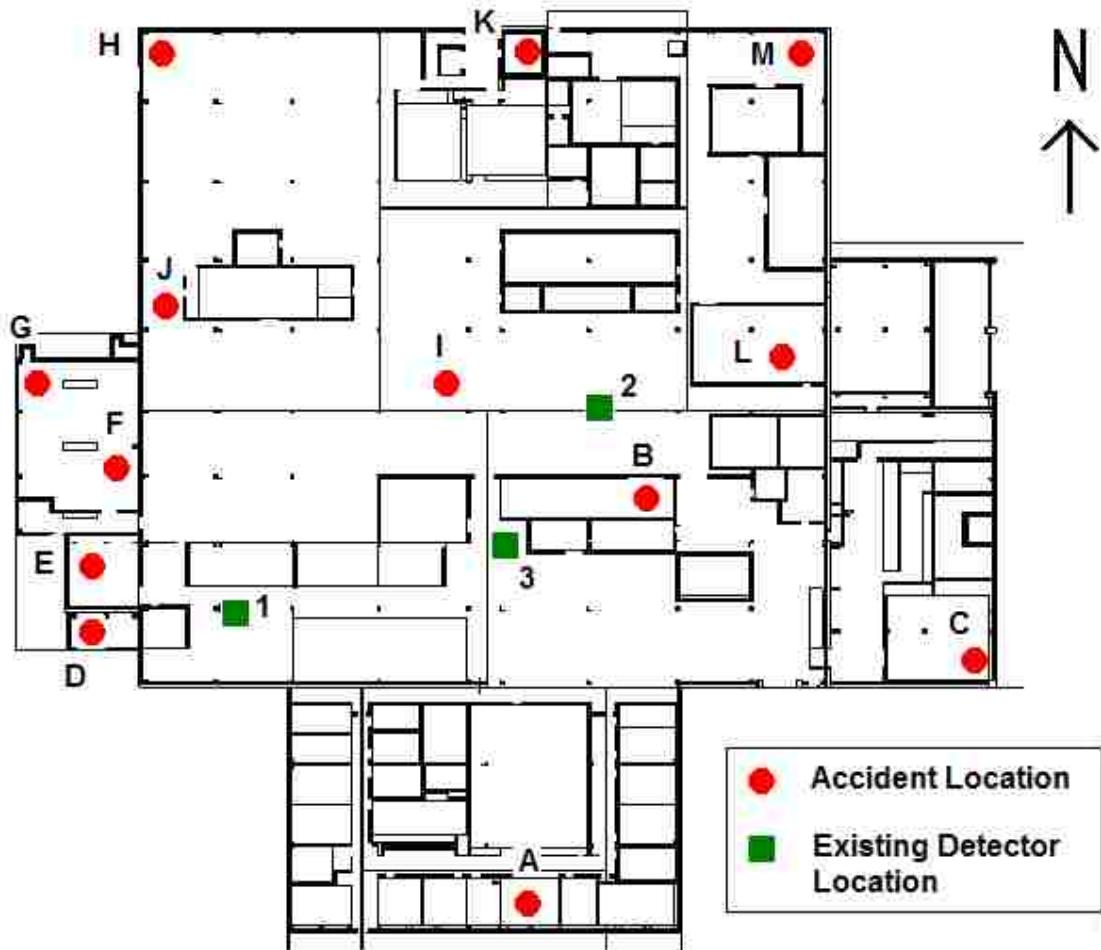


Figure 7. RPL Basement shown with modeled accident locations and the existing detector placement

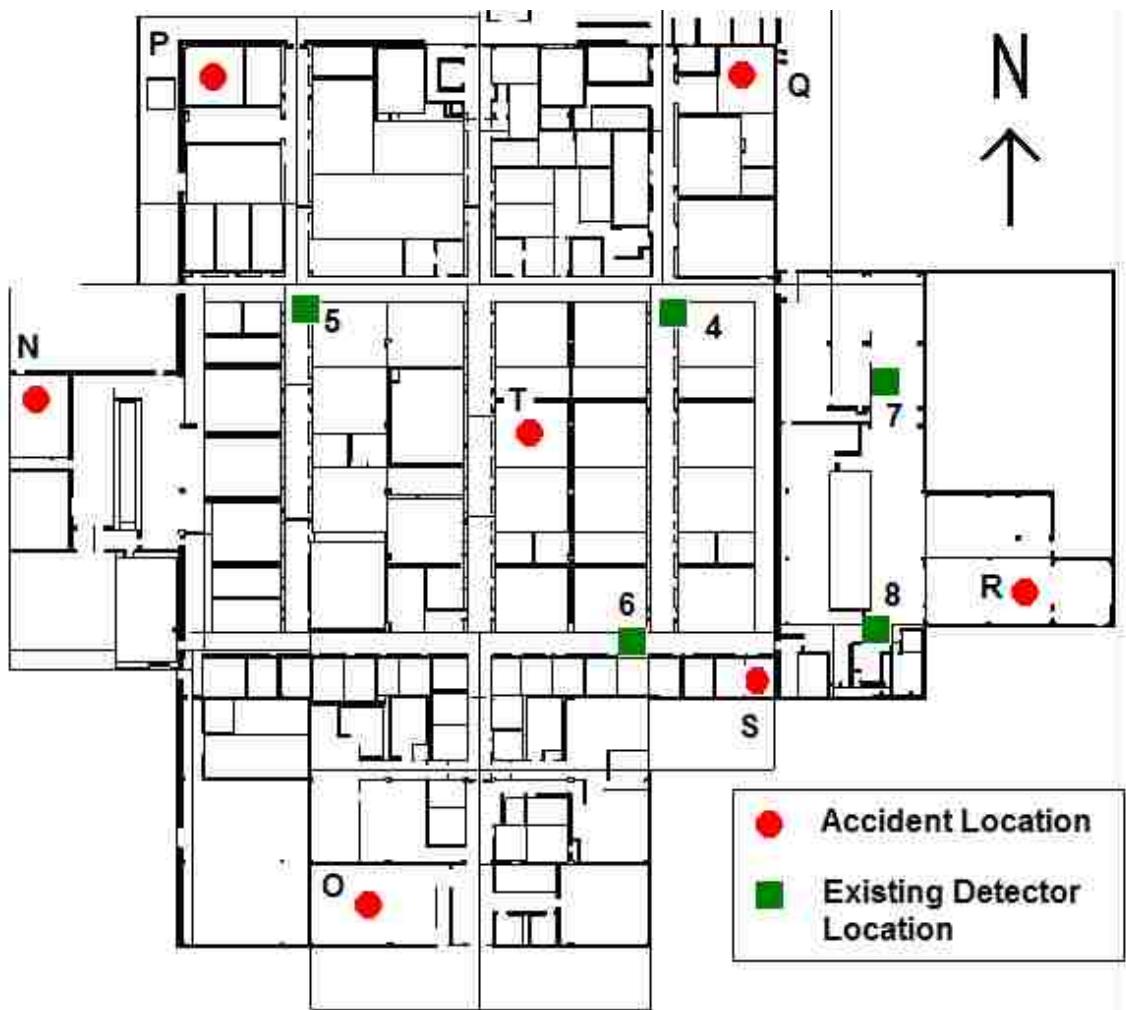
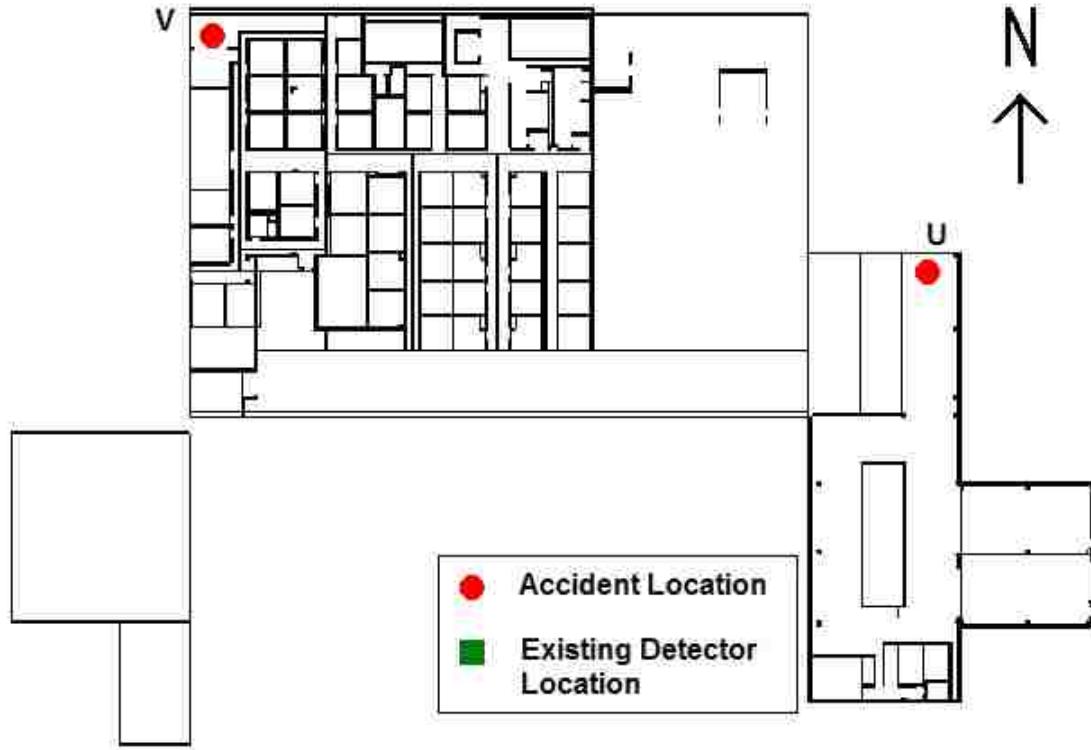


Figure 8. RPL First floor shown with modeled accident locations and the existing detector placement



**Figure 9. RPL Second floor layout**

#### *Facility Description*

Building 325 houses the Radiochemical Processing Laboratory (RPL). It is located in the 300 Area of the Hanford Site in Washington State. The building is used to conduct radiochemical research. RPL contains laboratories and other facilities designed for work with non-radioactive materials, microgram-to-kilogram quantities of fissionable materials, and up to mega-curie quantities of other radionuclides. It is a Class 2 nuclear facility.

The RPL consists of a central portion, a south (front) wing, east and west wings. The central portion of the building contains over 100 laboratories and offices on three floors. The second floor and basement contain mechanical areas such as supply fans, steam lines, etc. The south wing (two floors) contains offices, a conference room, a

machine shop, a lunchroom, and rest rooms. The east wing (one floor) houses the high-level radiochemistry facility (HLRF), truck lock, and manipulator repair area. The west wing (one floor) houses the shielded analytical laboratory (SAL).

### c. Materials Used in Computational Models

A note of caution: it was not determined until late in the analysis that the cinderblock walls of RPL were not hollow. During a QA mandated facility walkdown, it was discovered that the cinderblock walls were actually back-filled with concrete. Because this finding increases the amount of intervening material in the building, the models had to be updated and restarted. Fortunately the mistake was found early enough to not adversely impact the schedule.

#### *Empty Rooms*

Any room found to be “empty” was filled with air. The chemical composition of air is found in Appendix C. “Empty” was defined in the following way. Hallways were considered empty, including entryways and any space that looked to be wide open. Rooms void of furniture were likewise modeled as empty. Laboratories with empty cabinets built into the sides were modeled as empty. Bathrooms were modeled as empty.

#### *Full Office*

Offices that were fully functional, filled with a desk, full bookshelves, file cabinets, etc., were modeled as “full offices.” The justification and calculation of the material composition of a “full office” is provided in Appendix C. The office material

mixture was based on the dimensions of room 113 in the RPL. This room has dimensions of 350cm by 313.7cm by 442cm. It was assumed that the “typical” full office contained three full bookshelves, one full desk, and one full file cabinet. The measured dimensions of a typical bookshelf are 208.3cm by 91.5cm by 30.5cm. The measured dimensions of a typical file cabinet are 152.4cm by 38.1cm by 66cm. The desk was modeled as three file drawers with dimensions 91.5cm by 38.1cm by 66cm. It was assumed that all the bookshelves and file drawers (cabinets included) were full of paper. According to (Reppond, 1977), wood has a material composition of 44.44 weight percent carbon, 6.22% hydrogen, and 49.34% oxygen with an overall density of  $1.0 \text{ g/cm}^3$ . The density assumed for the wood is intentionally high to ensure that even water-logged wood is accounted for. Appendix C provides the calculations for the “full-office” homogeneous material. The “half-filled office” was assumed to have one half the material in the room.

### *Full Laboratory*

Laboratories were judged, upon personal inspection, to be “empty,” “full,” or “sparse.” The justification and calculation of the material composition of a “full laboratory” is provided in Appendix C. The laboratory material mixture was based on the dimensions of the room 312 in the RPL. This room has dimensions of 802.64 cm by 601.98 cm by 441.96 cm. There is also a wall section that cuts into the total volume of the room with dimensions 220.98 cm by 60.96 cm by 441.96 cm. It was assumed that the “typical” full laboratory contained four full bookshelves, four full file cabinets, and one glove box with six lead bricks. To represent the various instruments in the room, a 2-cm

thick sheet of stainless steel and a 2-cm thick sheet of glass was placed in the room. To represent all the tables, cabinets, and desktops, an 16-cm thick sheet of wood was placed in the room. The same dimensions for the desk, bookshelf, and file cabinet that were used in the office calculation were used in this calculation. The glove box has 6 panels of stainless steel and 4 panels of glass. The homogeneous material composition for the “full laboratory” is calculated in Appendix C.

### *Sparse Laboratory*

The justification and calculation of the material composition of a “sparse laboratory” is provided in Appendix C. The same dimensions were used that are described in “full laboratory.” For the sparse laboratory, it is assumed that there is one-half the total amount of material in full laboratory. The homogenous material composition for the “sparse laboratory” is calculated in Appendix C.

### *Additional Materials*

The rest of the materials used in the models were all approximated using existing published information on typical densities and compositions. For example the MCNP5 material card for the structural concrete used to model RPL is shown in Figure 10. The densities listed in Figure 10 are atom fractions with the units of atoms per barn centimeter.

c Calculated Density -2.3g/cc Standard Concrete

m3	1001.66c	-0.022100	\$ H Concrete (Ordinary)
	6000.66c	-0.002484	\$ C
	8016.66c	-0.574930	\$ O
	11023.66c	-0.015208	\$ Na
	12000.66c	-0.001266	\$ Mg
	13027.66c	-0.019953	\$ Al
	14000.60c	-0.304627	\$ Si
	19000.66c	-0.010045	\$ K
	20000.66c	-0.042951	\$ Ca
	26000.55c	-0.006435	\$ Fe

**Figure 10. Standard concrete material definition of 2.3g/cc density.**

d. Detectors

The detectors used in RPL are BF<sub>3</sub> gas proportional detectors, which have active dimensions of 21.6cm by 1.27cm. The Boron is 95% enriched <sup>10</sup>B and the pressure of the gas is approximately 0.70atm. Each BF<sub>3</sub> is surrounded by 5.75cm by 21.6cm Right cylinder of Polyethylene. The calculated efficiency of the detectors was on average 7 percent. These detectors are designed such that when a failure of the tube occurs, it causes an “alarm” signal. This failed alarm mode is important when the accident scenarios are maximized to determine the 12 rad boundary; another regulatory concern out of the scope of this document.

e. Source

To model the MAC discussed above for RPL, a variety of MCNP5 features were used. The SDEF card was used with the coefficients corresponding to a Watt fission spectrum for thermal fission of <sup>239</sup>Pu. To get the appropriate geometric distribution, the source was smeared isotropically throughout a sphere that contained the correct volume of water. Depending upon the location of the accident in the building, the number of

particles that were needed to get acceptable statistics varied considerably. The smallest number was only  $10^5$  but the largest number was  $10^{10}$ .

#### f. Tallies

The only technically useful information that is warranted here is to show how the F2 surface flux approximation tally differed from the F4 cell weighted flux tally. Otherwise the tallies are thoroughly discussed in the MCNP5 manual (X-5 Monte Carlo Team, 2005).

It was found that the F2 tally generally over reported the surface flux for cylindrical and spherical tally surfaces more than it did for planar surfaces. How much the F2 tally over reported the flux varied from almost none to as much as 10 percent. Whether the F2 tally is over reporting fluences or the F4 tally is under reporting is not known. To maintain conservatism, the decision was made to use only the F4 cell tallies because there is no large angle approximation used in its computation, and it reported the lowest fluences of the two tallies.

#### g. Accident Locations

All that must be done is to prove that the alarm system can see an accident anywhere in the facility, plausible or not. So enough accident locations must be selected to show the total facility coverage. Generally all the corners, all of the heavily shielded areas, and all of the hot cells should have accidents modeled there. To show complete coverage for RPL, a total of 24 accident locations were chosen. The number of accident locations chosen to prove coverage is dependent on the size of the facility and the

available computational capability. The 24 accident locations chosen for RPL represent all of the most difficult to detect areas for the CAS. Intuition should be used in the determination of these locations. Areas with large amounts of intervening shielding and places that are the furthest from the detectors will commonly be the hardest to see.

Figures 7, 8, and 9 show the modeled accident locations for RPL.

#### **Subtask 4 - Find count rates for the criticality detectors for known conditions**

The ratio of particles that result in a count is the actual efficiency of the detector. It makes little difference whether the efficiency is good or bad; what matters is that the efficiency is known, and known with confidence. PNNL operates a calibration lab where all of the NCD are routinely recalibrated and checked for problems. Their procedure for NCD calibration utilizes a neutron counting well with a  $^{252}\text{Cf}$  neutron source placed in a motorized elevator. More importantly their procedure uses a set of three  $\text{BF}_3$  tubes that were sent to the National Institute of Standards and Technology (NIST), where count rates for each tube were found at known dose rates with a high degree of certainty.

The NIST calibrated  $\text{BF}_3$  tubes are used to find an elevation for the source in the well that yields a count rate that corresponds to the known dose rate. The NCD to be calibrated is then placed in the well, and its count rate obtained. If this count rate is not within 10 percent of the golden count rate, the gain or the dwell time is changed until it is. The count rate data for each NCD is recorded and plotted over time to show any underlying trends and how the tubes are progressing over time. It was found that the average count rate for all three golden  $\text{BF}_3$  tubes was 563 counts per second at a distance of 1.61 meters from the source at 9:15am of March 3<sup>rd</sup> 2009. This information is used to recreate the calibration setup in MCNP5 in subtask 5 so that the DCTE can be found.

## **Subtask 5 - Modeling the Calibration/Counting Setup to find the Detector Cell Tally Efficiencies**

The data found in subtask 4 was used to create an accurate model of the calibration setup so that the DCTE could be found. Table 4 shows decay corrected activity data for the  $^{252}\text{Cf}$  NCD calibration source that was used in the model.

The neutron source was modeled using the spontaneous fission spectrum of  $^{252}\text{Cf}$  provided by MCNP5 and the decay corrected activity for the simulated source weight. In MCNP5, the source weight is used to scale the tallied results to a real world yield. The same geometric model and F4 cell flux tally of the NCD used in the facility model was placed in the calibration mock-up.

**Table 4.  $^{252}\text{Cf}$  calibration source information**

Date	Seconds Elapsed	Activity (Ci)	Activity (Bq)	Neutrons per second
9/27/1995	0.0000E+00	0.6880	2.5456E+10	2.9340E+09
3/4/2008	3.9243E+08	0.0264	9.7840E+08	1.1277E+08
1/19/2009	4.2016E+08	0.0210	7.7713E+08	8.9569E+07
3/9/2009	424396800	0.0203	7.5028E+08	8.6475E+07

The F4 tally indicated that 1440 particles strike the high density polyurethane (HDPE) collar per second for the identical calibration scenario described in task 4. Dividing the golden count rate by this tallied fluence gives a DCTE of 0.39 percent of the simulated particles entering the HDPE collar result in a real world count.

### **Subtask 6 - Adjust the value for the detector minimum trip setting**

The count rate found by NIST for the set of three BF<sub>3</sub> tubes corresponds to a dose rate in free air of 80mrem/hr. This was the dose rate and ultimately the count rate used for the trip setting of the NCD in RPL. To the best of the knowledge of the engineers at PNNL, there has never been a false alarm in the facility. This fact was important to note because the facility has been in operation for over 50 years. This established track record was a great help for basing the trip setting high enough to avoid false alarms. It is unlikely to ever see a natural or cosmic background source that would approach even ten percent of the required 563 counts per second alarm setting. What may be plausible is that man-made sources could potentially reach this trip setting. To avoid potential man-made triggered false alarms, every effort was made to not decrease the trip setting.

Each facility will present its own challenges but it is this balance between detection and false alarms that is the most likely to cause problems for the engineer. RPL has a large amount of concrete, both regular and Barytic. RPL also has dozens of heavily shielded hot cells spread throughout the building. All of this material adds to the challenge of detecting an accident in any location. With diligence, effective coverage can be obtained with trip settings that are high enough to avoid almost all false alarms.

### **Subtask 7 - Verify that adequate coverage has been obtained at the new minimum trip setting**

Once the initial accident modeling runs were completed and the trip setting agreed upon, the rest of the building inputs were run. Table 5 shows the final coverage for RPL. Table 6 shows the room locations of the accidents. These are the same accidents shown on the facility models in Figure 7, Figure 8, and Figure 9. Dividing the trip setting listed

in subtask 5 of 563 counts per second by the DCTE found in subtask 4 of 0.390 yields the computational equivalent of an alarm. Therefore the minimum F4 tally value that represents an alarm is 1440 particles. It can be seen in Table 8 that all the reported values are greater than the 1440 particles needed to trip a detector.

**Table 5. Detector counts for each MAC location in RPL**

Accident Location	Floor	NCD 1	NCD 2	NCD 3	NCD 4	NCD 5	NCD 6	NCD 7	NCD 8
Rm203	1	1.80E+06			2.37E+05	1.14E+05	4.66E+07		
Lunch Room	1	2.83E+07		8.89E+05		6.69E+06		1.10E+06	
Room 327A	1	1.64E+06	6.43E+06		3.33E+05		1.34E+07		
Room 528	1		6.90E+05		2.69E+07		2.21E+05		3.16E+05
HLRF Truck Lock	1				6.87E+06	3.96E+06		2.80E+08	2.12E+08
Room 119	1			4.14E+06	4.42E+06	3.49E+08		1.41E+08	
Room 410	1		1.18E+09	1.17E+08	1.73E+07	1.25E+07			
Mezzanine Lunch Room	B1	6.30E+05	6.11E+05	9.59E+06		9.49E+06			
Room 34	B1	1.52E+07	1.32E+09	8.27E+08		2.29E+07			
Room 40C	B1			3.66E+06		1.26E+07		3.14E+08	1.49E+07
Southwest of Room 23B	B1	3.09E+07	2.21E+05	2.31E+05		2.40E+04			
West of Room 23	B1	9.78E+07	4.74E+06			4.25E+04	3.25E+05		
East side of Room 32	B1	1.06E+08	6.57E+07	8.91E+06			5.68E+06		
Northwest side of Room 32	B1	3.02E+07	2.37E+07	2.63E+06			2.99E+06		
North of Room 63	B1	1.34E+08		1.80E+07	4.07E+05		2.22E+07		
Southwest of Room 57W	B1		2.78E+09	1.10E+09	1.20E+07		1.46E+07		
West of Room 55	B1	3.53E+08	1.37E+08	2.66E+07			8.12E+07		
Room 90	B1		5.58E+05	2.02E+05	2.29E+05		1.96E+05		
Room 48	B1		1.23E+08		9.86E+06			1.28E+06	2.63E+07
North of Room 52	B		1.32E+06		4.88E+06	1.15E+05			1.11E+06
Over Room 603	2				6.72E+08	7.75E+07		7.08E+08	4.35E+09
Over Room 327	2	8.26E+05		2.32E+05	3.41E+06		1.05E+08		

Note: All accident locations had a minimum of 4-detector coverage. B1=First basement floor 1=First floor, 2=Second floor

**Table 6. As modeled MAC locations in RPL**

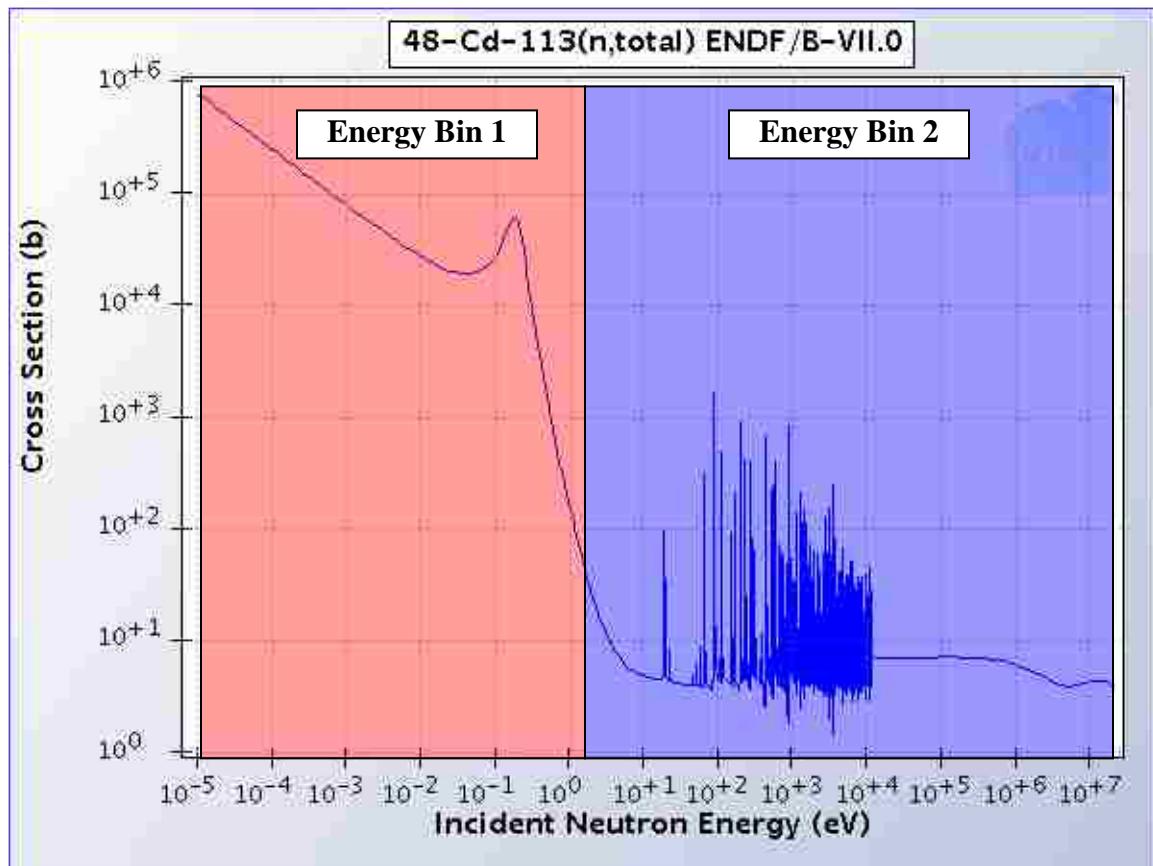
<b>Accident Location</b>	<b>Floor</b>	<b>Position X</b>	<b>Y</b>	<b>Z</b>
(A) Mezzanine Lunch Room	Basement	1334.6	-847.5	202.5
(B) Room 34	Basement	1753.5	680.5	50.0
(C) Room 40C	Basement	2882.0	40.0	50.0
(D) Southwest of Room 23B	Basement	-202.0	171.0	50.0
(E) West of Room 23	Basement	-202.0	474.0	50.0
(F) East side of Room 32	Basement	-92.0	921.0	50.0
(G) Northwest side of Room 32	Basement	-382.0	1141.0	50.0
(H) North of Room 63	Basement	44.5	2577.0	50.0
(I) Southwest of Room 57W	Basement	1144.5	1028.5	50.0
(J) West of Room 55	Basement	44.5	2338.5	50.0
(K) Room 90	Basement	1314.5	2300.5	50.0
(L) Room 48	Basement	2303.5	1228.5	50.0
(M) North of Room 52	Basement	2178.5	2288.5	50.0
(N) Rm203	First Floor	-634.5	1132.5	492.0
(O) Lunch Room	First Floor	541.5	-847.5	492.0
(P) Room 327A	First Floor	40.0	2332.5	492.0
(Q) Room 528	First Floor	2277.5	2340.5	492.0
(R) HLRF Truck Lock	First Floor	3355.5	402.0	492.0
(S) Room 119	First Floor	2261.5	27.5	492.0
(T) Room 410	First Floor	1367.5	960.5	492.0
(U) Over Room 603	Second	44.5	2350.0	884.0
(V) Over Room 327	Second	2875.0	1520.0	1072.0

### **Subtask 8 - Modify the Calibration Procedure**

The energy bins used to characterize the spectrum striking the detectors were first set to the same energy bins as the Hansen-Roach 16 Group Cross-section library (Hansen, 1964). In practice this was far more energy bins than were needed for making adjustments to the calibration procedure. Eventually, it was found that only two energy groups were needed to do the analysis. It may be beneficial in some facilities to include more than two groups, but because there are limited options available for spectrum modification more energy groups may not provide much advantage. The techniques used

for modifying the energy spectrum of neutrons and gammas were discussed in subtask 7 of Design Methodology. The two groups used for RPL were set to represent thermal and everything not thermal. The bin limits were zero to 4eV then from 4eV to 20MeV.

There are only two viable options for altering the energy distribution of a neutron spectrum. Either thermalize them by scattering, or use Cadmium to remove thermal neutrons thereby increasing the ratio of fast neutrons. The bin structure was set to make utilizing these two methods easier and more effective. The Cadmium cutoff is around 0.5eV but there is a broader structure than just a single peak. Figure 11 shows the total neutron absorption cross-section for  $^{113}\text{Cd}$ . The peak is clearly visible but what is more important is the overall structure of the cross section.



**Figure 11. Graph of the total cross-section of  $^{113}\text{Cd}$**

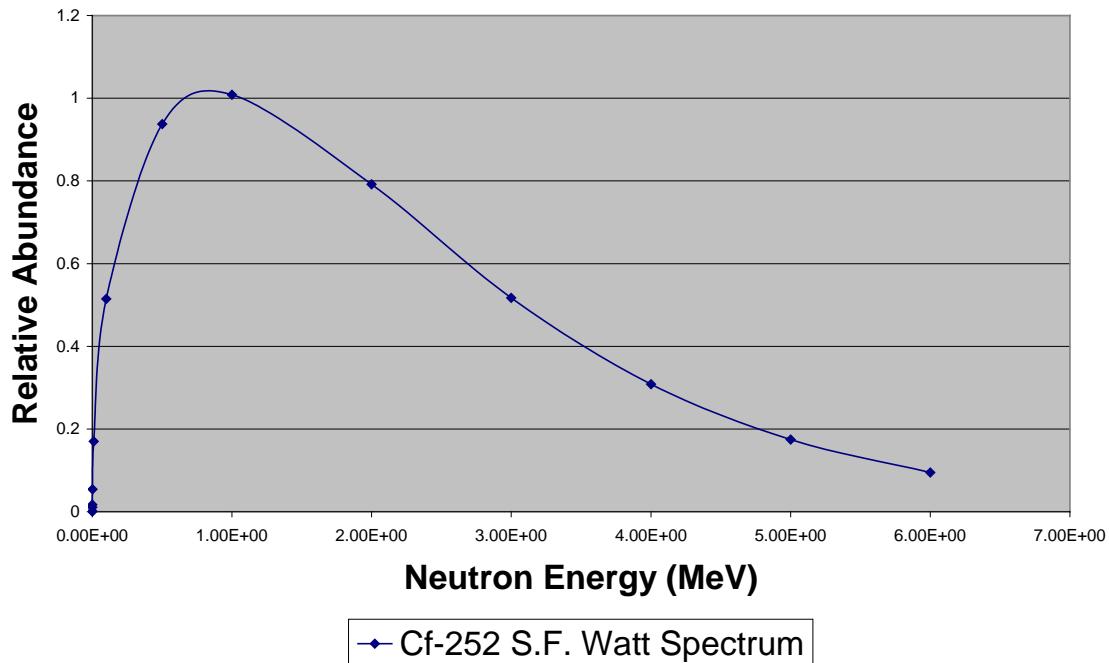
The total cross-section is large (1000's of barns) up to the single digit eV range, which is the main driver for the bin structure used for the detector tallies.

It was found from computer simulation of the MAC that approximately two-thirds of the fluence striking the tally surfaces in the facility model was in the 0 to 4eV range with the remaining third above that. The opposite ratio was found for the existing Nuclear Criticality Detector calibration setup. The same tally in the calibration model showed that roughly one-third of the incident spectrum fell below 4eV and two-thirds above it. To prove the NCD were calibrated correctly, the calibration procedure had to be modified to better resemble the average spectrum of the MAC. The next part of the document goes into detail on how the analysis was performed and the results obtained.

### **Example Nuclear Criticality Detector Calibration Procedure Evaluation**

The current calibration procedure for the NCD at PNNL utilizes a  $^{252}\text{Cf}$  source that generates the neutron energy spectrum seen in Figure 12.

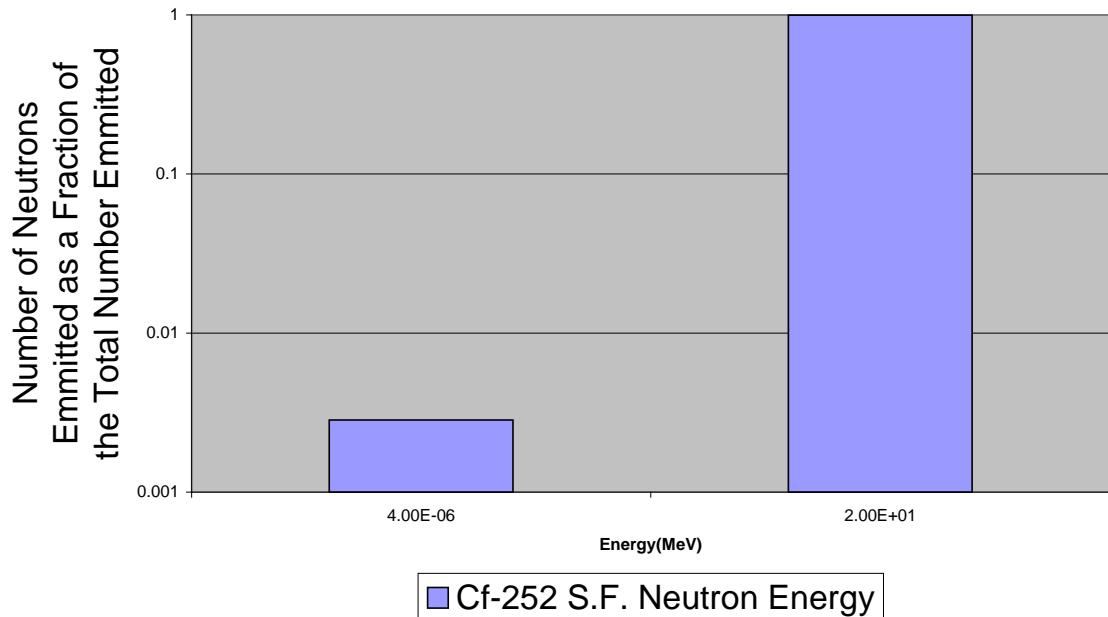
## Cf-252 S.F. Watt Spectrum Coefficients



**Figure 12. Neutron energy spectrum for the spontaneous fission of  $^{252}\text{Cf}$**

Placing the neutron emission spectrum of  $^{252}\text{Cf}$  into the same 0 to 4eV and 4eV to 20MeV energy bins from the facility model yields the graph shown in Figure 13 –Note the graph is in Log Scale.

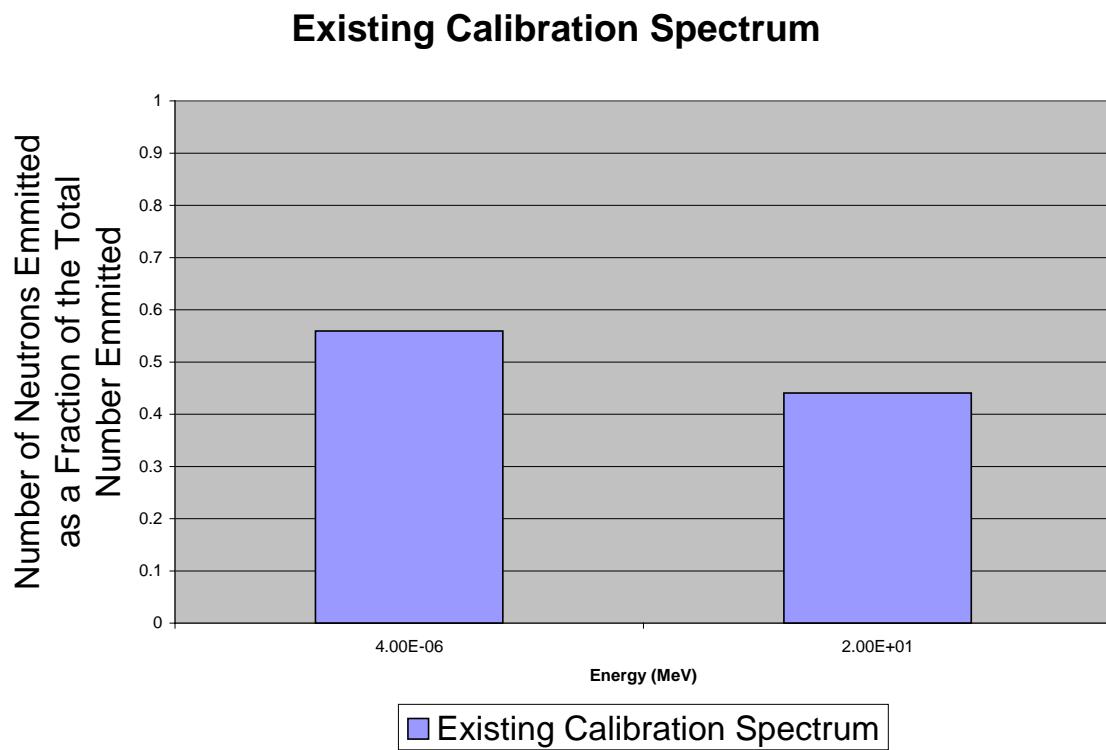
## Energy Distribution of the Nuclear Criticality Detector Calibration Source



**Figure 13. Neutron energy spectrum grouped into 4eV and 20 MeV energy bins for the spontaneous fission of  $^{252}\text{Cf}$  plotted on a log scale**

It is clear from Figure 13 that the spontaneous fission of Cf-252 has almost no thermal energy neutrons.

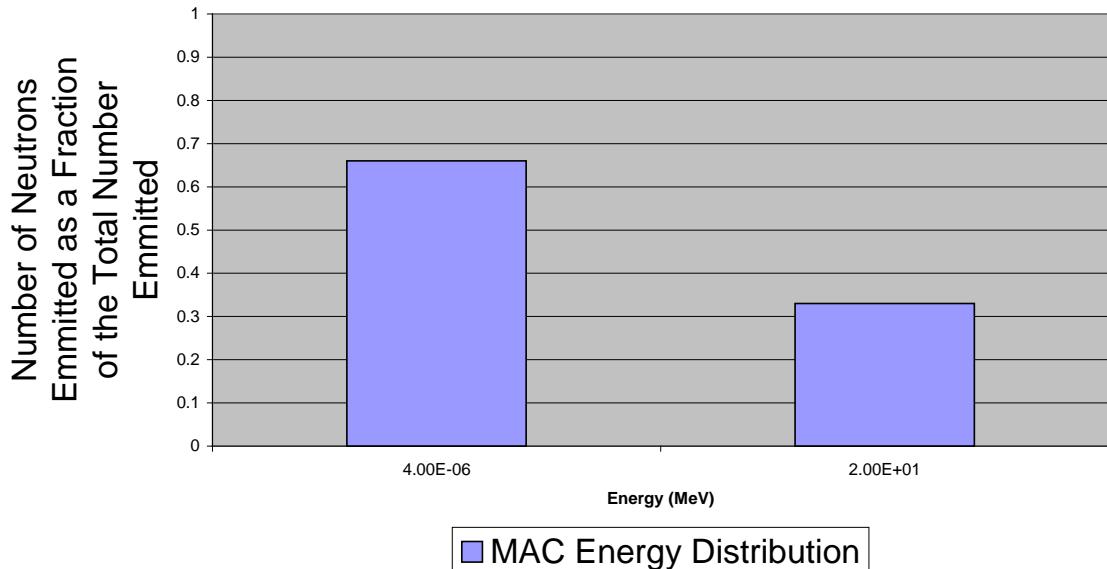
The  $^{252}\text{Cf}$  source shown in Figure 12 and Figure 13 is placed on a motorized elevator in a 10 meter deep counting well. The NCD are placed on top of the well and the source is raised to the desired height for the corresponding activity level. For the current activity of the  $^{252}\text{Cf}$  source, the distance between the elevator and the NCD is approximately 1.60 meters. The fluence that reaches the NCD was found to have the energy distribution shown in Figure 14.



**Figure 14.** Existing calibration spectrum

Using the same energy bins as Figure 13 and Figure 14 for the MAC in RPL generates the graph in Figure 15. It is clear that spontaneous fission spectrum of  $^{252}\text{Cf}$  is considerably thermalized by the materials around the counting wells.

## **Neutron Energy Distribution Incident on the Nuclear Criticality Detector During the Minimum Accident of Concern**

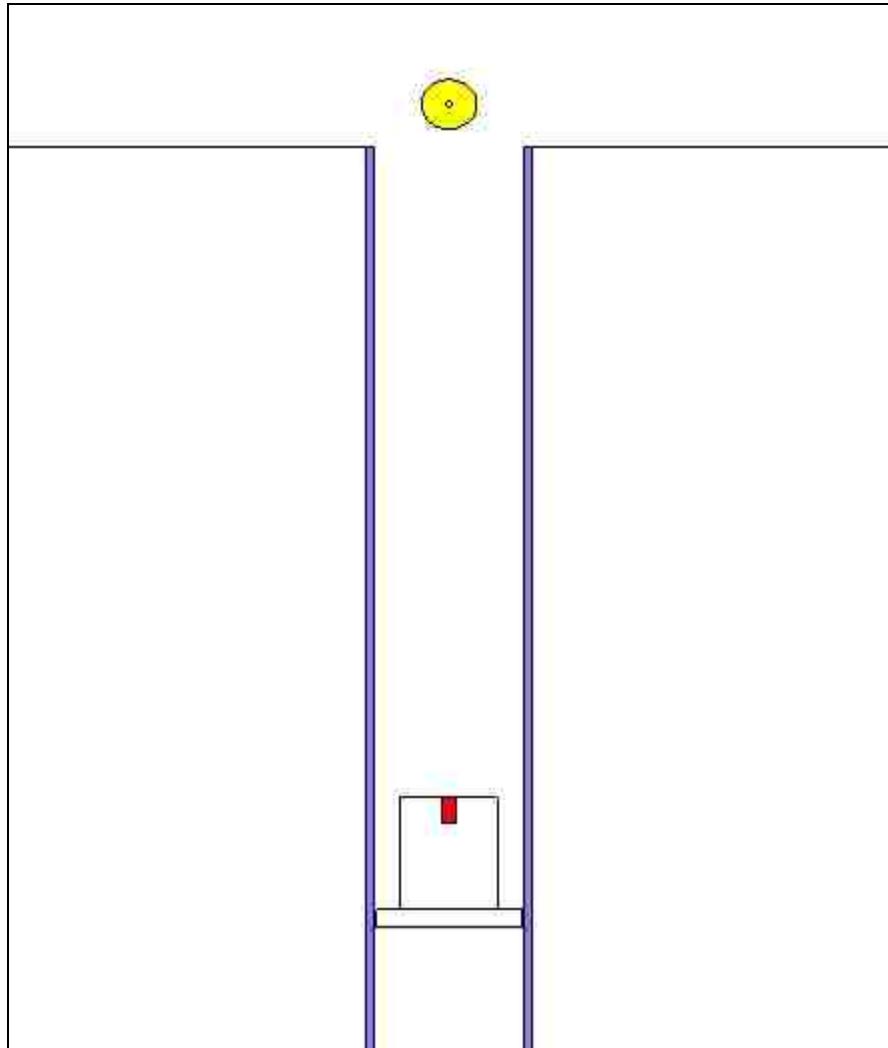


**Figure 15. Average neutron energy spectrum during the Minimum Accident of Concern grouped into 4eV and 20 MeV energy bins**

From Figure 14 and Figure 15, it can be seen that the spectrum used to calibrate the NCD was not the same spectrum the NCD was likely to be exposed to during the MAC; therefore it was necessary to modify how the NCD were calibrated. The existing calibration spectrum had approximately 56 percent of the spectrum below 4eV whereas the MAC spectrum had 66 percent. This discrepancy had to be resolved because if there was spectral dependence for the counting efficiency then the assumed known count rates used in subtask 4 would be incorrect.

To perform the analysis, an MCNP5 model was constructed. The basics of the calibration setup were included and flux tallies were used to find the energy distribution of neutrons striking the detector. Different materials were placed between the source and

the detector until the required energy distribution was obtained. A simple diagram of the calibration setup is shown in Figure 16. The NCD is yellow, the counting well is gray, and the  $^{252}\text{Cf}$  source holder is red. The drawing is to scale.

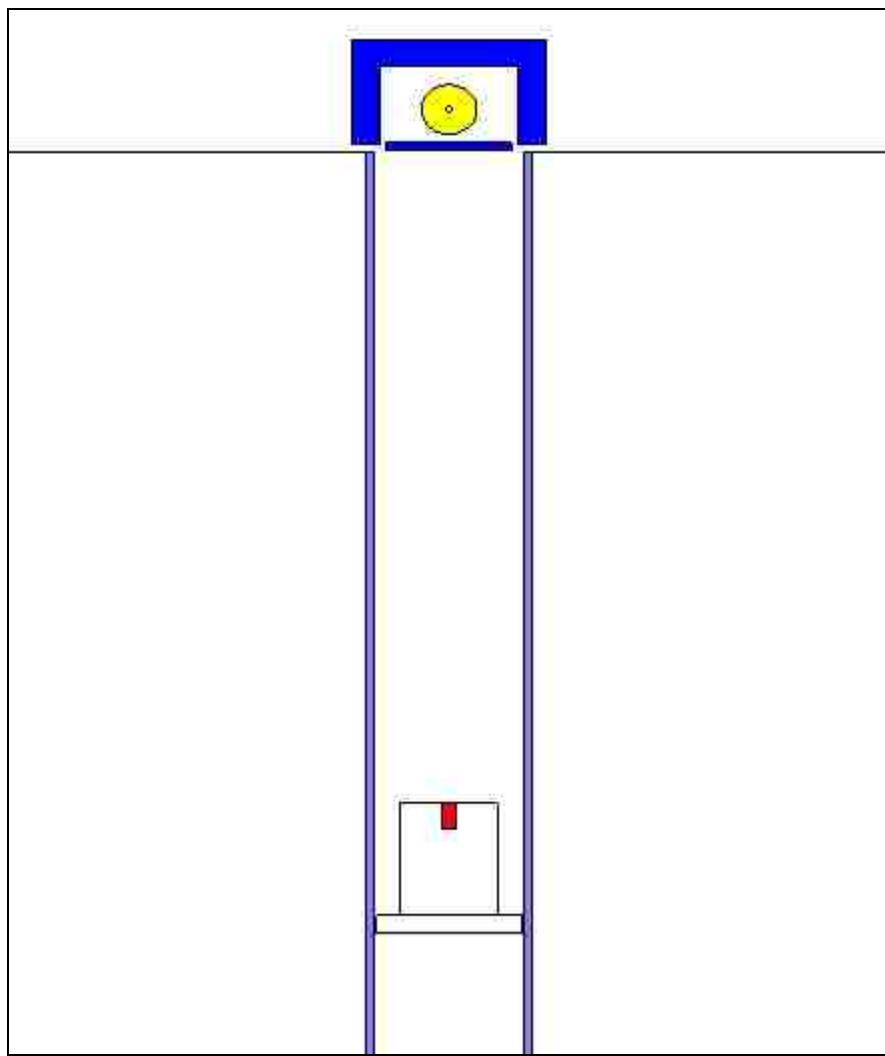


**Figure 16. Existing NCD calibration setup**

The entire well is surrounded by high density concrete. It was found that the following two steps could be inserted into the existing calibration spectrum to more effectively bound the average energy spectrum present during the MAC:

1. Construction and Placement of a 2cm thick, 13cm radius disc of High Density Polyurethane (HDPE) between the Californium Source and the NCD. The location of the plate should be just below the NCD.
2. Construction and placement of a hollow five sided box of HDPE 40cm x 40cm x 24cm around the NCD on top of the counting well. All sides of the box being roughly 6cm thick.

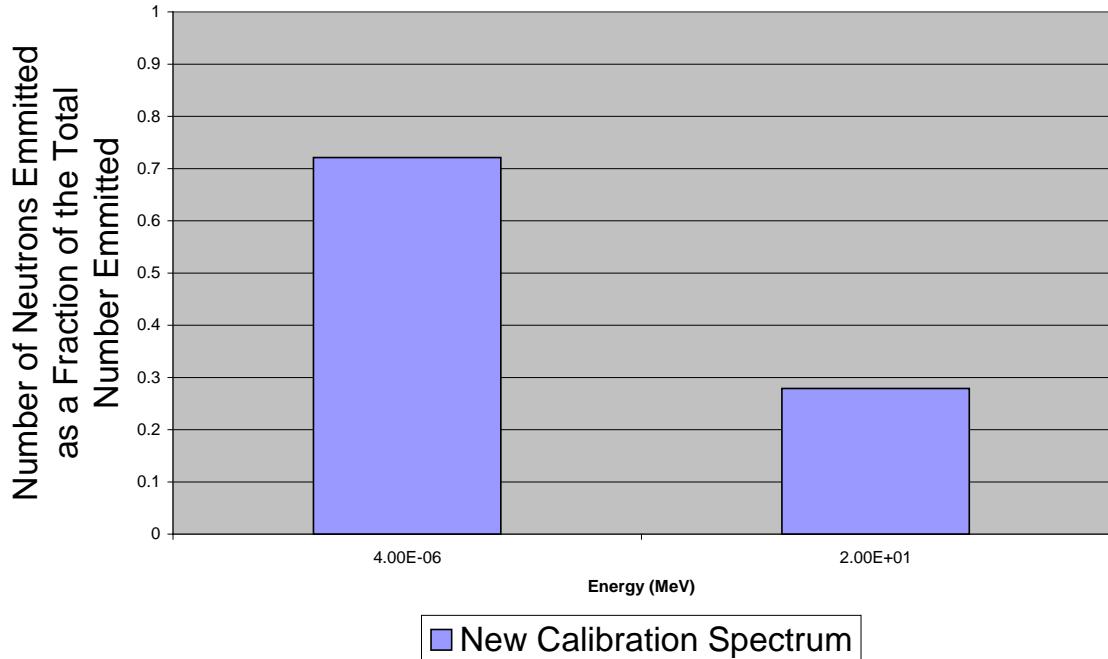
Figure 17 shows what the revised calibration setup will look like.



**Figure 17. Revised NCD calibration setup with the added HDPE**

The blue material is the added HDPE. After the proposed HDPE pieces are implemented, the spectrum hitting the NCD is altered to the distribution shown in Figure 18.

## Calibration Spectrum After Proposed Changes



**Figure 18. Modified calibration spectrum grouped into 4eV and 20 MeV energy bins**

Adding the HDPE to the calibration process creates a spectrum with a slightly larger thermal fraction than both the existing calibration setup and the MAC spectrum. In reality, there is a range of spectrums that are possible in the MAC. Therefore the increase in the thermal fraction to beyond the MAC is done intentionally to more effectively bound the calibration of the NCD. The HDPE slab used to slow down the neutrons also absorbed or reflected away a considerable number of them as well. The box was placed over the well to increase the amount of reflection back toward the NCD. Placing the box in this manner not only made up for what was lost to the HDPE slab but actually increased the fluence striking the detector beyond the existing calibration procedure by an extra 15 percent. Californium neutron sources are very expensive so prolonging their

usable life is very helpful. Table 7 gives a summary of all the values shown in the histograms.

**Table 7. Corresponding Data Used in the Histograms**

Energy Bins (MeV)	Cf-252 Emission Spectrum	MAC Average Spectrum	Old Calibration Spectrum	New Calibration Spectrum
4.00E-06	0.003	0.660	0.559	0.721
2.00E+01	0.997	0.330	0.441	0.279

The suggested changes discussed here only deal with the need to modify the calibration spectrum to better mimic the likely accident conditions. These proposed changes are intended as an addition to the existing calibration procedure, not as a total replacement of existing methods.

### **Subtask 9 - Apply Variance Reduction as needed**

During the modeling portion of the project it was found that the run times needed to obtain usable precision (less than 0.10 error) were very large. For the majority of the MAC locations needed to show complete facility coverage, the run times were upwards of 10 days on dual quad core 3.2GHz workstations. With 24 accident locations selected to prove coverage, it is apparent that if all went correctly it would take a minimum of 240 days to receive results. This amount of time exceeded the schedule of the project. The decision was then made to investigate using variance reduction in MCNP5.

The QA program at PNNL very clearly states that no variance reduction techniques may be used that alter the fundamental physics of the computer simulation. It was attempted to implement reduction strategies that complied with this requirement but

no solution was found that reduced run times to an acceptable level. To mitigate this problem, a compromise was made. Well documented variance reduction techniques could be used provided that standard Monte Carlo runs would be completed in the future to validate the results.

After extensive investigation, it was found through trial and error that implementing the deterministic transport option in MCNP5, DXTRAN, reduced the run times to 4 days plus or minus 2 days depending on the accident location. To initially verify the DXTRAN results were correct, 2 standard Monte Carlo runs were carried out. The first standard run represented the hardest accident location to detect, Room 90, a well-shielded location at the northern edge of the basement. The second run was for the easiest location to detect in the facility, (T) Room 410, a laboratory located in the center of the first floor. In both cases there was very little deviation of the DXTRAN results from standard Monte Carlo. Table 8 shows the results for these two sets of runs.

**Table 8. Comparison of deterministic transport results to standard Monte Carlo results**

Accident Location	Detector 2	Detector 3	Detector 4	Detector 5	Detector 6
(T) Room 410 - Standard	1.18E+09	1.18E+08	1.79E+07	1.34E+07	
(T) Room 410 - DXTRAN	1.18E+09	1.17E+08	1.73E+07	1.25E+07	
100*(Standard - DXTRAN)/ Standard	-0.1	0.7	3.2	6.8	
(K) Room 90 - Standard	5.57E+05	2.03E+05	2.34E+05		1.97E+05
(K) Room 90 - DXTRAN	5.58E+05	2.02E+05	2.29E+05		1.96E+05
100*(Standard - DXTRAN)/ Standard	-0.1	0.2	2.2		0.5

As mentioned earlier, extreme caution must be used when applying these techniques. Even though promising results have been demonstrated for this technique, the final analysis will not accept them. As per QA requirements, the final results will not be established on record until the standard Monte Carlo runs are complete. Techniques that reduce the variance have tremendous use for scoping and preliminary analysis, but are generally not acceptable as final numbers for the project.

#### **Subtask 10 - Perform sensitivity analysis on the final CAS design**

The sensitivity analysis conducted for RPL focused primarily on the effects of overloading the spaces in the facility with material that was twice as dense as the Full Office and Full Laboratory material definitions listed in Appendix C. This fill density was chosen because it represents the uppermost limit of the physical capacity of the spaces. Also the distribution of the super dense spaces was configured in the most challenging manner for accident detection. The spaces in the core of the building were filled with the super dense material and the spaces outside of the accident locations were left empty. Arranging the fill material in this manner represented a situation where the maximum amount of matter is placed between accidents and detectors. This represents the most limiting feasible scenario for the sensitivity analysis. Results for (T) Room 410 and for (K) Room 90 are given in Table 9.

**Table 9. Detector counts for preliminary sensitivity analysis for maximum loading within the facility**

<b>Accident Location</b>	<b>NCD 2</b>	<b>NCD 3</b>	<b>NCD 4</b>	<b>NCD 5</b>	<b>NCD 6</b>	<b>Number Alarming</b>
<b>Room 410</b>	1.18E+09	1.17E+08	1.73E+07	1.25E+07		<b>4</b>
<b>Overloaded Tally</b>	5.83E+08	5.20E+07	2.10E+06	1.39E+06		<b>4</b>
<b>% Lost from Overloading</b>	50	56	88	89		
<b>Room 90</b>	5.58E+05	2.02E+05	2.29E+05		1.96E+05	<b>4</b>
<b>Overloaded Tally</b>	3.71E+05	1.16E+05	1.19E+05		9.67E+04	<b>4</b>
<b>% Lost from Overloading</b>	34	43	48		51	

Again these results were obtained using deterministic transport and are not acceptable in the final report, but these preliminary results indicate that four detector coverage is maintained even at this loading. The standard Monte Carlo runs will provide the final data when they are completed sometime in the 2015 timeframe. It should be noted for the overloaded models, both standard and deterministic based MCNP5 run times increased dramatically.

## **VI. Show the calibration method follows simple and concise methodology for setting the minimum detector trip points;**

Simplifying the calibration method for setting the minimum detector trip points was fairly straightforward. The majority of the analysis needed to set the trip setting was completed after both the average MAC spectrum in the facility had been analyzed and the calibration setup modeled for subtask 4. Because of the methodology used to establish building coverage took into account the conversion from simulated count rate to actual count rate, all that remained was to state what that count rate was.

Given the historical absence of false alarms with the established trip setting for RPL, the decision was made to attempt establishing coverage for the entire building at or above that level. It was shown in Chapter 4 subtask 7 that coverage was established for the entire facility above the historical trip setting. The final revision of the calibration procedure simply removed all extraneous dose conversion wording to arrive at the following definition of the trip setting: “All Nuclear Criticality Detectors for the Radioisotope Production facility will be set to alarm at 563 counts per second.” This is the definition that will be submitted to the DOE to show compliance with their request for a more transparent and verifiable definition of the minimum detector trip setting.

## **VII. Assemble the final report;**

The final design report for the CAS of RPL was drafted in two parts that roughly followed the outline listed under the corresponding heading in Design Methodology. The initial draft contained four sections which were: the Introduction, Design Description, Requirements Documentation, and Methodology. The second draft contained:

- Evaluation and Results
- Conclusions
- References

Each draft was reviewed by a committee, and their comments were all submitted for evaluation of relevance. Because an outline was already provided, only general comments about the specific RPL report will be addressed here.

There is a reason the heading for this section is titled “Assemble the Final Report,” not “Write the Final Report.” In reality there is little writing that goes into the

final design report. What actually goes into the report is primarily tables, figures, diagrams, and references. It is advised to make all graphs, charts, etc., as plain and uncluttered as possible. Nothing seems to annoy management and tech editors more than a busy graphic.

The most challenging aspect of assembling the final report was finding, organizing, and citing all of the required References. The final design report contained over 60 different references, and hard copies had to be obtained for all of them. PNNL procedure required the references to be in the same order in the appendix that they were presented in the body of the text. PNNL document control system is also very strict, which made obtaining the necessary hard copies time consuming. It can not be overstated how important it is to retain all references that are encountered throughout the design phase, regardless of their perceived importance at that time.

## **Chapter 5 – Conclusion**

### **Summary**

A guide for designing a Criticality Alarm System was established. The focus of the guide was on producing a CAS that would meet applicable regulations and supply dependable coverage for personnel. The first half of the document provided an outline for the methodology behind each task and then thoroughly evaluated each task from a technical perspective. The second half of the document demonstrated how to apply this methodology by reviewing the analysis performed on the CAS of the Radiological Processing Laboratory of Richland, Washington. Results from the RPL system were included for each task and subtask. Potential pitfalls that were encountered during the design process were also included to aid the user in avoiding costly mistakes.

### **Future Work**

As technology and standards evolve, the requirements that will be placed on Criticality Alarm Systems will no doubt change, likely only becoming more stringent. To meet any increased constraints, it is likely that more labor and computational time will be needed to complete the design of a CAS. As computational technology advances, more in-depth and detailed analyses can be conducted that could utilize greater precision. Greater modeling detail will instill greater confidence in the results and reliance on established overly conservative methods could potentially be relaxed.

The development of more efficient detectors, as well as more in-depth analysis, would allow the minimum trip settings to be raised thereby increasing the margin for avoiding false alarms.

## **Enhancements**

Several improvements were made to the existing CAS design for RPL:

- Nearly all of the RPL facility was modeled and evaluated
- The number of modeling assumptions used was decreased
- Complete facility detector coverage was proven
- Detector coverage for the MAC was increased from 2 detectors to 4
- Better calibration methods were developed that more effectively bound the average spectrum likely to strike the NCD during the MAC
- The definition of the minimum trip setting was vastly streamlined to meet regulatory findings and to enhance transparency
- Direct dose calculation for the MAC was done, thereby eliminating the need for fluence to dose conversion factors

Each of these improvements increases the reliability of the CAS and streamlines any potential future analysis that may need to be performed. The increased detector coverage opens more areas in the facility where criticality work can be conducted. The increase in the number of detectors that will see the MAC impacts the operations in the building by allowing criticality work to continue even in the event of two separate detector failures. The modification of the calibration procedure enhances the reliability of the CAS by demonstrating that the NCD will more effectively see the energy spectrum of neutrons emitted during the MAC. Changing the definition of the minimum trip setting from a dose value to a simple count rate makes understanding what the CAS is set

to alarm for much easier. Changing the trip setting to a count rate also satisfies regulatory findings. The elimination of the dose conversion factors makes finding the corresponding fluence of the MAC clearer, again enhancing transparency of the overall design methodology.

The combination of all these improvements to the CAS in RPL provides better, more dependable coverage, which will send out prompt warning to personnel in the event of a criticality potentially saving lives of those involved.

## **Definitions**

**Criticality Alarm System (CAS):** The combination of nuclear criticality detectors, audible alarms, and comparator panel that is responsible for the prompt detection and immediate audible alarm issuance to personnel.

**Detector Cell Tally Efficiency (DCTE):** The ratio of the number of particles that strike the detector cell equivalent being tallied that will ultimately result in a count, this is a computational quantity.

**Detector Efficiency:** The ratio of the number of particles entering the active detector volume which result in a count, which is experimentally determined.

**Detector Surface Tally Efficiency (DSTE):** The ratio of the number of particles that strike the tally surface that will ultimately result in a count, this is a computational quantity.

**High Density Polyurethane (HDPE):** A polymer with the chemical composition of CH<sub>2</sub> with an assumed density of .933(g/cc).

**High Level Radiation Facility (HLRF):** An annex of building 325 in the 300 area of the Hanford, Washington Department of Energy site that contains large shielded hot cells for work with fissile material.

**Monte Carlo N-Particle Transport Code Version 5 (MCNP5):** A Monte Carlo based neutronics code developed by Los Alamos National Laboratories and maintained by the Radiation Safety Information Computational Center.

**Nuclear Criticality Detector (NCD):** The instrument used for the detection of particles resultant from fission.

**Radioisotope Production Laboratory (RPL):** Designated as building 325 in the 300 area of the Hanford, Washington Department of Energy site used for work conducted on fissile material, a Class 2 hazard facility.

**Shielded Analytical Laboratory (SAL):** An annex of building 325 in the 300 area of the Hanford, Washington Department of Energy site that contains shielded hot cells for work with fissile material.

## Appendix A: RPL Building Schematics with Accident and Detector Locations

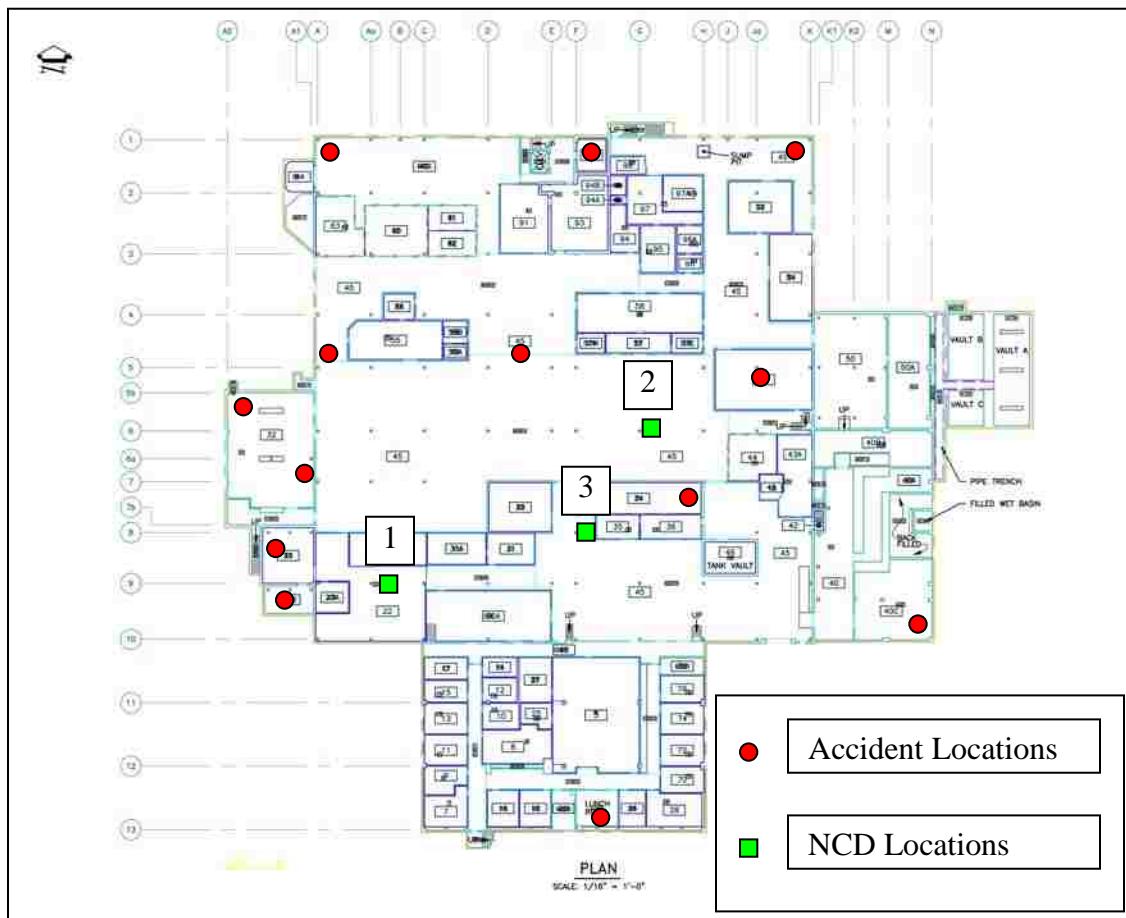
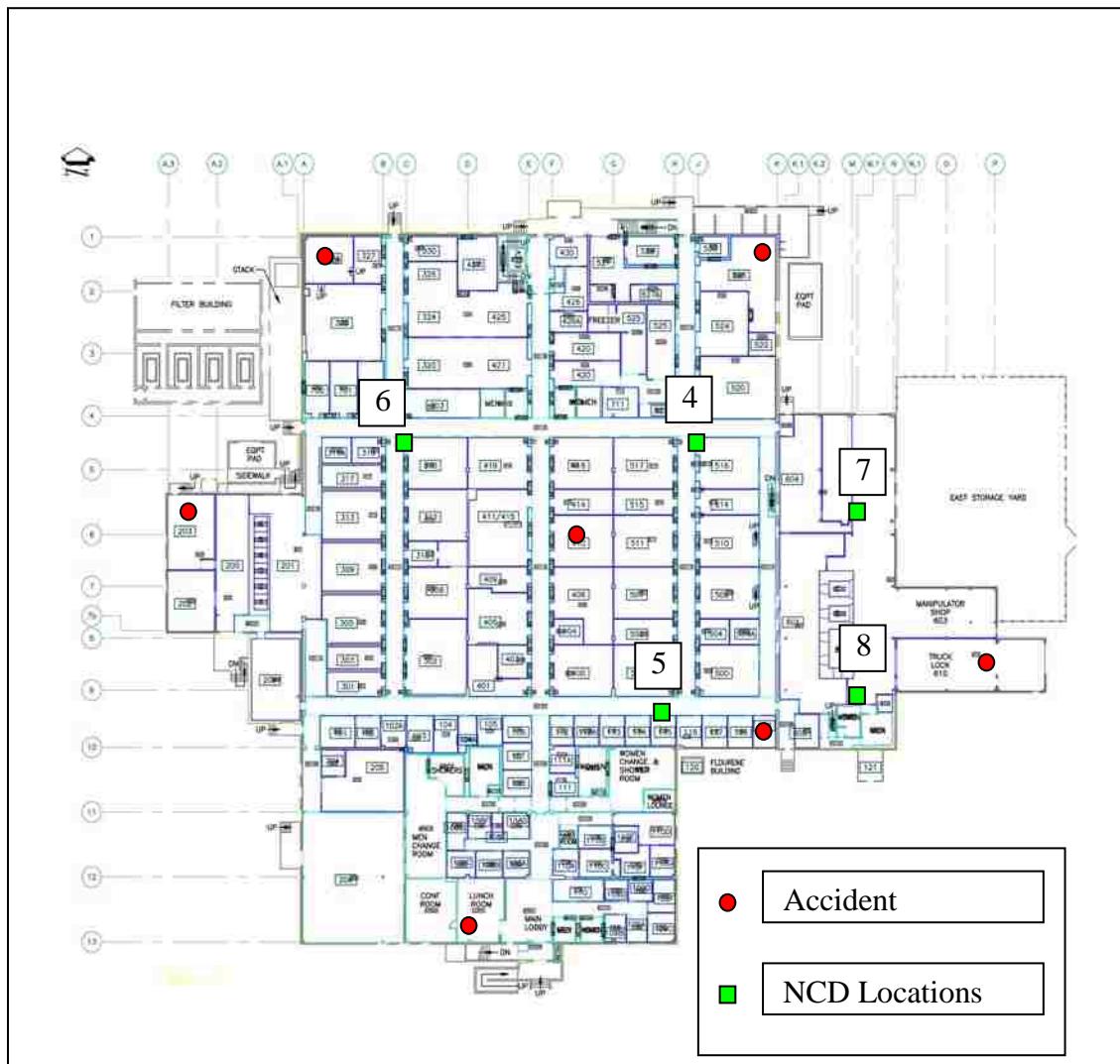
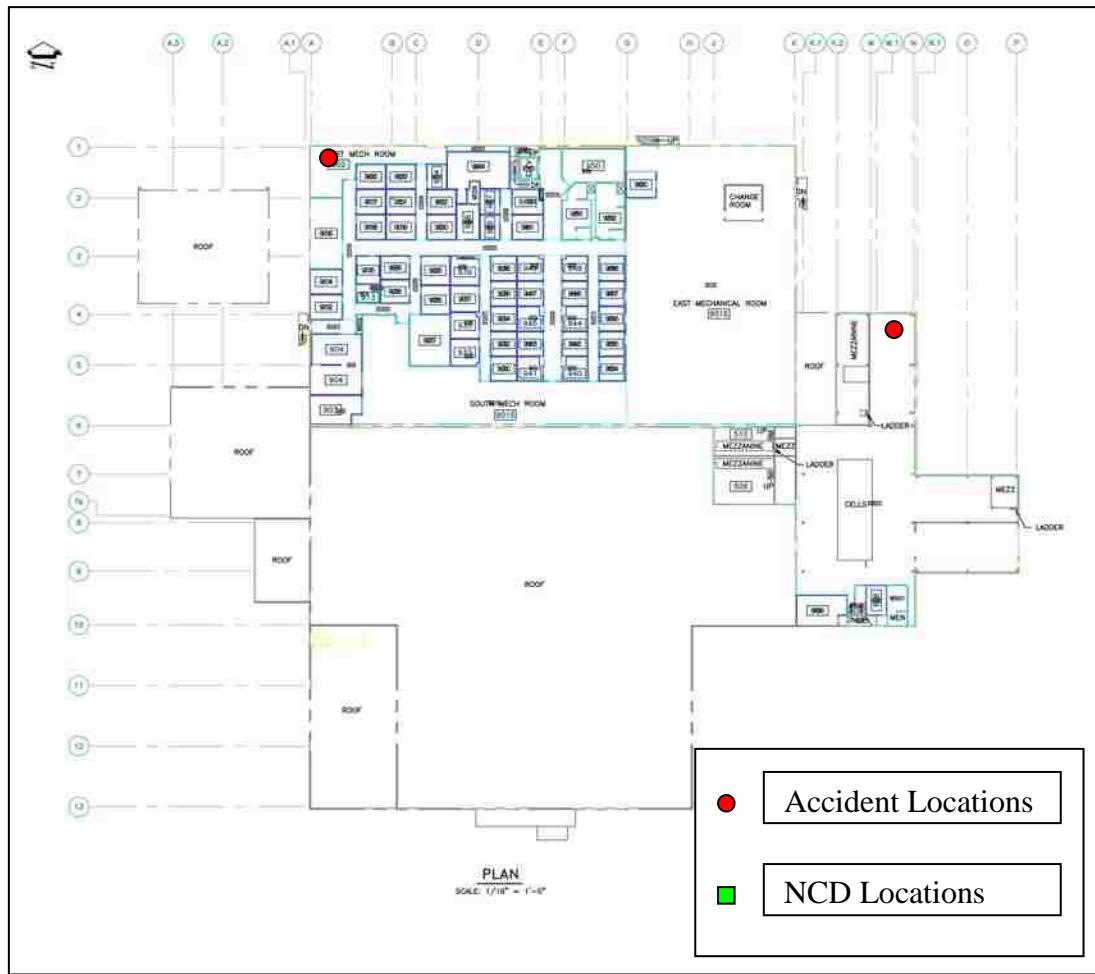


Figure 19. RPL Basement showing accident locations and NCD locations



**Figure 20.** RPL First Floor showing accident locations and NCD locations



**Figure 21. RPL Second Floor showing accident locations, no NCD are located on this floor**

## **Appendix B: CAS Component Descriptions**

### **Technical Description of the Comparator Panel**

ANSI/ANS-8.3-1997 dictates that the comparator panel shall not trigger a criticality alarm for any single malfunctioning detector and that great care must be taken in the avoidance of false alarms. The panel constantly generates a signal that is broadcast to all of the detectors in the system. If any detector ceases to return the signal, the board considers the detector failed, and a warning is generated. Note that this warning is not the audible criticality alarm; it is a different alarm that is sent to an area normally occupied by competent personnel. Another note about the panel is that it does not issue a criticality alarm until two or more channels have alarmed. This eliminates the possibility of a single detector failure causing a false alarm. This is an important design criterion that greatly impacts the physical design of the system. It should also be noted the ANSI/ANS-8.3-1997 words the alarm statement as "...requiring concurrent response of two or more detectors to initiate the alarm." So it is allowable to require greater than two concurrent detector responses for a criticality alarm to be generated.

### **Technical Description of the Radiation Detectors**

There are two types of radiation resultant from fission that are practically detectable: neutrons and gamma rays. The range of both neutrons and gammas is large enough that the number of detectors needed for adequate coverage is not prohibitive.

Typical CAS use either neutron or gamma detectors. A review of the literature did not identify any system that uses a combination of the two.

The selection of neutron or gamma ray detectors for the detection system has some important physical implications. Because the goal of the alarm system is to establish adequate coverage for the facility in question, it is desired from an engineering standpoint to set the trip setting of the detectors as low as possible. The lower the trip setting is then the fewer particles the detectors need to see for an alarm signal to be generated. But conversely the lower the trip setting is, the greater the risk of false alarm becomes. So there must be a balance made between lowering the minimum trip setting for detection limits and keeping the trip setting high enough to avoid false alarms. Finding and proving this balance is not trivial so appropriate detector selection is crucial.

Section 5.1 of ANSI/ANS-8.3-1997 addresses the reliability of the system in general, which is of course applicable to the detectors themselves. It says:

*"The system shall be designed for high reliability and should utilize components that do not require frequent servicing, such as lubrication or cleaning. The system should be designed to minimize the effects of non-use, deterioration, power surges, and other adverse conditions. The design of the system should be as simple as is consistent with the objectives of ensuring reliable actuation of the criticality alarm signal and avoidance of false alarms."*

This description is used to narrow the field of possible detectors that could be used in the system.

To investigate detector specific properties the book, Radiation Detection and Measurement by Glenn Knoll is extraordinarily useful. It goes into great detail for many different detector types. It provides operational data as well as counting efficiencies. It should be clear that the main detector selection criteria are gross count efficiency,

dependability, and the detection efficiency over the applicable incident particle energy range i.e., fission. There is no need for a detector that has spectral analysis capability. The list of potential detector candidates for both gamma and neutron detectors is quite large and beyond the focus of this document. What is of concern is the selection of which type of particle will be detected.

Background levels, both terrestrial and cosmic, are considerably different for gammas and neutrons. Background levels for neutrons are typically next to nothing in most areas. Generally it takes human effort to liberate neutrons, so man made sources are really the only area of concern for false alarms in a system utilizing neutron detection. This is not the case for gamma rays.

Natural background for gamma rays varies from location to location, sometimes considerably. Worse still is that the background levels for gamma rays can fluctuate with time. For example cosmic sources, such as solar flares, can cause significant increases in the gamma ray background levels. It is not all bad though because gamma rays are not attenuated in low Z materials as quickly as neutrons are. Most building construction materials are low-Z; concrete, wood, sheet rock, to name a few. Of course there can be large amounts of metal in buildings as well. Metals do a reasonably good job of shielding gammas. But metal will also absorb neutrons, which will then emit gammas as a result. This makes typical activity levels of gammas in facilities higher than that of neutrons during accident scenarios and therefore easier to detect.

Because the 300 area of Hanford, Washington is undergoing widespread demolition, the radiation detectors from other buildings have been salvaged and stockpiled. The majority of these detectors are  $\text{BF}_3$  filled neutron proportional detectors.

These are very reliable, simple devices that don't require any significant maintenance other than calibration. So it was "recommended" that the design utilize this excess resource, which it does.

Equation B-1 shows the detection efficiency of BF<sub>3</sub> Tube.  $\sum_a(E)$  is the Macroscopic Absorption Cross-Section of B<sup>10</sup> at an energy level E, and L is the active length of the tube. Be sure to note any end effects when making an active length determination.

$$E(E) = 1 - \exp[-\sum_a(E)*L] \quad \text{B-1}$$

This equation was provided to illustrate a point. The absorption cross-section of B<sup>10</sup> is very large so the corresponding detection efficiency is good.

## Appendix C: Material Definitions for Codes

32 g/l $^{239}\text{Pu}$ in $\text{H}_2\text{O}$ (From ARH 600)	
Nuclide $^{239}\text{Pu}$	Number Density (atoms/bn-cm) 8.0614E-05
$^{16}\text{O}$	3.3374E-02
$^1\text{H}$	6.6748E-02

$\text{H}_2\text{O}$	
Nuclide $^1\text{H}$	Number Density (atoms/bn-cm) 6.6890E-02
$^{16}\text{O}$	3.3440E-02

Iron	
Nuclide Fe	Mass Density (g/cm <sup>3</sup> ) 7.874

Air	
Nuclide $^{14}\text{N}$	Weight Fraction 79%
$^{16}\text{O}$	21%
Atom Density=1.197E-03 atoms/bn-cm	

Dirt	
Nuclide Si (nat.)	Atom Fraction 33%
$^{16}\text{O}$	67%
Mass Density = 2.32 g/cm <sup>3</sup> . With a 66% packing factor mass density = 1.53 g/cm <sup>3</sup> .	

Concrete (2.3g/cc)	
Nuclide	Atom Fraction
<sup>27</sup> Al	0.00175
Ca (nat.)	0.00152
Fe (nat.)	0.00035
<sup>1</sup> H	0.01375
<sup>16</sup> O	0.04608
<sup>23</sup> Na	0.00175
Si (nat.)	0.01663

Stainless Steel	
Nuclide	Weight Fraction
Fe (nat.)	74%
Cr (nat.)	18%
Ni (nat.)	8%

Stainless Steel Walls	
Nuclide	Atom Density (atoms/bn-cm)
Fe (nat.)	2.63792E-03
Cr (nat.)	6.89167E-04
Ni (nat.)	2.71250E-04
Total	3.59833E-03

Wall density changes from the 8" to the 4" because of construction method

8" Wood Walls	
Nuclide	Mass Density (g/cm <sup>3</sup> )
C (nat.)	2.6664E-02
<sup>1</sup> H	3.7320E-03
<sup>16</sup> O	2.9604E-02

4" Wood Walls	
Nuclide	Mass Density (g/cm <sup>3</sup> )
C (nat.)	5.3328E-02
<sup>1</sup> H	7.4640E-03
<sup>16</sup> O	5.9208E-02

Basement Ceiling/First Floor-Deck	
Nuclide	Mass Fraction
$^{27}\text{Al}$	0.03177
Ca (nat.)	0.04112
Fe (nat.)	0.06160
$^1\text{H}$	0.00934
$^{16}\text{O}$	0.49712
Si (nat.)	0.31491
$^{23}\text{Na}$	0.02710
Cr (nat.)	0.01180
Ni (nat.)	0.00524
The density of the mixture is 2.4121 g/cm <sup>3</sup> .	

First Floor-Ceiling/Second Floor-Deck	
Nuclide	Mass Fraction
$^{27}\text{Al}$	0.00454
$^{10}\text{B}$	0.01680
$^{16}\text{O}$	0.24290
Si (nat.)	0.1712
$^{23}\text{Na}$	0.01861
Fe (nat.)	0.40400
Cr (nat.)	0.09828
Ni (nat.)	0.04368
The density of the mixture is 0.47511 g/cm <sup>3</sup> .	

## Full-Office Material Composition

The typical full office has one desk, one file cabinet, and three bookshelves. The dimensions are as follows:

$$\text{Desk} = 36'' * 15'' * 26''$$

$$V_d = 14,040 \text{ inches}^3$$

$$\text{File Cabinet} = 60'' * 15'' * 26''$$

$$V_{fc} = 23,400 \text{ inches}^3$$

$$\text{Bookshelf} = 82'' * 36'' * 12''$$

$$V_s = 35,424 \text{ inches}^3$$

Therefore, the total volume of the wood in the room is  $V_d + V_{fc} + 3V_s$ , which is 143,712 in<sup>3</sup> or 2.35502E+6 cm<sup>3</sup>.

The percent volume of wood =  $V_w/V_{room}$  = 4.85496E-02

Wood is assumed to be cellulose (C<sub>6</sub>H<sub>10</sub>O<sub>5</sub>) at 1 g/cm<sup>3</sup>.

Therefore, the weight fractions are

$$C = 0.4444$$

$$H = 0.0622$$

$$O = 0.4934$$

The material densities are therefore:

$$C = 2.15754E-02 \text{ g/cm}^3$$

$$H = 3.01979E-03 \text{ g/cm}^3$$

$$O = 2.39544E-02 \text{ g/cm}^3$$

Total Room Density = 4.855E-02 g/cm<sup>3</sup>

## Full-Laboratory Material Composition

$$\begin{aligned}
 \text{Room Volume} &= (802.64 \text{ cm} * 601.98 \text{ cm} * 441.96 \text{ cm}) \\
 &- \\
 &(220.98 \text{ cm} * 60.96 \text{ cm} * 441.96 \text{ cm}) \\
 &= 2.0164E+08 \text{ cm}^3
 \end{aligned}$$

### Glove Box

#### SS panels

Number	x	y	z	Volume (in <sup>3</sup> )	Volume (cm <sup>3</sup> )
2	24	48	0.25	576	9,438.95
2	48	36	0.25	864	14,158.42
2	36	24	0.25	432	7,079.212

#### Glass panels

Number	x	y	z	Volume (in <sup>3</sup> )	Volume (cm <sup>3</sup> )
2	48	36	0.25	864	14,158.42
2	24	36	0.25	432	7,079.212

#### Lead Bricks

Number	x	y	z	Volume (in <sup>3</sup> )	Volume (cm <sup>3</sup> )
6	2	4	8	384	6,292.633

#### Stainless Steel Sheet to Represent Instruments

Number	x	y	z	Volume (cm <sup>3</sup> )
1	802.64	601.98	1.0	483,173

#### Glass Sheet to Represent Instruments

Number	x	y	z	Volume (cm <sup>3</sup> )
1	802.64	601.98	1.0	483,173

#### Wood Sheet to Represent Tables and Desks

Number	x	y	z	Volume (cm <sup>3</sup> )
1	802.64	601.98	1.0	483,173

Two Bookshelves  $1,160,991 \text{ cm}^3$

Two File Cabinets  $766,915 \text{ cm}^3$

#### Material Totals

	Volume ( $\text{cm}^3$ )	Volume Fraction	Density in Room ( $\text{g/cm}^3$ )
Glass	504,410	2.5016E-03	5.5785E-03
SS	513,849	2.5484E-03	2.0209E-02
Pb	6,292	3.1208E-05	3.5421E-04
Wood	2,411,078	1.1958E-02	1.1958E-02
Air	1.9820E+08	9.8296E-01	1.1815E-03

#### Densities (Repond, 1977)

$$\text{Glass} = 2.32 \text{ g/cm}^3$$

$$\text{SS} = 7.93 \text{ g/cm}^3$$

$$\text{Pb} = 11.35 \text{ g/cm}^3$$

$$\text{Wood} = 1.00 \text{ g/cm}^3$$

$$\text{Air} = 0.001202 \text{ g/cm}^3$$

Nuclide	Weight Fraction
Al	1.4202E-03
B	5.2546E-03
Na	5.8227E-03
O	2.3249E-01
Si	5.3541E-02
Fe	3.8071E-01
Cr	9.2605E-02
Ni	4.1158E-02
Pb	9.0174E-03
C	1.3528E-01
H	1.8935E-02
N	2.3762E-02
Total Density	0.03928 g/cm3

## Sparse-Laboratory Material Composition

$$\begin{aligned}
 \text{Room Volume} &= (802.64 \text{ cm} * 601.98 \text{ cm} * 441.96 \text{ cm}) \\
 &- \\
 &(220.98 \text{ cm} * 60.96 \text{ cm} * 441.96 \text{ cm}) \\
 &= 2.0164E+08 \text{ cm}^3
 \end{aligned}$$

It is assumed that there is one-half the total amount of material that is present in the full-laboratory model.

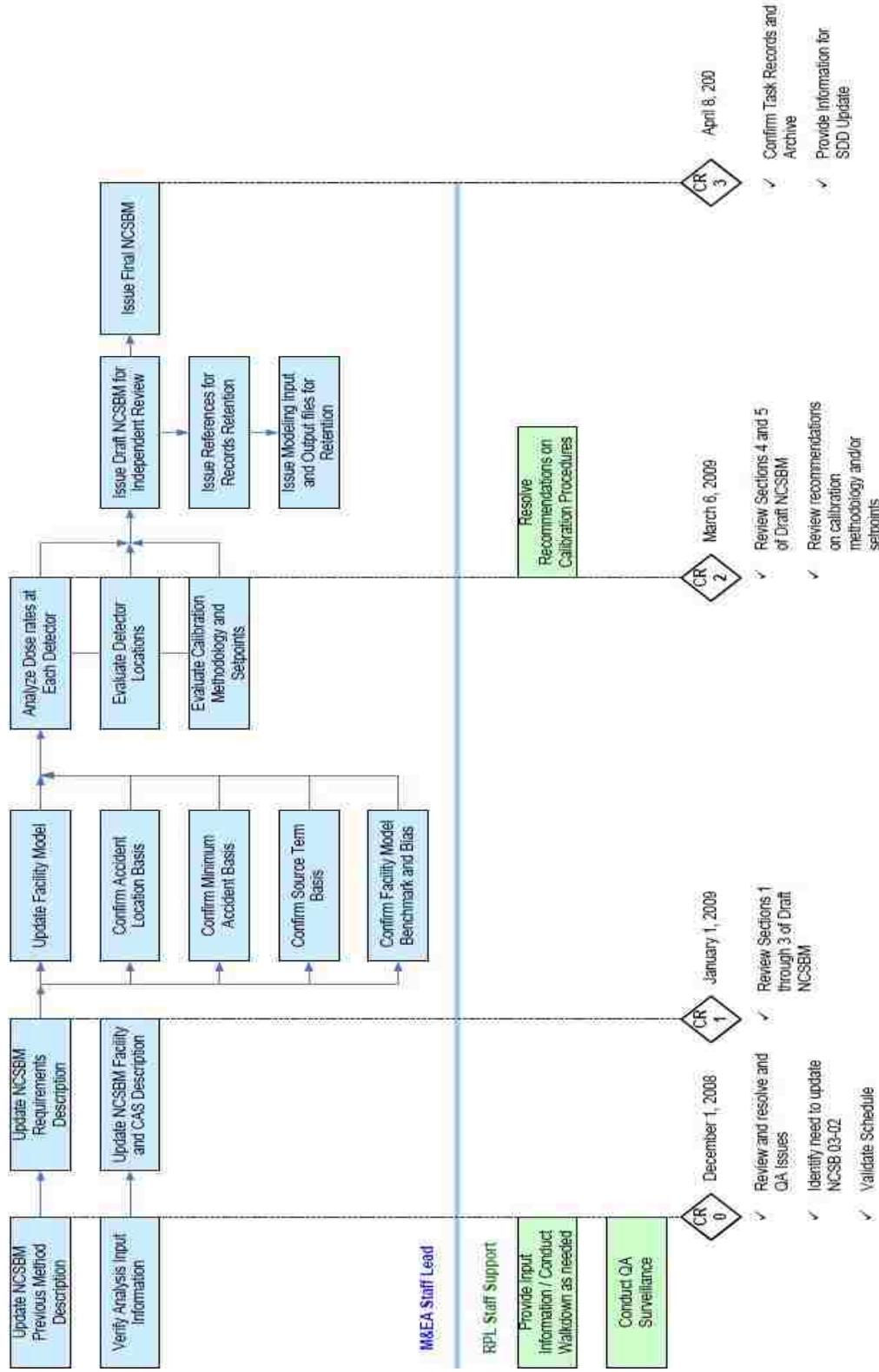
Material Totals	Volume (cm <sup>3</sup> )	Volume Fraction	Density in
Room			
Glass	252,205	1.2508E-03	2.7893E-03
SS	256,924	1.2742E-03	1.0104E-02
Pb	3,146	1.5604E-05	1.7710E-04
Wood	1,205,539	5.9788E-02	5.9788E-02
Air	1.9992E+08	9.9148E-01	1.1918E-03

## Densities (Repond, 1977)

$$\begin{aligned}
 \text{Glass} &= 2.32 \text{ g/cm}^3 \\
 \text{SS} &= 7.93 \text{ g/cm}^3 \\
 \text{Pb} &= 11.35 \text{ g/cm}^3 \\
 \text{Wood} &= 1.00 \text{ g/cm}^3 \\
 \text{Air} &= 0.001202 \text{ g/cm}^3
 \end{aligned}$$

Nuclide	Weight Fraction
Al	1.3780E-03
B	5.0986E-03
Na	5.6498E-03
O	2.3183E-01
Si	5.1951E-02
Fe	3.6941E-01
Cr	8.9855E-02
Ni	3.9936E-02
Pb	8.7497E-03
C	1.3126E-01
H	1.8372E-02
N	4.6513E-02
Total Density	0.020240 g/cm <sup>3</sup>

## **Appendix D: Schedule of Deliverables**



## **Appendix E: Assumptions Used in the CAS Design of RPL**

### **Modeling Assumptions**

- 1) 1st Floor Deck is a sandwiched 14 gauge steel honeycomb with a maximum of 5" of "standard Concrete". The ceiling composition is based on the elevation blue prints listed below, which show that the ceiling is on average 3.75" thick with 14-gauge steel (0.0766" thick, Reference 23). This works to a volume ratio of 0.98/0.02 concrete to stainless steel and a mass ratio of 0.934/0.066 concrete to stainless steel.
- 2) 2<sup>nd</sup> Floor Deck is a sandwiched 16 gauge steel honeycomb with a maximum of 5 inches of "Emmeshic Concrete". Dave Koontz indicated that this concrete was roughly 30% if the density of standard concrete.
- 3) The Gable of all roofs was modified to be a flat equivalent slab at the average height of the actual roof.
- 4) The ground surrounding 325 was assumed to be SiO<sub>2</sub> with a 66% packing fraction.
- 5) Room fill was approached as a combination of full, half-full, or empty office/lab.
- 6) Dave Koontz mentioned Asbestos in the hollow walls on the 300, 400, and 500 hallways. Have not included any Asbestos in the model because I was unable to verify its existence.
- 7) The offset of roof parapets were omitted. Walls are capped by the roofs.
- 8) Basement Deck is set as 1ft thick from drawing H-4-50013 –Hard to read
- 9) All staircases omitted
- 10) Altitudes/elevations are very difficult to verify. This is especially true for HLRF. The original schematics are in PDF format and are extremely cluttered but all non-roof elevations are referenced from H-4-50013-1 and H-3-12901.

- 11) The exterior wall of B325 changes from structural concrete to metal siding, insulation, metal support columns, and the occasional window. This change from concrete to metal conglomerate occurs at 404'-6" for the majority of the building. The Northern exterior walls do not change at this height. They change at 416'-4". For simplicity, I have set the ENTIRE buildings exterior concrete wall to a height of 404'-6". The material compositions of the exterior wall versus concrete support that making this change is conservative because reflection decreases with the omission of the concrete northern wall.
- 12) Roof elevations were taken from drawing H-3-305005. The roof in the NW corner of HLRF has been commented out. The roof composition was observed to be a conglomerate of asphalt, tar, gravel, and cement. Because I have found no documents that state the actual contents, I have set all roofs to concrete. All roofs run to the edge of the sections they cover –No overhangs. You will notice a rather large gap above the central section of floor 1 and the corresponding roof. This was done intentionally because there is a large crawl space. The gap is due to setting the roof position to the average height of the gable.
- 13) The Elevation for the roofs were taken from Drawings H-3-12901 and H-3-305005 to be 429'9" or 13098.8cm. The roof also has a gable that runs a delta of approximately 6" over the span of the roof over HLRF. The highest point is approximately 430' and the lowest is approximately 429'6".
- 14) The very small roof over the southern entrance to RPL was neglected.
- 15) The CAD Drawings clearly show the top floor of HLRF E wall at 230.9' (586.5cm) from the SW corner. The second floor CAD drawings clearly show the second floor E wall at 224.4' (570cm) from the same origin. I am leaving the dimensions as shown on the CAD drawings until inspection proves otherwise. The point of this statement is there is a noticeable overhang of the second floor HLRF E wall over the same first floor E wall.
- 16) ALL CHAIN LINK was omitted.
- 17) There are three vaults E of HLRF that have not been added to the model.
- 18) Men's and Women's restrooms were left empty

- 19) Tank 46 was modeled as empty.
- 20) The corresponding materials for SAL and HLRF hot cells were smeared to be the most limiting conservative cases.
- 21) From personal inspection, a grade was found in the deck of the Basement mezzanine. The altitude change was observed to be 1ft over the length of the deck. This slope was ignored and the deck of the mezzanine was held level at 8.5ft. The offset of the deck of the mezzanine to the deck of the central section of the basement was measured at 5ft.
- 22) The southern mezzanine section of B1 is set 5ft above the central B1 Deck. This is an observed distance because I have found no blueprint that clearly defines this distance.
- 23) There is a small gap between Rm23B and the top of Rm32 where there is no sand and just air.
- 24) There is no sand up to the grade height in the SE corner of the building. This was done to be conservative. There are numerous areas in the SE that do not have a backfill to the same grade as the rest of the building. There is also a loading dock located in the SE corner which is simply free space lined with concrete.
- 25) The material fill for all interior office/laboratory walls were set to be the same “metal fill” listed in the materials definition because there was no access to the interior of the walls

### **Translation notes**

The basement was translated in reference to the SW section. Floor1 was translated with reference to the NW section. The second floor was translated in reference to the SW section. TR4=basement translation, TR1=Floor1 translation, TR2=Floor2 translation. And TR3=Floor3 translation.

## Appendix F: MCNP5 Input Decks

Bldg. 325 RPL 10/15/2008

```
c =====
c 34567890123456789112345678921234567893123456789412345678951234567896123456789712345678
c Built by: Bryce Greenfield
c      Pacific Northwest National Laboratory, USA
c      <Bryce.Greenfield@pnl.gov>, 509-372-4384
c For: Crit. Safety Analysis of Bldg 325 -RPL Improved Detector Coverage
c
c Rev. Date: 2/2/2009
c
c =====
c
c
c
c Each Surface block contains a header with notes about that section.
c Whenever possible and or convenient the origin for each sections coordinate system
c was place in the most Southwestern point in that section. On some junctions between surfaces
c boundary errors arose even though the dimensions were correctly entered. The solution
c used to eliminate these errors was to back out the conflicting boundary by a very small margin~0.01cm.
c Each surface is followed by a brief description of what and where it is. Surfaces were modeled,
c grouped, and numbered according to their respective room numbers. The format for both the cell
c and surface cards is as follows #####. The ### signs are the room numbers with a
c range of 1-999 and the $$ signs are the surface/cell numbers that range from 1-99.
c For example 701 refers to room 7 surface 1. Wheras 7001 refers to room 70 surface 1.
c Cardinal directions relative to each room were used to roughly
c describe where a surface existed. For example: W wall Rm72.
c Hopefully it is easy to interpret as the western wall of Room 72. When multiple surfaces
c existed in the same room/plane they were described with SW, CentralW, or NW. If there were numerous
c bodies in the same room/plane then a numbering system was used that always started with the
c southwestern most body and the moved eastward. After a terminating surface was encountered
c the numbering was continued by moving back to the starting body(the most SW body) and moving North
c to continue the numbering sequence. For an example of this check the descriptions of the columns
c modeled in Room 45 of the Basement.
c
c =====
c
c Index of Section Identifier Tags <-Use Search to navigate through file
c
c
c TAG=TAGb1roomfill - B1 Room fills
c TAG=TAGf1roomfill - Floor 1 Room fills
c TAG=TAGf2roomfill - Floor 2 Room fills
c
c TAG=TAGPuPu - Accident Surfaces/Locations
c TAG=TAGdetectors - Detector surfaces/Locations
c TAG=TAGbasementsurfaces - B1 surfaces
c TAG=TAGfloor1surfaces - 1st floor surfaces
c TAG=TAGfloor2surfaces - 2nd floor surfaces
c TAG=TAGfloor3surfaces - 3rd floor surfaces
c TAG=TAGmaterials - Materials definition
c TAG=TAGsourcedef - Accident Locations Specific SDEF
c
c
c =====
c
c Legend of Abbreviations
c
c o = outside
c i = inside
c wl = wall
c Rm = Room
c LR = Lunch Room
c u = upper
c l = lower
c N = North
```



```

c
c
c Listed Below will be all of the cells related to the criticality detection portion of this model
c
c Pu Filled Sphere in Rm 22
440 17 0.100200 (-440) imp:n=1 $Pu-H2O Sphere
c
c
c Below are the cells for all of the Detectors in Building 325 .9detectors
c
461 19 -.9300 (-461) imp:n=1 $Detector 1 B1
462 19 -.9300 (-462) imp:n=1 $Detector 2 B1
463 19 -.9300 (-463) imp:n=1 $Detector 3 B1
464 19 -.9300 (-464) imp:n=1 $Detector 4 F1
465 19 -.9300 (-465) imp:n=1 $Detector 5 F1
466 19 -.9300 (-466) imp:n=1 $Detector 6 F1
467 19 -.9300 (-467) imp:n=1 $Detector 7 F1
468 19 -.9300 (-468) imp:n=1 $Detector 8 F1
c
c
c Basement1 Room 45
c This room contains mainly columns.
4536 13 -7.93 (-4536) imp:n=1 $SS-304
4537 13 -7.93 (-4537) imp:n=1 $SS-304
4538 13 -7.93 (-4538) imp:n=1 $SS-304
4539 13 -7.93 (-4539) imp:n=1 $SS-304
4540 13 -7.93 (-4540) imp:n=1 $SS-304
4541 13 -7.93 (-4541) imp:n=1 $SS-304
4542 13 -7.93 (-4542) imp:n=1 $SS-304
4543 13 -7.93 (-4543) imp:n=1 $SS-304
4544 13 -7.93 (-4544) imp:n=1 $SS-304
4545 13 -7.93 (-4545) imp:n=1 $SS-304
4546 13 -7.93 (-4546) imp:n=1 $SS-304
4547 13 -7.93 (-4547) imp:n=1 $SS-304
4548 13 -7.93 (-4548) imp:n=1 $SS-304
4549 13 -7.93 (-4549) imp:n=1 $SS-304
4550 13 -7.93 (-4550) imp:n=1 $SS-304
4551 13 -7.93 (-4551) imp:n=1 $SS-304
4552 13 -7.93 (-4552) imp:n=1 $SS-304
4553 13 -7.93 (-4553) imp:n=1 $SS-304
4554 13 -7.93 (-4554) imp:n=1 $SS-304
4555 13 -7.93 (-4555) imp:n=1 $SS-304
4556 13 -7.93 (-4556) imp:n=1 $SS-304
4557 13 -7.93 (-4557) imp:n=1 $SS-304
4558 13 -7.93 (-4558) imp:n=1 $SS-304
c
c
c Basement Room 55/55A/55B
5501 14 -0.539 (-5501) imp:n=1 $Cinder Block
5502 3 -2.3 (-5502 5501 5503) imp:n=1 $Conc Filled
5503 14 -0.539 (-5503) imp:n=1 $Cinder Block
5504 14 -0.539 (-5504) imp:n=1 $Cinder Block
5505 3 -2.3 (-5505) imp:n=1 $Conc Filled
5506 3 -2.3 (-5506) imp:n=1 $Conc Filled
5507 14 -0.539 (-5507) imp:n=1 $Cinder Block
5508 14 -0.539 (-5508) imp:n=1 $Cinder Block
5509 14 -0.539 (-5509) imp:n=1 $Cinder Block
5510 14 -0.539 (-5510) imp:n=1 $Cinder Block
5511 14 -0.539 (-5511) imp:n=1 $Cinder Block
5512 14 -0.539 (-5512) imp:n=1 $Cinder Block
5513 3 -2.3 (-5513) imp:n=1 $Conc Filled
c
c
c Basement Room 56
5601 14 -0.539 (-5601) imp:n=1 $Conc Filled
5602 14 -0.539 (-5602) imp:n=1 $Conc Filled
5603 14 -0.539 (-5603) imp:n=1 $Conc Filled
5604 14 -0.539 (-5604) imp:n=1 $Conc Filled
c
c

```

```

c
c
c
c Begin North-center Section of the Central Section of Basement1
c *****Notes for this section of Cells*****
c
c
c
c Basement1 Room 91
9101 3 -2.3 (-9101) imp:n=1 $Conc Filled
9102 3 -2.3 (-9102) imp:n=1 $Conc Filled
9103 3 -2.3 (-9103) imp:n=1 $Conc Filled
9104 3 -2.3 (-9104) imp:n=1 $Conc Filled
9105 3 -2.3 (-9105) imp:n=1 $Conc Filled
9106 3 -2.3 (-9106) imp:n=1 $Conc Filled
9107 3 -2.3 (-9107) imp:n=1 $Conc Filled
9108 3 -2.3 (-9108) imp:n=1 $Conc Filled
c
c
c Basement1 Room 93
9301 3 -2.3 (-9301) imp:n=1 $Conc Filled
9302 3 -2.3 (-9302) imp:n=1 $Conc Filled
9303 3 -2.3 (-9303) imp:n=1 $Conc Filled
9304 3 -2.3 (-9304) imp:n=1 $Conc Filled
9305 3 -2.3 (-9305) imp:n=1 $Conc Filled
9306 3 -2.3 (-9306) imp:n=1 $Conc Filled
9307 3 -2.3 (-9307) imp:n=1 $Conc Filled
9308 3 -2.3 (-9308) imp:n=1 $Conc Filled
9309 3 -2.3 (-9309) imp:n=1 $Conc Filled
9310 3 -2.3 (-9310) imp:n=1 $Conc Filled
9311 3 -2.3 (-9311) imp:n=1 $Conc Filled
9312 3 -2.3 (-9312) imp:n=1 $Conc Filled
9313 3 -2.3 (-9313) imp:n=1 $Conc Filled
9314 3 -2.3 (-9314) imp:n=1 $Conc Filled
9315 3 -2.3 (-9315) imp:n=1 $Conc Filled
9316 3 -2.3 (-9316) imp:n=1 $Conc Filled
9317 3 -2.3 (-9317) imp:n=1 $Conc Filled
9318 13 -7.93 (-9318) imp:n=1 $SS-304
c
c
c Basement1 Room 94/94A/94B
9401 14 -0.539 (-9401) imp:n=1 $Cinder Block
9402 14 -0.539 (-9402) imp:n=1 $Cinder Block
9403 14 -0.539 (-9403) imp:n=1 $Cinder Block
9404 14 -0.539 (-9404) imp:n=1 $Cinder Block
9405 3 -2.3 (-9405) imp:n=1 $Conc Filled
9406 14 -0.539 (-9406) imp:n=1 $Cinder Block
9407 14 -0.539 (-9407) imp:n=1 $Cinder Block
9408 3 -2.3 (-9408) imp:n=1 $Conc Filled
9409 3 -2.3 (-9409) imp:n=1 $Conc Filled
9410 3 -2.3 (-9410) imp:n=1 $Conc Filled
9411 3 -2.3 (-9411) imp:n=1 $Conc Filled
9412 14 -0.539 (-9412) imp:n=1 $Cinder Block
9413 14 -0.539 (-9413) imp:n=1 $Cinder Block
c
c
c Basement1 Room 95
9501 14 -0.539 (-9501) imp:n=1 $Cinder Block
9502 14 -0.539 (-9502) imp:n=1 $Cinder Block
9503 14 -0.539 (-9503) imp:n=1 $Cinder Block
9504 14 -0.539 (-9504) imp:n=1 $Cinder Block
c
c
c Basement1 Room 96/96A
9601 14 -0.539 (-9601) imp:n=1 $Cinder Block
9602 14 -0.539 (-9602) imp:n=1 $Cinder Block
9603 13 -7.93 (-9603) imp:n=1 $SS-304
9604 14 -0.539 (-9604) imp:n=1 $Cinder Block
9605 14 -0.539 (-9605) imp:n=1 $Cinder Block
9606 14 -0.539 (-9606) imp:n=1 $Cinder Block

```

9607 14 -0.539 (-9607) imp:n=1 \$Cinder Block  
 c  
 c  
 c Basement1 Room 97/97A  
 9701 14 -0.539 (-9701) imp:n=1 \$Cinder Block  
 9702 3 -2.3 (-9702) imp:n=1 \$Conc Filled  
 9703 14 -0.539 (-9703) imp:n=1 \$Cinder Block  
 9704 13 -7.93 (-9704) imp:n=1 \$SS-304  
 9705 14 -0.539 (-9705) imp:n=1 \$Cinder Block  
 9706 14 -0.539 (-9706) imp:n=1 \$Cinder Block  
 9707 13 -7.93 (-9707) imp:n=1 \$SS-304  
 c  
 c  
 c Basement Room 98  
 9801 14 -0.539 (-9801) imp:n=1 \$Cinder Block  
 c  
 c  
 c Basement Room 45  
 4560 3 -2.3 (-4560) imp:n=1 \$Conc Filled  
 4561 3 -2.3 (-4561) imp:n=1 \$Conc Filled  
 4562 3 -2.3 (-4562) imp:n=1 \$Conc Filled  
 4563 3 -2.3 (-4563) imp:n=1 \$Conc Filled  
 4564 13 -7.93 (-4564) imp:n=1 \$SS-304  
 4565 13 -7.93 (-4565) imp:n=1 \$SS-304  
 4566 3 -2.3 (-4566) imp:n=1 \$Conc Filled  
 4567 3 -2.3 (-4567) imp:n=1 \$Conc Filled  
 4568 3 -2.3 (-4568) imp:n=1 \$Conc Filled  
 4569 3 -2.3 (-4569) imp:n=1 \$Conc Filled  
 c 4570 3 -2.3 (-4570) imp:n=1 \$Conc Filled  
 c 4571 3 -2.3 (-4571) imp:n=1 \$Conc Filled  
 c  
 c  
 c Basement Room 90/Elev Room  
 9001 3 -2.3 (-9001) imp:n=1 \$Conc Filled  
 9002 3 -2.3 (-9002) imp:n=1 \$Conc Filled  
 9003 3 -2.3 (-9003) imp:n=1 \$Conc Filled  
 9004 3 -2.3 (-9004) imp:n=1 \$Conc Filled  
 9005 3 -2.3 (-9005) imp:n=1 \$Conc Filled  
 9006 3 -2.3 (-9006) imp:n=1 \$Conc Filled  
 9007 3 -2.3 (-9007) imp:n=1 \$Conc Filled  
 9008 3 -2.3 (-9008) imp:n=1 \$Conc Filled  
 9009 3 -2.3 (-9009) imp:n=1 \$Conc Filled  
 9010 3 -2.3 (-9010) imp:n=1 \$Conc Filled  
 9011 3 -2.3 (-9011) imp:n=1 \$Conc Filled  
 9012 3 -2.3 (-9012) imp:n=1 \$Conc Filled  
 9013 3 -2.3 (-9013) imp:n=1 \$Conc Filled  
 9014 3 -2.3 (-9014) imp:n=1 \$Conc Filled  
 9015 3 -2.3 (-9015) imp:n=1 \$Conc Filled  
 9016 3 -2.3 (-9016) imp:n=1 \$Conc Filled  
 c  
 c  
 c  
 c  
 c Begin Northeast Section of the Central Section of Basement1  
 c \*\*\*\*\*Notes for this section of Cells\*\*\*\*\*  
 c  
 c  
 c Basement Room 45  
 4575 13 -7.93 (-4575) imp:n=1 \$SS-304  
 4576 13 -7.93 (-4576) imp:n=1 \$SS-304  
 4577 13 -7.93 (-4577) imp:n=1 \$SS-304  
 4578 13 -7.93 (-4578) imp:n=1 \$SS-304  
 4579 13 -7.93 (-4579) imp:n=1 \$SS-304  
 4580 13 -7.93 (-4580) imp:n=1 \$SS-304  
 4581 13 -7.93 (-4581) imp:n=1 \$SS-304  
 4582 13 -7.93 (-4582) imp:n=1 \$SS-304  
 4583 13 -7.93 (-4583) imp:n=1 \$SS-304  
 c  
 c

c Basement1 Room 48

4801	3	-2.3	(-4801)	imp:n=1	\$Conc Filled
4802	3	-2.3	(-4802)	imp:n=1	\$Conc Filled
4803	3	-2.3	(-4803)	imp:n=1	\$Conc Filled
4804	3	-2.3	(-4804)	imp:n=1	\$Conc Filled
4805	3	-2.3	(-4805)	imp:n=1	\$Conc Filled
4806	13	-7.93	(-4806)	imp:n=1	SSS-304
4807	13	-7.93	(-4807)	imp:n=1	SSS-304

c

c

c Basement Room 57/57W/57E

5701	14	-0.539	(-5701)	imp:n=1	\$Cinder Block
5702	14	-0.539	(-5702)	imp:n=1	\$Cinder Block
5703	14	-0.539	(-5703)	imp:n=1	\$Cinder Block
5704	14	-0.539	(-5704)	imp:n=1	\$Cinder Block
5705	14	-0.539	(-5705)	imp:n=1	\$Cinder Block
5706	14	-0.539	(-5706)	imp:n=1	\$Cinder Block
5707	14	-0.539	(-5707)	imp:n=1	\$Cinder Block
5708	14	-0.539	(-5708)	imp:n=1	\$Cinder Block
5709	14	-0.539	(-5709)	imp:n=1	\$Cinder Block
5710	14	-0.539	(-5710)	imp:n=1	\$Cinder Block

c

c

c Basement Room 58

5801	14	-0.539	(-5801)	imp:n=1	\$Cinder Block
5802	13	-7.93	(-5802)	imp:n=1	SSS-304
5803	14	-0.539	(-5803)	imp:n=1	\$Cinder Block
5804	14	-0.539	(-5804)	imp:n=1	\$Cinder Block
5805	14	-0.539	(-5805)	imp:n=1	\$Cinder Block
5806	14	-0.539	(-5806)	imp:n=1	\$Cinder Block
5807	13	-7.93	(-5807)	imp:n=1	SSS-304
5808	13	-7.93	(-5808)	imp:n=1	SSS-304

c

c

c Basement Room 54

5401	13	-7.93	(-5401)	imp:n=1	SSS-304
5402	13	-7.93	(-5402)	imp:n=1	SSS-304
5403	14	-0.539	(-5403)	imp:n=1	\$Cinder Block
5404	14	-0.539	(-5404)	imp:n=1	\$Cinder Block
5405	14	-0.539	(-5405)	imp:n=1	\$Cinder Block
5406	14	-0.539	(-5406)	imp:n=1	\$Cinder Block
5407	3	-2.3	(-5407)	imp:n=1	\$Conc Filled

c

c

c Basement Room 52

5201	14	-0.539	(-5201)	imp:n=1	\$Cinder Block
5202	14	-0.539	(-5202)	imp:n=1	\$Cinder Block
5203	14	-0.539	(-5203)	imp:n=1	\$Cinder Block
5204	14	-0.539	(-5204)	imp:n=1	\$Cinder Block
5205	14	-0.539	(-5205)	imp:n=1	\$Cinder Block
5206	13	-7.93	(-5206)	imp:n=1	SSS-304

c

c

c

c

c

c

c Begin West Section of Basement

c \*\*\*\*\*Notes for this section of Cells\*\*\*\*\*

c

c

c Basement1 Room 23B

2310	3	-2.3	(-2310)	imp:n=1	\$Conc Filled
2311	3	-2.3	(-2311)	imp:n=1	\$Conc Filled
2312	13	-7.93	(-2312)	imp:n=1	SSS-304
2313	13	-7.93	(-2313)	imp:n=1	SSS-304
2314	13	-7.93	(-2314)	imp:n=1	SSS-304
2315	3	-2.3	(-2315)	imp:n=1	\$Conc Filled
2316	3	-2.3	(-2316)	imp:n=1	\$Conc Filled
2317	3	-2.3	(-2317)	imp:n=1	\$Conc Filled

```

2318 13 -7.93 (-2318) imp:n=1 $SS-304
2319 13 -7.93 (-2319) imp:n=1 $SS-304
2320 13 -7.93 (-2320) imp:n=1 $SS-304
c
c
c Basement1 Room 45
4501 3 -2.3 (-4501) imp:n=1 $Conc Filled
4502 3 -2.3 (-4502) imp:n=1 $Conc Filled
4503 3 -2.3 (-4503) imp:n=1 $Conc Filled
4504 3 -2.3 (-4504) imp:n=1 $Conc Filled
4505 3 -2.3 (-4505) imp:n=1 $Conc Filled
4506 3 -2.3 (-4506) imp:n=1 $Conc Filled
4507 3 -2.3 (-4507) imp:n=1 $Conc Filled
4508 3 -2.3 (-4508) imp:n=1 $Conc Filled
4509 3 -2.3 (-4509) imp:n=1 $Conc Filled
c
c
c Basement Room 32
3201 13 -7.93 (-3201) imp:n=1 $SS-304
3202 13 -7.93 (-3202) imp:n=1 $SS-304
3203 13 -7.93 (-3203) imp:n=1 $SS-304
3204 3 -2.3 (-3204) imp:n=1 $Conc Filled
3205 3 -2.3 (-3205) imp:n=1 $Conc Filled
3206 3 -2.3 (-3206) imp:n=1 $Conc Filled
3207 3 -2.3 (-3207) imp:n=1 $Conc Filled
3208 3 -2.3 (-3208) imp:n=1 $Conc Filled
3209 3 -2.3 (-3209) imp:n=1 $Conc Filled
3210 3 -2.3 (-3210) imp:n=1 $Conc Filled
3211 3 -2.3 (-3211) imp:n=1 $Conc Filled
3212 3 -2.3 (-3212) imp:n=1 $Conc Filled
3213 13 -7.93 (-3213) imp:n=1 $SS-304
3214 3 -2.3 (-3214) imp:n=1 $Conc Filled
3215 3 -2.3 (-3215) imp:n=1 $Conc Filled
3216 3 -2.3 (-3216) imp:n=1 $Conc Filled
3217 3 -2.3 (-3217) imp:n=1 $Conc Filled
c
c
c
c
c
c Begin South West Section of the Central Section of Basement1
c *****Notes for this section of Cells*****
c
c
c Basement Room 22
2201 13 -7.93 (-2201) imp:n=1 $SS-304
2202 13 -7.93 (-2202) imp:n=1 $SS-304
2203 13 -7.93 (-2203) imp:n=1 $SS-304
2204 3 -2.3 (-2204) imp:n=1 $Conc Filled
2205 13 -7.93 (-2205) imp:n=1 $SS-304
2206 13 -7.93 (-2206) imp:n=1 $SS-304
2207 3 -2.3 (-2207) imp:n=1 $Conc Filled
2208 13 -7.93 (-2208) imp:n=1 $SS-304
2209 3 -2.3 (-2209) imp:n=1 $Conc Filled
2210 3 -2.3 (-2210) imp:n=1 $Conc Filled
2211 3 -2.3 (-2211) imp:n=1 $Conc Filled
2212 13 -7.93 (-2212) imp:n=1 $SS-304
2213 3 -2.3 (-2213) imp:n=1 $Conc Filled
2214 13 -7.93 (-2214) imp:n=1 $SS-304
2215 3 -2.3 (-2215) imp:n=1 $Conc Filled
2216 3 -2.3 (-2216) imp:n=1 $Conc Filled
2217 3 -2.3 (-2217) imp:n=1 $Conc Filled
c 2218 3 -2.3 (-2218) imp:n=1 $Conc Filled
2219 3 -2.3 (-2219) imp:n=1 $Conc Filled
2220 3 -2.3 (-2220) imp:n=1 $Conc Filled
2221 3 -2.3 (-2221) imp:n=1 $Conc Filled
c
c
c New Hot Cells
2230 13 -7.93 (-2230) imp:n=1 $SW Mod Cell-1 Rm22

```

2231	13	-7.93	(-2231)	imp:n=1	\$W Mod Cell-1 Rm22A
2232	13	-7.93	(-2232)	imp:n=1	\$S Big Cell-3 Rm30A
2233	13	-7.93	(-2233)	imp:n=1	\$N Metalographycell-2 Rm31A
2234	13	-7.93	(-2234)	imp:n=1	\$SE Mod Cell-1 Rm31
2235	13	-7.93	(-2235)	imp:n=1	\$NE Mod Cell-1 Rm33

c

c

c

c Basement1 Room 23a

2301	3	-2.3	(-2301)	imp:n=1	\$Conc Filled
2302	3	-2.3	(-2302)	imp:n=1	\$Conc Filled
2303	3	-2.3	(-2303)	imp:n=1	\$Conc Filled
2304	3	-2.3	(-2304)	imp:n=1	\$Conc Filled
2305	13	-7.93	(-2305)	imp:n=1	SSS-304

c

c

c Basement1 Room 30a

3001	3	-2.3	(-3001)	imp:n=1	\$Conc Filled
3002	3	-2.3	(-3002)	imp:n=1	\$Conc Filled
3003	3	-2.3	(-3003)	imp:n=1	\$Conc Filled
3004	3	-2.3	(-3004)	imp:n=1	\$Conc Filled
3005	13	-7.93	(-3005)	imp:n=1	SSS-304
3006	13	-7.93	(-3006)	imp:n=1	SSS-304

c

c

c Basement1 Room 31 and Room 31A

c 3101	3	-2.3	(-3101)	imp:n=1	\$Conc Filled
3102	3	-2.3	(-3102)	imp:n=1	\$Conc Filled
3103	3	-2.3	(-3103)	imp:n=1	\$Conc Filled
3104	3	-2.3	(-3104)	imp:n=1	\$Conc Filled
c 3105	3	-2.3	(-3105)	imp:n=1	\$Conc Filled
3106	3	-2.3	(-3106)	imp:n=1	\$Conc Filled
3107	3	-2.3	(-3107)	imp:n=1	\$Conc Filled
3108	13	-7.93	(-3108)	imp:n=1	SSS-304

c

c

c Basement1 Room 33

3301	3	-2.3	(-3301)	imp:n=1	\$Conc Filled
3302	13	-7.93	(-3302)	imp:n=1	SSS-304
3303	3	-2.3	(-3303)	imp:n=1	\$Conc Filled
3304	3	-2.3	(-3304)	imp:n=1	\$Conc Filled
3305	3	-2.3	(-3305)	imp:n=1	\$Conc Filled

c

c

c Basement1 Room 45

4584	13	-7.93	(-4584)	imp:n=1	SSS-304
4585	13	-7.93	(-4585)	imp:n=1	SSS-304
4586	13	-7.93	(-4586)	imp:n=1	SSS-304
4587	13	-7.93	(-4587)	imp:n=1	SSS-304
4588	13	-7.93	(-4588)	imp:n=1	SSS-304
4589	13	-7.93	(-4589)	imp:n=1	SSS-304
4590	13	-7.93	(-4590)	imp:n=1	SSS-304
4591	13	-7.93	(-4591)	imp:n=1	SSS-304
4592	13	-7.93	(-4592)	imp:n=1	SSS-304
4593	13	-7.93	(-4593)	imp:n=1	SSS-304

c

c

c

c

c

c Begin South East Section of the Central Section of Basement1

c \*\*\*\*\*Notes for this section of Cells\*\*\*\*\*

c

c

c Basement1 Room 45

c This room contains mainly columns. The SE corner has a wall that does

c not appear in the other sections so I will include it in this section to be safe.

c Surface numbers are continued from the SW section which also contains Room 45.

4511	13	-7.93	(-4511)	imp:n=1	SSS-304
------	----	-------	---------	---------	---------

4512	13	-7.93	(-4512)	imp:n=1	SSS-304
------	----	-------	---------	---------	---------

4513	13	-7.93	(-4513)	imp:n=1	\$SS-304
4514	13	-7.93	(-4514)	imp:n=1	\$SS-304
4515	13	-7.93	(-4515)	imp:n=1	\$SS-304
4516	13	-7.93	(-4516)	imp:n=1	\$SS-304
4517	13	-7.93	(-4517)	imp:n=1	\$SS-304
4518	13	-7.93	(-4518)	imp:n=1	\$SS-304
4519	13	-7.93	(-4519)	imp:n=1	\$SS-304
4520	13	-7.93	(-4520)	imp:n=1	\$SS-304
4521	13	-7.93	(-4521)	imp:n=1	\$SS-304
4522	13	-7.93	(-4522)	imp:n=1	\$SS-304
4523	13	-7.93	(-4523)	imp:n=1	\$SS-304
4524	13	-7.93	(-4524)	imp:n=1	\$SS-304
4525	13	-7.93	(-4525)	imp:n=1	\$SS-304
4526	13	-7.93	(-4526)	imp:n=1	\$SS-304
4527	13	-7.93	(-4527)	imp:n=1	\$SS-304
4528	13	-7.93	(-4528)	imp:n=1	\$SS-304
4529	3	-2.3	(-4529)	imp:n=1	\$Conc Filled
4530	3	-2.3	(-4530)	imp:n=1	\$Conc Filled
4531	3	-2.3	(-4531)	imp:n=1	\$Conc Filled
4532	3	-2.3	(-4532)	imp:n=1	\$Conc Filled
4533	3	-2.3	(-4533)	imp:n=1	\$Conc Filled
4534	3	-2.3	(-4534)	imp:n=1	\$Conc Filled
c 4535	3	-2.3	(-4535)	imp:n=1	\$Conc Filled

c

c

#### c Basement Room 34

3401	3	-2.3	(-3401)	imp:n=1	\$Conc Filled
3402	13	-7.93	(-3402)	imp:n=1	\$SS-304
3403	3	-2.3	(-3403)	imp:n=1	\$Conc Filled
3404	3	-2.3	(-3404)	imp:n=1	\$Conc Filled
3405	3	-2.3	(-3405)	imp:n=1	\$Conc Filled
3406	3	-2.3	(-3406)	imp:n=1	\$Conc Filled
3407	3	-2.3	(-3407)	imp:n=1	\$Conc Filled

c

c

c

#### c Basement Room 35

3501	3	-2.3	(-3501)	imp:n=1	\$Conc Filled
3502	3	-2.3	(-3502)	imp:n=1	\$Conc Filled
3503	3	-2.3	(-3503)	imp:n=1	\$Conc Filled
3504	3	-2.3	(-3504)	imp:n=1	\$Conc Filled
3505	13	-7.93	(-3505)	imp:n=1	\$SS-304
3506	3	-2.3	(-3506)	imp:n=1	\$Conc Filled
3507	3	-2.3	(-3507)	imp:n=1	\$Conc Filled

c

c

#### c Basement Room 36

3601	3	-2.3	(-3601)	imp:n=1	\$Conc Filled
3602	13	-7.93	(-3602)	imp:n=1	\$SS-304

c

c

#### c Basement Room 46

4601	3	-2.3	(-4601)	imp:n=1	\$Conc Filled
4602	3	-2.3	(-4602)	imp:n=1	\$Conc Filled
4603	3	-2.3	(-4603)	imp:n=1	\$Conc Filled
4604	3	-2.3	(-4604)	imp:n=1	\$Conc Filled

c

c

c

#### c Modular Shielded Storage Container E of Tank Vault

4610	13	-7.93	(-4610 4611)	imp:n=1	\$SS-304
------	----	-------	--------------	---------	----------

4611	1	-0.001202	(-4611)	imp:n=1	\$Air
------	---	-----------	---------	---------	-------

c

c

#### c Modular Shielded Storage Container W of Tank Vault

4612	13	-7.93	(-4612 4613)	imp:n=1	\$SS-304
------	----	-------	--------------	---------	----------

4613	1	-0.001202	(-4613)	imp:n=1	\$Air
------	---	-----------	---------	---------	-------

c

c

#### c Basement Room 43a 43 44

```

4301 3 -2.3 (-4301) imp:n=1 $Conc Filled
4302 3 -2.3 (-4302) imp:n=1 $Conc Filled
4303 3 -2.3 (-4303) imp:n=1 $Conc Filled
4304 3 -2.3 (-4304) imp:n=1 $Conc Filled
4305 3 -2.3 (-4305) imp:n=1 $Conc Filled
4306 3 -2.3 (-4306) imp:n=1 $Conc Filled
4307 3 -2.3 (-4307) imp:n=1 $Conc Filled
4308 13 -7.93 (-4308) imp:n=1 $SS-304
4309 3 -2.3 (-4309) imp:n=1 $Conc Filled
4310 3 -2.3 (-4310) imp:n=1 $Conc Filled
4311 3 -2.3 (-4311) imp:n=1 $Conc Filled
4312 3 -2.3 (-4312) imp:n=1 $Conc Filled

c
c
c
c
c

c Begin East Section of Basement1
c *****Notes for this section of Cells*****
c West Main structural wall was left out from this section to be
c included in a later model of the central basement area
4001 3 -2.3 (-4001) imp:n=1 $Conc Filled
4002 3 -2.3 (-4002) imp:n=1 $Conc Filled
4003 3 -2.3 (-4003) imp:n=1 $Conc Filled
4004 3 -2.3 (-4004) imp:n=1 $Conc Filled
4005 3 -2.3 (-4005) imp:n=1 $Conc Filled
4006 3 -2.3 (-4006) imp:n=1 $Conc Filled
4007 3 -2.3 (-4007) imp:n=1 $Conc Filled
4008 13 -7.93 (-4008) imp:n=1 $SS-304
4009 13 -7.93 (-4009) imp:n=1 $SS-304
4010 3 -2.3 (-4010) imp:n=1 $Conc Filled
4011 3 -2.3 (-4011) imp:n=1 $Conc Filled
4012 3 -2.3 (-4012) imp:n=1 $Conc Filled
4013 3 -2.3 (-4013) imp:n=1 $Conc Filled
4014 3 -2.3 (-4014) imp:n=1 $Conc Filled
4015 13 -7.93 (-4015) imp:n=1 $SS-304
4016 13 -7.93 (-4016) imp:n=1 $SS-304
4017 3 -2.3 (-4017) imp:n=1 $Conc Filled
4018 3 -2.3 (-4018) imp:n=1 $Conc Filled
4019 3 -2.3 (-4019) imp:n=1 $Conc Filled
4020 3 -2.3 (-4020) imp:n=1 $Conc Filled
4021 13 -7.93 (-4021) imp:n=1 $SS-304
4022 3 -2.3 (-4022) imp:n=1 $Conc Filled
4023 3 -2.3 (-4023) imp:n=1 $Conc Filled
4024 3 -2.3 (-4024) imp:n=1 $Conc Filled
4025 3 -2.3 (-4025) imp:n=1 $Conc Filled
4026 3 -2.3 (-4026) imp:n=1 $Conc Filled
4027 3 -2.3 (-4027) imp:n=1 $Conc Filled
4028 3 -2.3 (-4028) imp:n=1 $Conc Filled
4029 3 -2.3 (-4029) imp:n=1 $Conc Filled
4030 3 -2.3 (-4030) imp:n=1 $Conc Filled
4031 3 -2.3 (-4031) imp:n=1 $Conc Filled
4032 3 -2.3 (-4032) imp:n=1 $Conc Filled
4033 3 -2.3 (-4033) imp:n=1 $Conc Filled
4034 3 -2.3 (-4034) imp:n=1 $Conc Filled
4035 3 -2.3 (-4035) imp:n=1 $Conc Filled
4036 3 -2.3 (-4036) imp:n=1 $Conc Filled
4037 3 -2.3 (-4037) imp:n=1 $Conc Filled

c
c
c Basement1 Room 40/40A
4038 3 -2.3 (-4038) imp:n=1 $Conc Filled
4039 3 -2.3 (-4039) imp:n=1 $Conc Filled
4040 3 -2.3 (-4040) imp:n=1 $Conc Filled
4041 3 -2.3 (-4041) imp:n=1 $Conc Filled
4042 3 -2.3 (-4042) imp:n=1 $Conc Filled
4043 3 -2.3 (-4043) imp:n=1 $Conc Filled

c
c
c Basement Room 50/50A

```

```

5001 3 -2.3 (-5001) imp:n=1 $Conc Filled
5002 3 -2.3 (-5002) imp:n=1 $Conc Filled
5003 3 -2.3 (-5003) imp:n=1 $Conc Filled
5004 13 -7.93 (-5004) imp:n=1 $SS-304
5005 13 -7.93 (-5005) imp:n=1 $SS-304
5006 13 -7.93 (-5006) imp:n=1 $SS-304
5007 3 -2.3 (-5007) imp:n=1 $Conc Filled
5008 13 -7.93 (-5008) imp:n=1 $SS-304
5009 13 -7.93 (-5009) imp:n=1 $SS-304
5010 13 -7.93 (-5010) imp:n=1 $SS-304
5011 13 -7.93 (-5011) imp:n=1 $SS-304
5012 13 -7.93 (-5012) imp:n=1 $SS-304
5013 13 -7.93 (-5013) imp:n=1 $SS-304
5014 3 -2.3 (-5014) imp:n=1 $Conc Filled
5015 3 -2.3 (-5015) imp:n=1 $Conc Filled
5016 3 -2.3 (-5016) imp:n=1 $Conc Filled
5017 3 -2.3 (-5017) imp:n=1 $Conc Filled
5018 3 -2.3 (-5018) imp:n=1 $Conc Filled
c
c
c
c
c Begin South Section of Basement1
c *****Notes for this section of Cells*****
c
c
c Base1 Rm 7
701 5 0.00359833 (-701) imp:n=1 $Metal wl
702 5 0.00359833 (-702) imp:n=1 $Metal wl
703 5 0.00359833 (-703) imp:n=1 $Metal wl
704 5 0.00359833 (-704) imp:n=1 $Metal wl
705 5 0.00359833 (-705) imp:n=1 $Metal wl
706 5 0.00359833 (-706) imp:n=1 $Metal wl
707 5 0.00359833 (-707) imp:n=1 $Metal wl
708 3 -2.3 (-708) imp:n=1 $Conc Filled
709 3 -2.3 (-709) imp:n=1 $Conc Filled
710 3 -2.3 (-710) imp:n=1 $Conc Filled
711 3 -2.3 (-711) imp:n=1 $Conc Filled
712 3 -2.3 (-712) imp:n=1 $Conc Filled
713 3 -2.3 (-713) imp:n=1 $Conc Filled
714 3 -2.3 (-714) imp:n=1 $Conc Filled
715 3 -2.3 (-715) imp:n=1 $Conc Filled
716 3 -2.3 (-716) imp:n=1 $Conc Filled
717 3 -2.3 (-717) imp:n=1 $Conc Filled
718 3 -2.3 (-718) imp:n=1 $Conc Filled
719 3 -2.3 (-719) imp:n=1 $Conc Filled
720 3 -2.3 (-720) imp:n=1 $Conc Filled
721 3 -2.3 (-721) imp:n=1 $Conc Filled
722 3 -2.3 (-722) imp:n=1 $Conc Filled
723 3 -2.3 (-723) imp:n=1 $Conc Filled
724 3 -2.3 (-724) imp:n=1 $Conc Filled
c
c
c Base1 Rm 9
901 13 -7.93 (-901) imp:n=1 $SS-304
902 5 0.00359833 (-902) imp:n=1 $Metal wl
903 5 0.00359833 (-903) imp:n=1 $Metal wl
c
c
c Base1 Rm 11
1101 5 0.00359833 (-1101) imp:n=1 $Metal wl
1102 5 0.00359833 (-1102) imp:n=1 $Metal wl
c
c
c Base1 Room 13
1301 5 0.00359833 (-1301) imp:n=1 $Metal wl
1302 13 -7.93 (-1302) imp:n=1 $SS-304
1303 5 0.00359833 (-1303) imp:n=1 $Metal wl
c

```

c  
 c Base1 Room 15  
 1501 5 0.00359833 (-1501) imp:n=1 \$Metal wl  
 1502 5 0.00359833 (-1502) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 17  
 1701 5 0.00359833 (-1701) imp:n=1 \$Metal wl  
 1702 5 0.00359833 (-1702) imp:n=1 \$Metal wl  
 1703 5 0.00359833 (-1703) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 16  
 1601 5 0.00359833 (-1601) imp:n=1 \$Metal wl  
 1602 5 0.00359833 (-1602) imp:n=1 \$Metal wl  
 1603 5 0.00359833 (-1603) imp:n=1 \$Metal wl  
 1604 5 0.00359833 (-1604) imp:n=1 \$Metal wl  
 1605 5 0.00359833 (-1605) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 18  
 1801 5 0.00359833 (-1801) imp:n=1 \$Metal wl  
 1802 5 0.00359833 (-1802) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 20  
 2001 5 0.00359833 (-2001) imp:n=1 \$Metal wl  
 2002 5 0.00359833 (-2002) imp:n=1 \$Metal wl  
 2003 5 0.00359833 (-2003) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room  
 2004 5 0.00359833 (-2004) imp:n=1 \$Metal wl  
 2005 5 0.00359833 (-2005) imp:n=1 \$Metal wl  
 2006 5 0.00359833 (-2006) imp:n=1 \$Metal wl  
 2007 5 0.00359833 (-2007) imp:n=1 \$Metal wl  
 2008 5 0.00359833 (-2008) imp:n=1 \$Metal wl  
 2009 5 0.00359833 (-2009) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 26  
 2601 5 0.00359833 (-2601) imp:n=1 \$Metal wl  
 2602 5 0.00359833 (-2602) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 28  
 2801 5 0.00359833 (-2801) imp:n=1 \$Metal wl  
 2802 5 0.00359833 (-2802) imp:n=1 \$Metal wl  
 2803 5 0.00359833 (-2803) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 70  
 7001 5 0.00359833 (-7001) imp:n=1 \$Metal wl  
 7002 5 0.00359833 (-7002) imp:n=1 \$Metal wl  
 7003 13 -7.93 (-7003) imp:n=1 \$SS-304  
 7004 5 0.00359833 (-7004) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room 72  
 7201 5 0.00359833 (-7201) imp:n=1 \$Metal wl  
 7202 5 0.00359833 (-7202) imp:n=1 \$Metal wl  
 c  
 c  
 c Base1 Room  
 7401 5 0.00359833 (-7401) imp:n=1 \$Metal wl  
 7402 5 0.00359833 (-7402) imp:n=1 \$Metal wl  
 7403 13 -7.93 (-7403) imp:n=1 \$SS-304  
 c  
 c  
 c Base1 Room

7601 5 0.00359833 (-7601) imp:n=1 \$Metal wl  
 7602 5 0.00359833 (-7602) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room  
 7801 5 0.00359833 (-7801) imp:n=1 \$Metal wl  
 7802 5 0.00359833 (-7802) imp:n=1 \$Metal wl  
 7803 5 0.00359833 (-7803) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room 14  
 1401 5 0.00359833 (-1401) imp:n=1 \$Metal wl  
 1402 5 0.00359833 (-1402) imp:n=1 \$Metal wl  
 1403 5 0.00359833 (-1403) imp:n=1 \$Metal wl  
 1404 5 0.00359833 (-1404) imp:n=1 \$Metal wl  
 1405 5 0.00359833 (-1405) imp:n=1 \$Metal wl  
 1406 5 0.00359833 (-1406) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room 12  
 1201 5 0.00359833 (-1201) imp:n=1 \$Metal wl  
 1202 5 0.00359833 (-1202) imp:n=1 \$Metal wl  
 1203 13 -7.93 (-1203) imp:n=1 SSS-304  
 1204 5 0.00359833 (-1204) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room 10  
 1001 5 0.00359833 (-1001) imp:n=1 \$Metal wl  
 1002 5 0.00359833 (-1002) imp:n=1 \$Metal wl  
 1003 5 0.00359833 (-1003) imp:n=1 \$Metal wl  
 1004 5 0.00359833 (-1004) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room 27  
 2701 5 0.00359833 (-2701) imp:n=1 \$Metal wl  
 2702 5 0.00359833 (-2702) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room 25  
 2501 5 0.00359833 (-2501) imp:n=1 \$Metal wl  
 2502 5 0.00359833 (-2502) imp:n=1 \$Metal wl  
 2503 5 0.00359833 (-2503) imp:n=1 \$Metal wl  
 2504 5 0.00359833 (-2504) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room 8  
 801 5 0.00359833 (-801) imp:n=1 \$Metal wl  
 802 5 0.00359833 (-802) imp:n=1 \$Metal wl  
 803 5 0.00359833 (-803) imp:n=1 \$Metal wl  
 804 5 0.00359833 (-804) imp:n=1 \$Metal wl  
 805 5 0.00359833 (-805) imp:n=1 \$Metal wl  
 806 5 0.00359833 (-806) imp:n=1 \$Metal wl  
 c  
 c  
 c Basel Room 5  
 501 5 0.00359833 (-501) imp:n=1 \$Metal wl  
 502 5 0.00359833 (-502) imp:n=1 \$Metal wl  
 503 5 0.00359833 (-503) imp:n=1 \$Metal wl  
 504 13 -7.93 (-504) imp:n=1 SSS-304  
 505 5 0.00359833 (-505) imp:n=1 \$Metal wl  
 506 13 -7.93 (-506) imp:n=1 SSS-304  
 507 5 0.00359833 (-507) imp:n=1 \$Metal wl  
 508 5 0.00359833 (-508) imp:n=1 \$Metal wl  
 509 5 0.00359833 (-509) imp:n=1 \$Metal wl  
 510 5 0.00359833 (-510) imp:n=1 \$Metal wl  
 511 5 0.00359833 (-511) imp:n=1 \$Metal wl  
 512 5 0.00359833 (-512) imp:n=1 \$Metal wl  
 513 5 0.00359833 (-513) imp:n=1 \$Metal wl  
 514 5 0.00359833 (-514) imp:n=1 \$Metal wl  
 515 5 0.00359833 (-515) imp:n=1 \$Metal wl



```

725 6 -0.04855 (-725 ) imp:n=1 $Roomspace 7
904 6 -0.04855 (-904 901) imp:n=1 $Roomspace 9
1103 6 -0.04855 (-1103 901) imp:n=1 $Roomspace 11
1304 6 -0.04855 (-1304 1302) imp:n=1 $Roomspace 13
1503 6 -0.04855 (-1503 1302) imp:n=1 $Roomspace 15
1704 6 -0.04855 (-1704) imp:n=1 $Roomspace 17
1606 6 -0.04855 (-1606) imp:n=1 $Roomspace 16
1803 6 -0.04855 (-1803) imp:n=1 $Roomspace 18
2010 6 -0.04855 (-2010 2002) imp:n=1 $Roomspace 20
2011 6 -0.04855 (-2011) imp:n=1 $Roomspace Lunch Room
2603 6 -0.04855 (-2603) imp:n=1 $Roomspace 26
2804 1 -0.001202 (-2804) imp:n=1 $Roomspace 28 Partially Filled
7005 6 -0.04855 (-7005 7003) imp:n=1 $Roomspace 70
7203 6 -0.04855 (-7203 7003) imp:n=1 $Roomspace 72
7404 6 -0.04855 (-7404 7403) imp:n=1 $Roomspace 74
7603 6 -0.04855 (-7603 7403) imp:n=1 $Roomspace 76
7804 6 -0.04855 (-7804) imp:n=1 $Roomspace 78
1407 6 -0.04855 (-1407) imp:n=1 $Roomspace 14
1205 6 -0.04855 (-1205 1203) imp:n=1 $Roomspace 12
1005 6 -0.04855 (-1005 1203) imp:n=1 $Roomspace 10
2703 6 -0.04855 (-2703) imp:n=1 $Roomspace 27
2505 6 -0.04855 (-2505) imp:n=1 $Roomspace 25 Partially Filled
807 1 -0.001202 (-807 ) imp:n=1 $Roomspace 8 Partially Filled
518 6 -0.04855 (-518 506 504 516 517) imp:n=1 $Roomspace 5

c
c
c
c
c Cell that contains the entire basement and first floors
999 0 999 imp:n=0
c
c
c
c Void surrounding basement and first floors
990 0 (-999 990 991 992) imp:n=1 $Void
c
c
c Cell that combines all of Basement1 subsections
400 0 (-990 401 402 9009 9005 #9306 #9008 403 404 405
      4569 406 407 408 409 #5407 410 411 412 413 414
      415 416 417 418 419 420 421 422 423 424 425 426
      427 428 #713 #3216 #3217 430 431 432 433 434
) imp:n=1

c
c
c Begin the NW Central section of Basement1
401 1 -0.001202 (-401 4536 4537 4538 4539 4541 4542 4543 4544 4545
      4546 4547 4548 4549 4550 4551 4552 4553 4554 4555
      4556 4557 4558 5501 5502 5503 5504 5505 5506 5507
      5508 5509 5510 5511 5512 5513 5601 5602 5603 5604
      5514 5515 5516 5605 ) imp:n=1 $Air Filled $Section Box

c
c
c Begin North-Center Section of the Central Section of Basement1
402 1 -0.001202 (-402 9001 9002 9003 9004 9006 9007 9008 9010 9011 9012
      9013 9014 9015 9016 9101 9102 9103 9104 9105 9106 9107
      9108 9109 9301 9302 9303 9304 9305 9306 9307 9308 9309
      9310 9311 9312 9313 9314 9315 9316 9317 9318 9319 9017
) imp:n=1 $Air Filled $W Section Box

c
c
403 1 -0.001202 (-403 4560 4561 4562 4563 4564 4565 4566 4567 4568 #4569
      9701 9702 9703 9704 9705 9706 9707 9801 9401 9402 9403
      9404 9405 9406 9407 9408 9409 9410 9411 9412 9413 9501
      9502 9503 9504 9601 9602 9603 9604 9605 9606 9607 9414
      9415 9505 9608 9609 9708 9709 9802 #421
) imp:n=1 $Air Filled $NW Section Box

c
c
c Begin Northeast Section of the Central Section of Basement1

```

404 1 -0.001202 (-404 4575 4576 4577 5701 5702 5703 5704 5705 5706 5707  
     5708 5709 5710 5711 5712 5713 5801 5802 5803 5804 5805  
     5806 5807 5808 5809 5711 5712 5713 5809 4540 4545  
     ) imp:n=1 \$Air Filled \$SW Section Box  
 c  
 c  
 405 1 -0.001202 (-405 4578 4579 4580 4581 4582 4583 4801 4802 4803 4804  
     4805 4806 4807 4808 5401 5402 5403 5404 5405 5406 5408  
     5201 5202 5203 5204 5205 5206 5207 5408 5207  
     ) imp:n=1 \$Air Filled \$E Section Box  
 c  
 c  
 c Begin West Section of Basement1  
 406 1 -0.001202 (-406 2310 2311 2312 2313 2314 2315 2316 2317 2318 2319  
     2320 4501 4502 4503 4504 4505 4506 4507 4508 4509 3201  
     3202 3203 3204 3205 3206 3207 3208 3209 3210 3211 3212  
     3213 3214 3215 3217 2321 2322 #425  
     ) imp:n=1 \$Air Filled \$ Section Box  
 c  
 c  
 c Begin Southwest Section of the Central Section of Basement1  
 407 1 -0.001202 (-407 2201 2202 2203 2204 2205 2206 2207 2208 2209 2210  
     2211 2212 2213 2214 2215 2216 2217 2219 2220 2221  
     2301 2302 2303 2304 2305 3001 3002 3003 3004 3005 3006  
     3102 3103 3104 3106 3107 3108 3301 3302 3303  
     3304 3305 4584 4585 4586 4587 4588 4589 4590 4591 4592  
     4593 2222 2306 3007 3109 3110 3306 #3216 461 2230  
     2231 2232 2233 2234 2235 ) imp:n=1 \$Air Filled \$ Section Box  
 c  
 c 3101 3105 2218  
 c Begin Southeast Section of the Central Section of Basement1  
 408 1 -0.001202 (-408 4511 4512 4513 4514 4515 4516 4517 4518 4519 4520  
     4521 4522 4523 4524 4525 4526 4527 4528 4529 4530 4531  
     4532 4533 4534 3401 3402 3403 3404 3405 3406 3407  
     3501 3502 3503 3504 3505 3506 3507 3601 3602 4601 4602  
     4603 4604 4301 4302 4303 4304 4305 4306 4307 4308 4309  
     4310 4311 4312 3408 3508 3603 4605 4313 4314 4315 462  
     463 4610 4612 ) imp:n=1 \$Air Filled \$ Section Box  
 c  
 c  
 c Begin East Section of Basement1  
 409 1 -0.001202 (-409 4001 4002 4003 4004 4005 4006 4007 4008 4009 4010  
     4011 4012 4013 4014 4015 4016 4017 4018 4019 4020 4021  
     4022 4023 4024 4025 4026 4027 4028 4029 4030 4031 4032  
     4033 4034 4035 4036 4037 4038 4039 4040 4041 4042 4043  
     5001 5002 5003 5004 5005 5006 5007 5008 5009 5010 5011  
     5012 5013 5014 5015 5016 5017 5018 4045 4046 4044 5019  
     5020 #5407 #422) imp:n=1 \$Air Filled \$ Section Box  
 c  
 c  
 410 1 -0.001202 (-410 701 702 703 704 705 706 707 708 709 710 711 712  
     901 902 903 1101 1102 1301 1302 1303 1501 1502 1701  
     1702 1703 725 904 1103 1304 1503 1704 #423  
     ) imp:n=1 \$W Section Box  
 c  
 c  
 411 1 -0.001202 (-411 1601 1602 1603 1604 1605 1801 1802 2001 2002 2003  
     2004 2005 2006 2007 2008 2009 2601 2602 1606 1803 2010  
     2011 2603 714 715 716 717 718 719 720 #713 #2804 #423  
     ) imp:n=1 \$S Section Box  
 c  
 c  
 412 1 -0.001202 (-412 2801 2802 2803 7001 7002 7003 7004 7201 7202  
     7401 7402 7403 7601 7602 7801 7802 7803 2804 7005  
     7203 7404 7603 7804 #713 721 722 723 724 #423  
     ) imp:n=1 \$E Section Box  
 c  
 413 1 -0.001202 (-413 1001 1002 1003 1004 2701 2702 2501 2502 2503 2504  
     801 802 803 804 805 806 501 502 503 504 505 506 507  
     508 509 510 511 512 513 514 515 516 517 1401 1402 1403

1404 1405 1406 1201 1202 1203 1204 1407 1205 1005 2703  
2505 807 518 ) imp:n=1 \$Central Section Box

70310	5	0.00359833	(-70310)	imp:n=1	\$Metal wl
70311	5	0.00359833	(-70311)	imp:n=1	\$Metal wl
70312	5	0.00359833	(-70312)	imp:n=1	\$Metal wl
70313	5	0.00359833	(-70313)	imp:n=1	\$Metal wl
70314	5	0.00359833	(-70314)	imp:n=1	\$Metal wl
70315	5	0.00359833	(-70315)	imp:n=1	\$Metal wl
c					
c					
c Floor1 Room 320/421					
32001	5	0.00359833	(-32001)	imp:n=1	\$Air Filled
32002	5	0.00359833	(-32002)	imp:n=1	\$Metal wl
32003	5	0.00359833	(-32003)	imp:n=1	\$Metal wl
32004	5	0.00359833	(-32004)	imp:n=1	\$Metal wl
32005	5	0.00359833	(-32005)	imp:n=1	\$Metal wl
32006	5	0.00359833	(-32006)	imp:n=1	\$Metal wl
32007	5	0.00359833	(-32007)	imp:n=1	\$Metal wl
32008	5	0.00359833	(-32008)	imp:n=1	\$Metal wl
32009	5	0.00359833	(-32009)	imp:n=1	\$Metal wl
32010	5	0.00359833	(-32010)	imp:n=1	\$Metal wl
32011	5	0.00359833	(-32011)	imp:n=1	\$Metal wl
32012	5	0.00359833	(-32012)	imp:n=1	\$Metal wl
32013	5	0.00359833	(-32013)	imp:n=1	\$Metal wl
32014	5	0.00359833	(-32014)	imp:n=1	\$Metal wl
32015	5	0.00359833	(-32015)	imp:n=1	\$Metal wl
32016	5	0.00359833	(-32016)	imp:n=1	\$Metal wl
c					
c					
c Floor1 Room 324/425					
32401	1	-0.001202	(-32401)	imp:n=1	\$Air Filled
32402	5	0.00359833	(-32402 32401)	imp:n=1	\$Metal wl
32403	1	-0.001202	(-32403)	imp:n=1	\$Air Filled
32404	5	0.00359833	(-32404 32403)	imp:n=1	\$Metal wl
32405	5	0.00359833	(-32405)	imp:n=1	\$Metal wl
32406	5	0.00359833	(-32406)	imp:n=1	\$Metal wl
32407	1	-0.001202	(-32407)	imp:n=1	\$Air Filled
32408	5	0.00359833	(-32408 32407)	imp:n=1	\$Metal wl
32409	5	0.00359833	(-32409)	imp:n=1	\$Metal wl
32410	5	0.00359833	(-32410)	imp:n=1	\$Metal wl
32411	5	0.00359833	(-32411)	imp:n=1	\$Metal wl
32412	5	0.00359833	(-32412)	imp:n=1	\$Metal wl
32413	5	0.00359833	(-32413)	imp:n=1	\$Metal wl
32414	1	-0.001202	(-32414)	imp:n=1	\$Air Filled
32415	5	0.00359833	(-32415 32414)	imp:n=1	\$Metal wl
32416	5	0.00359833	(-32416)	imp:n=1	\$Metal wl
32417	5	0.00359833	(-32417)	imp:n=1	\$Metal wl
c					
c					
c Floor1 Room 325/Filter Building					
32501	5	0.00359833	(-32501)	imp:n=1	\$Metal wl
32502	5	0.00359833	(-32502)	imp:n=1	\$Metal wl
32503	5	0.00359833	(-32503)	imp:n=1	\$Metal wl
32504	5	0.00359833	(-32504)	imp:n=1	\$Metal wl
32505	5	0.00359833	(-32505)	imp:n=1	\$Metal wl
32506	5	0.00359833	(-32506)	imp:n=1	\$Metal wl
32507	5	0.00359833	(-32507)	imp:n=1	\$Metal wl
32508	5	0.00359833	(-32508)	imp:n=1	\$Metal wl
32509	5	0.00359833	(-32509)	imp:n=1	\$Metal wl
32510	5	0.00359833	(-32510)	imp:n=1	\$Metal wl
32511	5	0.00359833	(-32511)	imp:n=1	\$Metal wl
32512	5	0.00359833	(-32512)	imp:n=1	\$Metal wl
32513	5	0.00359833	(-32513)	imp:n=1	\$Metal wl
32514	5	0.00359833	(-32514)	imp:n=1	\$Metal wl
32515	5	0.00359833	(-32515)	imp:n=1	\$Metal wl
32516	5	0.00359833	(-32516)	imp:n=1	\$Metal wl
32517	5	0.00359833	(-32517)	imp:n=1	\$Metal wl
32518	5	0.00359833	(-32518)	imp:n=1	\$Metal wl
32519	5	0.00359833	(-32519)	imp:n=1	\$Metal wl
32520	5	0.00359833	(-32520)	imp:n=1	\$Metal wl
32521	5	0.00359833	(-32521)	imp:n=1	\$Metal wl
32522	5	0.00359833	(-32522)	imp:n=1	\$Metal wl

c  
 c  
 c Floor1 Room 330/427/Elevator  
 33001 5 0.00359833 (-33001) imp:n=1 \$Ext wl Filled  
 33002 5 0.00359833 (-33002) imp:n=1 \$Metal wl  
 33003 5 0.00359833 (-33003) imp:n=1 \$Metal wl  
 33004 5 0.00359833 (-33004) imp:n=1 \$Metal wl  
 33005 5 0.00359833 (-33005) imp:n=1 \$Metal wl  
 33006 5 0.00359833 (-33006) imp:n=1 \$Metal wl  
 33007 5 0.00359833 (-33007) imp:n=1 \$Metal wl  
 33008 5 0.00359833 (-33008) imp:n=1 \$Metal wl  
 33009 5 0.00359833 (-33009) imp:n=1 \$Metal wl  
 33010 5 0.00359833 (-33010) imp:n=1 \$Metal wl  
 33011 5 0.00359833 (-33011) imp:n=1 \$Metal wl  
 33012 5 0.00359833 (-33012) imp:n=1 \$Metal wl  
 33013 5 0.00359833 (-33013) imp:n=1 \$Metal wl  
 33014 5 0.00359833 (-33014) imp:n=1 \$Metal wl  
 33015 5 0.00359833 (-33015) imp:n=1 \$Metal wl  
 33016 5 0.00359833 (-33016) imp:n=1 \$Metal wl  
 33017 5 0.00359833 (-33017) imp:n=1 \$Metal wl  
 33018 5 0.00359833 (-33018) imp:n=1 \$Metal wl  
 33019 5 0.00359833 (-33019) imp:n=1 \$Metal wl  
 33020 5 0.00359833 (-33020) imp:n=1 \$Metal wl  
 33021 5 0.00359833 (-33021) imp:n=1 \$Metal wl  
 33022 5 0.00359833 (-33022) imp:n=1 \$Metal wl  
 33023 5 0.00359833 (-33023) imp:n=1 \$Metal wl  
 33024 5 0.00359833 (-33024) imp:n=1 \$Metal wl  
 33025 5 0.00359833 (-33025) imp:n=1 \$Metal wl  
 33026 5 0.00359833 (-33026) imp:n=1 \$Metal wl  
 33027 5 0.00359833 (-33027) imp:n=1 \$Metal wl  
 33028 5 0.00359833 (-33028) imp:n=1 \$Metal wl  
 33031 15 -0.4751 (-33031) imp:n=1 \$Ext wl Filled  
 33032 15 -0.4751 (-33032) imp:n=1 \$Ext wl Filled  
 c  
 c  
 c Floor1 Room 327/327A  
 32701 5 0.00359833 (-32701) imp:n=1 \$Metal wl  
 32702 5 0.00359833 (-32702) imp:n=1 \$Metal wl  
 32703 5 0.00359833 (-32703) imp:n=1 \$Metal wl  
 32704 5 0.00359833 (-32704) imp:n=1 \$Metal wl  
 32705 5 0.00359833 (-32705) imp:n=1 \$Metal wl  
 32706 5 0.00359833 (-32706) imp:n=1 \$Metal wl  
 32707 5 0.00359833 (-32707) imp:n=1 \$Metal wl  
 32708 5 0.00359833 (-32708) imp:n=1 \$Metal wl  
 32709 5 0.00359833 (-32709) imp:n=1 \$Metal wl  
 32710 5 0.00359833 (-32710) imp:n=1 \$Metal wl  
 32711 5 0.00359833 (-32711) imp:n=1 \$Metal wl  
 32712 5 0.00359833 (-32712) imp:n=1 \$Metal wl  
 32713 5 0.00359833 (-32713) imp:n=1 \$Metal wl  
 32714 5 0.00359833 (-32714) imp:n=1 \$Metal wl  
 32715 5 0.00359833 (-32715) imp:n=1 \$Metal wl  
 32718 15 -0.4751 (-32718) imp:n=1 \$Ext wl Filled  
 c  
 c  
 c /////////////Begin Northeast Section of the central Section of Flo  
 c \*\*\*\*\*Notes for this section of Cells\*\*\*\*\*  
 c The origin was set as the SW corner of the inside wall of Room  
 c  
 c  
 c Floor1 Room 711/Womens Rm  
 c \*\*\*\*\*Wall on W of womens rm ignored  
 71101 5 0.00359833 (-71101) imp:n=1 \$Metal wl  
 71102 5 0.00359833 (-71102) imp:n=1 \$Metal wl  
 71103 5 0.00359833 (-71103) imp:n=1 \$Metal wl  
 71104 5 0.00359833 (-71104) imp:n=1 \$Metal wl  
 71105 5 0.00359833 (-71105) imp:n=1 \$Metal wl  
 71106 5 0.00359833 (-71106) imp:n=1 \$Metal wl  
 71107 5 0.00359833 (-71107) imp:n=1 \$Metal wl  
 71108 5 0.00359833 (-71108) imp:n=1 \$Metal wl

71109 5 0.00359833 (-71109) imp:n=1 \$Metal wl  
71110 5 0.00359833 (-71110) imp:n=1 \$Metal wl  
71111 5 0.00359833 (-71111) imp:n=1 \$Metal wl  
71112 5 0.00359833 (-71112) imp:n=1 \$Metal wl  
71113 5 0.00359833 (-71113) imp:n=1 \$Metal wl  
71114 5 0.00359833 (-71114) imp:n=1 \$Metal wl

c

c

c Floor1 Room 420

42001 5 0.00359833 (-42001) imp:n=1 \$Metal wl  
42002 5 0.00359833 (-42002) imp:n=1 \$Metal wl  
42003 5 0.00359833 (-42003) imp:n=1 \$Metal wl  
42004 5 0.00359833 (-42004) imp:n=1 \$Metal wl  
42005 5 0.00359833 (-42005) imp:n=1 \$Metal wl  
42006 5 0.00359833 (-42006) imp:n=1 \$Metal wl  
42007 5 0.00359833 (-42007) imp:n=1 \$Metal wl  
42008 5 0.00359833 (-42008) imp:n=1 \$Metal wl  
42009 5 0.00359833 (-42009) imp:n=1 \$Metal wl  
42010 5 0.00359833 (-42010) imp:n=1 \$Metal wl  
42011 5 0.00359833 (-42011) imp:n=1 \$Metal wl  
42012 5 0.00359833 (-42012) imp:n=1 \$Metal wl

c

c

c Floor1 Room 525/Freezer

52501 5 0.00359833 (-52501) imp:n=1 \$Metal wl  
52502 5 0.00359833 (-52502) imp:n=1 \$Metal wl  
52503 5 0.00359833 (-52503) imp:n=1 \$Metal wl  
52504 5 0.00359833 (-52504) imp:n=1 \$Metal wl  
52505 5 0.00359833 (-52505) imp:n=1 \$Metal wl  
52506 5 0.00359833 (-52506) imp:n=1 \$Metal wl  
52507 5 0.00359833 (-52507) imp:n=1 \$Metal wl  
52508 5 0.00359833 (-52508) imp:n=1 \$Metal wl  
52509 5 0.00359833 (-52509) imp:n=1 \$Metal wl  
52510 5 0.00359833 (-52510) imp:n=1 \$Metal wl  
52511 5 0.00359833 (-52511) imp:n=1 \$Metal wl  
52512 5 0.00359833 (-52512) imp:n=1 \$Metal wl  
52513 5 0.00359833 (-52513) imp:n=1 \$Metal wl  
52514 5 0.00359833 (-52514) imp:n=1 \$Metal wl  
52515 5 0.00359833 (-52515) imp:n=1 \$Metal wl  
52516 5 0.00359833 (-52516) imp:n=1 \$Metal wl  
52517 5 0.00359833 (-52517) imp:n=1 \$Metal wl  
52518 5 0.00359833 (-52518) imp:n=1 \$Metal wl  
52519 5 0.00359833 (-52519) imp:n=1 \$Metal wl

c

c

c Floor1 Room 426/426A

42601 5 0.00359833 (-42601) imp:n=1 \$Metal wl  
42602 5 0.00359833 (-42602) imp:n=1 \$Metal wl  
42603 5 0.00359833 (-42603) imp:n=1 \$Metal wl  
42604 5 0.00359833 (-42604) imp:n=1 \$Metal wl  
42605 5 0.00359833 (-42605) imp:n=1 \$Metal wl  
42606 5 0.00359833 (-42606) imp:n=1 \$Metal wl  
42607 5 0.00359833 (-42607) imp:n=1 \$Metal wl  
42608 5 0.00359833 (-42608) imp:n=1 \$Metal wl  
42609 5 0.00359833 (-42609) imp:n=1 \$Metal wl  
42610 5 0.00359833 (-42610) imp:n=1 \$Metal wl  
42611 5 0.00359833 (-42611) imp:n=1 \$Metal wl  
42612 5 0.00359833 (-42612) imp:n=1 \$Metal wl  
42613 5 0.00359833 (-42613) imp:n=1 \$Metal wl  
42614 5 0.00359833 (-42614) imp:n=1 \$Metal wl  
42615 5 0.00359833 (-42615) imp:n=1 \$Metal wl  
42616 5 0.00359833 (-42616) imp:n=1 \$Metal wl  
42617 5 0.00359833 (-42617) imp:n=1 \$Metal wl  
42618 5 0.00359833 (-42618) imp:n=1 \$Metal wl  
42619 5 0.00359833 (-42619) imp:n=1 \$Metal wl

c

c

c Floor1 Room 430/Receiving Room

43001 5 0.00359833 (-43001) imp:n=1 \$Metal wl  
43002 5 0.00359833 (-43002) imp:n=1 \$Metal wl

43003	5	0.00359833	(-43003)	imp:n=1	\$Metal wl
43004	5	0.00359833	(-43004)	imp:n=1	\$Metal wl
43005	5	0.00359833	(-43005)	imp:n=1	\$Metal wl
43006	5	0.00359833	(-43006)	imp:n=1	\$Metal wl
43007	5	0.00359833	(-43007)	imp:n=1	\$Metal wl
43008	5	0.00359833	(-43008)	imp:n=1	\$Metal wl
43009	5	0.00359833	(-43009)	imp:n=1	\$Metal wl
43010	5	0.00359833	(-43010)	imp:n=1	\$Metal wl
43011	5	0.00359833	(-43011)	imp:n=1	\$Metal wl
43012	5	0.00359833	(-43012)	imp:n=1	\$Metal wl
43013	5	0.00359833	(-43013)	imp:n=1	\$Metal wl
43015	15	-0.4751	(-43015)	imp:n=1	\$Ext wl Filled

c

c

c Floor1 Room 527/527A

52701	5	0.00359833	(-52701)	imp:n=1	\$Metal wl
52702	5	0.00359833	(-52702)	imp:n=1	\$Metal wl
52703	5	0.00359833	(-52703)	imp:n=1	\$Metal wl
52704	5	0.00359833	(-52704)	imp:n=1	\$Metal wl
52705	5	0.00359833	(-52705)	imp:n=1	\$Metal wl
52706	5	0.00359833	(-52706)	imp:n=1	\$Metal wl
52707	5	0.00359833	(-52707)	imp:n=1	\$Metal wl
52708	5	0.00359833	(-52708)	imp:n=1	\$Metal wl
52709	5	0.00359833	(-52709)	imp:n=1	\$Metal wl
52710	5	0.00359833	(-52710)	imp:n=1	\$Metal wl
52711	5	0.00359833	(-52711)	imp:n=1	\$Metal wl
52712	5	0.00359833	(-52712)	imp:n=1	\$Metal wl
52713	5	0.00359833	(-52713)	imp:n=1	\$Metal wl
52714	5	0.00359833	(-52714)	imp:n=1	\$Metal wl
52715	5	0.00359833	(-52715)	imp:n=1	\$Metal wl
52716	5	0.00359833	(-52716)	imp:n=1	\$Metal wl
52717	5	0.00359833	(-52717)	imp:n=1	\$Metal wl
52718	5	0.00359833	(-52718)	imp:n=1	\$Metal wl
52719	5	0.00359833	(-52719)	imp:n=1	\$Metal wl
52720	5	0.00359833	(-52720)	imp:n=1	\$Metal wl
52721	5	0.00359833	(-52721)	imp:n=1	\$Metal wl
52722	5	0.00359833	(-52722)	imp:n=1	\$Metal wl
52723	5	0.00359833	(-52723)	imp:n=1	\$Metal wl
52726	15	-0.4751	(-52726)	imp:n=1	\$Ext wl Filled

c

c

c Floor1 Room 529

52901	5	0.00359833	(-52901)	imp:n=1	\$Metal wl
52902	5	0.00359833	(-52902)	imp:n=1	\$Metal wl
52903	5	0.00359833	(-52903)	imp:n=1	\$Metal wl
52904	5	0.00359833	(-52904)	imp:n=1	\$Metal wl
52905	5	0.00359833	(-52905)	imp:n=1	\$Metal wl
52906	5	0.00359833	(-52906)	imp:n=1	\$Metal wl
52907	5	0.00359833	(-52907)	imp:n=1	\$Metal wl
52908	5	0.00359833	(-52908)	imp:n=1	\$Metal wl
52909	5	0.00359833	(-52909)	imp:n=1	\$Metal wl
52910	5	0.00359833	(-52910)	imp:n=1	\$Metal wl
52911	5	0.00359833	(-52911)	imp:n=1	\$Metal wl
52912	5	0.00359833	(-52912)	imp:n=1	\$Metal wl
52913	5	0.00359833	(-52913)	imp:n=1	\$Metal wl
52914	3	-2.3	(-52914)	imp:n=1	\$Conc. Filled
52915	3	-2.3	(-52915)	imp:n=1	\$Conc. Filled

c

c

c Floor1 Room 520

52001	5	0.00359833	(-52001)	imp:n=1	\$Metal wl
52002	5	0.00359833	(-52002)	imp:n=1	\$Metal wl
52003	5	0.00359833	(-52003)	imp:n=1	\$Metal wl
52004	5	0.00359833	(-52004)	imp:n=1	\$Metal wl
52005	5	0.00359833	(-52005)	imp:n=1	\$Metal wl
52006	5	0.00359833	(-52006)	imp:n=1	\$Metal wl
52007	5	0.00359833	(-52007)	imp:n=1	\$Metal wl
52008	5	0.00359833	(-52008)	imp:n=1	\$Metal wl
52009	5	0.00359833	(-52009)	imp:n=1	\$Metal wl
52010	5	0.00359833	(-52010)	imp:n=1	\$Metal wl

52011 5 0.00359833 (-52011) imp:n=1 \$Metal wl  
 52012 5 0.00359833 (-52012) imp:n=1 \$Metal wl  
 52013 5 0.00359833 (-52013) imp:n=1 \$Metal wl  
 52014 5 0.00359833 (-52014) imp:n=1 \$Metal wl  
 52015 5 0.00359833 (-52015) imp:n=1 \$Metal wl  
 c  
 c Floor1 Room 524  
 52401 5 0.00359833 (-52401) imp:n=1 \$Metal wl  
 52402 5 0.00359833 (-52402) imp:n=1 \$Metal wl  
 52403 5 0.00359833 (-52403) imp:n=1 \$Metal wl  
 52404 5 0.00359833 (-52404) imp:n=1 \$Metal wl  
 52405 5 0.00359833 (-52405) imp:n=1 \$Metal wl  
 52406 5 0.00359833 (-52406) imp:n=1 \$Metal wl  
 52407 5 0.00359833 (-52407) imp:n=1 \$Metal wl  
 52408 5 0.00359833 (-52408) imp:n=1 \$Metal wl  
 52409 5 0.00359833 (-52409) imp:n=1 \$Metal wl  
 c  
 c  
 c Floor1 Room 528  
 52801 5 0.00359833 (-52801) imp:n=1 \$Metal wl  
 52802 5 0.00359833 (-52802) imp:n=1 \$Metal wl  
 52803 5 0.00359833 (-52803) imp:n=1 \$Metal wl  
 52804 5 0.00359833 (-52804) imp:n=1 \$Metal wl  
 52805 5 0.00359833 (-52805) imp:n=1 \$Metal wl  
 52806 5 0.00359833 (-52806) imp:n=1 \$Metal wl  
 52807 5 0.00359833 (-52807) imp:n=1 \$Metal wl  
 52808 5 0.00359833 (-52808) imp:n=1 \$Metal wl  
 52809 15 -0.4751 (-52809) imp:n=1 \$Ext wl Filled  
 52810 5 0.00359833 (-52810) imp:n=1 \$Metal wl  
 52812 15 -0.4751 (-52812) imp:n=1 \$Ext wl Filled  
 c  
 c  
 c Floor1 Room 530/North Cylinder Dock  
 53001 5 0.00359833 (-53001) imp:n=1 \$Metal wl  
 53002 5 0.00359833 (-53002) imp:n=1 \$Metal wl  
 53003 5 0.00359833 (-53003) imp:n=1 \$Metal wl  
 53004 5 0.00359833 (-53004) imp:n=1 \$Metal wl  
 53005 5 0.00359833 (-53005) imp:n=1 \$Metal wl  
 53006 5 0.00359833 (-53006) imp:n=1 \$Metal wl  
 53007 5 0.00359833 (-53007) imp:n=1 \$Metal wl  
 53008 5 0.00359833 (-53008) imp:n=1 \$Metal wl  
 53009 3 -2.3 (-53009) imp:n=1 \$Conc. Filled  
 53010 3 -2.3 (-53010) imp:n=1 \$Conc. Filled  
 53011 3 -2.3 (-53011) imp:n=1 \$Conc. Filled  
 53012 3 -2.3 (-53012) imp:n=1 \$Conc. Filled  
 53013 3 -2.3 (-53013) imp:n=1 \$Conc. Filled  
 53014 3 -2.3 (-53014) imp:n=1 \$Conc. Filled  
 53015 3 -2.3 (-53015) imp:n=1 \$Conc. Filled  
 53016 5 0.00359833 (-53016) imp:n=1 \$Metal wl  
 53018 15 -0.4751 (-53018) imp:n=1 \$Ext wl Filled  
 c  
 c  
 c  
 c //Begin West Section of Floor1//  
 c \*\*\*\*\*Notes for this section of Cells\*\*\*\*\*  
 c The origin was set as the SW corner of the inside wall of Room  
 c  
 c  
 c  
 c Floor1 Room 209  
 20901 5 0.00359833 (-20901) imp:n=1 \$Metal wl  
 20902 5 0.00359833 (-20902) imp:n=1 \$Metal wl  
 20903 5 0.00359833 (-20903) imp:n=1 \$Metal wl  
 20904 5 0.00359833 (-20904) imp:n=1 \$Metal wl  
 20905 5 0.00359833 (-20905) imp:n=1 \$Metal wl  
 20906 5 0.00359833 (-20906) imp:n=1 \$Metal wl  
 20907 5 0.00359833 (-20907) imp:n=1 \$Metal wl  
 20908 5 0.00359833 (-20908) imp:n=1 \$Metal wl  
 20909 13 -7.92 (-20909) imp:n=1 \$\$S  
 20910 5 0.00359833 (-20910) imp:n=1 \$Metal wl

20911 5 0.00359833 (-20911) imp:n=1 \$Metal wl  
 20912 5 0.00359833 (-20912) imp:n=1 \$Metal wl  
 20913 5 0.00359833 (-20913) imp:n=1 \$Metal wl  
 20914 5 0.00359833 (-20914) imp:n=1 \$Metal wl  
 20915 5 0.00359833 (-20915) imp:n=1 \$Metal wl  
 20916 5 0.00359833 (-20916) imp:n=1 \$Metal wl  
 20917 5 0.00359833 (-20917) imp:n=1 \$Metal wl  
 20918 5 0.00359833 (-20918) imp:n=1 \$Metal wl  
 20920 5 0.00359833 (-20920) imp:n=1 \$Metal wl  
 20921 15 -0.4751 (-20921) imp:n=1 \$Ext wl Filled  
 20922 15 -0.4751 (-20922) imp:n=1 \$Ext wl Filled

c

c

c Floor1 Room 202/203

20201 5 0.00359833 (-20201) imp:n=1 \$Metal wl  
 20202 5 0.00359833 (-20202) imp:n=1 \$Metal wl  
 20203 15 -0.4751 (-20203) imp:n=1 \$Ext wl Filled  
 20204 5 0.00359833 (-20204) imp:n=1 \$Metal wl  
 20205 15 -0.4751 (-20205) imp:n=1 \$Ext wl Filled  
 20206 5 0.00359833 (-20206) imp:n=1 \$Metal wl  
 20207 5 0.00359833 (-20207) imp:n=1 \$Metal wl  
 20208 5 0.00359833 (-20208) imp:n=1 \$Metal wl  
 20209 5 0.00359833 (-20209) imp:n=1 \$Metal wl  
 20210 5 0.00359833 (-20210) imp:n=1 \$Metal wl  
 20211 5 0.00359833 (-20211) imp:n=1 \$Metal wl  
 20212 5 0.00359833 (-20212) imp:n=1 \$Metal wl  
 20213 5 0.00359833 (-20213) imp:n=1 \$Metal wl  
 20214 5 0.00359833 (-20214) imp:n=1 \$Metal wl  
 20215 5 0.00359833 (-20215) imp:n=1 \$Metal wl  
 20216 5 0.00359833 (-20216) imp:n=1 \$Metal wl  
 20217 5 0.00359833 (-20217) imp:n=1 \$Metal wl  
 20218 5 0.00359833 (-20218) imp:n=1 \$Metal wl  
 20219 5 0.00359833 (-20219) imp:n=1 \$Metal wl  
 20220 15 -0.4751 (-20220) imp:n=1 \$Ext wl Filled

c

c

c Floor1 Room 200

20001 5 0.00359833 (-20001) imp:n=1 \$Metal wl  
 20002 5 0.00359833 (-20002) imp:n=1 \$Metal wl  
 20003 5 0.00359833 (-20003) imp:n=1 \$Metal wl  
 20004 5 0.00359833 (-20004) imp:n=1 \$Metal wl  
 20005 5 0.00359833 (-20005) imp:n=1 \$Metal wl  
 20006 5 0.00359833 (-20006) imp:n=1 \$Metal wl  
 20007 5 0.00359833 (-20007) imp:n=1 \$Metal wl  
 20008 5 0.00359833 (-20008) imp:n=1 \$Metal wl  
 20009 5 0.00359833 (-20009) imp:n=1 \$Metal wl  
 20010 5 0.00359833 (-20010) imp:n=1 \$Metal wl  
 20011 5 0.00359833 (-20011) imp:n=1 \$Metal wl  
 20012 5 0.00359833 (-20012) imp:n=1 \$Metal wl  
 20013 5 0.00359833 (-20013) imp:n=1 \$Metal wl  
 20014 5 0.00359833 (-20014) imp:n=1 \$Metal wl

c

c

c Floor1 Room 201

c \*\*\*\*\*This room contains the SAL hot cellsL\*\*\*\*\*

c Neglected thin wall strip in NE border region

20101 13 -7.92 (-20101) imp:n=1 \$\$S  
 20102 5 0.00359833 (-20102) imp:n=1 \$Metal wl  
 20103 13 -7.92 (-20103) imp:n=1 \$\$S  
 20104 13 -7.92 (-20104) imp:n=1 \$\$S  
 20105 5 0.00359833 (-20105) imp:n=1 \$Metal wl  
 20106 5 0.00359833 (-20106) imp:n=1 \$Metal wl  
 20107 5 0.00359833 (-20107) imp:n=1 \$Metal wl  
 20108 5 0.00359833 (-20108) imp:n=1 \$Metal wl  
 20109 5 0.00359833 (-20109) imp:n=1 \$Metal wl  
 20110 5 0.00359833 (-20110) imp:n=1 \$Metal wl  
 20111 5 0.00359833 (-20111) imp:n=1 \$Metal wl  
 20112 15 -0.4751 (-20112) imp:n=1 \$Ext wl Filled  
 20113 5 0.00359833 (-20113) imp:n=1 \$Metal wl  
 20114 5 0.00359833 (-20114) imp:n=1 \$Metal wl



31303	5	0.00359833	(-31303)	imp:n=1	\$Metal wl
31304	5	0.00359833	(-31304)	imp:n=1	\$Metal wl
31305	5	0.00359833	(-31305)	imp:n=1	\$Metal wl
31306	5	0.00359833	(-31306)	imp:n=1	\$Metal wl
31307	5	0.00359833	(-31307)	imp:n=1	\$Metal wl
31308	5	0.00359833	(-31308)	imp:n=1	\$Metal wl
31309	5	0.00359833	(-31309)	imp:n=1	\$Metal wl
31310	5	0.00359833	(-31310)	imp:n=1	\$Metal wl
31311	5	0.00359833	(-31311)	imp:n=1	\$Metal wl
31312	5	0.00359833	(-31312)	imp:n=1	\$Metal wl
c					
c					
c Floor1 Room 317					
31701	5	0.00359833	(-31701)	imp:n=1	\$Metal wl
31702	5	0.00359833	(-31702)	imp:n=1	\$Metal wl
31703	5	0.00359833	(-31703)	imp:n=1	\$Metal wl
c					
c					
c Floor1 Room 319/319A					
31901	5	0.00359833	(-31901)	imp:n=1	\$Metal wl
31902	5	0.00359833	(-31902)	imp:n=1	\$Metal wl
31903	5	0.00359833	(-31903)	imp:n=1	\$Metal wl
31904	5	0.00359833	(-31904)	imp:n=1	\$Metal wl
31905	5	0.00359833	(-31905)	imp:n=1	\$Metal wl
31906	5	0.00359833	(-31906)	imp:n=1	\$Metal wl
31907	5	0.00359833	(-31907)	imp:n=1	\$Metal wl
31908	5	0.00359833	(-31908)	imp:n=1	\$Metal wl
31909	5	0.00359833	(-31909)	imp:n=1	\$Metal wl
31910	5	0.00359833	(-31910)	imp:n=1	\$Metal wl
31911	5	0.00359833	(-31911)	imp:n=1	\$Metal wl
c					
c					
c Floor1 Room 300					
30001	5	0.00359833	(-30001)	imp:n=1	\$Metal wl
30002	5	0.00359833	(-30002)	imp:n=1	\$Metal wl
30003	5	0.00359833	(-30003)	imp:n=1	\$Metal wl
30004	5	0.00359833	(-30004)	imp:n=1	\$Metal wl
30005	5	0.00359833	(-30005)	imp:n=1	\$Metal wl
30006	5	0.00359833	(-30006)	imp:n=1	\$Metal wl
30007	5	0.00359833	(-30007)	imp:n=1	\$Metal wl
30008	5	0.00359833	(-30008)	imp:n=1	\$Metal wl
30009	5	0.00359833	(-30009)	imp:n=1	\$Metal wl
30010	5	0.00359833	(-30010)	imp:n=1	\$Metal wl
30011	5	0.00359833	(-30011)	imp:n=1	\$Metal wl
30012	5	0.00359833	(-30012)	imp:n=1	\$Metal wl
30013	5	0.00359833	(-30013)	imp:n=1	\$Metal wl
30014	5	0.00359833	(-30014)	imp:n=1	\$Metal wl
30015	5	0.00359833	(-30015)	imp:n=1	\$Metal wl
30016	5	0.00359833	(-30016)	imp:n=1	\$Metal wl
30017	5	0.00359833	(-30017)	imp:n=1	\$Metal wl
30018	5	0.00359833	(-30018)	imp:n=1	\$Metal wl
30019	5	0.00359833	(-30019)	imp:n=1	\$Metal wl
30020	5	0.00359833	(-30020)	imp:n=1	\$Metal wl
30021	5	0.00359833	(-30021)	imp:n=1	\$Metal wl
30022	5	0.00359833	(-30022)	imp:n=1	\$Metal wl
30023	5	0.00359833	(-30023)	imp:n=1	\$Metal wl
c					
c					
c					
c Floor1 Room 306					
30601	5	0.00359833	(-30601)	imp:n=1	\$Metal wl
30602	5	0.00359833	(-30602)	imp:n=1	\$Metal wl
30603	5	0.00359833	(-30603)	imp:n=1	\$Metal wl
30604	5	0.00359833	(-30604)	imp:n=1	\$Metal wl
30605	5	0.00359833	(-30605)	imp:n=1	\$Metal wl
30606	5	0.00359833	(-30606)	imp:n=1	\$Metal wl
30607	5	0.00359833	(-30607)	imp:n=1	\$Metal wl
30608	5	0.00359833	(-30608)	imp:n=1	\$Metal wl
30609	5	0.00359833	(-30609)	imp:n=1	\$Metal wl
30610	5	0.00359833	(-30610)	imp:n=1	\$Metal wl

30611 5 0.00359833 (-30611) imp:n=1 \$Metal wl  
 c  
 c  
 c Floor1 Room 310  
 31001 5 0.00359833 (-31001) imp:n=1 \$Metal wl  
 31002 5 0.00359833 (-31002) imp:n=1 \$Metal wl  
 31003 5 0.00359833 (-31003) imp:n=1 \$Metal wl  
 31004 5 0.00359833 (-31004) imp:n=1 \$Metal wl  
 31005 5 0.00359833 (-31005) imp:n=1 \$Metal wl  
 c  
 c  
 c Floor1 Room 312  
 31201 5 0.00359833 (-31201) imp:n=1 \$Metal wl  
 31202 5 0.00359833 (-31202) imp:n=1 \$Metal wl  
 31203 5 0.00359833 (-31203) imp:n=1 \$Metal wl  
 31204 5 0.00359833 (-31204) imp:n=1 \$Metal wl  
 31205 5 0.00359833 (-31205) imp:n=1 \$Metal wl  
 31206 5 0.00359833 (-31206) imp:n=1 \$Metal wl  
 31207 5 0.00359833 (-31207) imp:n=1 \$Metal wl  
 31208 5 0.00359833 (-31208) imp:n=1 \$Metal wl  
 31209 5 0.00359833 (-31209) imp:n=1 \$Metal wl  
 31210 5 0.00359833 (-31210) imp:n=1 \$Metal wl  
 31211 5 0.00359833 (-31211) imp:n=1 \$Metal wl  
 31212 5 0.00359833 (-31212) imp:n=1 \$Metal wl  
 31213 5 0.00359833 (-31213) imp:n=1 \$Metal wl  
 31214 5 0.00359833 (-31214) imp:n=1 \$Metal wl  
 31215 5 0.00359833 (-31215) imp:n=1 \$Metal wl  
 31216 5 0.00359833 (-31216) imp:n=1 \$Metal wl  
 c  
 c  
 c Floor1 Room 316  
 31601 5 0.00359833 (-31601) imp:n=1 \$Metal wl  
 31602 13 -7.92 (-31602) imp:n=1 \$SS  
 31603 5 0.00359833 (-31603) imp:n=1 \$Metal wl  
 31604 5 0.00359833 (-31604) imp:n=1 \$Metal wl  
 31605 5 0.00359833 (-31605) imp:n=1 \$Metal wl  
 31606 5 0.00359833 (-31606) imp:n=1 \$Metal wl  
 31607 5 0.00359833 (-31607) imp:n=1 \$Metal wl  
 31608 5 0.00359833 (-31608) imp:n=1 \$Metal wl  
 31609 5 0.00359833 (-31609) imp:n=1 \$Metal wl  
 31610 5 0.00359833 (-31610) imp:n=1 \$Metal wl  
 31611 5 0.00359833 (-31611) imp:n=1 \$Metal wl  
 c  
 c  
 c Floor1 Room 401/403  
 40101 5 0.00359833 (-40101) imp:n=1 \$Metal wl  
 40102 5 0.00359833 (-40102) imp:n=1 \$Metal wl  
 40103 5 0.00359833 (-40103) imp:n=1 \$Metal wl  
 40104 5 0.00359833 (-40104) imp:n=1 \$Metal wl  
 40105 5 0.00359833 (-40105) imp:n=1 \$Metal wl  
 40106 5 0.00359833 (-40106) imp:n=1 \$Metal wl  
 40107 5 0.00359833 (-40107) imp:n=1 \$Metal wl  
 40108 5 0.00359833 (-40108) imp:n=1 \$Metal wl  
 40109 5 0.00359833 (-40109) imp:n=1 \$Metal wl  
 40110 5 0.00359833 (-40110) imp:n=1 \$Metal wl  
 40111 5 0.00359833 (-40111) imp:n=1 \$Metal wl  
 40112 5 0.00359833 (-40112) imp:n=1 \$Metal wl  
 40113 5 0.00359833 (-40113) imp:n=1 \$Metal wl  
 40114 5 0.00359833 (-40114) imp:n=1 \$Metal wl  
 40115 5 0.00359833 (-40115) imp:n=1 \$Metal wl  
 c  
 c  
 c Floor1 Room 405  
 40501 5 0.00359833 (-40501) imp:n=1 \$Metal wl  
 40502 5 0.00359833 (-40502) imp:n=1 \$Metal wl  
 40503 5 0.00359833 (-40503) imp:n=1 \$Metal wl  
 40504 5 0.00359833 (-40504) imp:n=1 \$Metal wl  
 40505 5 0.00359833 (-40505) imp:n=1 \$Metal wl  
 40506 5 0.00359833 (-40506) imp:n=1 \$Metal wl  
 40507 5 0.00359833 (-40507) imp:n=1 \$Metal wl



50105	5	0.00359833	(-50105)	imp:n=1	\$Metal wl
50106	5	0.00359833	(-50106)	imp:n=1	\$Metal wl
50107	5	0.00359833	(-50107)	imp:n=1	\$Metal wl
50108	5	0.00359833	(-50108)	imp:n=1	\$Metal wl
50109	5	0.00359833	(-50109)	imp:n=1	\$Metal wl
50110	5	0.00359833	(-50110)	imp:n=1	\$Metal wl
50111	5	0.00359833	(-50111)	imp:n=1	\$Metal wl
c					
c					
c	Floor1 Room 500				
50001	5	0.00359833	(-50001)	imp:n=1	\$Metal wl
50002	5	0.00359833	(-50002)	imp:n=1	\$Metal wl
50003	5	0.00359833	(-50003)	imp:n=1	\$Metal wl
50004	5	0.00359833	(-50004)	imp:n=1	\$Metal wl
50005	5	0.00359833	(-50005)	imp:n=1	\$Metal wl
50006	5	0.00359833	(-50006)	imp:n=1	\$Metal wl
50007	5	0.00359833	(-50007)	imp:n=1	\$Metal wl
50008	5	0.00359833	(-50008)	imp:n=1	\$Metal wl
50009	5	0.00359833	(-50009)	imp:n=1	\$Metal wl
50010	5	0.00359833	(-50010)	imp:n=1	\$Metal wl
50011	5	0.00359833	(-50011)	imp:n=1	\$Metal wl
50012	5	0.00359833	(-50012)	imp:n=1	\$Metal wl
50013	5	0.00359833	(-50013)	imp:n=1	\$Metal wl
50014	5	0.00359833	(-50014)	imp:n=1	\$Metal wl
50015	5	0.00359833	(-50015)	imp:n=1	\$Metal wl
50016	5	0.00359833	(-50016)	imp:n=1	\$Metal wl
c					
c					
c					
c	Floor1 Room 404				
40401	5	0.00359833	(-40401)	imp:n=1	\$Metal wl
40402	5	0.00359833	(-40402)	imp:n=1	\$Metal wl
40403	5	0.00359833	(-40403)	imp:n=1	\$Metal wl
40404	5	0.00359833	(-40404)	imp:n=1	\$Metal wl
c					
c					
c	Floor1 Room 505				
50501	13	-7.92	(-50501)	imp:n=1	\$SS
50502	5	0.00359833	(-50502)	imp:n=1	\$Metal wl
50503	5	0.00359833	(-50503)	imp:n=1	\$Metal wl
50504	5	0.00359833	(-50504)	imp:n=1	\$Metal wl
50505	5	0.00359833	(-50505)	imp:n=1	\$Metal wl
50506	5	0.00359833	(-50506)	imp:n=1	\$Metal wl
c					
c					
c	Floor1 Room 504/504A				
50401	5	0.00359833	(-50401)	imp:n=1	\$Metal wl
50402	5	0.00359833	(-50402)	imp:n=1	\$Metal wl
50403	5	0.00359833	(-50403)	imp:n=1	\$Metal wl
50404	5	0.00359833	(-50404)	imp:n=1	\$Metal wl
50405	5	0.00359833	(-50405)	imp:n=1	\$Metal wl
c					
c					
c	Floor1 Room 406				
40601	13	-7.92	(-40601)	imp:n=1	\$SS
40602	5	0.00359833	(-40602)	imp:n=1	\$Metal wl
40603	5	0.00359833	(-40603)	imp:n=1	\$Metal wl
40604	5	0.00359833	(-40604)	imp:n=1	\$Metal wl
40605	5	0.00359833	(-40605)	imp:n=1	\$Metal wl
40606	5	0.00359833	(-40606)	imp:n=1	\$Metal wl
40607	5	0.00359833	(-40607)	imp:n=1	\$Metal wl
40608	5	0.00359833	(-40608)	imp:n=1	\$Metal wl
40609	5	0.00359833	(-40609)	imp:n=1	\$Metal wl
40610	5	0.00359833	(-40610)	imp:n=1	\$Metal wl
40611	5	0.00359833	(-40611)	imp:n=1	\$Metal wl
40612	5	0.00359833	(-40612)	imp:n=1	\$Metal wl
40613	5	0.00359833	(-40613)	imp:n=1	\$Metal wl
40614	5	0.00359833	(-40614)	imp:n=1	\$Metal wl
c					
c					

c Floor1 Room 507

50701	5	0.00359833	(-50701)	imp:n=1	\$Metal wl
50702	5	0.00359833	(-50702)	imp:n=1	\$Metal wl
50703	5	0.00359833	(-50703)	imp:n=1	\$Metal wl
50704	5	0.00359833	(-50704)	imp:n=1	\$Metal wl
50705	5	0.00359833	(-50705)	imp:n=1	\$Metal wl
50706	5	0.00359833	(-50706)	imp:n=1	\$Metal wl
50707	5	0.00359833	(-50707)	imp:n=1	\$Metal wl
50708	5	0.00359833	(-50708)	imp:n=1	\$Metal wl
50709	5	0.00359833	(-50709)	imp:n=1	\$Metal wl
50710	5	0.00359833	(-50710)	imp:n=1	\$Metal wl
50711	5	0.00359833	(-50711)	imp:n=1	\$Metal wl

c

c

c Floor1 Room 506

50601	5	0.00359833	(-50601)	imp:n=1	\$Metal wl
50602	5	0.00359833	(-50602)	imp:n=1	\$Metal wl
50603	5	0.00359833	(-50603)	imp:n=1	\$Metal wl
50604	5	0.00359833	(-50604)	imp:n=1	\$Metal wl
50605	5	0.00359833	(-50605)	imp:n=1	\$Metal wl
50606	5	0.00359833	(-50606)	imp:n=1	\$Metal wl
50607	5	0.00359833	(-50607)	imp:n=1	\$Metal wl
50608	5	0.00359833	(-50608)	imp:n=1	\$Metal wl
50609	5	0.00359833	(-50609)	imp:n=1	\$Metal wl
50610	5	0.00359833	(-50610)	imp:n=1	\$Metal wl
50611	5	0.00359833	(-50611)	imp:n=1	\$Metal wl
50612	5	0.00359833	(-50612)	imp:n=1	\$Metal wl
50613	5	0.00359833	(-50613)	imp:n=1	\$Metal wl

c

c

c Floor1 Room 410

41001	5	0.00359833	(-41001)	imp:n=1	\$Metal wl
41002	5	0.00359833	(-41002)	imp:n=1	\$Metal wl
41003	5	0.00359833	(-41003)	imp:n=1	\$Metal wl
41004	5	0.00359833	(-41004)	imp:n=1	\$Metal wl
41005	5	0.00359833	(-41005)	imp:n=1	\$Metal wl
41006	13	-7.92	(-41006)	imp:n=1	\$SS
41007	5	0.00359833	(-41007)	imp:n=1	\$Metal wl
41008	5	0.00359833	(-41008)	imp:n=1	\$Metal wl
41009	5	0.00359833	(-41009)	imp:n=1	\$Metal wl
41010	5	0.00359833	(-41010)	imp:n=1	\$Metal wl
41011	5	0.00359833	(-41011)	imp:n=1	\$Metal wl
41012	5	0.00359833	(-41012)	imp:n=1	\$Metal wl
41013	5	0.00359833	(-41013)	imp:n=1	\$Metal wl

c

c

c Floor1 Room 511

51101	5	0.00359833	(-51101)	imp:n=1	\$Metal wl
51102	5	0.00359833	(-51102)	imp:n=1	\$Metal wl
51103	5	0.00359833	(-51103)	imp:n=1	\$Metal wl
51104	5	0.00359833	(-51104)	imp:n=1	\$Metal wl
51105	5	0.00359833	(-51105)	imp:n=1	\$Metal wl
51106	5	0.00359833	(-51106)	imp:n=1	\$Metal wl
51107	5	0.00359833	(-51107)	imp:n=1	\$Metal wl
51108	5	0.00359833	(-51108)	imp:n=1	\$Metal wl
51109	5	0.00359833	(-51109)	imp:n=1	\$Metal wl

c

c

c Floor1 Room 510

51001	5	0.00359833	(-51001)	imp:n=1	\$Metal wl
51002	5	0.00359833	(-51002)	imp:n=1	\$Metal wl
51003	5	0.00359833	(-51003)	imp:n=1	\$Metal wl
51004	5	0.00359833	(-51004)	imp:n=1	\$Metal wl
51005	5	0.00359833	(-51005)	imp:n=1	\$Metal wl
51006	5	0.00359833	(-51006)	imp:n=1	\$Metal wl
51007	5	0.00359833	(-51007)	imp:n=1	\$Metal wl
51008	5	0.00359833	(-51008)	imp:n=1	\$Metal wl
51009	5	0.00359833	(-51009)	imp:n=1	\$Metal wl

c

c



60002 3 -2.3 (-60002) imp:n=1 \$Conc Filled  
 60003 5 0.00359833 (-60003) imp:n=1 \$Metal wl  
 60004 5 0.00359833 (-60004) imp:n=1 \$Metal wl  
 60005 3 -2.3 (-60005) imp:n=1 \$Conc Filled  
 60006 5 0.00359833 (-60006) imp:n=1 \$Metal wl  
 60007 5 0.00359833 (-60007) imp:n=1 \$Metal wl  
 60008 5 0.00359833 (-60008) imp:n=1 \$Metal wl  
 60009 5 0.00359833 (-60009) imp:n=1 \$Metal wl  
 60010 5 0.00359833 (-60010) imp:n=1 \$Metal wl  
 60011 5 0.00359833 (-60011) imp:n=1 \$Metal wl  
 60012 5 0.00359833 (-60012) imp:n=1 \$Metal wl  
 60013 5 0.00359833 (-60013) imp:n=1 \$Metal wl  
 60014 5 0.00359833 (-60014) imp:n=1 \$Metal wl  
 60015 5 0.00359833 (-60015) imp:n=1 \$Metal wl  
 60017 15 -0.4751 (-60017) imp:n=1 \$Ext wl Filled  
 c  
 c

c Floor1 Room 602/605/606

c \*\*\*\*These rooms were all combined because it is\*\*\*\*\*  
c difficult to distinguish between them.

60201 5 0.00359833 (-60201) imp:n=1 \$Metal wl  
 60202 5 0.00359833 (-60202) imp:n=1 \$Metal wl  
 60203 5 0.00359833 (-60203) imp:n=1 \$Metal wl  
 60204 5 0.00359833 (-60204) imp:n=1 \$Metal wl  
 60205 5 0.00359833 (-60205) imp:n=1 \$Metal wl  
 60206 5 0.00359833 (-60206) imp:n=1 \$Metal wl  
 60207 5 0.00359833 (-60207) imp:n=1 \$Metal wl  
 60208 5 0.00359833 (-60208) imp:n=1 \$Metal wl  
 60209 5 0.00359833 (-60209) imp:n=1 \$Metal wl  
 60210 5 0.00359833 (-60210) imp:n=1 \$Metal wl  
 60211 5 0.00359833 (-60211) imp:n=1 \$Metal wl  
 60212 5 0.00359833 (-60212) imp:n=1 \$Metal wl  
 60213 5 0.00359833 (-60213) imp:n=1 \$Metal wl  
 60214 5 0.00359833 (-60214) imp:n=1 \$Metal wl  
 60215 5 0.00359833 (-60215) imp:n=1 \$Metal wl  
 60216 5 0.00359833 (-60216) imp:n=1 \$Metal wl  
 60217 5 0.00359833 (-60217) imp:n=1 \$Metal wl  
 60218 5 0.00359833 (-60218) imp:n=1 \$Metal wl  
 60219 5 0.00359833 (-60219) imp:n=1 \$Metal wl  
 60220 5 0.00359833 (-60220) imp:n=1 \$Metal wl  
 60221 5 0.00359833 (-60221) imp:n=1 \$Metal wl  
 60222 5 0.00359833 (-60222) imp:n=1 \$Metal wl  
 60223 5 0.00359833 (-60223) imp:n=1 \$Metal wl  
 60224 5 0.00359833 (-60224) imp:n=1 \$Metal wl  
 60225 5 0.00359833 (-60225) imp:n=1 \$Metal wl  
 60226 5 0.00359833 (-60226) imp:n=1 \$Metal wl  
 60227 5 0.00359833 (-60227) imp:n=1 \$Metal wl  
 60228 5 0.00359833 (-60228) imp:n=1 \$Metal wl  
 60232 15 -0.4751 (-60232) imp:n=1 \$Ext wl Filled  
 c  
 c

c Floor1 Room 610 Truck Lock

c \*\*\*\*\*Note: a .5cm thick material t

61001 15 -0.4751 (-61001) imp:n=1 \$Ext wl Filled  
 61002 5 0.00359833 (-61002) imp:n=1 \$Metal wl  
 61003 5 0.00359833 (-61003) imp:n=1 \$Metal wl  
 61004 13 -7.92 (-61004) imp:n=1 \$\$S  
 61005 13 -7.92 (-61005) imp:n=1 \$\$S  
 61006 13 -7.92 (-61006) imp:n=1 \$\$S  
 61007 5 0.00359833 (-61007) imp:n=1 \$Metal wl  
 61008 5 0.00359833 (-61008) imp:n=1 \$Metal wl  
 61009 5 0.00359833 (-61009) imp:n=1 \$Metal wl  
 61010 5 0.00359833 (-61010) imp:n=1 \$Metal wl  
 61011 5 0.00359833 (-61011) imp:n=1 \$Metal wl  
 61012 5 0.00359833 (-61012) imp:n=1 \$Metal wl  
 61013 5 0.00359833 (-61013) imp:n=1 \$Metal wl  
 61014 5 0.00359833 (-61014) imp:n=1 \$Metal wl  
 61015 13 -7.92 (-61015) imp:n=1 \$\$S  
 61016 5 0.00359833 (-61016) imp:n=1 \$Metal wl  
 61017 5 0.00359833 (-61017) imp:n=1 \$Metal wl

61018 5 0.00359833 (-61018) imp:n=1 \$Metal wl  
 61019 13 -7.92 (-61019) imp:n=1 \$SS  
 61020 5 0.00359833 (-61020) imp:n=1 \$Metal wl  
 61021 5 0.00359833 (-61021) imp:n=1 \$Metal wl  
 61022 15 -0.4751 (-61022) imp:n=1 \$Ext wl Filled  
 61023 5 0.00359833 (-61023) imp:n=1 \$Metal wl  
 61024 15 -0.4751 (-61024) imp:n=1 \$Ext wl Filled  
 61025 5 0.00359833 (-61025) imp:n=1 \$Metal wl  
 61026 15 -0.4751 (-61026) imp:n=1 \$Ext wl Filled  
 61027 5 0.00359833 (-61027) imp:n=1 \$Metal wl  
 61028 15 -0.4751 (-61028) imp:n=1 \$Ext wl Filled  
 61029 5 0.00359833 (-61029) imp:n=1 \$Metal wl  
 61030 15 -0.4751 (-61030) imp:n=1 \$Ext wl Filled  
 61031 13 -7.92 (-61031) imp:n=1 \$SS  
 61032 13 -7.92 (-61032) imp:n=1 \$SS  
 61033 13 -7.92 (-61033) imp:n=1 \$\$\$  
 61034 13 -7.92 (-61034) imp:n=1 \$\$\$  
 61035 5 0.00359833 (-61035) imp:n=1 \$Metal wl  
 61036 5 0.00359833 (-61036) imp:n=1 \$Metal wl  
 61037 5 0.00359833 (-61037) imp:n=1 \$Metal wl  
 61038 5 0.00359833 (-61038) imp:n=1 \$Metal wl

c

c

c Floor1 Room 603

60301 5 0.00359833 (-60301) imp:n=1 \$Metal wl  
 60302 15 -0.4751 (-60302) imp:n=1 \$Ext wl Filled  
 60303 13 -7.92 (-60303) imp:n=1 \$\$S  
 60304 13 -7.92 (-60304) imp:n=1 \$\$\$  
 60305 13 -7.92 (-60305) imp:n=1 \$\$\$  
 60306 13 -7.92 (-60306) imp:n=1 \$\$\$  
 60307 5 0.00359833 (-60307) imp:n=1 \$Metal wl  
 60308 15 -0.4751 (-60308) imp:n=1 \$Ext wl Filled  
 60309 13 -7.92 (-60309) imp:n=1 \$\$S  
 60310 13 -7.92 (-60310) imp:n=1 \$\$\$  
 60311 5 0.00359833 (-60311) imp:n=1 \$Metal wl  
 60312 5 0.00359833 (-60312) imp:n=1 \$Metal wl  
 60313 5 0.00359833 (-60313) imp:n=1 \$Metal wl  
 60314 5 0.00359833 (-60314) imp:n=1 \$Metal wl  
 60315 5 0.00359833 (-60315) imp:n=1 \$Metal wl  
 60316 5 0.00359833 (-60316) imp:n=1 \$Metal wl  
 60317 5 0.00359833 (-60317) imp:n=1 \$Metal wl  
 60318 5 0.00359833 (-60318) imp:n=1 \$Metal wl  
 60319 15 -0.4751 (-60319) imp:n=1 \$Ext wl Filled  
 60320 5 0.00359833 (-60320) imp:n=1 \$Metal wl  
 60321 5 0.00359833 (-60321) imp:n=1 \$Metal wl  
 60322 5 0.00359833 (-60322) imp:n=1 \$Metal wl  
 60323 5 0.00359833 (-60323) imp:n=1 \$Metal wl  
 60324 5 0.00359833 (-60324) imp:n=1 \$Metal wl  
 60325 5 0.00359833 (-60325) imp:n=1 \$Metal wl  
 60326 13 -7.92 (-60326) imp:n=1 \$\$S  
 60327 5 0.00359833 (-60327) imp:n=1 \$Metal wl  
 60328 5 0.00359833 (-60328) imp:n=1 \$Metal wl  
 60329 5 0.00359833 (-60329) imp:n=1 \$Metal wl  
 60330 5 0.00359833 (-60330) imp:n=1 \$Metal wl  
 60331 3 -2.3 (-60331) imp:n=1 \$Conc Filled Blank Concrete Box  
 60336 15 -0.4751 (-60336) imp:n=1 \$Ext wl Filled

c

c

c Floor1 Room 601

60101 13 -7.92 (-60101) imp:n=1 \$\$S  
 60102 13 -7.92 (-60102) imp:n=1 \$\$S  
 60103 13 -7.92 (-60103) imp:n=1 \$\$S  
 60104 5 0.00359833 (-60104) imp:n=1 \$Metal wl  
 60105 5 0.00359833 (-60105) imp:n=1 \$Metal wl

c

c

c Floor1 Room 604

60401 5 0.00359833 (-60401) imp:n=1 \$Metal wl  
 60403 5 0.00359833 (-60403) imp:n=1 \$Metal wl  
 60404 15 -0.4751 (-60404) imp:n=1 \$Ext wl Filled





10957 5 0.00359833 (-10957) imp:n=1 \$Metal wl  
 c Hallway above Room 109 and below Room 108  
 10958 5 0.00359833 (-10958) imp:n=1 \$Metal wl  
 10959 5 0.00359833 (-10959) imp:n=1 \$Metal wl  
 10960 5 0.00359833 (-10960) imp:n=1 \$Metal wl  
 10961 5 0.00359833 (-10961) imp:n=1 \$Metal wl  
 10966 15 -0.4751 (-10966) imp:n=1 \$Ext wl Filled  
 10967 15 -0.4751 (-10967) imp:n=1 \$Ext wl Filled  
 c  
 c  
 c  
 c  
 c Floor1 Room 110/ Men B Room Women B Room/ Conf Room Women change room/ copy room  
 c Mens Room - MR/Pipe Chase -PC/Womens Room - WR  
 11001 5 0.00359833 (-11001) imp:n=1 \$Metal wl  
 11002 5 0.00359833 (-11002) imp:n=1 \$Metal wl  
 11003 5 0.00359833 (-11003) imp:n=1 \$Metal wl  
 11004 5 0.00359833 (-11004) imp:n=1 \$Metal wl  
 11005 5 0.00359833 (-11005) imp:n=1 \$Metal wl  
 11006 5 0.00359833 (-11006) imp:n=1 \$Metal wl  
 11007 5 0.00359833 (-11007) imp:n=1 \$Metal wl  
 11008 5 0.00359833 (-11008) imp:n=1 \$Metal wl  
 11009 5 0.00359833 (-11009) imp:n=1 \$Metal wl  
 11010 5 0.00359833 (-11010) imp:n=1 \$Metal wl  
 11011 5 0.00359833 (-11011) imp:n=1 \$Metal wl  
 c Room 110/Conf Room - CR starts below here  
 11012 5 0.00359833 (-11012) imp:n=1 \$Metal wl  
 11013 5 0.00359833 (-11013) imp:n=1 \$Metal wl  
 11014 5 0.00359833 (-11014) imp:n=1 \$Metal wl  
 11015 5 0.00359833 (-11015) imp:n=1 \$Metal wl  
 11016 5 0.00359833 (-11016) imp:n=1 \$Metal wl  
 11017 5 0.00359833 (-11017) imp:n=1 \$Metal wl  
 11018 5 0.00359833 (-11018) imp:n=1 \$Metal wl  
 11019 5 0.00359833 (-11019) imp:n=1 \$Metal wl  
 11020 5 0.00359833 (-11020) imp:n=1 \$Metal wl  
 11021 5 0.00359833 (-11021) imp:n=1 \$Metal wl  
 11022 5 0.00359833 (-11022) imp:n=1 \$Metal wl  
 11023 5 0.00359833 (-11023) imp:n=1 \$Metal wl  
 11024 5 0.00359833 (-11024) imp:n=1 \$Metal wl  
 11025 5 0.00359833 (-11025) imp:n=1 \$Metal wl  
 11026 5 0.00359833 (-11026) imp:n=1 \$Metal wl  
 11027 5 0.00359833 (-11027) imp:n=1 \$Metal wl  
 c Room 110A - A/Room110C - C/Room 110B - B/Copy Room - copy/  
 11028 5 0.00359833 (-11028) imp:n=1 \$Metal wl  
 11029 5 0.00359833 (-11029) imp:n=1 \$Metal wl  
 11030 5 0.00359833 (-11030) imp:n=1 \$Metal wl  
 11031 5 0.00359833 (-11031) imp:n=1 \$Metal wl  
 11032 5 0.00359833 (-11032) imp:n=1 \$Metal wl  
 11033 5 0.00359833 (-11033) imp:n=1 \$Metal wl  
 11034 5 0.00359833 (-11034) imp:n=1 \$Metal wl  
 11035 5 0.00359833 (-11035) imp:n=1 \$Metal wl  
 11036 5 0.00359833 (-11036) imp:n=1 \$Metal wl  
 11037 5 0.00359833 (-11037) imp:n=1 \$Metal wl  
 11038 5 0.00359833 (-11038) imp:n=1 \$Metal wl  
 11039 5 0.00359833 (-11039) imp:n=1 \$Metal wl  
 11040 5 0.00359833 (-11040) imp:n=1 \$Metal wl  
 11041 5 0.00359833 (-11041) imp:n=1 \$Metal wl  
 11042 5 0.00359833 (-11042) imp:n=1 \$Metal wl  
 11043 5 0.00359833 (-11043) imp:n=1 \$Metal wl  
 11044 5 0.00359833 (-11044) imp:n=1 \$Metal wl  
 11045 5 0.00359833 (-11045) imp:n=1 \$Metal wl  
 c Women change room below here - WCR  
 11046 5 0.00359833 (-11046) imp:n=1 \$Metal wl  
 11047 5 0.00359833 (-11047) imp:n=1 \$Metal wl  
 11048 5 0.00359833 (-11048) imp:n=1 \$Metal wl  
 11049 5 0.00359833 (-11049) imp:n=1 \$Metal wl  
 11050 5 0.00359833 (-11050) imp:n=1 \$Metal wl  
 c Wall above copy room and 110B but below Room 111 and the North Eastern Womens restroom below here  
 11051 5 0.00359833 (-11051) imp:n=1 \$Metal wl  
 11052 13 -7.92 (-11052) imp:n=1 \$SS

11053	5	0.00359833	(-11053)	imp:n=1	\$Metal wl
11054	5	0.00359833	(-11054)	imp:n=1	\$Metal wl
11055	5	0.00359833	(-11055)	imp:n=1	\$Metal wl
11056	5	0.00359833	(-11056)	imp:n=1	\$Metal wl
11057	5	0.00359833	(-11057)	imp:n=1	\$Metal wl
c					
11058	5	0.00359833	(-11058)	imp:n=1	\$Metal wl
11059	5	0.00359833	(-11059)	imp:n=1	\$Metal wl
11060	5	0.00359833	(-11060)	imp:n=1	\$Metal wl
11061	5	0.00359833	(-11061)	imp:n=1	\$Metal wl
11062	5	0.00359833	(-11062)	imp:n=1	\$Metal wl
11063	5	0.00359833	(-11063)	imp:n=1	\$Metal wl
11064	5	0.00359833	(-11064)	imp:n=1	\$Metal wl
11065	5	0.00359833	(-11065)	imp:n=1	\$Metal wl
11066	5	0.00359833	(-11066)	imp:n=1	\$Metal wl
11067	5	0.00359833	(-11067)	imp:n=1	\$Metal wl
11068	5	0.00359833	(-11068)	imp:n=1	\$Metal wl
11069	5	0.00359833	(-11069)	imp:n=1	\$Metal wl
11075	15	-0.4751	(-11075)	imp:n=1	\$Ext wl Filled S wl MR-PC-WR
11076	5	0.00359833	(-11076)	imp:n=1	\$Metal wl
11077	5	0.00359833	(-11077)	imp:n=1	\$Metal wl 1
11078	15	-0.4751	(-11078)	imp:n=1	\$Ext wl Filled S o wl MR-PC-WR
c					
c					

c Floor1 Room 111/Room 111A/NW Women Rest Room - NWW/Women change and shower room - WSR

11101	5	0.00359833	(-11101)	imp:n=1	\$Metal wl
11102	5	0.00359833	(-11102)	imp:n=1	\$Metal wl
11103	5	0.00359833	(-11103)	imp:n=1	\$Metal wl
11104	5	0.00359833	(-11104)	imp:n=1	\$Metal wl
11105	5	0.00359833	(-11105)	imp:n=1	\$Metal wl
11106	5	0.00359833	(-11106)	imp:n=1	\$Metal wl
11107	5	0.00359833	(-11107)	imp:n=1	\$Metal wl
11108	5	0.00359833	(-11108)	imp:n=1	\$Metal wl
11109	5	0.00359833	(-11109)	imp:n=1	\$Metal wl
11110	5	0.00359833	(-11110)	imp:n=1	\$Metal wl
11111	5	0.00359833	(-11111)	imp:n=1	\$Metal wl
11112	5	0.00359833	(-11112)	imp:n=1	\$Metal wl
11113	5	0.00359833	(-11113)	imp:n=1	\$Metal wl
11114	5	0.00359833	(-11114)	imp:n=1	\$Metal wl
11115	5	0.00359833	(-11115)	imp:n=1	\$Metal wl
11116	5	0.00359833	(-11116)	imp:n=1	\$Metal wl
11117	5	0.00359833	(-11117)	imp:n=1	\$Metal wl
11118	5	0.00359833	(-11118)	imp:n=1	\$Metal wl
11119	5	0.00359833	(-11119)	imp:n=1	\$Metal wl
11120	5	0.00359833	(-11120)	imp:n=1	\$Metal wl
11121	5	0.00359833	(-11121)	imp:n=1	\$Metal wl
11122	5	0.00359833	(-11122)	imp:n=1	\$Metal wl
11123	5	0.00359833	(-11123)	imp:n=1	\$Metal wl
11124	5	0.00359833	(-11124)	imp:n=1	\$Metal wl
11125	5	0.00359833	(-11125)	imp:n=1	\$Metal wl
11126	5	0.00359833	(-11126)	imp:n=1	\$Metal wl
11127	5	0.00359833	(-11127)	imp:n=1	\$Metal wl
11128	5	0.00359833	(-11128)	imp:n=1	\$Metal wl
11129	5	0.00359833	(-11129)	imp:n=1	\$Metal wl
11130	5	0.00359833	(-11130)	imp:n=1	\$Metal wl
c					
c					

c Floor1 Room 107/108

10701	5	0.00359833	(-10701)	imp:n=1	\$Metal wl
10702	5	0.00359833	(-10702)	imp:n=1	\$Metal wl
10703	5	0.00359833	(-10703)	imp:n=1	\$Metal wl
10704	5	0.00359833	(-10704)	imp:n=1	\$Metal wl
10705	5	0.00359833	(-10705)	imp:n=1	\$Metal wl
10706	5	0.00359833	(-10706)	imp:n=1	\$Metal wl
10707	5	0.00359833	(-10707)	imp:n=1	\$Metal wl
c					
c					

c Floor1 Room 103/104/104A

10301	5	0.00359833	(-10301)	imp:n=1	\$Metal wl
10302	5	0.00359833	(-10302)	imp:n=1	\$Metal wl



42621 8 -0.10907 (-42621) imp:n=1 \$Roomspace 426  
 43014 1 -0.001202 (-43014 43003) imp:n=1 \$Roomspace 430  
 52724 8 -0.10907 (-52724) imp:n=1 \$Roomspace 527  
 52725 6 -0.04855 (-52725) imp:n=1 \$Roomspace 527A  
 52916 1 -0.001202 (-52916 52911 52912) imp:n=1 \$Roomspace 529  
 52016 1 -0.001202 (-52016) imp:n=1 \$Roomspace 520  
 52017 8 -0.10907 (-52017) imp:n=1 \$Roomspace 520N  
 52410 8 -0.10907 (-52410) imp:n=1 \$Roomspace 524  
 52811 8 -0.10907 (-52811 52807) imp:n=1 \$Roomspace 528 Partially Filled  
 53017 1 -0.001202 (-53017 53007 53008) imp:n=1 \$Roomspace 530

c

c

c West and Southwest Room Fill Sections

20221 8 -0.10907 (-20221) imp:n=1 \$Roomspace 202  
 20222 8 -0.10907 (-20222) imp:n=1 \$Roomspace 203  
 20919 7 -0.05514 (-20919 20909) imp:n=1 \$Roomspace 209  
 30113 6 -0.04855 (-30113 30111) imp:n=1 \$Roomspace 301  
 30309 1 -0.001202 (-30309) imp:n=1 \$Roomspace 303  
 30512 8 -0.10907 (-30512) imp:n=1 \$Roomspace 305 Partially Filled  
 30913 8 -0.10907 (-30913) imp:n=1 \$Roomspace 309  
 31313 8 -0.10907 (-31313) imp:n=1 \$Roomspace 313  
 31704 8 -0.10907 (-31704) imp:n=1 \$Roomspace 317  
 31912 6 -0.04855 (-31912) imp:n=1 \$Roomspace 319A  
 31913 6 -0.04855 (-31913) imp:n=1 \$Roomspace 319  
 30024 8 -0.10907 (-30024 30003 30005) imp:n=1 \$Roomspace 300  
 30025 8 -0.10907 (-30025) imp:n=1 \$Roomspace TBF 300  
 30612 8 -0.10907 (-30612 30602) imp:n=1 \$Roomspace 306  
 31006 8 -0.10907 (-31006) imp:n=1 \$Roomspace 310  
 31007 8 -0.10907 (-31007) imp:n=1 \$Roomspace 310 East  
 31217 8 -0.10907 (-31217 31201) imp:n=1 \$Roomspace 312  
 31612 8 -0.10907 (-31612 31602) imp:n=1 \$Roomspace 316  
 40116 8 -0.10907 (-40116 30003) imp:n=1 \$Roomspace 401 Partially Filled  
 40117 8 -0.10907 (-40117) imp:n=1 \$Roomspace 403  
 40514 8 -0.10907 (-40514 30006 40501) imp:n=1 \$Roomspace 405 Partially Filled  
 40902 8 -0.10907 (-40902 30603) imp:n=1 \$Roomspace 409 Partially Filled  
 41119 8 -0.10907 (-41119 31202) imp:n=1 \$Roomspace 411  
 41908 8 -0.10907 (-41908 31602) imp:n=1 \$Roomspace 419

c

c

c Southeast and East Room Fill Sections

40016 8 -0.10907 (-40016) imp:n=1 \$Roomspace 400 Partially Filled  
 50112 8 -0.10907 (-50112) imp:n=1 \$Roomspace 501 Partially Filled  
 50017 8 -0.10907 (-50017) imp:n=1 \$Roomspace 500  
 40405 1 -0.001202 (-40405) imp:n=1 \$Roomspace 404  
 50507 7 -0.05514 (-50507) imp:n=1 \$Roomspace 505 Partially Filled  
 50406 6 -0.02427 (-50407) imp:n=1 \$Roomspace 504 Partially Filled  
 50407 6 -0.02427 (-50406) imp:n=1 \$Roomspace 504A  
 40615 8 -0.10907 (-40615) imp:n=1 \$Roomspace 406 Partially Filled  
 50712 8 -0.10907 (-50712) imp:n=1 \$Roomspace 507 Partially Filled  
 50614 8 -0.10907 (-50614) imp:n=1 \$Roomspace 506  
 41014 8 -0.10907 (-41014) imp:n=1 \$Roomspace 410 Partially Filled  
 51110 8 -0.10907 (-51110) imp:n=1 \$Roomspace 511 Partially Filled  
 51010 8 -0.10907 (-51010) imp:n=1 \$Roomspace 510  
 51404 1 -0.001202 (-51404) imp:n=1 \$Roomspace 514  
 51502 8 -0.10907 (-51502) imp:n=1 \$Roomspace 515  
 41404 8 -0.10907 (-41404) imp:n=1 \$Roomspace 414  
 41615 8 -0.10907 (-41615) imp:n=1 \$Roomspace 416 Partially Filled  
 51711 8 -0.10907 (-51711) imp:n=1 \$Roomspace 517 Partially Filled  
 51614 8 -0.10907 (-51614) imp:n=1 \$Roomspace 516  
 60016 8 -0.10907 (-60016) imp:n=1 \$Roomspace 600  
 60231 8 -0.10907 (-60231) imp:n=1 \$Roomspace 606

c

c

c Southernmost and Southeasternmost Room Fill Sections

20405 6 -0.04855 (-20405) imp:n=1 \$Roomspace 204  
 20406 1 -0.001202 (-20406) imp:n=1 \$Roomspace 205 Partially Filled  
 20407 1 -0.001202 (-20407) imp:n=1 \$Roomspace 205  
 10115 6 -0.04855 (-10115) imp:n=1 \$Roomspace 101  
 10116 6 -0.04855 (-10116) imp:n=1 \$Roomspace 102  
 10117 6 -0.04855 (-10117 10108 10109) imp:n=1 \$Roomspace 102A



c  
 c  
 103 1 -0.001202 (-103 70302 70303 70304 70305 70306 70307 70308 70309  
     70310 70311 70312 70313 70314 70315 70316 32001 32002  
     32003 32015 32016 #32017  
     ) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 104 1 -0.001202 (-104 32004 32005 32006 32007 32008 32009 32010 32011  
     32012 32013 32014 32401 32402 32403 32404 32405 32406  
     32407 32408 32409 32410 32411 32412 32413 32414 32415  
     32416 32417 70316 32017 32418 32419 33029 33030 33001  
     33002 33003 33004 33005 33006 33007 33008 33009 33010  
     33011 33012 33013 33014 33015 33016 33017 33018 33019  
     33020 33021 33022 33023 33024 33025 33026 33027 33028  
     33031 33032) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c Begin Northeast Section of the Central Section of Floor1  
 105 1 -0.001202 (-105 71101 71102 71103 71104 71105 71106 71107 71108  
     71109 71110 71111 71112 71113 71114 71115 42001 42002  
     42003 42004 42005 42006 42007 42008 42009 42010 42011  
     42012 42013 42014 52501 52502 52503 52504 52505 52506  
     52507 52508 52509 52511 52510 52512 52513 52514 52515  
     52516 52517 52518 52519 52520 52521 52522 42601 42602  
     42619 42620 #42621  
     ) imp:n=1 \$ NE Air Filled Section Box  
 c  
 c  
 c  
 106 1 -0.001202 (-106 42603 42604 42605 42606 42607 42608 42609 42610  
     42611 42612 42613 42614 42615 42616 42617 42618 42621  
     43001 43002 43003 43004 43006 43013 43014 52701  
     52702 52703 52704 52705 52706 52707 52708 52709 52710  
     52711 52712 52714 52715 52716 52717 52718 52719  
     52720 52721 52722 52723 52724 52725 52901 52902 52903  
     52904 52905 52906 52907 52908 52909 52910 52911 52912  
     52913 52916 #52519 #52510 #52512 #52513  
     ) imp:n=1 \$ NE Air Filled Section Box  
 c  
 c  
 c  
 134 1 -0.001202 (-134 43007 43008 43009 43010 43011 43012 52914 52713  
     52915 52726 43005 43015) imp:n=1 \$ NW Air Filled Section Box  
 c  
 c  
 c  
 107 1 -0.001202 (-107 52001 52002 52003 52004 52005 52006 52007 52008  
     52009 52010 52011 52012 52013 52014 52015 52016 52017  
     52401 52402 52403 52404 52405 52406 52407 52408 52409  
     52410 52801 52802 52803 52804 52805 52806 52807 52808  
     52809 52810 52811 52812 53001 53002 53003 53004 53005  
     53006 53007 53008 53009 53010 53011 53012 53013 53014  
     53015 53016 53017 53018 #60406 #60408 60403 60404  
     60405 60409 60317 60318 60319) imp:n=1 \$ E Air Filled Section Box  
 c  
 c  
 c Begin West Section of Floor1  
 108 1 -0.001202 (-108 20001 20002 20003 20004 20005 20006 20007 20008  
     20009 20010 20011 20012 20013 20014 20905 20906 20907  
     20908 20909 20915 20916 20917 20918 20919 20920 20921  
     20101 20102 20103 20104 20105 20106 20107 20108 20109  
     20110 20111 20112 20113 20114 20115 20116 20117 20118  
     20201 20202 20203 20204 20205 20206 20207 20208 20209  
     20210 20211 20212 20213 20214 20215 20216 20217 20218  
     20219 20220 20221 20222) imp:n=1 \$Air Filled N Section Box  
 c  
 c  
 c

109 1 -0.001202 (-109 20901 20902 20903 20904 20910 20911 20912  
     20913 20914 20922 #20908 #20919  
     ) imp:n=1 \$Air Filled S Section Box  
 c  
 c  
 c Begin SouthWest Section of Floor1  
 110 1 -0.001202 (-110 30101 30102 30103 30104 30105 30106 30107 30108  
     30109 30110 30111 30112 30113 30301 30302 30303 30304  
     30305 30306 30307 30308 30309 30501 30502 30503 30504  
     30505 30506 30507 30508 30509 30510 30511 30512 30901  
     30902 30903 30904 30905 30906 30907 30908 30909 30910  
     30911 30912 30913 #31904 #31313 31303 #20920  
     ) imp:n=1 \$Air Filled SW Section Box  
 c  
 c  
 c  
 111 1 -0.001202 (-111 31301 31302 31304 31305 31306 31307 31308  
     31309 31310 31311 31312 31313 31701 31702 31703 31704  
     31901 31902 31903 31904 31905 31906 31907 31908 31909  
     31910 31911 31912 31913) imp:n=1 \$Air Filled NW Section Box  
 c  
 c  
 c  
 112 1 -0.001202 (-112 30001 30002 30003 30004 30005 30006 30007  
     30008 30009 30010 30011 30012 30013 30014 30015  
     30016 30017 30018 30019 30020 30021 30022 30023  
     30024 40101 40102 40103 40104 40105 40106 40107  
     40108 40109 40110 40111 40112 40113 40114 40115  
     40116 40117 40501 #40514 #30601 30025 40505  
     40506 40507 40508 40509 #30612  
     ) imp:n=1 \$Air Filled SE Section Box  
 c  
 c  
 c  
 113 1 -0.001202 (-113 40502 40503 40504 40510 40511 40512 40513  
     40514 40901 40902 30601 30602 30603 30604 30605  
     30606 30607 30608 30609 30610 30611 31001 31002  
     31003 31004 31005 31006 31007 31201 31202 31203  
     31204 31205 31206 31207 31208 31209 31210 31211  
     31212 41102 41103 41104 41105 41106 41107 41108  
     41109 41110 41111 41112 41113 #30024 #31217 #41119  
     30612 ) imp:n=1 \$Air Filled E Section Box  
 c  
 c  
 c  
 114 1 -0.001202 (-114 31213 31214 31215 31216 31217 41114 41115  
     41116 41117 41118 41119 31601 31602 31603 31604  
     31605 31606 31607 31608 31609 31610 31611 31612  
     41901 41902 41903 41904 41905 41906 41907 41908  
     #31001 31202 31203 41101 466  
     ) imp:n=1 \$Air Filled NE Section Box  
 c  
 c  
 c Begin SouthEast Section of Floor1  
 115 1 -0.001202 (-115 40001 40002 40003 40004 40005 40006 40007  
     40008 40009 40010 40011 40012 40013 40014 40015  
     40016 50101 50102 50103 50104 50105 50106 50107  
     50108 50109 50110 50111 50112 40401 40402 40403  
     40404 40405 50501 50502 50503 50504 50505 50506  
     50507 #40615 #50712 40606 40607 40608 50703  
     50704 50705) imp:n=1 \$Air Filled SW Section Box  
 c  
 c  
 c  
 116 1 -0.001202 (-116 40601 40602 40603 40604 40605 40609 40610  
     40611 40612 40613 40614 40615 50701 50702 50706  
     50707 50708 50709 50710 50711 50712 41001 41005  
     41006 41007 41008 41009 41010 41014 51101 51104  
     51105 51106 51110 #50502  
     ) imp:n=1 \$Air Filled W Section Box

c  
 c  
 c  
 117 1 -0.001202 (-117 41011 41012 41013 51107 51108 51109 51501  
     51502 41401 41402 41403 41404 41601 41602 41603  
     41604 41605 41606 41607 41608 41609 41610 41611  
     41612 41613 41614 41615 51701 51702 51703 51704  
     51705 51706 51707 51708 51709 51710 51711  
     #41014 #51110 #41005 41004 41002 41003 51102  
     51103 ) imp:n=1 \$Air Filled NW Section Box  
 c  
 c  
 c  
 118 1 -0.001202 (-118 50001 50002 50003 50004 50005 50006 50007  
     50008 50009 50010 50011 50012 50013 50014 50015  
     50016 50017 50401 50402 50403 50404 50405 50406  
     50407 50601 50602 50603 50604 50605 50606 50607  
     50608 50609 50610 50611 50612 50613 50614 51001  
     51002 51003 51004 51005 51006 51007 51008 51009  
     51010 51401 51402 51403 51404 51601 51602 51603  
     51604 51605 51606 51607 51608 51609 51610 51611  
     51612 51613 51614 464  
     ) imp:n=1 \$Air Filled E Section Box  
 c  
 c  
 c Begin East Section of Floor  
 119 1 -0.001202 (-119 60001 60002 60003 60004 60005 60006 60007  
     60008 60009 60010 60011 60012 60013 60014 60015  
     60016 60017 60201  
     ) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 120 1 -0.001202 (-120 60202 60203 60204 60223 60224 60226 60231  
     60205 60206 60207 60208 60209 60210 60211 60216  
     60217 60218 60219 467) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 121 1 -0.001202 (-121 #60007 #60008 #60224 #60017 60220 60221  
     60222 60225) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 122 1 -0.001202 (-122 60212 60213 60214 60215 60220 60221 60222  
     60223 60224 60225 60226 60227 60228 60231 60232  
     #60224 #60017 #60007 #60008 #61002  
     ) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 123 1 -0.001202 (-123 60311 60312 60313 60314 60315 60316 60317  
     60320 60321 60322 60323 60324 60325 60326 60327  
     60328 60329 60330 60331 60336 #60227 61007 61008  
     61003 #61002 #61013 #61014 61009 61010 61011  
     #60301 #60302 60101 60102 60103 60104 60105 60401  
     #60406 60407 60408 60409 60410 60411 60412 60413  
     60414 60415 60416 #60004 #60005 #60006  
     468) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 124 1 -0.001202 (-124 60301 60302 60303 60304 60305 60306 60307  
     60308 60309 60310 61001 61002 61004 61005 61006  
     61012 61013 61014 61015 61016 61017 61018 61019  
     61020 61021 61022 61023 61024 61025 61026 61027  
     61028 61029 61030 61031 61032 61033 61034 61035  
     61036 61037 61038  
     ) imp:n=1 \$E Truck Lock Air Filled Section Box  
 c

c  
 c  
 125 1 -0.001202 (-125 #60318 #60319 60317 60320 #60311 #60312  
     #60336 ) imp:n=1 \$NE Air Filled Section Box  
 c  
 c  
 c Begin Southernmost Section of Floor1  
 126 1 -0.001202 (-126 20601 20602 20603 20604 20605 20606 20607  
     20617 20619 20621 20622 20623 #20615 10113 10114  
     #20616 #20624) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 127 1 -0.001202 (-127 20607 20608 20609 20610 20611 20612 20613  
     20614 20615 20616 20618 20620 20624 20401 20402  
     20403 20404 20405 20406 20407 10101 10102 10103  
     10104 10105 10106 10107 10108 10109 10110 10111  
     10112 10115 10116 10117 #108  
     ) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 128 1 -0.001202 (-128 ) imp:n=1 \$Air Filled NW Small Section Box  
 c  
 c  
 c Begin Southernmost East Section of Floor1  
 129 1 -0.001202 (-129 10901 10902 10903 10904 10905 10906 10907  
     10908 10909 10910 10911 10912 10913 10914 10915  
     10916 10917 10918 10919 10920 10921 10922 10923  
     10924 10925 10926 10929 10958 10959 10960 10961  
     10962 10963 10966 ) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 130 1 -0.001202 (-130 10701 10702 10703 10704 10705 10706 10707  
     10708 10709 10301 10302 10303 10304 10305 10306  
     10307 10308 10309 10310 10311 10312 10313 10314  
     10315 10316 10317 10930 10931 10932 10933 10934  
     10935 10936 10937 10938 10939 10940 10941 10942  
     10943 10944 10945 10946 10947 10948 10949 10950  
     10951 10952 10953 10954 10955 10956 10957 #10901  
     #10902 #10105 #10117 ) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 131 1 -0.001202 (-131 11001 11002 11003 11004 11005 11006 11007  
     11008 11009 11010 11011 11012 11015 11016 11017  
     11021 11022 11023 11024 11025 11026 11027  
     10928 11070 11129 11130 10967  
     11075 11076 11077 10927 11078) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 132 1 -0.001202 (-132 11013 11014 11019 11020 11018 11028 11029  
     11030 11031 11032 11033 11034 11035 11036 11037  
     11038 11039 11040 11041 11042 11043 11044 11045  
     11046 11047 11048 11049 11050 11051 11052 11053  
     11054 11055 11056 11057 11058 11061 11062 11063  
     11064 11065 11066 11067 11068 11069 11071 11072  
     11073 11074 #11129  
     #11130 #11059 11104 ) imp:n=1 \$Air Filled Section Box  
 c  
 c  
 c  
 133 1 -0.001202 (-133 11101 11102 11103 11105 11106 11107  
     11108 11109 11110 11111 11112 11113 11114 11115  
     11116 11117 11118 11119 11120 11121 11122 11123  
     11124 11125 11126 11127 11128 #11129 #11130 11131  
     11132 11201 11202 11203 11204 11205 11206 11207  
     11208 11209 11210 11211 11212 11213 11214 11215



91803	5	0.00359833	(-91803)	imp:n=1	\$Metal wl
91804	5	0.00359833	(-91804)	imp:n=1	\$Metal wl
91805	5	0.00359833	(-91805)	imp:n=1	\$Metal wl
91806	5	0.00359833	(-91806)	imp:n=1	\$Metal wl
91807	5	0.00359833	(-91807)	imp:n=1	\$Metal wl
91808	5	0.00359833	(-91808)	imp:n=1	\$Metal wl
91809	5	0.00359833	(-91809)	imp:n=1	\$Metal wl
91810	5	0.00359833	(-91810)	imp:n=1	\$Metal wl
91811	5	0.00359833	(-91811)	imp:n=1	\$Metal wl
91812	5	0.00359833	(-91812)	imp:n=1	\$Metal wl
91813	5	0.00359833	(-91813)	imp:n=1	\$Metal wl
91814	5	0.00359833	(-91814)	imp:n=1	\$Metal wl
91815	5	0.00359833	(-91815)	imp:n=1	\$Metal wl
91816	5	0.00359833	(-91816)	imp:n=1	\$Metal wl
91817	5	0.00359833	(-91817)	imp:n=1	\$Metal wl
91818	5	0.00359833	(-91818)	imp:n=1	\$Metal wl
91819	15	-0.4751	(-91819)	imp:n=1	\$Ext wl
91820	5	0.00359833	(-91820)	imp:n=1	\$Metal wl

c

c

c Floor2 Room 927/933/935/926/937/925/939 section contains some hallway remnants

92701	5	0.00359833	(-92701)	imp:n=1	\$Metal wl
92702	5	0.00359833	(-92702)	imp:n=1	\$Metal wl
92703	5	0.00359833	(-92703)	imp:n=1	\$Metal wl
92704	5	0.00359833	(-92704)	imp:n=1	\$Metal wl
92705	5	0.00359833	(-92705)	imp:n=1	\$Metal wl
92706	5	0.00359833	(-92706)	imp:n=1	\$Metal wl
92707	5	0.00359833	(-92707)	imp:n=1	\$Metal wl
92708	5	0.00359833	(-92708)	imp:n=1	\$Metal wl
92709	5	0.00359833	(-92709)	imp:n=1	\$Metal wl
92710	5	0.00359833	(-92710)	imp:n=1	\$Metal wl
92711	5	0.00359833	(-92711)	imp:n=1	\$Metal wl
92712	5	0.00359833	(-92712)	imp:n=1	\$Metal wl
92713	5	0.00359833	(-92713)	imp:n=1	\$Metal wl
92714	5	0.00359833	(-92714)	imp:n=1	\$Metal wl
92715	5	0.00359833	(-92715)	imp:n=1	\$Metal wl
92716	5	0.00359833	(-92716)	imp:n=1	\$Metal wl
92717	5	0.00359833	(-92717)	imp:n=1	\$Metal wl
92718	5	0.00359833	(-92718)	imp:n=1	\$Metal wl
92719	5	0.00359833	(-92719)	imp:n=1	\$Metal wl
92720	5	0.00359833	(-92720)	imp:n=1	\$Metal wl
92721	5	0.00359833	(-92721)	imp:n=1	\$Metal wl
92722	5	0.00359833	(-92722)	imp:n=1	\$Metal wl
92723	5	0.00359833	(-92723)	imp:n=1	\$Metal wl
92724	5	0.00359833	(-92724)	imp:n=1	\$Metal wl
92725	5	0.00359833	(-92725)	imp:n=1	\$Metal wl
92726	5	0.00359833	(-92726)	imp:n=1	\$Metal wl
92727	5	0.00359833	(-92727)	imp:n=1	\$Metal wl

c

c

c Floor2 Room 920/927/924/968/965/967/964

92001	5	0.00359833	(-92001)	imp:n=1	\$Metal wl
92002	5	0.00359833	(-92002)	imp:n=1	\$Metal wl
92003	5	0.00359833	(-92003)	imp:n=1	\$Metal wl
92004	5	0.00359833	(-92004)	imp:n=1	\$Metal wl
92005	5	0.00359833	(-92005)	imp:n=1	\$Metal wl
92006	5	0.00359833	(-92006)	imp:n=1	\$Metal wl
92007	5	0.00359833	(-92007)	imp:n=1	\$Metal wl
92008	5	0.00359833	(-92008)	imp:n=1	\$Metal wl
92009	5	0.00359833	(-92009)	imp:n=1	\$Metal wl
92010	5	0.00359833	(-92010)	imp:n=1	\$Metal wl
92011	5	0.00359833	(-92011)	imp:n=1	\$Metal wl
92012	5	0.00359833	(-92012)	imp:n=1	\$Metal wl
92013	5	0.00359833	(-92013)	imp:n=1	\$Metal wl
92014	5	0.00359833	(-92014)	imp:n=1	\$Metal wl
92015	5	0.00359833	(-92015)	imp:n=1	\$Metal wl
92016	5	0.00359833	(-92016)	imp:n=1	\$Metal wl
92017	5	0.00359833	(-92017)	imp:n=1	\$Metal wl
92018	5	0.00359833	(-92018)	imp:n=1	\$Metal wl
92019	5	0.00359833	(-92019)	imp:n=1	\$Metal wl

92020 5 0.00359833 (-92020) imp:n=1 \$Metal wl  
92021 5 0.00359833 (-92021) imp:n=1 \$Metal wl  
92022 5 0.00359833 (-92022) imp:n=1 \$Metal wl  
92023 15 -0.4751 (-92023) imp:n=1 \$Exterior wl  
92024 5 0.00359833 (-92024) imp:n=1 \$Metal wl  
92025 5 0.00359833 (-92025) imp:n=1 \$Metal wl  
92026 5 0.00359833 (-92026) imp:n=1 \$Metal wl

c

c

c Floor2 Room 930/932/934/936/938/941/943/945/947/949  
93001 5 0.00359833 (-93001) imp:n=1 \$Metal wl  
93002 5 0.00359833 (-93002) imp:n=1 \$Metal wl  
93003 5 0.00359833 (-93003) imp:n=1 \$Metal wl  
93004 5 0.00359833 (-93004) imp:n=1 \$Metal wl  
93005 5 0.00359833 (-93005) imp:n=1 \$Metal wl  
93006 5 0.00359833 (-93006) imp:n=1 \$Metal wl  
93007 5 0.00359833 (-93007) imp:n=1 \$Metal wl  
93008 5 0.00359833 (-93008) imp:n=1 \$Metal wl  
93009 5 0.00359833 (-93009) imp:n=1 \$Metal wl  
93010 5 0.00359833 (-93010) imp:n=1 \$Metal wl  
93011 5 0.00359833 (-93011) imp:n=1 \$Metal wl  
93012 5 0.00359833 (-93012) imp:n=1 \$Metal wl  
93013 5 0.00359833 (-93013) imp:n=1 \$Metal wl  
93014 5 0.00359833 (-93014) imp:n=1 \$Metal wl  
93015 5 0.00359833 (-93015) imp:n=1 \$Metal wl  
93016 5 0.00359833 (-93016) imp:n=1 \$Metal wl  
93017 5 0.00359833 (-93017) imp:n=1 \$Metal wl  
93018 5 0.00359833 (-93018) imp:n=1 \$Metal wl  
93019 5 0.00359833 (-93019) imp:n=1 \$Metal wl  
93020 5 0.00359833 (-93020) imp:n=1 \$Metal wl  
93021 5 0.00359833 (-93021) imp:n=1 \$Metal wl  
93022 5 0.00359833 (-93022) imp:n=1 \$Metal wl  
93023 5 0.00359833 (-93023) imp:n=1 \$Metal wl  
93024 5 0.00359833 (-93024) imp:n=1 \$Metal wl  
93025 5 0.00359833 (-93025) imp:n=1 \$Metal wl  
93026 5 0.00359833 (-93026) imp:n=1 \$Metal wl  
93027 5 0.00359833 (-93027) imp:n=1 \$Metal wl

c

c

c Floor2 Room 940/942/944/946/948/954/955/956/957/958  
94001 5 0.00359833 (-94001) imp:n=1 \$Metal wl  
94002 5 0.00359833 (-94002) imp:n=1 \$Metal wl  
94003 5 0.00359833 (-94003) imp:n=1 \$Metal wl  
94004 5 0.00359833 (-94004) imp:n=1 \$Metal wl  
94005 5 0.00359833 (-94005) imp:n=1 \$Metal wl  
94006 5 0.00359833 (-94006) imp:n=1 \$Metal wl  
94007 5 0.00359833 (-94007) imp:n=1 \$Metal wl  
94008 5 0.00359833 (-94008) imp:n=1 \$Metal wl  
94009 5 0.00359833 (-94009) imp:n=1 \$Metal wl  
94010 5 0.00359833 (-94010) imp:n=1 \$Metal wl  
94011 5 0.00359833 (-94011) imp:n=1 \$Metal wl  
94012 5 0.00359833 (-94012) imp:n=1 \$Metal wl  
94013 5 0.00359833 (-94013) imp:n=1 \$Metal wl  
94014 5 0.00359833 (-94014) imp:n=1 \$Metal wl  
94015 5 0.00359833 (-94015) imp:n=1 \$Metal wl  
94016 5 0.00359833 (-94016) imp:n=1 \$Metal wl  
94017 5 0.00359833 (-94017) imp:n=1 \$Metal wl  
94018 5 0.00359833 (-94018) imp:n=1 \$Metal wl  
94019 5 0.00359833 (-94019) imp:n=1 \$Metal wl  
94020 5 0.00359833 (-94020) imp:n=1 \$Metal wl  
94021 5 0.00359833 (-94021) imp:n=1 \$Metal wl  
94022 5 0.00359833 (-94022) imp:n=1 \$Metal wl  
94023 5 0.00359833 (-94023) imp:n=1 \$Metal wl  
94024 5 0.00359833 (-94024) imp:n=1 \$Metal wl  
94025 5 0.00359833 (-94025) imp:n=1 \$Metal wl  
94026 5 0.00359833 (-94026) imp:n=1 \$Metal wl  
94027 5 0.00359833 (-94027) imp:n=1 \$Metal wl  
94028 5 0.00359833 (-94028) imp:n=1 \$Metal wl  
94029 5 0.00359833 (-94029) imp:n=1 \$Metal wl

c

c	Floor2 Room	961/960/951/952/950	with the Elevator
96101	5	0.00359833	(-96101)
96102	5	0.00359833	(-96102)
96103	5	0.00359833	(-96103)
96104	5	0.00359833	(-96104)
96105	5	0.00359833	(-96105)
96106	5	0.00359833	(-96106)
96107	5	0.00359833	(-96107)
96108	5	0.00359833	(-96108)
96109	5	0.00359833	(-96109)
96110	5	0.00359833	(-96110)
96111	5	0.00359833	(-96111)
96112	5	0.00359833	(-96112)
96113	5	0.00359833	(-96113)
96114	5	0.00359833	(-96114)
96115	5	0.00359833	(-96115)
96116	5	0.00359833	(-96116)
96117	5	0.00359833	(-96117)
96118	5	0.00359833	(-96118)
96119	5	0.00359833	(-96119)
96120	5	0.00359833	(-96120)
96121	5	0.00359833	(-96121)
96122	5	0.00359833	(-96122)
96123	5	0.00359833	(-96123)
96124	5	0.00359833	(-96124)
96125	5	0.00359833	(-96125)
96126	5	0.00359833	(-96126)
96127	5	0.00359833	(-96127)
96128	5	0.00359833	(-96128)
96129	5	0.00359833	(-96129)
96130	5	0.00359833	(-96130)
96131	5	0.00359833	(-96131)
96132	5	0.00359833	(-96132)
96133	5	0.00359833	(-96133)
96134	5	0.00359833	(-96134)
96135	5	0.00359833	(-96135)
96136	5	0.00359833	(-96136)
96137	5	0.00359833	(-96137)
96138	5	0.00359833	(-96138)
96139	5	0.00359833	(-96139)
96140	5	0.00359833	(-96140)
96141	5	0.00359833	(-96141)
96142	5	0.00359833	(-96142)
96143	5	0.00359833	(-96143)
96144	5	0.00359833	(-96144)

C  
C

c

c

c This room contains all of the surfaces fo

90001 5 0.00359833 (-90001) imp:n=1 \$Me

90002	5	0.00359833	(-90002)	imp:n=1	\$Metal wl
90003	5	0.00359833	(-90003)	imp:n=1	\$Metal wl
90004	5	0.00359833	(-90004)	imp:n=1	\$Metal wl
90005	5	0.00359833	(-90005)	imp:n=1	\$Metal wl
90006	5	0.00359833	(-90006)	imp:n=1	\$Metal wl
90007	5	0.00359833	(-90007)	imp:n=1	\$Metal wl
90008	5	0.00359833	(-90008)	imp:n=1	\$Metal wl
90009	15	-0.4751	(-90009)	imp:n=1	\$Exterior wl
90010	15	-0.4751	(-90010)	imp:n=1	\$Exterior wl
90011	15	-0.4751	(-90011)	imp:n=1	\$Exterior wl

c

C

c

c

c Floor2 Room 903/904/South Mechanical - Mech/Roofs  
88281-15-0-4751 (88281) rev 1 \$E+1

90301 15 -0.4751 (-90301) imp:n=1 \$Ext wl  
 90302 15 -0.4751 (-90302) imp:n=1 \$Ext wl

90303 3 -2.3 (-90303) imp:n=1 \$Conc Filled  
 90304 5 0.00359833 (-90304) imp:n=1 \$Metal wl  
 90305 5 0.00359833 (-90305) imp:n=1 \$Metal wl  
 90306 5 0.00359833 (-90306) imp:n=1 \$Metal wl  
 90307 5 0.00359833 (-90307) imp:n=1 \$Metal wl  
 90308 5 0.00359833 (-90308) imp:n=1 \$Metal wl  
 90309 5 0.00359833 (-90309) imp:n=1 \$Metal wl  
 90310 3 -2.3 (-90310) imp:n=1 \$Conc Filled  
 90311 3 -2.3 (-90311) imp:n=1 \$Conc Filled  
 90312 3 -2.3 (-90312) imp:n=1 \$Conc Filled  
 90313 3 -2.3 (-90313) imp:n=1 \$Conc Filled  
 90314 3 -2.3 (-90314) imp:n=1 \$Conc Filled  
 90315 3 -2.3 (-90315) imp:n=1 \$Conc Filled  
 90316 3 -2.3 (-90316) imp:n=1 \$Conc Filled  
 90319 3 -2.3 (-90319) imp:n=1 \$Conc Filled  
 90320 3 -2.3 (-90320) imp:n=1 \$Conc Filled  
 c  
 c  
 c //Begin East Section of Floor2///  
 c  
 c  
 c Floor2 Room 609/608/607/Topp of hot cells  
 60901 15 -0.4751 (-60901) imp:n=1 \$Ext wl  
 60902 3 -2.3 (-60902) imp:n=1 \$Conc Filled  
 60903 5 0.00359833 (-60903) imp:n=1 \$Metal wl  
 60905 5 0.00359833 (-60905) imp:n=1 \$Metal wl  
 60906 5 0.00359833 (-60906) imp:n=1 \$Metal wl  
 60907 5 0.00359833 (-60907) imp:n=1 \$Metal wl  
 60908 15 -0.4751 (-60908) imp:n=1 \$Ext wl  
 60909 5 0.00359833 (-60909) imp:n=1 \$Metal wl  
 60910 5 0.00359833 (-60910) imp:n=1 \$Metal wl  
 60911 5 0.00359833 (-60911) imp:n=1 \$Metal wl  
 60912 5 0.00359833 (-60912) imp:n=1 \$Metal wl  
 60913 5 0.00359833 (-60913) imp:n=1 \$Metal wl  
 60914 5 0.00359833 (-60914) imp:n=1 \$Metal wl  
 60915 5 0.00359833 (-60915) imp:n=1 \$Metal wl  
 60916 5 0.00359833 (-60916) imp:n=1 \$Metal wl  
 60917 5 0.00359833 (-60917) imp:n=1 \$Metal wl  
 60918 13 -7.92 (-60918) imp:n=1 \$\$S  
 60919 5 0.00359833 (-60919) imp:n=1 \$Metal wl  
 60920 15 -0.4751 (-60920) imp:n=1 \$Ext wl  
 60921 3 -2.3 (-60921) imp:n=1 \$Conc Filled  
 60922 15 -0.4751 (-60922) imp:n=1 \$Ext wl  
 60923 15 -0.4751 (-60923) imp:n=1 \$Ext wl  
 60924 3 -2.3 (-60924) imp:n=1 \$Conc Filled  
 60925 3 -2.3 (-60925) imp:n=1 \$Conc Filled  
 60926 13 -7.92 (-60926) imp:n=1 \$\$S  
 60927 3 -2.3 (-60927) imp:n=1 \$Conc Filled  
 60928 13 -7.92 (-60928) imp:n=1 \$\$S  
 60929 13 -7.92 (-60929) imp:n=1 \$\$S  
 60930 3 -2.3 (-60930) imp:n=1 \$Conc Filled  
 60931 3 -2.3 (-60931) imp:n=1 \$Conc Filled  
 60932 13 -7.92 (-60932) imp:n=1 \$\$S  
 60933 13 -7.92 (-60933) imp:n=1 \$\$S  
 60934 13 -7.92 (-60934) imp:n=1 \$\$S  
 60935 3 -2.3 (-60935) imp:n=1 \$Conc Filled  
 60936 15 -0.4751 (-60936) imp:n=1 \$Ext wl  
 60937 15 -0.4751 (-60937) imp:n=1 \$Ext wl  
 60938 13 -7.92 (-60938) imp:n=1 \$\$S  
 60939 13 -7.92 (-60939) imp:n=1 \$\$S  
 60940 3 -2.3 (-60940) imp:n=1 \$Conc Filled  
 60941 15 -0.4751 (-60941) imp:n=1 \$Ext wl  
 60942 15 -0.4751 (-60942) imp:n=1 \$Ext wl  
 60943 15 -0.4751 (-60943) imp:n=1 \$Ext wl  
 60944 15 -0.4751 (-60944) imp:n=1 \$Ext wl  
 60945 3 -2.3 (-60945) imp:n=1 \$Conc Filled  
 60946 3 -2.3 (-60946) imp:n=1 \$Conc Filled  
 60947 13 -7.92 (-60947) imp:n=1 \$\$S  
 60948 13 -7.92 (-60948) imp:n=1 \$\$S  
 60949 13 -7.92 (-60949) imp:n=1 \$\$S



```

90318 6 -0.04855 (-90318) imp:n=1 $Roomspace 904
60957 6 -0.04855 (-60957) imp:n=1 $Roomspace 609 Room Partial Fill
60958 6 -0.04855 (-60958) imp:n=1 $Roomspace 608
60959 6 -0.04855 (-60959) imp:n=1 $Roomspace 607
60960 1 -0.001202 (-60960) imp:n=1 $Roomspace 607N
c
c
c Begin Northwest Section of Floor3
c *****Notes for this section of Cells*****
c
c Floor3 Room 611/Top of the Hot Cells
61101 3 -2.3 (-61101) imp:n=1 $Conc Filled
61102 3 -2.3 (-61102) imp:n=1 $Conc Filled
61103 3 -2.3 (-61103) imp:n=1 $Conc Filled
61104 3 -2.3 (-61104) imp:n=1 $Conc Filled
61105 5 0.00359833 (-61105) imp:n=1 $Metal wl
61106 5 0.00359833 (-61106) imp:n=1 $Metal wl
61107 5 0.00359833 (-61107) imp:n=1 $Metal wl
61108 5 0.00359833 (-61108) imp:n=1 $Metal wl
61109 3 -2.3 (-61109) imp:n=1 $Conc Filled
61110 3 -2.3 (-61110) imp:n=1 $Cone Filled
61111 3 -2.3 (-61111) imp:n=1 $Conc Filled
61112 3 -2.3 (-61112) imp:n=1 $Conc Filled
61113 3 -2.3 (-61113) imp:n=1 $Conc Filled
61114 3 -2.3 (-61114) imp:n=1 $Cone Filled
61115 3 -2.3 (-61115) imp:n=1 $Conc Filled
61116 3 -2.3 (-61116) imp:n=1 $Conc Filled
61117 3 -2.3 (-61117) imp:n=1 $Conc Filled
61118 3 -2.3 (-61118) imp:n=1 $Cone Filled
61119 3 -2.3 (-61119) imp:n=1 $Conc Filled
61120 13 -7.92 (-61120) imp:n=1 $SS
61121 13 -7.92 (-61121) imp:n=1 $SS
61122 13 -7.92 (-61122) imp:n=1 $SS
61123 13 -7.92 (-61123) imp:n=1 $SS
61124 13 -7.92 (-61124) imp:n=1 $SS
61125 13 -7.92 (-61125) imp:n=1 $SS
c
c
c
c
c
c Cell that combines all of the 2nd floors subsections
201 0 (-992 201 212 213 214 215 218 90311 90312 90313
         90314 90315 90316 90319 90320 92023 90318 #60956
         #90301 ) imp:n=1
c
c
c
c Begin Cells for NW Section of Floor2
c
c Largest cell that envelopes all of the NW Section
202 1 -0.001202 (-201 203 204 205 206 207 #91012 #91819 #92701
         #92728 #92703 208 #92023 209 210 211 #96104
         #92023 #90318 #90301 #90308) imp:n=1 $NW Section Box
c
c
c SW Box
203 1 -0.001202 (-203 91002 91003 91004 91005 91006 91013 91007
         91008 91014 90308 90301 ) imp:n=1
c
c
c W Box
204 1 -0.001202 (-204 91011 91201 91202 91203 91204 91205 91206 91207
         91208 91209 91210 91211 91805 ) imp:n=1
c
c
c NW Box
205 1 -0.001202 (-205 91301 91302 91303 91304 91305 91306 91307 91308
         91309 91310 91311 91312 91313 91314 91315 91316 91317

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91318 91801 91802 91803 91804 91806 91807 91808 91809
91810 91811 91812 91813 91814 91815 91816 91818 91821
91822 91823 91824 91825 91826 ) imp:n=1
c
c
c S1 Box
206 1 -0.001202 (-206 91009 91010 92724 92725 92726 92727 #92701
#92728 92702 #90308 #90318) imp:n=1
c
c
c S2 Box
207 1 -0.001202 (-207 #92703 92704 92705 92706 92707 92708 92709
92710 92711 92712 92713 92714 92715 92716 92717
92718 92719 92720 92721 92722 92723 92728 92729
92730 92731 92732 92733 92734 93001 ) imp:n=1
c
c
c N Box
208 1 -0.001202 (-208 92001 92002 92003 92004 92005 92006 92007
92008 92009 92010 92011 92012 92013 92014 92015
92016 92017 92018 92019 92020 92021 92022 92024
92025 92026 92027 92028 92029 92030 92031 92032
92033 91820 #96104 ) imp:n=1
c
c
c SE1 Box
209 1 -0.001202 (-209 93002 93003 93004 93005 93006 93007 93008
93009 93010 93011 93012 93013 93014 93015 93016
93017 93018 93019 93020 93021 93022 93023 93024
93025 93026 93027 93028 93029 93030 93031 93032
93033 93034 93035 93036 93037 ) imp:n=1
c
c
c SE2 Box
210 1 -0.001202 (-210 94001 94002 94003 94004 94005 94006 94007
94008 94009 94010 94011 94012 94013 94014 94015
94016 94017 94018 94019 94020 94021 94022 94023
94024 94025 94026 94027 94028 94029 94030 94031
94032 94033 94034 94035 94036 94037 94038 94039
) imp:n=1
c
c
c NE Box
211 1 -0.001202 (-211 96101 96102 96103 96105 96106 96107 96108
96109 96110 96111 96112 96113 96114 96115 96116
96117 96118 96119 96120 96121 96122 96123 96124
96125 96126 96127 96128 96129 96130 96131 96132
96133 96134 96135 96136 96137 96138 96139 96140
96141 96142 96143 96144 96145 96146 96147 #96104
) imp:n=1
c
c
c
c Begin Cells for NE Section of Floor2
c
212 1 -0.001202 (-212 90001 90002 90003 90004 90005 90006 90007
90008 90009 90010 90011 #92023 #60956 #61101
) imp:n=1
c
c
c Begin Cells for S Section of Floor2
c
213 1 -0.001202 (-213 90301 90302 90303 90304 90305 90306 90307
90309 90310 90317 #90318 #60956 #90308
) imp:n=1
c
c
c
c Begin Cells for E Section of Floor2
c

```



c the cells together. This had to be done to avoid overloading the data type associated with  
 c cell cards. These boxes are purely for the codes sake and in no way affect the actual geometry  
 c of the model.  
 c  
 999 rpp -1200 4000 -3000 4000 -304.8 1498.6 \$Void  
 c  
 c  
 c Void box surrounding model  
 990 rpp -1200 4000 -3000 4000 -304.8 442 \$Void  
 c  
 c  
 c NW Section of Basement 1  
 401 46 rpp -4.5 817 -290 1091.5 0 432.5 \$Cell box NW Section  
 c  
 c  
 c Begin North-Center Section of the Central Section of Basement1  
 402 45 rpp -48 526 -96 549.5 0 432.5 \$Cell box W  
 403 45 rpp 526 998 -96 621.5 0 432.5 \$Cell box E  
 c  
 c  
 c Begin Northeast Section of the Central Section of Basement1  
 404 44 rpp -407 639 -290 446 0 432.5 \$Cell box SW  
 405 44 rpp 639 1123.5 -290 1091.5 0 432.5 \$Cell box E  
 c  
 c  
 c Begin West Section of Basement1  
 406 41 rpp -179 242 0 1152 0 432.5 \$Cell box W Section  
 c  
 c  
 c Begin Southwest Section of the Central Section of Basement1  
 407 rpp -10 1187.5 -10 998.5 0 432.5 \$Cell box S Section  
 c  
 c  
 c Begin Southeast Section of the Central Section of Basement1  
 408 42 rpp -41 1123.5 -15.5 993 0 432.5 \$Section Cell box  
 c  
 c  
 c Begin East Section of Basement1  
 409 43 rpp -10 1083 -10 1600 0 432.5 \$Section Cell box  
 c  
 c  
 c Begin South Section of Basement1  
 410 47 rpp -12.8 245 -101.75 867.5 152.4 432.5 \$W Cell box  
 411 47 rpp 245 1080 -101.75 200 152.4 432.5 \$S Cell box  
 412 47 rpp 1080 1335.2 -101.75 867.5 152.4 432.5 \$E Cell box  
 413 47 rpp 245 1080 200 867.5 152.4 432.5 \$Central Cell box  
 c  
 c  
 c Below are the Decks of Basement1 and the Sand surrounding the building  
 c The southern mezzanine section is set 5ft above the B1 Deck. This is an observed measured distance because  
 c I have found no blueprint that clearly defines this distance. There is a small gap between Rm23B and the  
 c top of Rm32 where there is no sand and just air. This gap was left for the sake of saving time. No conservancy  
 c is lost. There is no sand up to the grade height in the SE corner of the building. This was done to be conservative.  
 c There are numerous areas in the SE that do not have a backfill to the same grade as the rest of the building.  
 c There is also a loading dock located in the SE corner which is simply free space.  
 414 rpp -10 2390 -10 2390 -30.5 0 \$Central Section of Basement foundation Deck  
 415 rpp 2390 2931.5 -10 1551.5 -30.5 0 \$East Section of B1 foundation Deck  
 416 rpp 501.8 1849.8 -903 -10 121.9 152.4 \$South Section of B1 foundation Deck  
 417 rpp -264 -10 121 538.5 -30.5 0 \$\$SW B1 foundation Deck  
 418 rpp -431 -10 538.5 1186.5 -30.5 0 \$W B1 foundation Deck  
 419 rpp -1000 4000 -2000 4000 -304.8 -30.5 \$Sand 10ft thick under building  
 420 rpp 501.8 1849.8 -903 -10 -30.5 121.9 \$Sand filling the gap below South Section of B1  
 421 rpp -10 2390 2390 2999.6 -30.5 327.7 \$N of B1 20ft Thick sand up to a building grade of 327.7cm  
 422 rpp 2390 2999.6 1551.5 2999.6 -30.5 327.7 \$NE of B1 20ft Thick sand up to a building grade of 327.7cm  
 423 rpp 501.8 1849.8 -1512.6 -903 -30.5 327.7 \$S of B1 20ft Thick sand up to a building grade of 327.7cm  
 424 rpp -619.6 501.8 -1512.6 -10 -30.5 327.7 \$S2 20ft Thick sand up to a building grade of 327.7cm  
 425 rpp -873.6 -264 121 536.5 -30.5 327.7 \$\$SW 20ft Thick sand up to a building grade of 327.7cm  
 426 rpp -1040.6 -431 536.5 1186.5 -30.5 327.7 \$W 20ft Thick sand up to a building grade of 327.7cm  
 427 rpp -609.6 -10 -10 121 -30.5 327.7 \$\$SW B1 20ft Thick sand up to a building grade of 327.7cm  
 428 rpp -609.6 -10 1186.5 2999.6 -30.5 327.7 \$NW 20ft Thick sand up to a building grade of 327.7cm

c  
 c  
 c  
 c Basement1 ceiling/First Floor Deck From the previous methodology of NCS99 the ceiling of B1 was smeared  
 c to a slab with a thickness of 3.75". It was found from investigation that 3.75" was the approximate  
 c average of the thickness of the ceiling. Drawing H-3-306083-2.DWG shows the structure of the ceiling and is to scale.  
 430 rpp -10 2390 -10 2390 432.5 442 \$Central Section of Basement ceiling  
 431 rpp 2390 2931.5 -10 1551.5 432.5 442 \$East Section of B1 ceiling  
 432 rpp 501.8 1849.8 -903 -10 432.5 442 \$South Section of B1 ceiling  
 433 rpp -264 -10 121 548.5 432.5 442 \$SW B1 ceiling  
 434 rpp -431 -10 548.5 1186.5 432.5 442 \$W B1 ceiling  
 c  
 c  
 c First Crack at a minimum accident TAG=TAGPuPu  
 440 44 s 950 1000 50 19.54 \$ Pu Sphere N Rm52 in Rm45  
 c 440 s 390 200 50 19.54 \$ Pu Sphere in Rm22  
 c 440 s 2303.5 1228.5 50 19.54 \$ Pu Sphere in Rm48 in cells 405 and 4808  
 c 440 s 1314.5 2300.5 50 19.54 \$ Pu Sphere in Rm90  
 c 440 46 s 40 1288.5 50 19.54 \$ Pu Sphere in NW corner B1 Rm45  
 c 440 46 s 1140 -260 50 19.54 \$ Pu Sphere in SW corner of NW section -Center of B1  
 c 440 41 s 50 50 50 19.54 \$ Pu Sphere in SW corner of Rm23B in cell 425 2321  
 c 440 41 s 50 353 50 19.54 \$ Pu Sphere in W of Rm23 in cell 425 2322  
 c 440 41 s 160 800 50 19.54 \$ Pu Sphere in E of Rm32 (Under SAL) in cell 426  
 c 440 41 s -130 1020 50 19.54 \$ Pu Sphere in NW of Rm32 (Under SAL)  
 c 440 42 s 525 675 50 19.54 \$ Pu Sphere in Rm34 B1  
 c 440 47 s 820 30 202.5 19.54 \$ Pu Sphere in LR Mezzanine  
 c 440 43 s 520 40 50 19.54 \$ Pu Sphere in Rm40c  
 c  
 c  
 c First Floor Accident Locations  
 c 440 12 s -370 1000 492 19.54 \$ Pu Sphere in Rm203  
 c 440 17 s 50 50 492 19.54 \$ Pu Sphere in LR  
 c 440 18 s 40 780 492 19.54 \$ Pu Sphere in Rm327A  
 c 440 11 s 1075 810 492 19.54 \$ Pu Sphere in Rm528  
 c 440 15 s 1020 400 492 19.54 \$ Pu Sphere in Truck Lock  
 c 440 17 s 1770 925 492 19.54 \$ Pu Sphere in Rm119  
 c 440 14 s 165 720 492 19.54 \$ Pu Sphere in Rm410  
 c  
 c  
 c Second Floor Accident Locations  
 c  
 c 440 s 2875 1520 1122 19.54 \$ Pu Sphere Above Rm 603 in cell 214  
 c 440 s 44.5 2350 934 19.54 \$ Pu Sphere Above Rm 327 in Rm903 cell202  
 c  
 c  
 c  
 c 440 s 50 19.54 \$ Pu Sphere in Rm  
 c  
 c  
 c  
 c Below are all of the Detectors for all of building 325. The detectors are all in one section  
 c Because doing so makes it much easier to iterate their locations throughout the model TAG=TAGdetectors  
 c  
 c Location of the Surface the detector is attached to  
 c rpp 257 267 269.5 277.5 0 432.5  
 461 rcc 272.7 263.35 412.2 0 20.3 0 5.7 \$B1 N Column Rm22  
 c rpp 267 297.5 258.25 288.75 391.9 432.5  
 c  
 c  
 c Location of the Surface the detector is attached to  
 c 42 rpp 302 312 983 993 391.9 432.5  
 462 42 rcc 317.7 977.85 412.2 0 20.3 0 5.7 \$B1 Next(2nd) Column moving E  
 c  
 c 42 rpp 312 342.5 972.75 1003.25 391.9 432.5  
 c  
 c Location of the Surface the detector is attached to  
 c 42 rpp 0 10 504 512 391.9 432.5  
 463 42 rcc 15.7 497.85 412.2 0 20.3 0 5.7 \$B1 W Column above(4516) 2nd column above origin  
 c 42 rpp 10 40.5 492.75 523.25 391.9 432.5  
 c





9303 45 rpp	310.5	526	0	15	0	432.5	\$S wall	Rm93
9304 45 rpp	514	526	15	241	0	432.5	\$E wall	Rm93
9305 45 rpp	524	526	241	273	0	432.5	\$E wall	Rm93
9306 45 rpp	513.75	526	273	549.5	0	304.1	\$E wall	Rm 93-Rm90
9307 45 rpp	355	513.75	372	384	0	304.1	\$N wall	Rm93
9308 45 rpp	355	371.5	329	372	0	432.5	\$N wall	Rm93
9309 45 rpp	351.5	355	329	341	0	432.5	\$N wall stub	Rm93
9310 45 rpp	187	312.5	329	341	0	432.5	\$NW wall	Rm93
9311 45 rpp	235	241	325	329	0	432.5	\$N Closet stub	Rm93
9312 45 rpp	187	199	280	329	0	432.5	\$W Closet wall	Rm93
9313 45 rpp	199	246	280	293	0	432.5	\$S closet Wall	Rm93
9314 45 rpp	232	246	268	280	0	432.5	\$Closet Stub	Rm93
9315 45 rpp	246	260.5	278	295	0	432.5	\$Closet Stub	Rm93
9316 45 rpp	241	246	293	295	0	432.5	\$Closet Stub	Rm93
9317 45 rpp	235	241	293	297	0	432.5	\$Closet Stub	Rm93
9318 45 rpp	355	373	280	296	0	432.5	\$Central Column	Rm93
9319 45 rpp	246	513.75	15	278	0	432.5	\$Roomspace	93

c

c

c Basement1 Room 94/94A/94B

9401 45 rpp	526	606	0	8	0	432.5	\$S wall	Rm94
9402 45 rpp	642	662	0	8	0	432.5	\$S wall	Rm94
9403 45 rpp	662	670	-42	133	0	432.5	\$E wall	Rm94
9404 45 rpp	670	671	-5	5	0	432.5	\$\$E Wall Stub	Rm94-Rm95
9405 45 rpp	661	662	-5	0	0	432.5	\$\$E Wall Stub	Rm94-Rm95
9406 45 rpp	599.5	728.5	133	141	0	432.5	\$N wall	Rm94-Rm95
9407 45 rpp	599.5	607.5	141	239	0	432.5	\$W wall	
9408 45 rpp	580.75	599.5	231.5	235	0	432.5	\$S wall	Rm94A
9409 45 rpp	526	545.75	231.5	235	0	432.5	\$S wall	Rm94A
9410 45 rpp	526	559	275	278.5	0	432.5	\$N wall	Rm94A
9411 45 rpp	592	599.5	275	278.5	0	432.5	\$N wall	Rm94A
9412 45 rpp	599.5	607.5	271	369	0	432.5	\$W wall	Rm94B
9413 45 rpp	526	700	369	377	0	432.5	\$N wall	Rm94B
9414 45 rpp	526	662	8	133	0	432.5	\$Roomspace	94 Partially Filled
9415 45 rpp	526	599.5	278.5	369	0	432.5	\$Roomspace	94B

c

c

c Basement1 Room 95

9501 45 rpp	662	670	-96	-78	0	432.5	\$\$SW wall	Rm95
9502 45 rpp	670	877.5	-96	-88	0	432.5	\$\$S wall	Rm95
9503 45 rpp	833.5	841.5	-88	133	0	432.5	\$E wall	Rm95
9504 45 rpp	764.5	878.5	133	141	0	432.5	\$N wall	Rm95
9505 45 rpp	670	833.5	-88	133	0	432.5	\$Roomspace	95

c

c

c Basement1 Room 96/96A

9601 45 rpp	913.5	972	-96	-88	0	432.5	\$S wall	Rm96
9602 45 rpp	964	972	-88	-6	0	432.5	\$E wall	Rm96-Rm96a
9603 45 rpp	962	974	-6	6	0	432.5	\$Column in wall	Rm96
9604 45 rpp	915.5	962	-4	4	0	432.5	\$N wall	Rm96
9605 45 rpp	841.5	879.5	-4	4	0	432.5	\$N wall	Rm96
9606 45 rpp	964	972	6	282	0	432.5	\$E wall	Rm96-Rm96A-Rm97-Rm97A
9607 45 rpp	914.5	964	133	141	0	432.5	\$N wall	Rm96A
9608 45 rpp	841.5	964	-88	-4	0	432.5	\$Roomspace	96
9609 45 rpp	841.5	964	4	133	0	432.5	\$Roomspace	96A

c

c

c Basement Room 97/97A

9701 45 rpp	773	964	197.5	201.5	0	432.5	\$S wall	Rm97A
9702 45 rpp	773	777	201.5	205.5	0	432.5	\$S wall stub	Rm97A
9703 45 rpp	773	777	277.5	369	0	432.5	\$W wall	Rm97A
9704 45 rpp	962	974	282	294	0	432.5	\$Column in E wall	Rm97A
9705 45 rpp	964	972	294	377	0	432.5	\$E wall	Rm97A
9706 45 rpp	771	964	369	377	0	432.5	\$N wall	Rm97A
9707 45 rpp	660	672	282	294	0	432.5	\$Column Rm97	
9708 45 rpp	607.5	773	141	369	0	432.5	\$Roomspace	97
9709 45 rpp	777	962	201.5	369	0	432.5	\$Roomspace	97A

c

c

c Basement Room 98

9801 45 rpp 526 667.8 459 467 0 432.5 \$N wall Rm98  
 9802 45 rpp 526 667.8 377 459 0 432.5 \$Rooms space 98

c

c

c Basement Room 45 East Section

4560	45	rrp	938	942	453.5	513.5	0	432.5	\$W	wall	Sump	Rm45
4561	45	rrp	942	998	509.5	513.5	0	432.5	\$N	wall	Sump	Rm45
4562	45	rrp	994	998	453.5	509.5	0	432.5	\$E	wall	Sump	Rm45
4563	45	rrp	942	994	453.5	457.5	0	432.5	\$S	wall	Sump	Rm45
4564	45	rrp	661	671	535	545	0	432.5	\$Column	NW	Rm45	
4565	45	rrp	963	973	535	545	0	432.5	\$Column	NE	Rm45	
4566	45	rrp	526	530.5	549.5	559.5	0	432.5	\$Stub	NW	Rm45	
4567	45	rrp	530.5	532	549.5	557.5	0	432.5	\$Stub	NW	Rm45	
4568	45	rrp	568	570	549.5	557.5	0	432.5	\$Stub	N	wall	Rm45
4569	45	rrp	570	1482	549.5	559.5	0	432.5	\$N	wall	Rm45	
-4570	45	rrp	516	526	561.5	621.5	0	432.5	\$W	wall	Steinwall	Rm45

c 4570 45 rpp 516 526 561.5 621.5 0 432.5 \$W wall Stairwell Rm4.

3

C

c = R<sub>1</sub> + R<sub>2</sub> + R<sub>3</sub> + R<sub>4</sub> + R<sub>5</sub>

c Basement Room 90/Elevator Room

9001	45	ppp	355	367	384	446.5	0	304.1	\$W wall Rm90
9002	45	ppp	367	513.75	384	391.5	0	304.1	\$Inside S wall Rm90
9003	45	ppp	506.25	513.75	391.5	549.5	0	304.1	\$Inside E wall Rm90
9004	45	ppp	372.5	506.25	542	549.5	0	304.1	\$Inside N wall Rm90
9005	45	ppp	367	526	549.5	561.5	0	432.5	\$N outside wall Rm90
9006	45	ppp	355	367	485.5	549.5	0	304.1	\$W wall Rm90
9007	45	ppp	367	372.5	529	549.5	0	304.1	\$W wall Stub Rm90
9008	45	ppp	364	367	559.5	561.5	0	432.5	\$NW wall Stub Rm90
9009	45	ppp	-879.5	367	549.5	559.5	0	432.5	\$N wall hallway Rm90-----
9010	45	ppp	241	257	532	549.5	0	432.5	\$Stub wall Elev Rm
9011	45	ppp	95	103	375	549.5	0	432.5	\$W wall Elevator Rm
9012	45	ppp	145	153	379	493	0	432.5	\$W wall Elev
9013	45	ppp	153	242	485	493	0	432.5	\$N wall Elev
9014	45	ppp	233	242	473	485	0	432.5	\$E wall Elev
9015	45	ppp	233	242	387	405	0	432.5	\$E wall Elev
9016	45	ppp	153	242	379	387	0	432.5	\$S wall Elev
9017	45	ppp	372.5	506.25	391.5	542	0	304.1	\$Rooms space 90 Partially Filled

C

6

c

\*\*\*\*\*Begin Northeast Section of the Central Section of Basement\*\*\*\*\*

c The origin (0,0,0) was designated as the south west corner of the south westernmost pillar of the exploded basement drawing H-3-3050010-1.DWG. This pillar is not under the yellow dashed line because these pillars were included in the south east Section model.

6

c

### c Basement Room 45

C Basement Room 45

4575	44	ropp	0	10	0	10	0	432.5	\$SW Column ORIGIN Designated (0,0,0) Here
4576	44	ropp	302	312	0	10	0	432.5	\$Next(2nd) Column moving Eastward Rm45
4577	44	ropp	603	615	-1	11	0	432.5	\$3rd Column moving East Rm45
4578	44	ropp	856.5	865.5	249	259	0	432.5	\$Column between Rm58 and Rm54
4579	44	ropp	856.5	865.2	537	547	0	432.5	\$Column directly N of (4504)
4580	44	ropp	1109	1119	825	835	0	432.5	\$Column between Rm52 and Main wall
4581	44	ropp	719	729	1077	1087	0	432.5	\$NW most Column Rm45
4582	44	ropp	856.5	865.5	1077	1087	0	432.5	\$Next(2nd) Column moving Eastward Rm45
4583	44	ropp	1109	1119	1077	1087	0	432.5	\$3rd Column moving East Rm45

6

6

c Basement room 48

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c  
c





c

c Basement Room 22A

2210 rpp 155 160.5 363.5 511.5 0 432.5 \$W wall Rm22a  
 2211 rpp 153.5 257 511.5 515.5 0 432.5 \$N wall Rm22a  
 2212 rpp 257 267 509.5 517.5 0 432.5 \$Column in N wall Rm22a  
 2213 rpp 267 509.5 511.5 515.5 0 432.5 \$N wall Rm22a  
 2214 rpp 509.5 519.5 509.5 517.5 0 432.5 \$Column in N wall Rm22a  
 2215 rpp 519.5 811.5 511.5 515.5 0 432.5 \$N wall Rm22a-Rm31a  
 2216 rpp 524.5 528.5 351.5 511.5 0 432.5 \$E wall Rm22a  
 2217 rpp 478.25 524.5 356 359 0 432.5 \$SE wall Rm22a  
 c 2218 rpp 279.25 443.25 356 359 0 432.5 \$SW Wall Rm22a  
 2219 rpp -10 0 0 287.5 0 432.5 \$Boundary wall between West and Southwest Sections  
 2220 rpp -10 0 359.5 564 0 432.5 \$Boundary wall between West and Southwest Sections  
 2221 rpp -10 1187.5 -10 0 0 432.5 \$Boundary wall between West and Southeast Sections  
 2222 rpp 160.5 524.5 359 511.5 0 432.5 \$Roomspace 22A Partially Filled

c

c

c Basement Room 23A

2301 rpp 0 161 130 135.5 0 432.5 \$S wall Rm23a  
 2302 rpp 155.5 161 135.5 284.5 0 432.5 \$E wall Rm23a  
 2303 rpp 61 155.5 279 284.5 0 432.5 \$NE wall Rm23a  
 2304 rpp 0 26 279 284.5 0 432.5 \$NW wall Rm23a  
 2305 rpp 5 14.5 268.5 278.5 0 432.5 \$NW Column Rm23a  
 2306 rpp 0 155.5 135.5 279 0 432.5 \$Roomspace 23A

c

c

c Basement Room 30A

3001 rpp 523.5 576.25 237.75 242.75 0 432.5 \$NW wall Rm30a  
 3002 rpp 611.25 1118.5 237.75 242.75 0 432.5 \$NE wall Rm30a  
 3003 rpp 1113.5 1118.5 158.5 237.75 0 432.5 \$SE wall Rm30a  
 3004 rpp 1113.5 1118.5 13.5 86.5 0 432.5 \$SE wall Rm30a  
 3005 rpp 1113.5 1123.5 5.5 13.5 0 432.5 \$SE Column Rm30a  
 3006 rpp 811.5 821.5 4.5 14.5 0 432.5 \$S Column Rm30a  
 3007 rpp 523.5 1113.5 0 237.75 0 432.5 \$Roomspace 30A

c

c

c Basement Room 31/31A

c 3101 rpp 528.5 818.25 358 363 0 432.5 \$S wall Rm31  
 3102 rpp 806.75 811.75 363.5 402.75 0 432.5 \$E wall Rm31  
 3103 rpp 806.75 811.75 438.75 508.5 0 432.5 \$E wall Rm31 major wall  
 3104 rpp 806.75 811.5 508.5 511.5 0 432.5 \$E wall Rm31(Small piece atop major wall)  
 c 3105 rpp 854.25 1041 358 363 0 432.5 \$S wall Rm31a  
 3106 rpp 1037 1041 363 509.5 0 432.5 \$E wall Rm31a  
 3107 rpp 821.5 1123.5 509.5 517.5 0 432.5 \$N wall Rm31a  
 3108 rpp 811.5 821.5 508.5 518.5 0 432.5 \$NW Column in N wall Rm31A  
 3109 rpp 528.5 806.75 363 511.5 0 432.5 \$Roomspace 31A  
 3110 rpp 811.75 1037 363 509.5 0 432.5 \$Roomspace 31 Partially Filled

c

c

c Basement Room 33

3301 rpp 812.5 820.5 518.5 748.5 0 432.5 \$W wall Rm33  
 3302 rpp 811.5 821.5 748.5 758.5 0 432.5 \$NW wall Rm33  
 3303 rpp 821.5 1140 749.5 757.5 0 432.5 \$N wall Rm33  
 3304 rpp 1117 1121 608 749.5 0 432.5 \$E wall Rm33  
 3305 rpp 1117 1121 517.5 548 0 432.5 \$SE wall Rm33  
 3306 rpp 820.5 1117 517.5 749.5 0 432.5 \$Roomspace 33

c

c

c Basement Room 45

4584 rpp 4.5 14.5 748.5 758.5 0 432.5 \$W Column Rm45  
 4585 rpp 257 267 749.5 757.5 0 432.5 \$W Central Column Rm45  
 4586 rpp 509.5 519.5 749.5 757.5 0 432.5 \$E Central Column Rm45  
 4587 rpp 4.5 14.5 988.5 998.5 0 432.5 \$NW Column Rm45 ON BORDER OF SECTION  
 4588 rpp 257 267 988.5 998.5 0 432.5 \$NW Column Rm45 ON BORDER OF SECTION  
 4589 rpp 509.5 519.5 988.5 998.5 0 432.5 \$N Column Rm45 ON BORDER OF SECTION  
 4590 rpp 811.5 821.5 988.5 998.5 0 432.5 \$NE Column Rm45 ON BORDER OF SECTION  
 4591 rpp 1113.5 1123.5 988.5 998.5 0 432.5 \$NE Column Rm45 ON BORDER OF SECTION  
 4592 rpp 811.5 821.5 268.5 278.5 0 432.5 \$W Central Column between Rm31 and Rm30  
 4593 rpp 1113.5 1123.5 269.5 277.5 0 432.5 \$E Central Column between Rm31 and Rm30

c







c Basement1 Room 7

701 47 rpp -4.8 0 -4 805.5 152.4 432.5 \$West wall Rm7-Rm17  
 702 47 rpp 0 147.5 146 152 152.4 432.5 \$N wall  
 703 47 rpp 141.5 147.5 152 198.25 152.4 432.5 \$N wall  
 704 47 rpp 147.5 203.5 192.25 198.25 152.4 432.5 \$N wall  
 705 47 rpp 203.5 208.5 180.5 241.75 152.4 432.5 \$NE wall Rm7-Rm9  
 706 47 rpp 203.5 208.5 -4 144.5 152.4 432.5 \$E wall Rm7  
 707 47 rpp 0 203.5 -4 0 152.4 432.5 \$S wall Rm7  
 708 47 rpp -12.8 -4.8 -25.5 867.5 152.4 432.5 \$W Main Structural Wall South Section Basement1  
 709 47 rpp -4.8 8.7 -17.5 -4 152.4 432.5 \$Block1 in SW corner Main wall  
 710 47 rpp -4.8 220.7 -25.5 -17.5 152.4 432.5 \$SW Main Structural Wall South Section Basement1  
 711 47 rpp 94.7 106.7 -17.5 -4 152.4 432.5 \$Block2 in main Wall  
 712 47 rpp 195.7 207.7 -17.5 -4 152.4 432.5 \$Block3 in main Wall  
 713 47 rpp 258.7 1335.2 -25.5 -17.5 152.4 432.5 \$S Main Structural Wall South Section Basement1  
 714 47 rpp 292.7 307.7 -17.5 -4 152.4 432.5 \$Block4 in main Wall  
 715 47 rpp 396.7 408.7 -17.5 -4 152.4 432.5 \$Block5 in main Wall  
 716 47 rpp 496.7 508.7 -17.5 -4 152.4 432.5 \$Block6 in main Wall  
 717 47 rpp 597.7 609.7 -17.5 -4 152.4 432.5 \$Block7 in main Wall  
 718 47 rpp 712.7 719.2 -17.5 -4 152.4 432.5 \$Block8 in main Wall  
 719 47 rpp 813.7 825.7 -17.5 -4 152.4 432.5 \$Block9 in main Wall  
 720 47 rpp 913.7 925.7 -17.5 -4 152.4 432.5 \$Block10 in main Wall  
 721 47 rpp 1115.7 1127.7 -17.5 -4 152.4 432.5 \$Block11 in main Wall  
 722 47 rpp 1215.7 1227.7 -17.5 -4 152.4 432.5 \$Block12 in main Wall  
 723 47 rpp 1313.7 1327.2 -17.5 -4 152.4 432.5 \$Block13 in main Wall  
 724 47 rpp 1327.2 1335.2 -17.5 867.5 152.4 432.5 \$E Main Structural Wall South Section Basement1  
 725 47 rpp 0 203.5 0 146 152.4 432.5 \$Roomspace 7

c

c

c Basement1 Room 9

901 47 rpp 0 9.75 279 300 152.4 432.5 \$pillar NW corner  
 902 47 rpp 9.75 203.5 287 292 152.4 432.5 \$N Wall Rm13  
 903 47 rpp 203.5 208.5 277.75 389.75 152.4 432.5 \$E wall through Rm09  
 904 47 rpp 0 141.5 152 287 152.4 432.5 \$Roomspace 9 Partially Filled

c

c

c Basement1 Room 11

1101 47 rpp 203.5 208.5 425.75 447.4 152.4 432.5 \$E wall Rm9-Rm11  
 1102 47 rpp 0 203.5 434.5 439.5 152.4 432.5 \$N wall Rm11  
 1103 47 rpp 0 203.5 292 434.5 152.4 432.5 \$Roomspace 11 Partially Filled

c

c

c Basement1 Room 13

1301 47 rpp 203.5 208.5 483.4 597.4 152.4 432.5 \$E wall Rm13  
 1302 47 rpp 0 9.75 576.5 598 152.4 432.5 \$pillar NW corner Rm13  
 1303 47 rpp 9.75 203.5 584.5 589.5 152.4 432.5 \$N wall Rm13  
 1304 47 rpp 0 203.5 439.5 584.5 152.4 432.5 \$Roomspace 13 Partially Filled

c

c

c Basement1 Room 15

1501 47 rpp 203.8 208.5 633.4 706.4 152.4 432.5 \$E wall Rm15-Rm17  
 1502 47 rpp 0 203.5 692.5 697.5 152.4 432.5 \$N wall Rm15  
 1503 47 rpp 0 203.5 589.5 692.5 152.4 432.5 \$Roomspace 15 Partially Filled

c

c

c Basement1 Room 17

1701 47 rpp 0 208.5 800.5 805.5 152.4 432.5 \$N wall Rm17  
 1702 47 rpp 203.5 208.5 742.4 800.5 152.4 432.5 \$E wall Rm17  
 1703 47 rpp 208.5 228 767.4 772.4 152.4 432.5 \$E Stub wall Rm17  
 1704 47 rpp 0 203.5 697.5 800.5 152.4 432.5 \$Roomspace 17

c

c

c Basement1 Room 16

1601 47 rpp 292.7 298.7 -4 178 152.4 432.5 \$W wall Rm16  
 1602 47 rpp 298.7 318.7 173 178 152.4 432.5 \$N stub wall rm16  
 1603 47 rpp 354.7 558.7 173 178 152.4 432.5 \$N wall Rm16-Rm18  
 1604 47 rpp 447.2 452.2 0 173 152.4 432.5 \$E wall Rm16  
 1605 47 rpp 298.7 600.2 -4 0 152.4 432.5 \$South Wall Rm16-Rm18  
 1606 47 rpp 298.7 447.2 1 173 152.4 432.5 \$Roomspace 16

c

c

c Basement1 Room 18

1801 47 rpp	594.7	613.7	173	178	152.4	432.5	\$N Stub wall Rm18
1802 47 rpp	600.2	604.2	-4	173	152.4	432.5	\$E wall Rm18
1803 47 rpp	452.2	600.2	1	173	152.4	432.5	\$Roomspace 18

c

c

c Basement1 Room 20

2001 47 rpp	714.2	719.2	-4	173	152.4	432.5	\$E wall Rm20
2002 47 rpp	694	714.2	153.5	173	152.4	432.5	\$NE Box Rm20
2003 47 rpp	652.7	762.2	173	178	152.4	432.5	\$N wall Rm20-LRm
2010 47 rpp	604.2	714.2	-4	173	152.4	432.5	\$Roomspace 20 Partially Filled

c

c

c Basement1 Lunch Room

2004 47 rpp	762.2	873.7	173	174	152.4	432.5	\$N Thin LR wall
2005 47 rpp	909.7	916.7	173	174	152.4	432.5	\$N Thin LR wall
2006 47 rpp	916.7	929.7	173	178	152.4	432.5	\$NE Block LR
2007 47 rpp	917.2	922.2	-4	173	152.4	432.5	\$E wall LR
2008 47 rpp	749.2	917.2	-5	4.5	152.4	432.5	\$S wall LR
2009 47 rpp	719.2	749.2	-17.5	4.5	152.4	432.5	\$SW Block LR
2011 47 rpp	719.2	917.2	4.5	173	152.4	432.5	\$Roomspace Lunch Room

c

c

c Basement1 Room 26

2601 47 rpp	965.7	1058.7	173	178	152.4	432.5	\$N wall Rm26
2602 47 rpp	1047.7	1052.7	1.5	173	152.4	432.5	\$E wal Rm26
2603 47 rpp	922.2	1047.7	1.5	173	152.4	432.5	\$Roomspace 26

c

c

c Basement1 Room 28 <<<Not Defining Southwall>>>

2801 47 rpp	1114.7	1324	157	162	152.4	432.5	\$N wall Rm28
2802 47 rpp	1114.7	1119.7	162	239.5	152.4	432.5	\$N Stub wall Rm28
2803 47 rpp	1094.7	1114.7	173	178	152.4	432.5	\$N per. wall Rm28
2804 47 rpp	1052.7	1315.2	1.5	157	152.4	432.5	\$Roomspace 28 Partially Filled

c

c

c Basement1 Room 70

7001 47 rpp	1114.7	1119.7	275.5	296.5	152.4	432.5	\$NW wall Rm70
7002 47 rpp	1119.7	1310.4	283.7	289.7	152.4	432.5	\$N wall Rm70
7003 47 rpp	1310.4	1324	271.2	305.2	152.4	432.5	\$NE Block Rm70
7004 47 rpp	1324	1327.2	162	797.75	152.4	432.5	\$E Inside wall Rm70-72-74-76-78
7005 47 rpp	1119.7	1324	162	283.7	152.4	432.5	\$Roomspace 70 Partially Filled

c

c

c Basement1 Room 72

7201 47 rpp	1114.7	1119.7	332.5	539.5	152.4	432.5	\$W wall Rm72-Rm74
7202 47 rpp	1119.7	1324	434.5	439.5	152.4	432.5	\$N wall Rm72
7203 47 rpp	1119.7	1324	289.7	434.5	152.4	432.5	\$Roomspace 72 Partially Filled

c

c

c Basement1 Room 74

7401 47 rpp	1114.7	1119.7	575.5	597.5	152.4	432.5	\$NW Stub wall Rm74
7402 47 rpp	1119.7	1310.4	584.5	589.5	152.4	432.5	\$N wall Rm74
7403 47 rpp	1310.4	1324	572	603	152.4	432.5	\$NE Block Rm74
7404 47 rpp	1119.7	1324	439.5	584.5	152.4	432.5	\$Roomspace 74 Partially Filled

c

c

c Basement1 Room 76

7601 47 rpp	1114.7	1119.7	633.5	728	152.4	432.5	\$W wall Rm76
7602 47 rpp	1119.7	1324	714.5	719.5	152.4	432.5	\$N wall Rm76
7603 47 rpp	1119.7	1324	589.5	714.5	152.4	432.5	\$Roomspace 76 Partially Filled

c

c

c Basement1 Room 78

7801 47 rpp	1114.7	1119.7	764	805.5	152.4	432.5	\$W wall Rm78
7802 47 rpp	1119.7	1327.2	797.75	805.5	152.4	432.5	\$N wall Rm78
7803 47 rpp	1107.5	1114.7	767.5	772.5	152.4	432.5	\$W walstub Rm78ish
7804 47 rpp	1119.7	1324	719.5	797.75	152.4	432.5	\$Roomspace 78

c

c

c Basement1 Room 14

1401 47 rpp	263.75	270.75	767.4	772.4	152.4	432.5	\$W	stub wall Rm14
1402 47 rpp	270.75	275.75	755	805.5	152.4	432.5	\$W	wall Rm14
1403 47 rpp	275.75	757.7	800.5	805.5	152.4	432.5	\$N	wall Rm14-Rm27-Rm5
1404 47 rpp	438.5	448.2	589.5	800.5	152.4	432.5	\$E	wall Rm14-Rm12
1405 47 rpp	275.75	438.5	704	709	152.4	432.5	\$S	wall Rm14
1406 47 rpp	270.75	275.75	633.75	719	152.4	432.5	\$W	wall Rm14-12
1407 47 rpp	275.75	438.5	709	800.5	152.4	432.5	\$Roomspace	14

c

c

c Basement1 Room 12

1201 47 rpp	270.75	275.75	573.5	597.8	152.4	432.5	\$W	wall Rm12-Rm10
1202 47 rpp	275.75	293.75	584.5	589.5	152.4	432.5	\$\$W	wall Rm12
1203 47 rpp	293.75	309.75	578.5	594.5	152.4	432.5	\$\$W	Block Rm12
1204 47 rpp	309.75	602.7	584.5	589.5	152.4	432.5	\$\$S	wall Rm12-Rm25
1205 47 rpp	275.75	438.5	589.5	704	152.4	432.5	\$Roomspace	12 Partially Filled

c

c

c Basement1 Room 10

1001 47 rpp	449	457.2	482	584.5	152.4	432.5	\$E	wall Rm10
1002 47 rpp	449	456.2	457.5	482	152.4	432.5	\$E	wall Rm10
1003 47 rpp	275.75	449	457.5	462.5	152.4	432.5	\$\$S	wall Rm10
1004 47 rpp	270.75	275.75	454.5	537.5	152.4	432.5	\$\$W	wall Rm10
1005 47 rpp	275.75	449	462.5	584.5	152.4	432.5	\$Roomspace	10 Partially Filled

c

c

c Basement1 Room 27

2701 47 rpp	602.7	607.7	656	800.5	152.4	432.5	\$E	wall Rm27
2702 47 rpp	602.7	607.7	535	620	152.4	432.5	\$E	wall Rm27-Rm25
2703 47 rpp	448.2	602.7	589.5	800.5	152.4	432.5	\$Roomspace	27

c

c

c Basement1 Room 25

2501 47 rpp	457.2	540.7	482	487.5	152.4	432.5	\$\$S	wall Rm25
2502 47 rpp	535.7	540.7	457.5	482	152.4	432.5	\$\$S	wall Rm25
2503 47 rpp	540.7	602.7	457.5	462.5	152.4	432.5	\$\$S	wall Rm25
2504 47 rpp	602.7	607.7	323	487.5	152.4	432.5	\$E	wall Rm25-Rm8
2505 47 rpp	457.2	602.7	487.5	584.5	152.4	432.5	\$Roomspace	25 Partially Filled

c

c

c Basement1 Room 8

801 47 rpp	564.5	607.7	250.5	323	152.4	432.5	\$\$E	Block Rm8
802 47 rpp	270.75	275.75	291	418.5	152.4	432.5	\$\$W	wall Rm8
803 47 rpp	315.7	564.5	294	299	152.4	432.5	\$\$S	wall Rm8
804 47 rpp	292.75	315.7	250.5	299	152.4	432.5	\$\$SW	Block Rm8
805 47 rpp	275.75	292.75	291	299	152.4	432.5	\$\$SW	wall Rm8
806 47 rpp	315.7	564.5	274.5	279.5	152.4	432.5	\$\$S	wall Rm8
807 47 rpp	275.75	602.7	323	457.5	152.4	432.5	\$Roomspace	8 Partially Filled

c

c

c Basement1 Room 5

501 47 rpp	793.5	1024	800.5	805.5	152.4	432.5	\$N	wall Rm5
502 47 rpp	1019	1024	595	800.5	152.4	432.5	\$E	wall Rm5
503 47 rpp	1024	1071.7	767.5	772.5	152.4	432.5	\$E	wall Rm5hall
504 47 rpp	1012.7	1028.7	579	595	152.4	432.5	\$Column in East	wall Rm5
505 47 rpp	1019	1024	295	579	152.4	432.5	\$E	wall Rm5
506 47 rpp	1012.7	1028.7	279	295	152.4	432.5	\$\$S	Column in East wall Rm5
507 47 rpp	1019	1024	250.5	279	152.4	432.5	\$\$SE	wall Rm5
508 47 rpp	1024	1055	250.5	258	152.4	432.5	\$\$SE	wallRm5hall
509 47 rpp	1010.5	1019	250.5	255.5	152.4	432.5	\$\$SE	stub wall Rm5
510 47 rpp	819	974.7	250.5	255.5	152.4	432.5	\$\$S	wall Rm5
511 47 rpp	819	824	255.5	283	152.4	432.5	\$\$S	spur wallRm5
512 47 rpp	806.7	819	278	283	152.4	432.5	\$\$S	spur wallRm5
513 47 rpp	717	734.7	278	283	152.4	432.5	\$\$S	spur wallRm5
514 47 rpp	717	722	250.5	278	152.4	432.5	\$\$S	spur wallRm5
515 47 rpp	607.7	717	250.5	255.5	152.4	432.5	\$\$S	wall Rm5
516 47 rpp	653.2	669.2	579	595	152.4	432.5	\$\$NW	Column Rm5
517 47 rpp	653.2	669.2	279	295	152.4	432.5	\$\$SW	Column Rm5
518 47 rpp	607.7	1019	283	800.5	152.4	432.5	\$Roomspace	5

c



125 15 rpp 214.5 580.5 1503 1552 442 883.9 \$NE Cell box  
 c  
 c  
 c Begin Southernmost Section of Floor1  
 126 16 rpp 0 64.75 0 1012 442 883.9 \$W Section Cell box  
 127 16 rpp 64.75 517 0 1083.75 442 883.9 \$E Section Cell box  
 128 16 rpp 106 517 1083.75 1145 442 883.9 \$E Section Cell box  
 c  
 c  
 c Begin Southernmost East Section of Floor1  
 129 17 rpp 0 670 -232 640 442 883.9 \$SW Cell box  
 130 17 rpp 0 670 640 1137.5 442 883.9 \$NW Cell box  
 131 17 rpp 670 1343 -232 294 442 883.9 \$SE Cell box  
 132 17 rpp 670 1343 294 640 442 883.9 \$E Cell box  
 133 17 rpp 670 1827.5 640 1137.5 442 883.9 \$NE Cell box  
 c  
 c  
 c  
 c  
 c  
 c  
 c  
 c Start of Wing Surfaces ======  
 c  
 c The exterior wall height is set at 404'-6" at which point the material changes  
 c concrete to the "Exterior Wall" material. See the explanation in the assumptions  
 c exterior walls for a more thorough explanation of why.  
 c  
 c  
 c  
 c  
 c ///////////////Begin Northwest Section of the central Section of Floor1\\\\\\\\\\\\\\\\\  
 c \*\*\*\*\*Notes for this section of Surfaces\*\*\*\*\*  
 c The origin was set as the SW corner of the inside wall of Room 700.  
 c  
 c  
 c  
 c  
 c Floor1 Room 700  
 70001 18 rpp -3 0 0 243.5 442 883.9 \$W wall Rm700  
 70002 18 rpp 0 14.25 240.5 243.5 442 883.9 \$NW wall Rm700  
 70003 18 rpp 51 153 240.5 243.5 442 883.9 \$N wall Rm700-Rm701  
 70004 18 rpp 120 123 0 240.5 442 883.9 \$E wall Rm700  
 70005 18 rpp -3 33 -3 0 442 883.9 \$SE wall Rm700  
 70006 18 rpp 72 170.5 -3 0 442 883.9 \$Box Rm700  
 70007 18 rpp 30 33 -21 -3 442 883.9 \$Box Rm700  
 70008 18 rpp -1.25 34.5 -24 -21 442 883.9 \$Box Rm700  
 70009 18 rpp -1.25 1.75 -45.5 -24 442 883.9 \$Box Rm700  
 70010 18 rpp -10.75 -1.25 -45.5 -42.5 442 883.9 \$Box Rm700  
 70012 18 rpp -14 -10.75 -45.5 281.5 442 883.9 \$W 2nd wl  
 70013 18 rpp -18 -14 -45.5 281.5 442 518.2 \$W 3rd wl Exterior  
 70014 18 rpp 72 75 -21 -3 442 883.9 \$Box Rm700-701  
 70015 18 rpp 70.5 172 -24 -21 442 883.9 \$Box Rm700-701  
 70016 18 rpp 167.5 170.5 -21 -3 442 883.9 \$Box Rm700-701  
 70017 18 rpp 0 120 0 240.5 442 883.9 \$Roomspace 700  
 70018 18 rpp -18 -14 -45.5 281.5 518.2 883.9 \$W 3rd wl Exterior  
 c  
 c  
 c Floor1 Room 701  
 70101 18 rpp 189 280.2 240.5 243.5 442 883.9 \$N wl Rm701-702  
 70102 18 rpp 258 261 0 240.5 442 883.9 \$E wl Rm701  
 70103 18 rpp 209.5 309 -3 0 442 883.9 \$Box Rm701-702  
 70104 18 rpp 209.5 212.5 -21 -3 442 883.9 \$Box Rm701-702  
 70105 18 rpp 208 310.5 -24 -21 442 883.9 \$Box Rm701-702  
 70106 18 rpp 306 309 -21 -3 442 883.9 \$Box Rm701-702  
 70107 18 rpp 123 258 0 240.5 442 883.9 \$Roomspace 701  
 c  
 c  
 c Floor1 Room 702  
 70201 18 rpp 316.2 390 240.5 243.5 442 883.9 \$N wl Rm702  
 70202 18 rpp 387 390 0 240.5 442 883.9 \$E i wall Rm702  
 70203 18 rpp 348 390 -3 0 442 883.9 \$Box Rm702

70204 18 rpp 396.75 399.75 -24 386.75 442 883.9 \$Eo wl Rm702  
 70205 18 rpp 348 351 -21 -3 442 883.9 \$Box Rm702  
 70206 18 rpp 346.5 396.75 -24 -21 442 883.9 \$Box Rm702  
 70207 18 rpp 261 387 0 240.5 442 883.9 \$Roomspace 702

c

c

c Floor1 Room 703/Mens Bathroom/Unlabeled Room Next to it

70301 18 rpp 486.75 504.75 -20.5 -5.5 442 883.9 \$Box i air Rm703  
 70302 18 rpp 483.75 507.75 -23.5 -2.5 442 883.9 \$Box o wl Rm703  
 70303 18 rpp 483.75 486.75 -2.5 150.75 442 883.9 \$W wl Rm703  
 70304 18 rpp 486.75 981.75 112 115 442 883.9 \$N wl  
 70305 18 rpp 507.75 569.75 -23.5 -20.5 442 883.9 \$SE wl  
 70306 18 rpp 604.75 821.75 -23.5 -20.5 442 883.9 \$S wl  
 70307 18 rpp 856.75 995.75 -23.5 -20.5 442 883.9 \$S wl Mens Rm  
 70308 18 rpp 1030.25 1118.75 -23.5 -20.5 442 883.9 \$SE wl Mens Rm  
 70309 18 rpp 861.75 864.75 -20.5 112 442 883.9 \$W wl Mens Rm  
 70310 18 rpp 981.75 989.75 -20.5 27 442 883.9 \$Divider wl Mens Rm  
 70311 18 rpp 981.75 989.75 63 103 442 883.9 \$Divider wl Mens Rm  
 70312 18 rpp 981.75 1094.75 103 115 442 883.9 \$N Block Mens Rm  
 70313 18 rpp 1034.25 1094.75 -20.5 -15.5 442 883.9 \$S Block Mens Rm  
 70314 18 rpp 1094.75 1097.75 -20.5 174.25 442 883.9 \$E wl Mens Rm  
 70315 18 rpp 1115.75 1118.75 -20.5 133.75 442 883.9 \$E o wl Mens Rm  
 70316 18 rpp 486.75 861.75 -20.5 112 442 883.9 \$Roomspace 703

c

c

c Floor1 Room 320/421

32001 18 rpp 504.75 507.75 115 211 442 883.9 \$W box Rm320  
 32002 18 rpp 486.75 504.75 208 211 442 883.9 \$W box Rm320  
 32003 18 rpp 483.75 486.75 178 212.5 442 883.9 \$W box Rm320  
 32004 18 rpp 483.75 486.75 248.5 445 442 883.9 \$NW box Rm320-324  
 32005 18 rpp 486.75 507.75 250 253 442 883.9 \$NW box Rm320  
 32006 18 rpp 504.75 507.75 253 511 442 883.9 \$NW box Rm320  
 32007 18 rpp 486.75 504.75 508 511 442 883.9 \$NW box Rm320  
 32008 18 rpp 483.75 486.75 481 512.5 442 883.9 \$NW box Rm320  
 32009 18 rpp 507.75 1094.75 350.5 353.5 442 883.9 \$NW wl Rm320  
 32010 18 rpp 1094.75 1097.75 250.25 510.25 442 883.9 \$E box Rm320  
 32011 18 rpp 1097.75 1118.75 507.25 510.25 442 883.9 \$E box Rm320  
 32012 18 rpp 1115.75 1118.75 369.25 507.25 442 883.9 \$E box Rm320  
 32013 18 rpp 1097.75 1115.75 250.25 253.25 442 883.9 \$E box Rm320  
 32014 18 rpp 1115.75 1118.75 248.25 339.25 442 883.9 \$E box Rm320  
 32015 18 rpp 1097.75 1115.75 171.25 174.25 442 883.9 \$E box Rm320  
 32016 18 rpp 1115.75 1118.75 160.75 176.25 442 883.9 \$E box Rm320  
 32017 18 rpp 507.75 1094.75 115 350.5 442 883.9 \$Roomspace 320/421

c

c

c Floor1 Room 324/425

32401 18 rpp 486.75 504.75 553 627.5 442 883.9 \$W i box air filled  
 32402 18 rpp 483.75 507.75 550 630.5 442 883.9 \$W o box Conc filled  
 32403 18 rpp 486.75 504.75 672.5 742.5 442 883.9 \$NW i box air filled  
 32404 18 rpp 483.75 507.75 669.5 745.5 442 883.9 \$NW o box Conc filled  
 32405 18 rpp 507.75 749.75 701.5 704.5 442 883.9 \$N wl Rm324  
 32406 18 rpp 749.75 752.75 569 742.5 442 883.9 \$NE wl  
 32407 18 rpp 752.75 806 542.5 566 442 883.9 \$NE i box air filled  
 32408 18 rpp 749.75 809 539.5 569 442 883.9 \$NE o box Conc filled  
 32409 18 rpp 847.25 949.25 566 569 442 883.9 \$NE wl  
 32410 18 rpp 946.25 949.25 569 606 442 883.9 \$NE wl  
 32411 18 rpp 949.25 1027.25 603 606 442 883.9 \$NE wl  
 32412 18 rpp 1024.25 1027.25 561.75 603 442 883.9 \$NE wl  
 32413 18 rpp 1027.25 1093.75 561.75 564.75 442 883.9 \$NE wl  
 32414 18 rpp 1096.75 1116.75 553.75 571.75 442 883.9 \$NE i box air filled  
 32415 18 rpp 1093.75 1119.75 550.75 574.75 442 883.9 \$NE o box Conc filled  
 32416 18 rpp 1115.75 1118.75 546.25 550.75 442 883.9 \$E Stub wl  
 32417 18 rpp 1119.75 1142.75 550.75 553.75 442 883.9 \$E stub wl  
 32418 18 rpp 507.75 749.75 353.5 701.5 442 883.9 \$Roomspace 324  
 32419 18 rpp 749.75 1094.75 353.5 539.5 442 883.9 \$Roomspace 425 Partially Filled

c

c

c Floor1 Room 330/Room 427/Elevator

c \*\*\*\*\*Small protrusions ignored in west and east hallways\*\*\*\*\*

c I also omitted the strange caps on the E edge of the elevator because I was unable to

c to verify they existed.

33001 18 rpp 504.75 507.75 784.5 821.5 442 883.9 \$NW Block  
33002 18 rpp 486.75 504.75 784.5 787.5 442 883.9 \$  
33003 18 rpp 483.75 486.75 783 813.5 442 883.9 \$  
33004 18 rpp 461.25 483.75 810.5 813.5 442 883.9 \$  
33005 18 rpp 461.25 464.25 813.5 824.75 442 883.9 \$  
33006 18 rpp 507.75 947 818 821.5 442 883.9 \$N i wl  
33007 18 rpp 464.25 947 821.5 824.75 442 883.9 \$N wl 2nd wl moving north  
33008 18 rpp 473.25 947 824.75 836 442 518.2 \$N Exterior wl  
33009 18 rpp 749.75 752.75 779.5 818 442 883.9 \$E wl Rm330  
33010 18 rpp 752.75 848.75 808.5 811.5 442 883.9 \$Extension wl into Rm427  
33011 18 rpp 845.75 848.75 811.5 818 442 883.9 \$Extension wl into Rm427  
33012 18 rpp 946.25 947 606 818 442 883.9 \$Very thin E wl Rm427  
33013 18 rpp 947 955 606 829 442 883.9 \$W wl Elevator  
33014 18 rpp 955 1141.25 821 829 442 518.2 \$N o Elev wl  
33015 18 rpp 955 1093.75 606 614 442 883.9 \$S Elev wl  
33016 18 rpp 997 1005 655.5 770.25 442 883.9 \$W Elev shaft  
33017 18 rpp 1005 1094 762.25 770.25 442 883.9 \$N Elev shaft  
33018 18 rpp 1005 1094 655.5 663.5 442 883.9 \$S Elev shaft  
33019 18 rpp 1086.25 1094 663.5 682.25 442 883.9 \$E Elev shaft stub wl  
33020 18 rpp 1086.25 1094 750.25 762.25 442 883.9 \$E Elev shaft stub wl  
33021 18 rpp 1044.75 1050.75 564.75 606 442 883.9 \$SE compartment wl  
33022 18 rpp 1050.75 1093.75 564.75 570.75 442 883.9 \$S compartment wl  
33023 18 rpp 1085.75 1093.75 570.75 576.75 442 883.9 \$E compartment stub wl  
33024 18 rpp 1085.75 1093.75 602 606 442 883.9 \$E compartment stub wl  
33025 18 rpp 1093.75 1098.75 574.75 616.75 442 883.9 \$E compartment capping wl  
33026 18 rpp 1093.75 1141.25 815.75 821 442 883.9 \$Doodad in E hallway on N wl  
33027 18 rpp 1093.75 1111 809.75 815.75 442 883.9 \$Doodad in E hallway on N wl  
33028 18 rpp 1093.75 1098.75 806 809.75 442 883.9 \$Doodad in E hallway on N wl  
33029 18 rpp 507.75 749.75 704.5 818 442 883.9 \$Roomspace 330  
33030 18 rpp 752.75 946.25 569 808.5 442 883.9 \$Roomspace 427 Partially Filled  
33031 18 rpp 955 1141.25 821 829 518.2 883.9 \$N o Elev wl  
33032 18 rpp 473.25 947 824.75 836 518.2 883.9 \$N Exterior wl

c

c Floor1 Room 325/Filter Building

c \*\*\*\*\*Ignored small blocks on ramp\*\*\*\*\*

32501 18 rpp 7 10 243.5 284.5 442 883.9 \$SW Block Rm325  
32502 18 rpp -14 7 281.5 284.5 442 883.9 \$  
32503 18 rpp -3 0 359.5 546.5 442 883.9 \$W wl  
32504 18 rpp 0 23 543.5 546.5 442 883.9 \$NW Block  
32505 18 rpp 20 23 546.5 577.5 442 883.9 \$  
32506 18 rpp -3 20 574.5 577.5 442 883.9 \$  
32507 18 rpp -3 0 577.5 810 442 883.9 \$W wl Rm325-Rm327  
32508 18 rpp 0 62.25 598 601 442 883.9 \$N wl Rm235  
32509 18 rpp 98.25 375.75 598 601 442 883.9 \$N wl Rm235  
32510 18 rpp 375.75 378.75 556.5 641 442 883.9 \$NE BlockRm235  
32511 18 rpp 378.75 396.75 638 641 442 883.9 \$NE BlockRm235  
32512 18 rpp 396.75 399.75 613.75 642.5 442 883.9 \$NE BlockRm235  
32513 18 rpp 396.75 399.75 555 577.5 442 883.9 \$NE BlockRm235  
32514 18 rpp 378.75 396.75 556.5 559.5 442 883.9 \$NE BlockRm235  
32515 18 rpp 375.75 378.75 243.5 481.5 442 883.9 \$E wl Rm235  
32516 18 rpp 378.75 396.75 478.5 481.5 442 883.9 \$E Block  
32517 18 rpp 396.75 399.75 459 483 442 883.9 \$  
32518 18 rpp -6 -3 362.5 811.5 442 883.9 \$W 2nd wl moving outward  
32519 18 rpp -10.75 -6 362.5 811.5 442 883.9 \$W 3rd wl moving outward  
32520 18 rpp -14 -10.75 362.5 824.75 442 883.9 \$W 4th wl moving outward  
32521 18 rpp -18.25 -14 362.5 829 442 518.2 \$W 5th wl moving outward  
32522 18 rpp -147.25 -32.25 585 693 442 883.9 \$Cover of Filter  
32523 18 rpp 10 375.75 243.5 460 442 883.9 \$Roomspace 325 Partially Filled <-----Fix  
This-----

32524 18 rpp -18.25 -14 362.5 829 518.2 883.9 \$W 5th wl moving outward

c

c

c Floor1 Room 327/327A

32701 18 rpp 237.75 240.75 601 638 442 883.9 \$Dividing wl Rm327/327A  
32702 18 rpp 237.75 240.75 674 818 442 883.9 \$Dividing wl Rm327/327A  
32703 18 rpp 375.75 378.75 680 818 442 883.9 \$E wl Rm327  
32704 18 rpp 378.75 396.75 680 683 442 883.9 \$E Block wl  
32705 18 rpp 396.75 399.75 678.5 813.5 442 883.9 \$E Block wl  
32706 18 rpp 399.75 422.25 810.5 813.5 442 883.9 \$E Block wl



52511	11	rpp	624	638	460	463	442	883.9	\$NE block wl Rm525
52512	11	rpp	635	638	463	621	442	883.9	\$NE block wl Rm525
52513	11	rpp	624	635	618	621	442	883.9	\$NE block wl Rm525
52514	11	rpp	191.5	621	525	528	442	883.9	\$N wl Rm525
52515	11	rpp	478.5	483.5	174.5	525	442	883.9	\$Central wl Rm525
52516	11	rpp	483.5	514.5	174.5	179.5	442	883.9	\$Central wl Rm525
52517	11	rpp	441.75	478.5	199	204	442	883.9	\$Central wl Rm525
52518	11	rpp	329	334	485	525	442	883.9	\$E Freezer wl
52519	11	rpp	188.5	191.5	399.5	843	442	883.9	\$W Freezer wl
52520	11	rpp	355	478.5	204	394.5	442	883.9	\$Roomspace 525
52521	11	rpp	334	478.5	399.5	525	442	883.9	\$Roomspace 525
52522	11	rpp	483.5	621	179.5	525	442	883.9	\$Roomspace 525

c

c

c Floor1 Room 426/426A

42601	11	rpp	3	83	493.5	498.5	442	883.9	\$S wl Rm426
42602	11	rpp	125	188.5	493.5	498.5	442	883.9	\$S wl Rm426
42603	11	rpp	156.75	188.5	700.5	703.5	442	883.9	\$N wl Rm426
42604	11	rpp	79.5	107.75	700.5	703.5	442	883.9	\$N wl Rm426
42605	11	rpp	69.5	79.5	636.25	703.5	442	883.9	\$E Closet wl Rm426
42606	11	rpp	76.5	79.5	578.25	636.25	442	883.9	\$E Closet wl Rm426
42607	11	rpp	69	76.5	578.25	581.25	442	883.9	\$SE Closet wl Rm426
42608	11	rpp	4	33	578.25	581.25	442	883.9	\$SW Closet wl Rm426
42609	11	rpp	4	25	581.25	591.75	442	883.9	\$SW Closet Block wl Rm426
42610	11	rpp	4	29	591.75	596.75	442	883.9	\$SW Closet Block wl Rm426
42611	11	rpp	0	3	548.75	578.25	442	883.9	\$SW Closet wl Rm426
42612	11	rpp	-24	-1	572.75	575.75	442	883.9	\$SW Closet wl Rm426
42613	11	rpp	-1	0	575.75	578.25	442	883.9	\$Very Small Wall Remainder SW wl Rm426
42614	11	rpp	-1	4	578.25	645.5	442	883.9	\$W Closet wl Rm426
42615	11	rpp	4	30	639.25	645.5	442	883.9	\$NW Closet wl Rm426
42616	11	rpp	25	30	645.5	697.25	442	883.9	\$NW Closet wl Rm426
42617	11	rpp	25	69.5	697.25	703.5	442	883.9	\$N Closet wl Rm426
42618	11	rpp	-1	25	692.75	703.5	442	883.9	\$N Closet wl Rm426
42619	11	rpp	0	3	397.5	513.75	442	883.9	\$W wl Rm426A
42620	11	rpp	3	188.5	397.5	493.5	442	883.9	\$Roomspace 426A
42621	11	rpp	79.5	188.5	498.5	700.5	442	883.9	\$Roomspace 426

c

c

c Floor1 Room 430/Receiving Room

43001	11	rpp	-1	2	703.5	737.75	442	883.9	\$W wl Rm430
43002	11	rpp	-1	2	809.75	843	442	883.9	\$W wl Rm430
43003	11	rpp	2	22.5	827.75	840	442	883.9	\$NW block Rm430
43004	11	rpp	2	76.5	840	843	442	883.9	\$N wl Rm430
43005	11	rpp	-23.5	76.5	843	851	442	518.2	\$N o wl Rm430
43006	11	rpp	-23.5	-1	837.75	843	442	883.9	\$NE wl Rm430
43007	11	rpp	177.5	208.5	843	851	442	883.9	\$N Cap wl Rm430
43008	11	rpp	-9	37	928	930	442	883.9	\$NW Receiving Room
43009	11	rpp	-9	-7	930	1005.25	442	883.9	\$NW Receiving Room
43010	11	rpp	-7	157.4	1003.25	1005.25	442	883.9	\$NW Receiving Room
43011	11	rpp	155.4	157.4	928	1003.25	442	883.9	\$NW Receiving Room
43012	11	rpp	111	155.4	928	930	442	883.9	\$NW Receiving Room
43013	11	rpp	177.5	188.5	840	843	442	883.9	\$NE wl Rm430
43014	11	rpp	2	188.5	703.5	840	442	883.9	\$Roomspace 430
43015	11	rpp	-23.5	76.5	843	851	518.2	883.9	\$N o wl Rm430

c

c

c Floor1 Room 527/527A

52701	11	rpp	199.5	621	536	539	442	883.9	\$S wl Rm527A
52702	11	rpp	489	621	616.75	619.75	442	883.9	\$N wl Rm527A
52703	11	rpp	402	453	616.75	619.75	442	883.9	\$NW wl Rm527A
52704	11	rpp	399	402	539	619.75	442	883.9	\$W wl Rm527A
52705	11	rpp	322.5	325.5	539	619.75	442	883.9	\$SW wl in SW Room of Rm527
52706	11	rpp	309.5	322.5	579.75	582.75	442	883.9	\$Box in SW wl Rm527
52707	11	rpp	309.5	312.5	582.75	595.75	442	883.9	\$Box in SW wl Rm527
52708	11	rpp	312.5	322.5	592.75	595.75	442	883.9	\$Box in SW wl Rm527
52709	11	rpp	294.5	322.5	616.75	619.75	442	883.9	\$N wl in SW Room of Rm527
52710	11	rpp	202.5	237	616.75	619.75	442	883.9	\$N wl in SW Room of Rm527
52711	11	rpp	199.5	202.5	539	843	442	883.9	\$W wl Rm527
52712	11	rpp	202.5	208.5	840	843	442	883.9	\$NW small wl Rm527
52713	11	rpp	304.5	663	843	851	442	518.2	\$N o Major wl Rm527

52714	11	rpp	304.5	310.5	840	843	442	883.9	\$N i minor wl Rm527
52715	11	rpp	307.5	310.5	830	840	442	883.9	\$N i minor wl Rm527
52716	11	rpp	310.5	328.5	830	833	442	883.9	\$N i minor wl Rm527
52717	11	rpp	325.5	328.5	833	840	442	883.9	\$N i minor wl Rm527
52718	11	rpp	325.5	372.5	840	843	442	883.9	\$N i minor wl Rm527
52719	11	rpp	369.5	372.5	810.5	840	442	883.9	\$N i minor wl Rm527
52720	11	rpp	372.5	383.5	813.5	816.5	442	883.9	\$N i minor wl Rm527
52721	11	rpp	380.5	383.5	816.5	843	442	883.9	\$N i minor wl Rm527/Rm529
52722	11	rpp	369.5	372.5	696	743.5	442	883.9	\$NE wl Rm527
52723	11	rpp	372.5	635	696	699	442	883.9	\$NE wl Rm527
52724	11	rpp	202.5	369.5	619.75	830	442	883.9	\$Roomspace 527
52725	11	rpp	402	621	539	616.75	442	883.9	\$Roomspace 527A
52726	11	rpp	304.5	663	843	851	518.2	883.9	\$N o Major wl Rm527

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c

c Floor1 Room 529

52901	11	rpp	372.5	383.5	737.5	740.5	442	883.9	\$W wl Rm529
52902	11	rpp	380.5	383.5	707	737.5	442	883.9	\$W wl Rm529
52903	11	rpp	383.5	621	707	710	442	883.9	\$S wl Rm529
52904	11	rpp	621	624	699	756	442	883.9	\$SE wl Rm529
52905	11	rpp	624	635	753	756	442	883.9	\$SE wl Rm529
52906	11	rpp	635	638	694.5	757.5	442	883.9	\$SE wl Rm529
52907	11	rpp	635	638	793.5	843	442	883.9	\$E wl Rm529
52908	11	rpp	638	663	840	843	442	883.9	\$NE wl Rm529
52909	11	rpp	621	635	795	798	442	883.9	\$NE wl Rm529
52910	11	rpp	621	624	798	834	442	883.9	\$NE wl Rm529
52911	11	rpp	613	621	831	834	442	883.9	\$NE wl Rm529
52912	11	rpp	613	616	834	843	442	883.9	\$NE wl Rm529
52913	11	rpp	383.5	613	840	843	442	883.9	\$N wl Rm529
52914	11	rpp	341.5	530	851	858	442	883.9	\$S Stairwell wl Rm529
52915	11	rpp	341.5	630	913	917.5	442	883.9	\$N stairwell wl Rm529
52916	11	rpp	383.5	621	710	840	442	883.9	\$Roomspace 529

c

c

c Floor1 Room 520

52001	11	rpp	719	1052	-6	-3	442	883.9	\$SW
52002	11	rpp	1088	1116.5	-6	-3	442	883.9	\$SE
52003	11	rpp	719	722	-3	110	442	883.9	\$SW Box
52004	11	rpp	722	745	105.5	108.5	442	883.9	\$SW Box
52005	11	rpp	742	745	-3	105.5	442	883.9	\$SW Box
52006	11	rpp	719	722	182	264	442	883.9	\$NW Box
52007	11	rpp	719	722	294	328	442	883.9	\$NW Box
52008	11	rpp	722	745	323.5	326.5	442	883.9	\$NW Box
52009	11	rpp	742	745	183.5	323.5	442	883.9	\$NW Box
52010	11	rpp	722	742	183.5	186.5	442	883.9	\$NW Box
52011	11	rpp	745	1034.5	285	288	442	883.9	\$N
52012	11	rpp	1070.5	1116.5	285	288	442	883.9	\$N
52013	11	rpp	981.5	984.5	288	538.5	442	883.9	\$W wl small rm 520-Rm524
52014	11	rpp	984.5	1119.5	394.25	397.25	442	883.9	\$N wl small rm520
52015	11	rpp	1116.5	1119.5	285	394.25	442	883.9	\$E wl small rm520
52016	11	rpp	745	1116.5	-3	285	442	883.9	\$Roomspace 520
52017	11	rpp	984.5	1116.5	288	394.25	442	883.9	\$Roomspace 520N

c

c

c Floor1 Room 524

52401	11	rpp	719	722	397.5	632	442	883.9	\$NW block rm524
52402	11	rpp	722	745	399	402	442	883.9	\$NW block rm524
52403	11	rpp	742	745	402	630.5	442	883.9	\$NW block rm524
52404	11	rpp	722	742	627.5	630.5	442	883.9	\$NW block rm524
52405	11	rpp	745	984.5	585	588	442	883.9	\$N wl rm524
52406	11	rpp	981.5	984.5	574.5	585	442	883.9	\$E wl rm524
52407	11	rpp	984.5	1005.5	497.25	500.25	442	883.9	\$E box wl rm524
52408	11	rpp	1002.5	1005.5	453.25	497.25	442	883.9	\$E box wl rm524
52409	11	rpp	984.5	1002.5	453.25	456.25	442	883.9	\$E box wl rm524
52410	11	rpp	745	981.5	288	585	442	883.9	\$Roomspace 524

c

c

c Floor1 Room 528

52801	11	rpp	719	722	704	771.5	442	883.9	\$NE box Rm528
52802	11	rpp	722	745	705.5	708.5	442	883.9	\$NE box Rm528

52803	11	rrp	742	745	708.5	733	442	883.9	\$NE	box	Rm528	
52804	11	rrp	722	737	767	770	442	883.9	\$NE	box	Rm528-Rm530	
52805	11	rrp	734	737	741	767	442	883.9	\$NE	box	Rm528-Rm530	
52806	11	rrp	745	897.5	730	733	442	883.9	\$NW	wl	Rm528	
52807	11	rrp	897.5	900.5	730	840	442	883.9	\$NW	wl	Rm528	
52808	11	rrp	800.75	1119.75	840	843	442	883.9	\$N	i	wl	Rm528-Rm530
52809	11	rrp	1119.75	1129	-21.5	843	442	883.9	\$W	wl	Rm528	
52810	11	rrp	800.75	1137	843	851	442	518.2	\$N	o	wl	Rm528-Rm530
52811	11	rrp	897.5	1119.5	588	840	442	883.9	\$Rooms	space	528	Partially Filled
52812	11	rrp	800.75	1137	843	851	518.2	883.9	\$N	o	wl	Rm528-Rm530

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c Floor1 Room 530/North Cylinder Dock

53001	11	rrp	737	886.5	741	744	442	883.9	\$ \$ wl Rm530
53002	11	rrp	883.5	886.5	744	840	442	883.9	\$ E wl Rm530
53003	11	rrp	699	764.5	840	843	442	883.9	\$ NW wl Rm530
53004	11	rrp	719	722	806.5	840	442	883.9	\$ NW block wl Rm530
53005	11	rrp	722	734	808	811	442	883.9	\$ NW block wl Rm530
53006	11	rrp	734	737	808	834	442	883.9	\$ NW block wl Rm530
53007	11	rrp	737	745	831	834	442	883.9	\$ NW block wl Rm530
53008	11	rrp	742	745	834	840	442	883.9	\$ NW block wl Rm530
53009	11	rrp	711	719	851	941	442	883.9	\$ Cylinder Dock wl
53010	11	rrp	815	823	851	941	442	883.9	\$ Cylinder Dock wl
53011	11	rrp	948	956	851	941	442	883.9	\$ Cylinder Dock wl
53012	11	rrp	1062	1070	851	941	442	883.9	\$ Cylinder Dock wl
53013	11	rrp	1137	1162	777.5	781.5	442	883.9	\$ Cylinder Dock small wl
53014	11	rrp	1137	1162	813	817	442	883.9	\$ Cylinder Dock small wl
53015	11	rrp	1129	1137	851	941	442	883.9	\$ Cylinder Dock wl
53016	11	rrp	699	764.5	843	851	442	518.2	\$ Cylinder Dock exterior wl
53017	11	rrp	737	883.5	744	840	442	883.9	\$ Roomspace 530
53018	11	rrp	699	764.5	843	851	518.2	883.9	\$ Cylinder Dock exterior w

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## c \*\*\*\*\*Notes for this section of Surfaces\*\*\*\*\*

c The origin was set as the SW corner of the inside wall of Room 209. For conservancy the hot cells in SAL were modelled as a solid RPP of metal.

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c Floor1 Room 200

20001	12	rrp	-174	-161.25	485.5	487.5	442	883.9	\$SW	thin	wl	Rm200	
20002	12	rrp	-89	-82	485.5	487.5	442	883.9	\$SW	thin	wl	Rm200	
20003	12	rrp	-85.5	-83.5	410.5	485.5	442	883.9	\$SW	thin	wl	Rm200	
20004	12	rrp	-87	-82	406.5	410.5	442	883.9	\$SW	thin	wl	Rm200	
20005	12	rrp	-87	-82	402.5	406.5	442	883.9	\$SW	thin	wl	Rm200	
20006	12	rrp	-46	-13	485.5	487.5	442	883.9	\$SW	thin	wl	Rm200	
20007	12	rrp	89	91	410.5	422	442	883.9	\$S	divider	thin	wl	Rm200
20008	12	rrp	89	91	458	485.5	442	883.9	\$S	divider	thin	wl	Rm200
20009	12	rrp	-13	-11	955.4	990.25	442	883.9	\$NW	thin	wl	Rm200	
20010	12	rrp	-13	-11	1038	1044.5	442	883.9	\$NW	thin	wl	Rm200	
20011	12	rrp	-45.25	28	406.5	410.5	442	883.9	\$S	i	wl	Rm200	
20012	12	rrp	-45.25	28	402.5	406.5	442	883.9	\$S	o	wl	Rm200	
20013	12	rrp	66	250.25	406.5	410.5	442	883.9	\$S	i	wl	Rm200-Rm201	
20014	12	rrp	66	246	402.5	406.5	442	883.9	\$S	o	wl	Rm200-Rm201	

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c Floor1 Room 201

c \*\*\*\*\*This room contains the actual SAL hot cells\*\*\*\*\*

c Neglected thin wall strip in NE border region There are two types of concrete in SAL-

c Heavy Aggregate and Sump concrete. Currently only std concrete is being used for both.

c The roof and floor .....

20101 12 rpp 250.25 266.25 457.5 481 442 883.9 \$E Block Rm201

20102 12 rpp 266.25 345 464.25 469.25 442 883.9 \$E wl Rm201

20103 12 rpp 250.25 266.25 613 630 442 883.9 \$E Column Rm201

20104 12 rpp 253.5 263.5 854.5 864.5 442 883.9 \$NE column Rm201

20105 12 rpp 263.5 307.5 857 862 442 883.9 \$NE wall off of

20106 12 rpp 265 266.5 862 1037 442 883.9 \$NE wl Rm201

20107 12 rpp 263.5 266.5 1037 1335.5 442 883.9 \$NE wl Rm201

20108 12 rpp 253.5 263.5 1037 1335.5 442 518.2 \$NE wl Rm201

20109	12	rrp	250.25	253.5	1037	1335.5	442	883.9	\$NE	wl	Rm201
20110	12	rrp	246	250.25	1052.5	1335.5	442	883.9	\$NE	wl	Rm201
20111	12	rrp	239	246	1052.5	1323	442	883.9	\$NE	wl	Rm201
20112	12	rrp	186	250	1048.5	1052.5	442	883.9	\$N	o	wl Rm201
20113	12	rrp	186	250	1044.5	1048.5	442	883.9	\$N	i	wl Rm201
20114	12	rrp	-13	13	485.5	955.4	442	883.9	\$W	wl	SAL Cell-Heavey Agg. Conc
20115	12	rrp	13	80	485.5	511.5	442	883.9	\$S	wl	SAL Cell -Heavey Agg. Conc
20116	12	rrp	80	91	485.5	955.4	442	883.9	\$E	SAL	wl Cell -Metal Walls and Windows, Windows ignored
20117	12	rrp	13	80	943.4	955.4	442	883.9	\$E	SAL	wl Cell -Metal Walls
20118	12	rrp	253.5	263.5	1037	1335.5	518.2	883.9	\$NE	wl	Rm201<-----

Check the comps of this very cluttered wall-----

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c Floor1 Room 202/203

20201	12	rrp	-418	-159.25	406.5	410.5	442	883.9	\$ \$ i wl Rm202
20202	12	rrp	-422	-159.25	402.5	406.5	442	883.9	\$ \$ o wl Rm202
20203	12	rrp	-422	-418	406.5	1052.5	442	883.9	\$ W o wl Rm202-Rm203
20204	12	rrp	-418	-414	410.5	1048.5	442	883.9	\$ W i wl Rm202-Rm203
20205	12	rrp	-418	-397	1048.5	1052.5	442	883.9	\$ NW o wl Rm203
20206	12	rrp	-414	-397	1044.5	1048.5	442	883.9	\$ NW i wl Rm203
20207	12	rrp	-414	-178	692	696	442	883.9	\$ N wl Rm202
20208	12	rrp	-182	-178	598.5	692	442	883.9	\$ E i wl Rm202
20209	12	rrp	-178	-174	598.5	702	442	883.9	\$ E o wl Rm202
20210	12	rrp	-182	-178	410.5	526.5	442	883.9	\$ SE i wl Rm202
20211	12	rrp	-178	-174	410.5	526.5	442	883.9	\$ SE o wl Rm202
20212	12	rrp	-252	-248	696	702	442	883.9	\$ Stub Doorway wl Rm203
20213	12	rrp	-252	-248	738	747	442	883.9	\$ Stub Doorway wl Rm203
20214	12	rrp	-248	-178	743	747	442	883.9	\$ Doorway wl Rm203
20215	12	rrp	-182	-178	696	702	442	883.9	\$ Doorway wl Rm203
20216	12	rrp	-182	-178	738	743	442	883.9	\$ Doorway wl Rm203
20217	12	rrp	-178	-174	738	1044.5	442	883.9	\$ E o wl Rm203
20218	12	rrp	-182	-178	747	1044.5	442	883.9	\$ E i wl Rm203
20219	12	rrp	-361	151	1044.5	1048.5	442	883.9	\$ N i wl Rm203
20220	12	rrp	-361	151	1048.5	1052.5	442	883.9	\$ N o wl Rm203
20221	12	rrp	-414	-182	410.5	692	442	883.9	\$ Roomspace 202
20222	12	rrp	-414	-182	747	1044.5	442	883.9	\$ Roomspace 203

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c Floor1 Room 209

c \*\*\*\*Neglected some layers on interior walls\*\*\*\*\*

20901	12	rrp	0	134	-15	0	442	883.9	\$S wl Rm209
20902	12	rrp	134	206	-9	0	442	883.9	\$S wl thin Rm209
20903	12	rrp	206	246	-15	0	442	883.9	\$SE wl Rm209
20904	12	rrp	239	246	0	46.25	442	883.9	\$SE wl Rm209
20905	12	rrp	239	246	85.25	377.5	442	883.9	\$E wl Rm209
20906	12	rrp	66	246	377.5	402.5	442	883.9	\$NE wl Rm209
20907	12	rrp	0	28	377.5	402.5	442	883.9	\$NW wl Rm209
20908	12	rrp	-6	0	-15	402.5	442	883.9	\$W wl Rm209
20909	12	rrp	224.5	232.5	106	114	442	883.9	\$SW column Rm209
20910	12	rrp	246	250.25	-25.5	46.25	442	883.9	\$SE wl Rm209
20911	12	rrp	250.25	253.5	-25.5	46.25	442	883.9	\$SE wl Rm209
20912	12	rrp	253.5	256.5	-25.5	46.25	442	883.9	\$SE wl Rm209
20913	12	rrp	256.5	263.5	20.5	46.25	442	518.2	\$SE Block Rm209
20914	12	rrp	263.5	266.5	20.5	46.25	442	883.9	\$SE o/wl Rm209
20915	12	rrp	246	250.25	85.25	377.5	442	883.9	\$E wl Rm209
20916	12	rrp	250.25	253.5	85.25	421.5	442	883.9	\$E wl Rm209
20917	12	rrp	253.5	263.5	85.25	421.5	442	518.2	\$E wl Rm209
20918	12	rrp	263.5	266.5	85.25	421.5	442	883.9	\$E wl Rm209
20919	12	rrp	0	239	0	377.5	442	883.9	\$Roomsphere 209
20920	12	rrp	303.75	369	107.5	112.5	442	883.9	\$Hallway wl stub R
20921	12	rrp	253.5	263.5	85.25	421.5	518.2	883.9	\$E wl Rm209
20922	12	rrp	256.5	263.5	20.5	46.25	518.2	883.9	\$SE Block Rm209

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## \*\*\*\*\*Begin Southwest Section of 1900\*\*\*\*\*

## \*\*\*\*\*Notes for this section of Surfaces\*\*\*\*\*

c The origin was set as the SOUTH EAST CORNER of the inside wall of Room 301. The origin

c The origin was set as the SOUTH EAST CORNER of  
c was placed here for simplicities sake. I am the walrus

$c$  was placed here for simplicities sake. I am the warus  
 $c$

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c Floor1 Room 301

30101	13 rpp	-237	3	-3.5	0	442	883.9	\$S wl Rm301
30102	13 rpp	0	3	0	42	442	883.9	\$SE block wl Rm301
30103	13 rpp	3	21	39	42	442	883.9	\$SE block wl Rm301
30104	13 rpp	21	24	0	43.75	442	883.9	\$SE block wl Rm301
30105	13 rpp	3	24	-3	0	442	883.9	\$SE block wl Rm301
30106	13 rpp	0	3	81.5	156.75	442	883.9	\$NE block wl Rm301
30107	13 rpp	3	21	153.75	156.75	442	883.9	\$NE block wl Rm301
30108	13 rpp	21	24	79.75	157.25	442	883.9	\$NE block wl Rm301
30109	13 rpp	3	21	81.5	84.5	442	883.9	\$NE block wl Rm301
30110	13 rpp	-266	0	112	120	442	883.9	\$N wl Rm301
30111	13 rpp	-266	-237	-3.5	1	442	883.9	\$SW wl Rm301
30112	13 rpp	-271	-266	-3.5	356	442	883.9	\$W wl Rm301-Rm305
30113	13 rpp	-266	0	0	112	442	883.9	\$Roomspace 301

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c Floor1 Room 303

30301	13 rpp	-266	0	120	127.5	442	883.9	\$S i wl Rm303
30302	13 rpp	0	3	195.75	283	442	883.9	\$NE block wl Rm303
30303	13 rpp	3	21	280	283	442	883.9	\$NE block wl Rm303
30304	13 rpp	21	24	255.25	284.25	442	883.9	\$NE block wl Rm303
30305	13 rpp	21	24	195.25	224.75	442	883.9	\$NE block wl Rm303
30306	13 rpp	3	21	195.75	198.75	442	883.9	\$NE block wl Rm303
30307	13 rpp	-266	0	229.5	237	442	883.9	\$Ni wl Rm303
30308	13 rpp	-266	0	237	240	442	883.9	\$No wl Rm303
30309	13 rpp	-266	0	127.5	229.5	442	883.9	\$Roomspace 303

c

c

c Floor1 Room 305

30501	13 rpp	-249.5	0	240	247.5	442	883.9	\$S wl Rm305
30502	13 rpp	0	3	322	396.5	442	883.9	\$E block wl Rm305
30503	13 rpp	3	21	393.5	396.5	442	883.9	\$E block wl Rm305
30504	13 rpp	21	24	320.75	398	442	883.9	\$E block wl Rm305
30505	13 rpp	3	21	325	328	442	883.9	\$E block wl Rm305
30506	13 rpp	0	3	435.5	522.25	442	883.9	\$NE block wl Rm305
30507	13 rpp	3	21	519.25	522.25	442	883.9	\$NE block wl Rm305
30508	13 rpp	21	24	434.25	522.75	442	883.9	\$NE block wl Rm305
30509	13 rpp	3	21	435.5	438.5	442	883.9	\$NE block wl Rm305
30510	13 rpp	-292	0	469.5	477	442	883.9	\$N wl Rm305
30511	13 rpp	-292	0	477	480	442	883.9	\$N wl Rm305
30512	13 rpp	-266	0	247.5	469.5	442	883.9	\$Roomspace 305 Partially Filled

c

c

c Floor1 Room 309

30901	13 rpp	-292	0	480	487.5	442	883.9	\$S wl Rm309
30902	13 rpp	0	3	561.25	636.25	442	883.9	\$E block wl Rm309
30903	13 rpp	3	21	633.25	636.25	442	883.9	\$E block wl Rm309
30904	13 rpp	21	24	561.75	636.75	442	883.9	\$E block wl Rm309
30905	13 rpp	3	21	561.25	564.25	442	883.9	\$E block wl Rm309
30906	13 rpp	-292	0	709.5	717	442	883.9	\$N wl Rm309
30907	13 rpp	-292	0	717	720	442	883.9	\$N wl Rm309
30908	13 rpp	-292	-271	351	356	442	883.9	\$W dogleg in wl Rm305
30909	13 rpp	0	3	675.25	762.25	442	883.9	\$NE block wl Rm309
30910	13 rpp	3	21	759.25	762.25	442	883.9	\$NE block wl Rm309
30911	13 rpp	21	24	674.75	762.75	442	883.9	\$NE block wl Rm309
30912	13 rpp	3	21	675.25	678.25	442	883.9	\$NE block wl Rm309
30913	13 rpp	-292	0	487.5	709.5	442	883.9	\$Roomspace 309

c

c

c Floor1 Room 313

31301	13 rpp	-292	0	949.5	957	442	883.9	\$N wl Rm313
31302	13 rpp	-292	0	957	960	442	883.9	\$N wl Rm313
31303	13 rpp	-292	0	720	727.5	442	883.9	\$S wl Rm313
31304	13 rpp	0	3	801.25	876	442	883.9	\$E block wl Rm313
31305	13 rpp	3	21	873	876	442	883.9	\$E block wl Rm313
31306	13 rpp	21	24	800.75	876.75	442	883.9	\$E block wl Rm313
31307	13 rpp	3	21	801.25	804.25	442	883.9	\$E block wl Rm313
31308	13 rpp	0	3	915	996.75	442	883.9	\$NE block wl Rm313
31309	13 rpp	3	21	993.75	996.75	442	883.9	\$NE block wl Rm313

31310 13 rpp 21 24 972.75 996.75 442 883.9 \$NE block wl Rm313  
 31311 13 rpp 21 24 914.25 942.75 442 883.9 \$NE block wl Rm313  
 31312 13 rpp 3 21 915 918 442 883.9 \$NE block wl Rm313  
 31313 13 rpp -292 0 727.5 949.5 442 883.9 \$Roomspace 313  
 c  
 c  
 c Floor1 Room 317  
 31701 13 rpp -292 0 960 967.5 442 883.9 \$S wl Rm317  
 31702 13 rpp -292 0 1069.5 1077 442 883.9 \$N wl Rm317  
 31703 13 rpp -292 0 1077 1080 442 883.9 \$N wl Rm317  
 31704 13 rpp -292 0 967.5 1069.5 442 883.9 \$Roomspace 317  
 c  
 c  
 c Floor1 Room 319/319A  
 31901 13 rpp -292 24 1197.25 1200.25 442 883.9 \$N wl Rm319  
 31902 13 rpp -148.25 -145.25 1080 1197.25 442 883.9 \$Dividing wl Rm319  
 31903 13 rpp -295 -292 1191 1197.25 442 883.9 \$W wl Rm319  
 31904 13 rpp -295 -292 351 1155 442 883.9 \$W wl Rm309-319  
 31905 13 rpp 0 3 1036 1116.5 442 883.9 \$SE block wl Rm319  
 31906 13 rpp 3 21 1113.5 1116.5 442 883.9 \$SE block wl Rm319  
 31907 13 rpp 21 24 1036 1118.5 442 883.9 \$SE block wl Rm319  
 31908 13 rpp 3 21 1036 1039 442 883.9 \$SE block wl Rm319  
 31909 13 rpp 0 3 1155.5 1197.25 442 883.9 \$NE block wl Rm319  
 31910 13 rpp 3 21 1155.5 1158.5 442 883.9 \$NE block wl Rm319  
 31911 13 rpp 21 24 1153.5 1197.25 442 883.9 \$NE block wl Rm319  
 31912 13 rpp -292 -148.25 1080 1197.25 442 883.9 \$Roomspace 319A  
 31913 13 rpp -145.25 0 1080 1197.25 442 883.9 \$Roomspace 319  
 c  
 c  
 c Floor1 Room 300  
 30001 13 rpp 108 743 -3.5 -.5 442 883.9 \$S wl Rm300  
 30002 13 rpp 121.25 417 -.5 8 442 883.9 \$S wl Rm300  
 30003 13 rpp 417 434 -.5 36.5 442 883.9 \$SE Block in wl Rm300  
 30004 13 rpp 420.5 427 36.5 357.25 442 883.9 \$E wl Rm300  
 30005 13 rpp 417 420.5 258.5 278.5 442 883.9 \$Block in E wl Rm300  
 30006 13 rpp 427 433.5 260.5 276.5 442 883.9 \$Block in E wl Rm300  
 30007 13 rpp 129.75 427 357.25 360.25 442 883.9 \$N wl Rm300  
 30008 13 rpp 108 111 0 43 442 883.9 \$SE block wl Rm300  
 30009 13 rpp 111 118.25 38.5 41.5 442 883.9 \$SE block wl Rm300  
 30010 13 rpp 118.25 121.25 0 41.25 442 883.9 \$SE block wl Rm300  
 30011 13 rpp 108 111 79 283 442 883.9 \$W block wl Rm300  
 30012 13 rpp 111 120.5 157.75 160.75 442 883.9 \$W block wl Rm300  
 30013 13 rpp 120.5 123.5 80.5 160.75 442 883.9 \$W block wl Rm300  
 30014 13 rpp 111 120.5 80.5 83.5 442 883.9 \$W block wl Rm300  
 30015 13 rpp 111 120.5 278.5 281.5 442 883.9 \$W block wl Rm300  
 30016 13 rpp 120.5 123.5 192.5 281.5 442 883.9 \$W block wl Rm300  
 30017 13 rpp 111 120.5 192.5 195.5 442 883.9 \$W block wl Rm300  
 30018 13 rpp 108 111 319 342.75 442 883.9 \$NW block wl Rm300  
 30019 13 rpp 111 136 320.5 323.5 442 883.9 \$NW block wl Rm300  
 30020 13 rpp 136 139 320.5 357.25 442 883.9 \$NW block wl Rm300  
 30021 13 rpp 108 111 373.25 397.75 442 883.9 \$NW block wl Rm300  
 30022 13 rpp 111 129.75 393.25 396.25 442 883.9 \$NW block wl Rm300  
 30023 13 rpp 129.75 132.75 360.25 396.25 442 883.9 \$NW block wl Rm300  
 30024 13 rpp 123.5 420.5 8 320.5 442 883.9 \$Roomspace 300  
 30025 13 rpp 139 420.5 320.5 357.25 442 883.9 \$Roomspace 300  
 c  
 c  
 c Floor1 Room 306  
 30601 13 rpp 424 427 360.25 598 442 883.9 \$E wl Rm306  
 30602 13 rpp 416.5 424 498.5 518.5 442 883.9 \$Block in E wl Rm306  
 30603 13 rpp 427 434.5 498.5 517.5 442 883.9 \$Block in E wl Rm306  
 30604 13 rpp 108 111 433.75 523.5 442 883.9 \$W block wl Rm306  
 30605 13 rpp 111 129.75 519 523.5 442 883.9 \$W block wl Rm306  
 30606 13 rpp 129.75 132.75 435.25 523.5 442 883.9 \$W block wl Rm306  
 30607 13 rpp 111 129.75 435.25 438.25 442 883.9 \$W block wl Rm306  
 30608 13 rpp 108 111 559.5 638 442 883.9 \$NW block wl Rm306  
 30609 13 rpp 111 129.75 633 636 442 883.9 \$NW block wl Rm306  
 30610 13 rpp 129.75 132.75 561 636 442 883.9 \$NW block wl Rm306  
 30611 13 rpp 111 129.75 561 564 442 883.9 \$NW block wl Rm306  
 30612 13 rpp 132.75 424 360.25 595.75 442 883.9 \$Roomspace 306 Partially Filled

c  
c  
c Floor1 Room 310

31001	13	rpp	424	432	598	960	442	883.9	\$E	wl	Rm310
31002	13	rpp	132.75	340.75	595.75	600.75	442	883.9	\$S	wl	Rm310
31003	13	rpp	275.75	280.75	600.75	636	442	883.9	\$Center	wl	Rm310
31004	13	rpp	275.75	280.75	673.25	716.5	442	883.9	\$Center	wl	Rm310
31005	13	rpp	132.75	424	716.5	719.5	442	883.9	\$N	wl	Rm310
31006	13	rpp	132.75	275.75	600.75	716.5	442	883.9	\$Roomspace	310	
31007	13	rpp	280.75	424	600.75	716.5	442	883.9	\$Roomspace	310	East

c  
c  
c Floor1 Room 312

31201	13	rpp	416.5	424	739.5	757.5	442	883.9	\$Block	in E	wl	Rm312
31202	13	rpp	432	468.5	908	956	442	883.9	\$NE	Block	Rm312	
31203	13	rpp	132.75	424	957	960	442	883.9	\$N	wl	Rm312	
31204	13	rpp	108	111	672.75	763.75	442	883.9	\$SW	block	wl	Rm312
31205	13	rpp	111	129.75	759.25	762.25	442	883.9	\$SW	block	wl	Rm312
31206	13	rpp	129.75	132.75	674.75	762.25	442	883.9	\$SW	block	wl	Rm312
31207	13	rpp	111	129.75	674.75	677.75	442	883.9	\$SW	block	wl	Rm312
31208	13	rpp	108	111	799.5	823.5	442	883.9	\$W	block	wl	Rm312
31209	13	rpp	108	111	853.5	877.5	442	883.9	\$W	block	wl	Rm312
31210	13	rpp	111	129.75	873	876	442	883.9	\$W	block	wl	Rm312
31211	13	rpp	129.75	132.75	801.25	876	442	883.9	\$W	block	wl	Rm312
31212	13	rpp	111	129.75	801.25	804.25	442	883.9	\$W	block	wl	Rm312
31213	13	rpp	108	111	913.5	997.5	442	883.9	\$NW	block	wl	Rm312
31214	13	rpp	111	129.75	993	996	442	883.9	\$NW	block	wl	Rm312
31215	13	rpp	129.75	132.75	915	996	442	883.9	\$NW	block	wl	Rm312
31216	13	rpp	111	129.75	918	921	442	883.9	\$NW	block	wl	Rm312
31217	13	rpp	132.75	424	719.5	957	442	883.9	\$Roomspace	312	Partially Filled	

c  
c  
c Floor1 Room 316

31601	13	rpp	424	427	960	1039.5	442	883.9	\$SE	wl	Rm316	
31602	13	rpp	416.5	434.5	1039.5	1057.5	442	883.9	\$Block	in E	wl	Rm316
31603	13	rpp	424	427	1057.5	1197.25	442	883.9	\$E	wl	Rm316	
31604	13	rpp	108	743	1197.25	1200.25	442	883.9	\$N	wl	Rm316	
31605	13	rpp	108	111	1033.5	1117.25	442	883.9	\$W	block	wl	Rm316
31606	13	rpp	111	129.75	1112.75	1115.75	442	883.9	\$W	block	wl	Rm316
31607	13	rpp	129.75	132.75	1035	1115.75	442	883.9	\$W	block	wl	Rm316
31608	13	rpp	111	129.75	1035	1038	442	883.9	\$W	block	wl	Rm316
31609	13	rpp	108	111	1153.25	1197.25	442	883.9	\$NW	block	wl	Rm316
31610	13	rpp	129.75	132.75	1154.75	1197.25	442	883.9	\$NW	block	wl	Rm316
31611	13	rpp	111	129.75	1154.75	1157.75	442	883.9	\$NW	block	wl	Rm316
31612	13	rpp	132.75	424	960	1197.25	442	883.9	\$Roomspace	316	Partially Filled	

c  
c  
c Floor1 Room 401/403

40101	13	rpp	572	681.5	80.5	83.5	442	883.9	\$S	wl	Rm403	
40102	13	rpp	572	575.	83.5	236.5	442	883.9	\$N	wl	Rm401	
40103	13	rpp	427	430.25	236.5	239.5	442	883.9	\$NW	stub	wl	Rm401
40104	13	rpp	462.25	719	236.5	239.5	442	883.9	\$N	wl	Rm401-Rm403	
40105	13	rpp	719	722	-5	41.5	442	883.9	\$SE	block	wl	Rm401
40106	13	rpp	722	740	38.5	41.5	442	883.9	\$SE	block	wl	Rm401
40107	13	rpp	740	743	-5	43	442	883.9	\$SE	block	wl	Rm401
40108	13	rpp	719	722	83.5	155.5	442	883.9	\$E	block	wl	Rm403
40109	13	rpp	722	740	152.5	155.5	442	883.9	\$E	block	wl	Rm403
40110	13	rpp	740	743	79	157	442	883.9	\$E	block	wl	Rm403
40111	13	rpp	717.5	740	80.5	83.5	442	883.9	\$SE	block	wl	Rm403
40112	13	rpp	719	722	194.5	281.5	442	883.9	\$NE	block	wl	Rm403
40113	13	rpp	722	740	278.5	281.5	442	883.9	\$NE	block	wl	Rm403
40114	13	rpp	740	743	193	283	442	883.9	\$NE	block	wl	Rm403
40115	13	rpp	722	740	194.5	197.5	442	883.9	\$NE	block	wl	Rm403
40116	13	rpp	427	572	-5	236.5	442	883.9	\$Roomspace	401		
40117	13	rpp	575	719	83.5	236.5	442	883.9	\$Roomspace	403		

c  
c  
c Floor1 Room 405

40501	13	rpp	476.75	576.25	239.5	247	442	883.9	\$S	thick	wl	Rm405
40502	13	rpp	434.5	546	498.5	501.5	442	883.9	\$NW	wl	Rm405	

40503	13	rrp	543	546	478	498.5	442	883.9	\$NW	wl	Rm405
40504	13	rrp	546	719	478	481	442	883.9	\$N	wl	Rm405
40505	13	rrp	719	722	320.5	394	442	883.9	\$E	block	wl Rm405
40506	13	rrp	722	740	391	394	442	883.9	\$E	block	wl Rm405
40507	13	rrp	740	743	376	397	442	883.9	\$E	block	wl Rm405
40508	13	rrp	722	740	320.5	323.5	442	883.9	\$E	block	wl Rm405
40509	13	rrp	740	743	319	343	442	883.9	\$E	block	wl Rm405
40510	13	rrp	719	722	436	522	442	883.9	\$NE	block	wl Rm405
40511	13	rrp	722	740	519	522	442	883.9	\$NE	block	wl Rm405
40512	13	rrp	740	743	433	523.5	442	883.9	\$NE	block	wl Rm405
40513	13	rrp	722	740	433	436	442	883.9	\$NE	block	wl Rm405
40514	13	rrp	427	719	239.5	478	442	883.9	\$Rooms	space	405 Partially Filled

C

c

c Floor1 Room 409

40901 13 rpp 432 724 598 602 442 883.9 \$N wl Rm409

40902 13 rpp 427 719 501.5 598 442 883.9 \$Roomspace 409 Partially Filled

c

c

c Floor1 Room 411

41101	13	rrp	432	724	956	960	442	883.9	\$N	wl	Rm411
41102	13	rrp	719	722	561	598	442	883.9	\$SE	block	wl Rm411
41103	13	rrp	721	724	602	634.5	442	883.9	\$SE	block	wl Rm411
41104	13	rrp	724	740	631.5	634.5	442	883.9	\$SE	block	wl Rm411
41105	13	rrp	739	743	634.5	636	442	883.9	\$SE	block	wl Rm411
41106	13	rrp	740	743	559.5	634.5	442	883.9	\$SE	block	wl Rm411
41107	13	rrp	722	740	561	564	442	883.9	\$SE	block	wl Rm411
41108	13	rrp	721	724	673.5	873.5	442	883.9	\$E	block	wl Rm411
41109	13	rrp	724	740	870.5	873.5	442	883.9	\$E	block	wl Rm411
41110	13	rrp	740	743	856	873.5	442	883.9	\$E	block	wl Rm411
41111	13	rrp	740	743	672	820	442	883.9	\$E	block	wl Rm411
41112	13	rrp	724	740	673.5	676.5	442	883.9	\$E	block	wl Rm411
41113	13	rrp	739	740	672	673.5	442	883.9	\$E	block	wl Rm411
41114	13	rrp	721	724	931.5	956	442	883.9	\$NE	block	wl Rm411
41115	13	rrp	719	722	960	996	442	883.9	\$NE	block	wl Rm411
41116	13	rrp	722	740	993	996	442	883.9	\$NE	block	wl Rm411
41117	13	rrp	740	743	931.5	997.5	442	883.9	\$NE	block	wl Rm411
41118	13	rrp	724	740	931.5	934.5	442	883.9	\$NE	block	wl Rm411
41119	13	rrp	432	721	602	956	442	883.9	\$Rooms	space	411 Par

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6

6

c Floor1 Room 419

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C

C

c \*\*\*\*\*Notes for this section of Surfaces\*\*\*\*\*

c The origin was set as the SW outside corner of the Southwesternmost wall of Room 400

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C

c Floor1 Room 400

40001	14	rrp	0	635	0	3	442	883.9	\$S	wl	Rm400-Rm501
40002	14	rrp	309.5	325.5	3	39.5	442	883.9	\$SE	Block	wl Rm400
40003	14	rrp	316	319	39.5	240	442	883.9	\$E	wl	Rm400
40004	14	rrp	24	611	240	243	442	883.9	\$N	wl	Rm400-Rm501
40005	14	rrp	0	3	196.5	286.5	442	883.9	\$W	wl	Rm400
40006	14	rrp	0	3	82.5	160.5	442	883.9	\$W	wl	Rm400
40007	14	rrp	0	3	3	46.5	442	883.9	\$W	wl	Rm400
40008	14	rrp	3	21	42	45	442	883.9	\$SW	block	wl Rm400
40009	14	rrp	21	24	3	45	442	883.9	\$SW	block	wl Rm400
40010	14	rrp	3	21	84	87	442	883.9	\$W	block	wl Rm400
40011	14	rrp	21	24	84	159	442	883.9	\$W	block	wl Rm400
40012	14	rrp	3	21	156	159	442	883.9	\$W	block	wl Rm400

40013 14 rpp 3 21 198 201 442 883.9 \$NW block wl Rm400  
 40014 14 rpp 21 24 198 285 442 883.9 \$NW block wl Rm400  
 40015 14 rpp 3 21 282 285 442 883.9 \$NW block wl Rm400  
 40016 14 rpp 24 309.5 3 240 442 883.9 \$Roomspace 400 Partially Filled  
 c  
 c  
 c Floor1 Room 501  
 50101 14 rpp 632 635 196.5 286.5 442 883.9 \$E wl Rm501  
 50102 14 rpp 632 635 82.5 160.5 442 883.9 \$E wl Rm501  
 50103 14 rpp 632 635 3 46.5 442 883.9 \$E wl Rm501  
 50104 14 rpp 614 632 42 45 442 883.9 \$SE block wl Rm501  
 50105 14 rpp 611 614 3 45 442 883.9 \$SE block wl Rm501  
 50106 14 rpp 614 632 84 87 442 883.9 \$E block wl Rm501  
 50107 14 rpp 611 614 84 159 442 883.9 \$E block wl Rm501  
 50108 14 rpp 614 632 156 159 442 883.9 \$E block wl Rm501  
 50109 14 rpp 614 632 198 201 442 883.9 \$NE block wl Rm501  
 50110 14 rpp 611 614 198 285 442 883.9 \$NE block wl Rm501  
 50111 14 rpp 614 632 282 285 442 883.9 \$NE block wl Rm501  
 50112 14 rpp 325.5 611 3 240 442 883.9 \$Roomspace 501 Partially Filled  
 c  
 c  
 c Floor1 Room 500  
 50001 14 rpp 719 1038 0 3 442 883.9 \$S wl Rm500  
 50002 14 rpp 1035 1038 3 46.5 442 883.9 \$SE wl Rm500  
 50003 14 rpp 1035 1038 82.5 160.5 442 883.9 \$E wl Rm500  
 50004 14 rpp 1035 1038 196.5 286.5 442 883.9 \$E wl Rm500-Rm504A  
 50005 14 rpp 743 1035 240 243 442 883.9 \$N wl Rm500  
 50006 14 rpp 719 722 196.5 286.5 442 883.9 \$W wl Rm500  
 50007 14 rpp 719 722 82.5 160.5 442 883.9 \$W wl Rm500  
 50008 14 rpp 719 722 3 46.5 442 883.9 \$W wl Rm500  
 50009 14 rpp 722 740 39 42 442 883.9 \$SW block wl Rm500  
 50010 14 rpp 740 743 3 42 442 883.9 \$SW block wl Rm500  
 50011 14 rpp 722 740 84 87 442 883.9 \$W block wl Rm500  
 50012 14 rpp 740 743 84 159 442 883.9 \$W block wl Rm500  
 50013 14 rpp 722 740 156 159 442 883.9 \$W block wl Rm500  
 50014 14 rpp 722 740 198 201 442 883.9 \$NW block wl Rm500  
 50015 14 rpp 740 743 198 285 442 883.9 \$NW block wl Rm500  
 50016 14 rpp 722 740 282 285 442 883.9 \$NW block wl Rm500  
 50017 14 rpp 743 1035 3 240 442 883.9 \$Roomspace 500  
 c  
 c  
 c Floor1 Room 404  
 40401 14 rpp 168.5 171.5 243 363 442 883.9 \$E wl Rm404  
 40402 14 rpp 24 168.5 360 363 442 883.9 \$N wl Rm404  
 40403 14 rpp 0 3 377.5 400.5 442 883.9 \$W wl Rm404  
 40404 14 rpp 0 3 322.5 347 442 883.9 \$W wl Rm404  
 40405 14 rpp 24 168.5 243 360 442 883.9 \$Roomspace 404  
 c  
 c  
 c Floor1 Room 505  
 50501 14 rpp 309.5 325.5 263.5 279.5 442 883.9 \$W column in wl Rm505  
 50502 14 rpp 316 319 279.5 503.5 442 883.9 \$W wl Rm505-Rm507  
 50503 14 rpp 319 611 360 363 442 883.9 \$N wl Rm505  
 50504 14 rpp 632 635 377.5 400.5 442 883.9 \$E wl Rm505  
 50505 14 rpp 632 635 322.5 347 442 883.9 \$E wl Rm505  
 50506 14 rpp 316 319 243 263.5 442 883.9 \$SE wl Rm505  
 50507 14 rpp 325.5 611 243 360 442 883.9 \$Roomspace 505 Partially Filled  
 c  
 c  
 c Floor1 Room 504/504A  
 50401 14 rpp 719 722 322.5 347 442 883.9 \$W wl Rm504  
 50402 14 rpp 719 722 377.5 400.5 442 883.9 \$W wl Rm504  
 50403 14 rpp 743 1035 360 363 442 883.9 \$N wl Rm504  
 50404 14 rpp 888 891 243 360 442 883.9 \$Central wl Rm504-Rm504A  
 50405 14 rpp 1035 1038 322.5 526.5 442 883.9 \$E wl Rm504A  
 50406 14 rpp 743 888 244 360 442 883.9 \$Roomspace 504  
 50407 14 rpp 891 1035 244 360 442 883.9 \$Roomspace 504  
 c  
 c  
 c Floor1 Room 406

40601 14 rpp 309.5 325.5 503.5 519.5 442 883.9 \$E block in wl Rm406  
 40602 14 rpp 316 319 519.5 600 442 883.9 \$E wl Rm406  
 40603 14 rpp 24 611 600 603 442 883.9 \$N wl Rm406-Rm507  
 40604 14 rpp 0 3 562.5 640.5 442 883.9 \$W wl Rm406  
 40605 14 rpp 0 3 436.5 526.5 442 883.9 \$W wl Rm406  
 40606 14 rpp 3 21 324 327 442 883.9 \$SW block wl Rm406  
 40607 14 rpp 21 24 324 399 442 883.9 \$SW block wl Rm406  
 40608 14 rpp 3 21 396 399 442 883.9 \$SW block wl Rm406  
 40609 14 rpp 21 24 438 525 442 883.9 \$W block wl Rm406  
 40610 14 rpp 3 21 438 441 442 883.9 \$W block wl Rm406  
 40611 14 rpp 3 21 522 525 442 883.9 \$W block wl Rm406  
 40612 14 rpp 3 21 564 567 442 883.9 \$NW block wl Rm406  
 40613 14 rpp 21 24 564 639 442 883.9 \$NW block wl Rm406  
 40614 14 rpp 3 21 636 639 442 883.9 \$NW block wl Rm406  
 40615 14 rpp 24 309.5 363 600 442 883.9 \$Roomspace 406 Partially Filled

c

c

c Floor1 Room 507

50701 14 rpp 632 635 562.5 640.5 442 883.9 \$E wl Rm507  
 50702 14 rpp 632 635 436.5 526.5 442 883.9 \$E wl Rm507  
 50703 14 rpp 614 632 324 327 442 883.9 \$SE block wl Rm507  
 50704 14 rpp 611 614 324 399 442 883.9 \$SE block wl Rm507  
 50705 14 rpp 614 632 396 399 442 883.9 \$SE block wl Rm507  
 50706 14 rpp 614 632 438 441 442 883.9 \$E block wl Rm507  
 50707 14 rpp 611 614 438 525 442 883.9 \$E block wl Rm507  
 50708 14 rpp 614 632 522 525 442 883.9 \$E block wl Rm507  
 50709 14 rpp 614 632 564 567 442 883.9 \$NE block wl Rm507  
 50710 14 rpp 611 614 564 639 442 883.9 \$NE block wl Rm507  
 50711 14 rpp 614 632 636 639 442 883.9 \$NE block wl Rm507  
 50712 14 rpp 325.5 611 363 600 442 883.9 \$Roomspace 507 Partially Filled

c

c

c Floor1 Room 506

50601 14 rpp 719 722 562.5 640.5 442 883.9 \$W wl Rm506  
 50602 14 rpp 719 722 436.5 526.5 442 883.9 \$W wl Rm506  
 50603 14 rpp 743 1035 600 603 442 883.9 \$N wl Rm506  
 50604 14 rpp 1035 1038 562.5 640.5 442 883.9 \$E wl Rm506  
 50605 14 rpp 722 740 325 328 442 883.9 \$SW block wl Rm506  
 50606 14 rpp 740 743 325 399 442 883.9 \$SW block wl Rm506  
 50607 14 rpp 722 740 396 399 442 883.9 \$SW block wl Rm506  
 50608 14 rpp 722 740 438 441 442 883.9 \$W block wl Rm506  
 50609 14 rpp 740 743 438 525 442 883.9 \$W block wl Rm506  
 50610 14 rpp 722 740 522 525 442 883.9 \$W block wl Rm506  
 50611 14 rpp 722 740 564 567 442 883.9 \$NW block wl Rm506  
 50612 14 rpp 740 743 564 639 442 883.9 \$NW block wl Rm506  
 50613 14 rpp 722 740 636 639 442 883.9 \$NW block wl Rm506  
 50614 14 rpp 743 1035 363 600 442 883.9 \$Roomspace 506

c

c

c Floor1 Room 410

41001 14 rpp 0 3 676.5 766.5 442 883.9 \$W wl Rm410  
 41002 14 rpp 0 3 802.5 826.5 442 883.9 \$W wl Rm410  
 41003 14 rpp 0 3 855.25 880.5 442 883.9 \$W wl Rm410  
 41004 14 rpp 24 611 840 843 442 883.9 \$N wl Rm410  
 41005 14 rpp 316 319 759.5 840 442 883.9 \$E wl Rm410  
 41006 14 rpp 309.5 325.5 743.5 759.5 442 883.9 \$E Column in wl Rm410  
 41007 14 rpp 316 319 603 743.5 442 883.9 \$SE wl Rm410  
 41008 14 rpp 3 21 678 681 442 883.9 \$W block wl Rm410  
 41009 14 rpp 21 24 678 765 442 883.9 \$W block wl Rm410  
 41010 14 rpp 3 21 762 765 442 883.9 \$W block wl Rm410  
 41011 14 rpp 3 21 804 807 442 883.9 \$NW block wl Rm410  
 41012 14 rpp 21 24 804 879 442 883.9 \$NW block wl Rm410  
 41013 14 rpp 3 21 876 879 442 883.9 \$NW block wl Rm410  
 41014 14 rpp 24 309.5 603 840 442 883.9 \$Roomspace 410 Partially Filled

c

c

c Floor1 Room 511

51101 14 rpp 632 635 676.5 766.5 442 883.9 \$E wl Rm511  
 51102 14 rpp 632 635 802.5 826.5 442 883.9 \$E wl Rm511  
 51103 14 rpp 632 635 855.25 880.5 442 883.9 \$E wl Rm511

51104	14	rpp	614	632	678	681	442	883.9	\$E	block	wl	Rm511
51105	14	rpp	611	614	678	765	442	883.9	\$E	block	wl	Rm511
51106	14	rpp	614	632	762	765	442	883.9	\$E	block	wl	Rm511
51107	14	rpp	614	632	804	807	442	883.9	\$NE	block	wl	Rm511
51108	14	rpp	611	614	804	879	442	883.9	\$NE	block	wl	Rm511
51109	14	rpp	614	632	876	879	442	883.9	\$NE	block	wl	Rm511
51110	14	rpp	325.5	611	603	840	442	883.9	\$Roomspace	511	Partially Filled	
c												
c												
c	Floor1	Room	510									
51001	14	rpp	719	722	676.5	766.5	442	883.9	\$W	wl	Rm510	
51002	14	rpp	743	1035	840	843	442	883.9	\$N	wl	Rm510	
51003	14	rpp	1035	1038	676.5	1000	442	883.9	\$E	wl	Rm510	
51004	14	rpp	722	740	678	681	442	883.9	\$W	block	wl	Rm510
51005	14	rpp	740	743	678	765	442	883.9	\$W	block	wl	Rm510
51006	14	rpp	722	740	762	765	442	883.9	\$W	block	wl	Rm510
51007	14	rpp	722	740	804	807	442	883.9	\$NW	block	wl	Rm510
51008	14	rpp	740	743	804	879	442	883.9	\$NW	block	wl	Rm510
51009	14	rpp	722	740	876	879	442	883.9	\$NW	block	wl	Rm510
51010	14	rpp	743	1035	603	840	442	883.9	\$Roomspace	510		
c												
c												
c	Floor1	Room	514									
51401	14	rpp	719	722	802.5	880.5	442	883.9	\$W	wl	Rm514	
51402	14	rpp	743	1035	960	963	442	883.9	\$N	wl	Rm514	
51403	14	rpp	719	722	916.5	1000	442	883.9	\$W	wl	Rm514	
51404	14	rpp	743	1035	843	960	442	883.9	\$Roomspace	514		
c												
c												
c	Floor1	Room	515									
51501	14	rpp	632	635	916.5	1000	442	883.9	\$E	wl	Rm515	
51502	14	rpp	319	611	843	960	442	883.9	\$Roomspace	515		
c												
c												
c	Floor1	Room	414									
41401	14	rpp	316	319	843	960	442	883.9	\$E	wl	Rm414	
41402	14	rpp	24	611	960	963	442	883.9	\$N	wl	Rm414	
41403	14	rpp	0	3	916.5	1000	442	883.9	\$W	wl	Rm414	
41404	14	rpp	24	316	843	960	442	883.9	\$Roomspace	414		
c												
c												
c	Floor1	Room	416									
41601	14	rpp	0	3	1037	1120	442	883.9	\$W	wl	Rm416	
41602	14	rpp	0	3	1156.5	1203	442	883.9	\$W	wl	Rm416	
41603	14	rpp	3	635	1200	1203	442	883.9	\$N	wl	Rm416-Rm517	
41604	14	rpp	316	319	963	1043.5	442	883.9	\$E	wl	Rm416	
41605	14	rpp	309.5	325.5	1043.5	1059.5	442	883.9	\$E	block	Rm416	
41606	14	rpp	316	319	1059.5	1200	442	883.9	\$E	wl	Rm416	
41607	14	rpp	3	21	918	921	442	883.9	\$SW	block	wl	Rm416
41608	14	rpp	21	24	918	999	442	883.9	\$SW	block	wl	Rm416
41609	14	rpp	3	21	996	999	442	883.9	\$SW	block	wl	Rm416
41610	14	rpp	3	21	1038	1041	442	883.9	\$W	block	wl	Rm416
41611	14	rpp	21	24	1038	1118	442	883.9	\$W	block	wl	Rm416
41612	14	rpp	3	21	1115	1118	442	883.9	\$W	block	wl	Rm416
41613	14	rpp	3	21	1158	1161	442	883.9	\$NW	block	wl	Rm416
41614	14	rpp	21	24	1158	1200	442	883.9	\$NW	block	wl	Rm416
41615	14	rpp	24	309.5	963	1200	442	883.9	\$Roomspace	416	Partially Filled	
c												
c												
c	Floor1	Room	517									
51701	14	rpp	632	635	1156.5	1200	442	883.9	\$E	wl	Rm517	
51702	14	rpp	632	635	1037	1119.75	442	883.9	\$E	wl	Rm517	
51703	14	rpp	614	632	918	921	442	883.9	\$SE	block	wl	Rm517
51704	14	rpp	611	614	918	999	442	883.9	\$SE	block	wl	Rm517
51705	14	rpp	614	632	996	999	442	883.9	\$SE	block	wl	Rm517
51706	14	rpp	614	632	1038	1041	442	883.9	\$E	block	wl	Rm517
51707	14	rpp	611	614	1038	1118	442	883.9	\$E	block	wl	Rm517
51708	14	rpp	614	632	1115	1118	442	883.9	\$E	block	wl	Rm517
51709	14	rpp	614	632	1158	1161	442	883.9	\$NE	block	wl	Rm517
51710	14	rpp	611	614	1158	1200	442	883.9	\$NE	block	wl	Rm517



60222	15	ropp	478.5	560	247	252	442	883.9	\$NE	wl	Rm606
60223	15	ropp	478.5	483.5	242	247	442	883.9	\$NE	wl	protrusion Rm606
60224	15	ropp	366	573	0	14	442	883.9	\$S	wl	Rm602
60225	15	ropp	400.75	405.75	14	16.75	442	883.9	\$S	wl	protrusion Rm602
60226	15	ropp	512.75	529	14	17.75	442	883.9	\$SE	wl	protrusion Rm602
60227	15	ropp	573	577	0	288	442	883.9	\$E	i	wl Rm602<-----Some anomalies here-----
60228	15	ropp	577	580.5	-4	259.5	442	518.2	\$E	o	wl Rm602
60231	15	ropp	487	560	169	247	442	883.9	\$Roomspace	606	
60232	15	ropp	577	580.5	-4	259.5	518.2	883.9	\$E	o	wl Rm602

c

c

#### c Floor1 Room 610 Truck Lock

c \*\*\*\*\*Note: a .5cm thick material that borders the dock was neglected\*\*\*\*\*

61001	15	ropp	580.5	1078.5	257	259.5	442	883.9	\$S	exterior	wl Rm610
61002	15	ropp	577	1076	259.5	264.5	442	883.9	\$S	interior	wl Rm610
61003	15	ropp	577	580.5	264.5	288	442	883.9	\$SW	wl	Rm610
61004	15	ropp	581.5	589.5	266	274	442	883.9	\$SW	column	Rm610
61005	15	ropp	821.5	829.5	266	274	442	883.9	\$S	column	Rm610
61006	15	ropp	1061.5	1069.5	266	274	442	883.9	\$SE	column	Rm610
61007	15	ropp	573	577	324	342	442	883.9	\$W	wl	stub Rm610
61008	15	ropp	577	580.5	324	342	442	883.9	\$W	wl	stub Rm610
61009	15	ropp	573	577	462	506.5	442	883.9	\$NW	wl	Rm610
61010	15	ropp	577	580.5	462	509	442	883.9	\$NW	wl	Rm610
61011	15	ropp	558.5	576.5	506.5	513.5	442	883.9	\$NW	Block	<-----What is this?
61012	15	ropp	580.5	819.5	508	509	442	883.9	\$N	wl	Rm610
61013	15	ropp	577	819.5	509	511	442	883.9	\$N	wl	Rm610
61014	15	ropp	577	819.5	511	512	442	883.9	\$N	wl	Rm610
61015	15	ropp	819.5	831.5	505	515	442	883.9	\$N	column	in wl Rm610
61016	15	ropp	831.5	1060.5	508	509	442	883.9	\$N	wl	Rm610
61017	15	ropp	831.5	1060.5	509	511	442	883.9	\$N	wl	Rm610
61018	15	ropp	831.5	1060.5	511	512	442	883.9	\$N	wl	Rm610
61019	15	ropp	1060.5	1070.5	506	514	442	883.9	\$NW	column	in wl Rm610
61020	15	ropp	1071	1076	486	527	442	883.9	\$NW	perependicular	dividing wl Rm610
61021	15	ropp	1076	1078.5	486	527	442	883.9	\$NW	perependicular	dividing wl Rm610
61022	15	ropp	1078.5	1310.5	506	514	442	883.9	\$N	wl	Rm610-1
61023	15	ropp	1311	1316	486	514	442	883.9	\$NE	i	wl Rm610-1
61024	15	ropp	1316	1318.5	486	514	442	883.9	\$NE	o	wl Rm610-1
61025	15	ropp	1311	1316	264.5	342	442	883.9	\$NE	i	wl Rm610-1
61026	15	ropp	1316	1318.5	259.5	342	442	883.9	\$NE	o	wl Rm610-1
61027	15	ropp	1282.5	1316	259.5	264.5	442	883.9	\$SE	i	wl Rm610-1
61028	15	ropp	1282.5	1318.5	257	259.5	442	883.9	\$SE	o	wl Rm610-1
61029	15	ropp	1078.5	1246.5	259.5	264.5	442	883.9	\$SW	i	wl Rm610-1
61030	15	ropp	1078.5	1246.5	257	259.5	442	883.9	\$SW	o	wl Rm610-1
61031	15	ropp	1079.5	1087.5	266	274	442	883.9	\$SW	column	Rm610-1
61032	15	ropp	1301.5	1309.5	266	274	442	883.9	\$SE	column	Rm610-1
61033	15	ropp	1079.5	1087.5	496	504	442	883.9	\$NW	column	Rm610-1
61034	15	ropp	1301.5	1309.5	496	504	442	883.9	\$NE	column	Rm610-1
61035	15	ropp	1071	1076	264.5	288	442	883.9	\$dividing	i	wl Rm610-Rm610-1
61036	15	ropp	1076	1078.5	259.5	288	442	883.9	\$dividing	o	wl Rm610-Rm610-1
61037	15	ropp	1071	1076	324	342	442	883.9	\$dividing	i	wl Rm610-Rm610-1
61038	15	ropp	1076	1078.5	324	342	442	883.9	\$dividing	o	wl Rm610-Rm610-1

c

c

#### c Floor1 Room 603

c \*\*\*\*\*Neglected block in SE corner, above room 606\*\*\*\*\*

60301	15	ropp	577	1076	742.5	747.5	442	883.9	\$N	i	wl Rm610
60302	15	ropp	577	1078.5	747.5	750	442	883.9	\$N	o	wl Rm610
60303	15	ropp	581.5	589.5	733	741	442	883.9	\$N	column	Rm610
60304	15	ropp	821.5	829.5	733	741	442	883.9	\$N	2nd	column Rm610
60305	15	ropp	941.5	949.5	733	741	442	883.9	\$N	3rd	column Rm610
60306	15	ropp	1061.5	1069.5	733	741	442	883.9	\$N	4th	column Rm610
60307	15	ropp	1071	1076	562	742.5	442	883.9	\$E	i	wl Rm610
60308	15	ropp	1076	1078.5	562	747.5	442	883.9	\$E	o	wl Rm610
60309	15	ropp	941.5	949.5	579.75	587.75	442	883.9	\$SE	column	Rm610
60310	15	ropp	1061.5	1069.5	579.75	587.75	442	883.9	\$SE	2n	column
60311	15	ropp	573	577	753.5	1548.5	442	883.9	\$E	i	wl Rm603
60312	15	ropp	577	580.5	750	1552	442	518.2	\$E	o	wl Rm603
60313	15	ropp	558.5	576.5	746.5	753.5	442	883.9	\$E	Block	in wl Rm603
60314	15	ropp	554	572	986	994	442	883.9	\$E	Block	next one N of 60313
60315	15	ropp	551	572	1048.5	1057.5	442	883.9	\$E	Block	next one N of 60314





10917 17 rpp 202.5 205.5 560 606.5 442 883.9 \$Central dividing wl MCR  
 10918 17 rpp 205.5 302 603.5 606.5 442 883.9 \$N wl MCR  
 10919 17 rpp 302 318 597 613 442 883.9 \$N column in wl MCR  
 10920 17 rpp 318 562 603.5 606.5 442 883.9 \$N wl MCR-Rm109  
 10921 17 rpp 466.5 469.5 360.5 603.5 442 883.9 \$E wl MCR  
 10922 17 rpp 469.5 616.5 360.5 363.5 442 883.9 \$E wl MCR  
 c Room 109/109A Below here  
 10923 17 rpp 616.5 619.5 354 594 442 883.9 \$E wl Rm109-109A  
 10924 17 rpp 469.5 509.5 498.5 501.5 442 883.9 \$S wl Rm109  
 10925 17 rpp 545.5 616.5 498.5 501.5 442 883.9 \$S wl Rm109  
 c Main lobby area - MLA  
 10926 17 rpp 603.5 616.5 3 13 442 883.9 \$S column MLA  
 10927 17 rpp 703.5 731.5 0 4.5 442 518.2 \$SE wl MLA  
 10928 17 rpp 722.5 731.5 4.5 13 442 883.9 \$SE block in wl MLA  
 c Second half of Mens Change Room - MCR/Showers - SH/Pipe Chase - PC/Mens Bathroom - MB  
 10929 17 rpp 5.5 15.5 597 613 442 883.9 \$W block in wl MCR  
 10930 17 rpp 5.5 295.5 871.5 874.5 442 883.9 \$N wl MCR-PC-SH  
 10931 17 rpp 5.5 304.5 876.5 879.5 442 883.9 \$N wl MCR-PC-SH  
 10932 17 rpp 111.5 114.5 762.5 871.5 442 883.9 \$E wl MCR  
 10933 17 rpp 117.5 120.5 762.5 871.5 442 883.9 \$E wl MCR  
 10934 17 rpp 111.5 158.5 759.5 762.5 442 883.9 \$NE wl MCR- Hallway  
 10935 17 rpp 120.5 158.5 762.5 764.5 442 883.9 \$SW i wl SH  
 10936 17 rpp 120.5 122.5 764.5 871.5 442 883.9 \$W i wl SH  
 10937 17 rpp 122.5 292.5 869.5 871.5 442 883.9 \$N i wl SH  
 10938 17 rpp 290.5 292.5 678.5 869.5 442 883.9 \$E i wl SH  
 10939 17 rpp 204 290.5 678.5 680.5 442 883.9 \$S i wl SH  
 10940 17 rpp 204 206 680.5 718.5 442 883.9 \$SW i wl SH  
 10941 17 rpp 201 204 675.5 718.5 442 883.9 \$SW o wl SH  
 10942 17 rpp 204 366 675.5 678.5 442 883.9 \$S o wl SH-PC-MB  
 10943 17 rpp 292.5 295.5 678.5 871.5 442 883.9 \$W wl PC  
 10944 17 rpp 316 319 678.5 908 442 883.9 \$E wl PC  
 10945 17 rpp 320.5 360.5 678.5 680 442 883.9 \$SW i wl MB  
 10946 17 rpp 319 320.5 678.5 905 442 883.9 \$W i wl MB  
 10947 17 rpp 320.5 467.5 903.5 905 442 883.9 \$N i wl MB  
 10948 17 rpp 466 467.5 729.5 903.5 442 883.9 \$E i wl MB  
 10949 17 rpp 407.5 466 729.5 731 442 883.9 \$SE wl MB  
 10950 17 rpp 407.5 409 678.5 729.5 442 883.9 \$SE wl MB  
 10951 17 rpp 402 414 675.5 678.5 442 883.9 \$S o wl MB  
 10952 17 rpp 409 412 678.5 729.5 442 883.9 \$SE o wl MB  
 10953 17 rpp 412 467.5 726.5 729.5 442 883.9 \$SE o wl MB  
 10954 17 rpp 467.5 470.5 678.5 908 442 883.9 \$E o wl MB  
 10955 17 rpp 319 467.5 905 908 442 883.9 \$N o wl MB  
 10956 17 rpp 444 624 675.5 678.5 442 883.9 \$S wl MB-Rm108  
 10957 17 rpp 463 466 660.5 675.5 442 883.9 \$S hallway wl MB  
 c  
 c Hallway above Room 109 and below Room 108  
 c Very small wall fragments were ignored on the block defined in this section  
 10958 17 rpp 463 466 606.5 624.5 442 883.9 \$W Hallway wl  
 10959 17 rpp 540 543 606.5 623 442 883.9 \$E hallway wl  
 10960 17 rpp 602.5 648 594 606.5 442 883.9 \$Block in hallway above E wl of Rm109  
 10961 17 rpp 603.5 627 606.5 613 442 883.9 \$Block in hallway above E wl of Rm109  
 10962 17 rpp 469.5 616.5 363.5 498.5 442 883.9 \$Roomspace 109A  
 10963 17 rpp 469.5 616.5 501.5 603.5 442 883.9 \$Roomspace 109 Partially Filled  
 c 10964 17 rpp 442 883.9 \$Roomspace  
 c 10965 17 rpp 442 883.9 \$Roomspace  
 10966 17 rpp 535.5 635.5 0 3 518.2 883.9 \$SE wl LR u  
 10967 17 rpp 703.5 731.5 0 4.5 518.2 883.9 \$SE wl MLA  
 c  
 c  
 c Floor1 Room 110/ Men B Room Women B Room/ Conf Room Women change room/ copy room  
 c Mens Room - MR/Pipe Chase -PC/Womens Room - WR  
 c small piece of wall omitted in the south west corner of the Mens room  
 11001 17 rpp 726.5 734.5 13 120.5 442 883.9 \$W wl MR  
 11002 17 rpp 734.5 741.5 117.5 120.5 442 883.9 \$NW wl MR  
 11003 17 rpp 777.5 930.5 117.5 120.5 442 883.9 \$N wl MR-WR  
 11004 17 rpp 785.5 844 112.5 117.5 442 883.9 \$N wl MR  
 11005 17 rpp 841 844 3.5 112.5 442 883.9 \$E wl MR  
 11006 17 rpp 731.5 1024 0 3.5 442 518.2 \$S wl MR-PC-WR  
 11007 17 rpp 864.5 868 3.5 112.5 442 883.9 \$W wl WR  
 11008 17 rpp 864.5 923.5 112.5 117.5 442 883.9 \$NW wl WR

11009 17 rpp 974.5 982.5 3.5 120.5 442 883.9 \$E wl WR  
 11010 17 rpp 966.5 974.5 117.5 120.5 442 883.9 \$NE stub wl WR  
 11011 17 rpp 979.5 982.5 120.5 138 442 883.9 \$NE stub wl WR  
 c Room 110/Conf Room - CR starts below here  
 11012 17 rpp 726.5 729.5 189.5 294 442 883.9 \$W wl Rm110  
 11013 17 rpp 718.5 795 294 304 442 883.9 \$N wl Rm110  
 11014 17 rpp 718.5 786 304 313 442 883.9 \$N wl Rm110  
 11015 17 rpp 729.5 809.5 189.5 192.5 442 883.9 \$SW wl Rm110  
 11016 17 rpp 845.5 979.5 189.5 192.5 442 883.9 \$SE wl Rm110  
 11017 17 rpp 979.5 982.5 174 294 442 883.9 \$E wl Rm110  
 11018 17 rpp 831.5 1335.5 294 297 442 883.9 \$N wl Rm110-CR  
 11019 17 rpp 831.5 834 297 301 442 883.9 \$N wl stub Rm110  
 11020 17 rpp 831.5 1023.5 301 304 442 883.9 \$N wl Rm110 or S wl Rm 110c  
 11021 17 rpp 1020.5 1024 3.5 10 442 883.9 \$S wl box CR  
 11022 17 rpp 1020.5 1036.5 10 13.5 442 883.9 \$S wl box CR  
 11023 17 rpp 1033 1036.5 3.5 10 442 883.9 \$S wl box CR  
 11024 17 rpp 1033 1325.5 0 3.5 442 883.9 \$S wl CR  
 11025 17 rpp 1322 1325.5 3.5 10 442 883.9 \$SEwl Cr  
 11026 17 rpp 1322 1332 10 13.5 442 883.9 \$SE wl CR  
 11027 17 rpp 1332 1335.5 10 294 442 883.9 \$E wl CR  
 c Room 110A - A/Room110C - C/Room 110B - B/Copy Room - copy/  
 11028 17 rpp 727 731 313 392 442 883.9 \$W wl A  
 11029 17 rpp 727 731 428 434 442 883.9 \$NW wl stub A  
 11030 17 rpp 727 1020.5 434 438 442 883.9 \$N wl A-C  
 11031 17 rpp 856.5 860.5 346 434 442 883.9 \$Dividing wl A-C  
 11032 17 rpp 856.5 860.5 304 310 442 883.9 \$ " wl A-c stub  
 11033 17 rpp 1020.5 1023.5 304 338 442 883.9 \$SE wl C  
 11034 17 rpp 1025.5 1028.5 312 338 442 883.9 \$SE wl C  
 11035 17 rpp 1028.5 1038.5 312 315 442 883.9 \$SE wl C  
 11036 17 rpp 1035.5 1038.5 302 312 442 883.9 \$SE wl C  
 11037 17 rpp 1038.5 1325 302 305 442 883.9 \$S wl C - WCR  
 11038 17 rpp 1060 1063 305 385 442 883.9 \$E closed wl C  
 11039 17 rpp 1028.5 1060 382 385 442 883.9 \$N closet wl C  
 11040 17 rpp 1025.5 1028.5 368 548 442 883.9 \$E wl C-B  
 11041 17 rpp 1020.5 1023.5 368 554 442 883.9 \$E wl C-B  
 11042 17 rpp 898.5 1020.5 542 545 442 883.9 \$N wl B  
 11043 17 rpp 851.25 862.5 542 545 442 883.9 \$NW wl stub B  
 11044 17 rpp 851.25 855.25 438 542 442 883.9 \$W wl copy  
 11045 17 rpp 759 762 438 546 442 883.9 \$W wl copy  
 c Women change room below here - WCR  
 11046 17 rpp 1322 1325 305 312 442 883.9 \$SE corner wl WCR  
 11047 17 rpp 1322 1335.5 312 315 442 883.9 \$SE corner wl WCR  
 11048 17 rpp 1332 1335.5 315 600 442 883.9 \$E wl WCR  
 11049 17 rpp 1158.5 1332 561.5 564.5 442 883.9 \$N wl WCR  
 11050 17 rpp 1080.5 1083.5 521.5 606.5 442 883.9 \$W wl WCR  
 c Wall above copy room and 110B but below Room 111 and the North Eastern Womens restroom below here  
 11051 17 rpp 1036.5 1080.5 603.5 606.5 442 883.9 \$E section hallway wl  
 11052 17 rpp 1020.5 1036.5 597 613 442 883.9 \$Block in hallway wl  
 11053 17 rpp 1020.5 1023.5 590 597 442 883.9 \$Stub out of block in hallway wl  
 11054 17 rpp 734.5 1020.5 603.5 606.5 442 883.9 \$Central section of hallway wl  
 11055 17 rpp 711 734.5 594 613 442 883.9 \$Block on western edge hallway wl  
 11056 17 rpp 690 711 594 606.5 442 883.9 \$Block on western edge hallway wl  
 11057 17 rpp 711 714 613 623 442 883.9 \$Block stub hallway wl  
 c Womens lounge - WL  
 11058 17 rpp 1175.5 1178.5 564.5 568.5 442 883.9 \$Sw wl stub WL  
 11059 17 rpp 1175.5 1178.5 603.5 712 442 883.9 \$W wl WL  
 11060 17 rpp 1178.5 1332 709 712 442 883.9 \$N wl WL  
 11061 17 rpp 1330.5 1332 613.5 709 442 883.9 \$E i wl WL  
 11062 17 rpp 1332 1335.5 610 898 442 883.9 \$E o wl WL  
 11063 17 rpp 1322 1332 610 613.5 442 883.9 \$E box in wl WL  
 11064 17 rpp 1320.5 1330.5 613.5 615 442 883.9 \$E box in wl WL  
 11065 17 rpp 1322 1325.5 595 610 442 883.9 \$E box in wl WL  
 11066 17 rpp 1320.5 1322 593.5 613.5 442 883.9 \$E box in wl WL  
 11067 17 rpp 1325.5 1332 595 600 442 883.9 \$E box in wl WL  
 11068 17 rpp 1322 1332 593.5 595 442 883.9 \$E box in wl WL  
 11069 17 rpp 1330.5 1332 564.5 593.5 442 883.9 \$SE wl WL  
 11070 17 rpp 729.5 979.5 192.5 294 442 883.9 \$Roomspace 110  
 11071 17 rpp 731.25 856.5 313 434 442 883.9 \$Roomspace 110A Partially Filled  
 11072 17 rpp 860.5 1020.5 304 434 442 883.9 \$Roomspace 110C  
 11073 17 rpp 764.25 851.25 438 542 442 883.9 \$Roomspace Copy Room

11074 17 rpp 855.25 1020.5 438 542 442 883.9 \$Roomspace 110B  
 11075 17 rpp 731.5 1024 0 3.5 518.2 883.9 \$S wl MR-PC-WR u  
 11076 17 rpp 725.5 1335.5 -3.25 0 442 883.9 \$S wl MR-PC-WR  
 11077 17 rpp 778 1338.75 -7.5 -3.25 442 518.2 \$S o wl MR-PC-WR 1  
 11078 17 rpp 778 1338.75 -7.5 -3.25 518.2 883.9 \$S o wl MR-PC-WR 1  
 c  
 c  
 c Floor1 Room 111/Room 111A/NW Women Rest Room - NWW/Women change and shower room - WSR  
 11101 17 rpp 711 714 659 702.25 442 883.9 \$SW o wl Rm111  
 11102 17 rpp 714 871 675.5 678.5 442 883.9 \$S wl Rm111  
 11103 17 rpp 795 798 659 675.5 442 883.9 \$S hallway wl Rm111  
 11104 17 rpp 795 798 606.5 623 442 883.9 \$S hallway wl Rm111  
 11105 17 rpp 720 723 678.5 750.75 442 883.9 \$W wl Rm111  
 11106 17 rpp 714 720 747.75 750.75 442 883.9 \$W wl Rm111  
 11107 17 rpp 711 714 744.75 750.75 442 883.9 \$W wl Rm111  
 11108 17 rpp 711 714 782.75 855.75 442 883.9 \$W wl Rm111a  
 11109 17 rpp 714 723 782.25 786.5 442 883.9 \$S wl Rm111a  
 11110 17 rpp 723 840 783.5 786.5 442 883.9 \$S wl Rm111a  
 11111 17 rpp 840 843 764.5 910 442 883.9 \$E wl Rm111a  
 11112 17 rpp 843 855 764.5 767.5 442 883.9 \$SE wl Rm111a  
 11113 17 rpp 855 858 678.5 908 442 883.9 \$E wl Rm111  
 11114 17 rpp 711 714 890.75 897 442 883.9 \$W wl stub Rm111a  
 11115 17 rpp 711 734.5 897 914.5 442 883.9 \$NW block Rm111a  
 11116 17 rpp 734.5 835 910 914.5 442 883.9 \$N wl Rm111a  
 11117 17 rpp 835 1335.5 910 913 442 883.9 \$N wl Rm111a-S wl of Rm112A-Rm115  
 11118 17 rpp 907 924 675.5 678.5 442 883.9 \$S stub wl NWW  
 11119 17 rpp 920 923 678.5 714.5 442 883.9 \$SE wl NWW  
 11120 17 rpp 923 992 711.5 714.5 442 883.9 \$SE wl NWW  
 11121 17 rpp 992 995 678.5 905 442 883.9 \$E wl NWW  
 11122 17 rpp 960 1008 675.5 678.5 442 883.9 \$S wl NWW  
 11123 17 rpp 1005 1008 678.5 898 442 883.9 \$W wl WSR  
 11124 17 rpp 1008 1037 895 898 442 883.9 \$NW wl WSR  
 11125 17 rpp 1034 1037 898 905 442 883.9 \$NW wl WSR  
 11126 17 rpp 858 1323.5 905 908 442 883.9 \$N wl NWW-WSR  
 11127 17 rpp 1323.5 1325.5 898 908 442 883.9 \$NE wl WSR  
 11128 17 rpp 1323.5 1332 895 898 442 883.9 \$NE wl WSR  
 11129 17 rpp 1335.5 1338.75 -3.25 900.45 442 883.9 \$E i wl Exterior to the whole section  
 11130 17 rpp 1338.75 1343 -7.51 897.25 442 518.2 \$E o wl Exterior to the whole section  
 11131 17 rpp 723 840 678.5 783.5 442 883.9 \$Roomspace 111 Partially Filled  
 11132 17 rpp 714 840 786.5 910 442 883.9 \$Roomspace 111A Partially Filled  
 11133 17 rpp 1338.75 1343 -7.51 897.25 518.2 883.9 \$E o wl Exterior to the whole section  
 c  
 c  
 c Floor1 Room 107/108  
 10701 17 rpp 540 543 659 675.5 442 883.9 \$S hallway wall Rm 108  
 10702 17 rpp 624 627 674 759 442 883.9 \$E wl Rm108  
 10703 17 rpp 624 627 794 806.5 442 883.9 \$NE wl Rm108  
 10704 17 rpp 483 624 799 802 442 883.9 \$N wl Rm108  
 10705 17 rpp 480 483 678.5 1050.5 442 883.9 \$W wl Rm108-Rm107-Rm106  
 10706 17 rpp 624 627 842 933.5 442 883.9 \$E wl Rm107  
 10707 17 rpp 483 624 924.5 927.5 442 883.9 \$N wl Rm107  
 10708 17 rpp 483 624 678.5 799 442 883.9 \$Roomspace 108  
 10709 17 rpp 483 624 802 924.5 442 883.9 \$Roomspace 107  
 c  
 c  
 c Floor1 Room 103/104/104A/105/106  
 10301 17 rpp 12.5 15.5 879.5 913 442 883.9 \$SW box wl Rm103  
 10302 17 rpp 6 9 913 1050.5 442 883.9 \$W wl Rm103  
 10303 17 rpp 50 148.5 1050.5 1053.5 442 883.9 \$N wl Rm103  
 10304 17 rpp 140 143 879.5 1050.5 442 883.9 \$E wl Rm103  
 10305 17 rpp 309 439 1050.5 1053.5 442 883.9 \$N wl Rm104  
 10306 17 rpp 183 274.5 1050.5 1053.5 442 883.9 \$N wl Rm104  
 10307 17 rpp 261 264 879.5 1050.5 442 883.9 \$W wl Rm104A  
 10308 17 rpp 304.5 480 910 913 442 883.9 \$S wl Rm104A-Rm105  
 10309 17 rpp 354 357 913 1050.5 442 883.9 \$E wl Rm104A  
 10310 17 rpp 301.5 304.5 879.5 913 442 883.9 \$SE wl Rm104A  
 10311 17 rpp 475 627 1050.5 1053.5 442 883.9 \$N wl Rm106  
 10312 17 rpp 624 627 968 1050.5 442 883.9 \$E wl Rm106  
 10313 17 rpp 15.5 140 879.5 1050.5 442 883.9 \$Roomspace 103  
 10314 17 rpp 143 261 879.5 1050.5 442 883.9 \$Roomspace 104





91303 24 rpp	257.5	476	299.5	304.5	883.9	1468.1	\$S wl Rm913	928
91304 24 rpp	216	329	393.5	398.5	883.9	1468.1	\$N wl Rm913	
91305 24 rpp	329	334	304.5	534.5	883.9	1468.1	\$E wl Rm913-915	
91306 24 rpp	291	296	358.5	393.5	883.9	1468.1	\$NE compartment Rm913	
91307 24 rpp	296	329	358.5	363.5	883.9	1468.1	\$NE compartment Rm913	
91308 24 rpp	216	274	534.5	539.5	883.9	1468.1	\$NW wl Rm915	
91309 24 rpp	310	476	534.5	539.5	883.9	1468.1	\$NE wl Rm915-Rm929	
91310 24 rpp	391	405	539.5	542.5	883.9	1468.1	\$Block in N wl Rm929	
91311 24 rpp	334	471	417	422	883.9	1468.1	\$N wl Rm928	
91312 24 rpp	471	476	304.5	346	883.9	1468.1	\$SE wl Rm928	
91313 24 rpp	471	476	382	493.5	883.9	1468.1	\$NE wl Rm928	
91314 24 rpp	471	476	529.5	534.5	883.9	1468.1	\$NE wl Rm929	
91315 24 rpp	216	291	304.5	393.5	883.9	1468.1	\$Roomspace	913
91316 24 rpp	216	329	398.5	534.5	883.9	1468.1	\$Roomspace	915
91317 24 rpp	334	471	304.5	417	883.9	1468.1	\$Roomspace	928
91318 24 rpp	334	471	422	534.5	883.9	1468.1	\$Roomspace	929

c

c

c Floor2 Room 918/919/917/921/905/923/mech room

91801 24 rpp	211	216	613.5	697.5	883.9	1468.1	\$W wl Rm918	
91802 24 rpp	211	216	733.5	749	883.9	1468.1	\$W wl Rm918	
91803 24 rpp	211	216	785	871.5	883.9	1468.1	\$W wl Rm917	
91804 24 rpp	211	216	907.5	993	883.9	1468.1	\$W wl Rm905	
91805 24 rpp	151	168.5	911	916	883.9	1468.1	\$NW hallway wl	
91806 24 rpp	204.5	211	911	916	883.9	1468.1	\$NW hallway wl	
91807 24 rpp	500	505	613.5	698	883.9	1468.1	\$E wl Rm919	
91808 24 rpp	500	505	734	749	883.9	1468.1	\$E wl Rm 919	
91809 24 rpp	500	505	785	874	883.9	1468.1	\$E wl Rm 921	
91810 24 rpp	500	505	910	993	883.9	1468.1	\$E wl Rm 923	
91811 24 rpp	216	500	739	744	883.9	1468.1	\$N wl Rm919	
91812 24 rpp	216	500	864	869	883.9	1468.1	\$N wl Rm921	
91813 24 rpp	216	500	988	993	883.9	1468.1	\$N wl Rm923	
91814 24 rpp	355.5	360.5	618.5	739	883.9	1468.1	\$E wl Rm918	
91815 24 rpp	355.5	360.5	744	864	883.9	1468.1	\$E wl Rm917	
91816 24 rpp	355.5	360.5	869	988	883.9	1468.1	\$E wl Rm905	
91817 24 rpp	381	395	817.75	827.25	883.9	1468.1	\$Block Rm921	
91818 24 rpp	216	500	613.5	618.5	883.9	1468.1	\$S wl Rm918	
91819 24 rpp	-7.25	552	1079.75	1082.75	883.9	1468.1	\$N wl mech rm	
91820 24 rpp	549	552	1072.75	1079.75	883.9	1468.1	\$N wl mech rm	
91821 24 rpp	216	355.5	618.5	739	883.9	1468.1	\$Roomspace	918
91822 24 rpp	216	355.5	744	864	883.9	1468.1	\$Roomspace	917
91823 24 rpp	216	355.5	869	988	883.9	1468.1	\$Roomspace	905
91824 24 rpp	360.5	500	618.5	739	883.9	1468.1	\$Roomspace	919
91825 24 rpp	360.5	500	744	864	883.9	1468.1	\$Roomspace	921
91826 24 rpp	360.5	500	869	988	883.9	1468.1	\$Roomspace	923

c

c

c Floor2 Room 927(Conference Room)/933/935/926/937/925/939 section contains some hallway remnants

92701 24 rpp	469	474	-10.5	248.5	883.9	1468.1	\$W wl Rm927	
92702 24 rpp	474	481	243.5	248.5	883.9	1468.1	\$NW wl stub Rm927	
92703 24 rpp	474	808	-10.5	-5.5	883.9	1468.1	\$S wl Rm927	
92704 24 rpp	666	671	-5.5	534.5	883.9	1468.1	\$E wl Rm927	
92705 24 rpp	517	666	243.5	248.5	883.9	1468.1	\$NE wl Rm927	
92706 24 rpp	796.75	808	-5.5	7	883.9	1468.1	\$SE block Rm933	
92707 24 rpp	808	813	-85.5	82.5	883.9	1468.1	\$SE wl Rm933	
92708 24 rpp	808	813	118.5	134.5	883.9	1468.1	\$NE wl Rm933	
92709 24 rpp	671	808	124	129	883.9	1468.1	\$N wl Rm933	
92710 24 rpp	808	813	170.5	346.5	883.9	1468.1	\$E wl Rm935	
92711 24 rpp	795	808	235.25	256	883.9	1468.1	\$NE block Rm935	
92712 24 rpp	671	808	256	261	883.9	1468.1	\$N wl Rm935	
92713 24 rpp	808	813	382.5	479.5	883.9	1468.1	\$NE wl Rm937	
92714 24 rpp	671	808	388	393	883.9	1468.1	\$N wl Rm937	
92715 24 rpp	524	529	381	492	883.9	1468.1	\$W wl Rm926	
92716 24 rpp	529	666	389	394	883.9	1468.1	\$N wl Rm926	
92717 24 rpp	524	529	528	539.5	883.9	1468.1	\$W wl Rm925	
92718 24 rpp	529	718	534.5	539.5	883.9	1468.1	\$N wl Rm925	
92719 24 rpp	704.5	709.5	520.5	534.5	883.9	1468.1	\$NE wl jog Rm939	
92720 24 rpp	709.5	813	520.5	525.5	883.9	1468.1	\$NE wl jog Rm939	
92721 24 rpp	808	813	515.5	520.5	883.9	1468.1	\$NE wl jog Rm939	
92722 24 rpp	794.5	813	525.5	539.5	883.9	1468.1	\$NE wl jog Rm939	

92723	24	ropp	792.5	794.5	534.5	539.5	883.9	1468.1	\$NE wl jog Rm939
92724	24	ropp	405	410	202.5	243.5	883.9	1468.1	\$Hallway wl W of Rm927
92725	24	ropp	410	428	202.5	207.5	883.9	1468.1	\$Hallway wl W of Rm927
92726	24	ropp	464	469	202.5	207.5	883.9	1468.1	\$Hallway wl W of Rm927
92727	24	ropp	381	395	248.5	251.5	883.9	1468.1	\$Hallway wl W of Rm927
92728	24	ropp	474	666	-5.5	243.5	883.9	1468.1	\$Roomspace 927
92729	24	ropp	529	666	248.5	389	883.9	1468.1	\$Roomspace 926
92730	24	ropp	529	666	394	534.5	883.9	1468.1	\$Roomspace 925
92731	24	ropp	671	808	-5.5	124	883.9	1468.1	\$Roomspace 933 Room Partial Fill
92732	24	ropp	671	808	129	256	883.9	1468.1	\$Roomspace 935 Room Partial Fill
92733	24	ropp	671	808	261	388	883.9	1468.1	\$Roomspace 937
92734	24	ropp	671	808	393	520.5	883.9	1468.1	\$Roomspace 939 Room Partial Fill

c

c

c Floor2 Room 920/927/924/968/965/967/964

92001	24	ropp	552.5	557.5	613.5	698	883.9	1468.1	\$W wl Rm920
92002	24	ropp	552.5	557.5	734	749	883.9	1468.1	\$W wl Rm920
92003	24	ropp	552.5	557.5	785	874	883.9	1468.1	\$W wl Rm927
92004	24	ropp	552.5	557.5	910	988	883.9	1468.1	\$W wl Rm924
92005	24	ropp	557.5	706	613.5	618.5	883.9	1468.1	\$S wl Rm920
92006	24	ropp	695.5	700.5	618.5	863	883.9	1468.1	\$E wl Rm920
92007	24	ropp	557.5	695.5	739	744	883.9	1468.1	\$N wl Rm920
92008	24	ropp	557.5	706	863	868	883.9	1468.1	\$N wl Rm927
92009	24	ropp	650	655	868	1079.75	883.9	1468.1	\$E wl Rm924
92010	24	ropp	546.75	650	988	993	883.9	1468.1	\$N wl Rm924
92011	24	ropp	742	912	613.5	618.5	883.9	1468.1	\$S wl Rm965
92012	24	ropp	907	912	618.5	697	883.9	1468.1	\$E wl Rm965
92013	24	ropp	813	907	738.5	743.5	883.9	1468.1	\$N wl Rm965
92014	24	ropp	907	912	733	749	883.9	1468.1	\$NE wl Rm965
92015	24	ropp	907	912	785	865	883.9	1468.1	\$E wl Rm967
92016	24	ropp	813	914	865	870	883.9	1468.1	\$N wl Rm967
92017	24	ropp	700.5	808	791	796	883.9	1468.1	\$N wl Rm968
92018	24	ropp	748	753	796	863	883.9	1468.1	\$Rm N of Rm968
92019	24	ropp	742	765	863	868	883.9	1468.1	\$S wl Rm964
92020	24	ropp	760	765	868	907	883.9	1468.1	\$S wl Rm964
92021	24	ropp	765	808	902	907	883.9	1468.1	\$S wl Rm964
92022	24	ropp	655	954.5	1050	1055	883.9	1468.1	\$N wl Rm964
92023	24	ropp	646	1676	1079.75	1082.75	883.9	1468.1	\$N o wl Rm964-Edge of section
92024	24	ropp	954.5	959.5	870	1079.75	883.9	1468.1	\$E wl Rm964
92025	24	ropp	646	649	1072.75	1079.75	883.9	1468.1	\$NE o wl fragment Rm964
92026	24	ropp	808	813	618.5	907	883.9	1468.1	\$E wl Rm968
92027	24	ropp	557.5	695.5	618.5	739	883.9	1468.1	\$Roomspace 920
92028	24	ropp	557.5	695.5	744	863	883.9	1468.1	\$Roomspace 927
92029	24	ropp	557.5	650	868	988	883.9	1468.1	\$Roomspace 924
92030	24	ropp	700.5	808	618.5	791	883.9	1468.1	\$Roomspace 968
92031	24	ropp	813	907	618.5	738.5	883.9	1468.1	\$Roomspace 965
92032	24	ropp	813	907	743.5	865	883.9	1468.1	\$Roomspace 967
92033	24	ropp	655	954.5	907	1050	883.9	1468.1	\$Roomspace 964-Conf. Room Partial Fill

c

c

c Floor2 Room 930/932/934/936/938/941/943/945/947/949

93001	24	ropp	813	819	-85.5	-80.5	883.9	1468.1	\$SW hallway wl stub W of Rm930
93002	24	ropp	854.5	1145.5	-85.5	-80.5	883.9	1468.1	\$S wl Rm930
93003	24	ropp	861	866	-80.5	-5.5	883.9	1468.1	\$W wl Rm930
93004	24	ropp	861	866	30.5	119.5	883.9	1468.1	\$W wl Rm930
93005	24	ropp	861	866	155.5	171.5	883.9	1468.1	\$W wl Rm932
93006	24	ropp	861	866	207.5	368.5	883.9	1468.1	\$W wl Rm934
93007	24	ropp	861	866	404.5	420.5	883.9	1468.1	\$W wl Rm936
93008	24	ropp	861	866	456.5	539.5	883.9	1468.1	\$W wl Rm938
93009	24	ropp	866	1116.5	37.75	42.75	883.9	1468.1	\$N wl Rm930-941
93010	24	ropp	866	1116.5	161	166	883.9	1468.1	\$N wl Rm932-943
93011	24	ropp	866	1116.5	285.5	290.5	883.9	1468.1	\$N wl Rm934-945
93012	24	ropp	866	1116.5	410	415	883.9	1468.1	\$N wl Rm936-947
93013	24	ropp	866	1116.5	534.5	539.5	883.9	1468.1	\$N wl Rm938-949
93014	24	ropp	988.75	993.75	-80.5	37.75	883.9	1468.1	\$E wl Rm930
93015	24	ropp	988.75	993.75	42.75	161	883.9	1468.1	\$E wl Rm932
93016	24	ropp	988.75	993.75	166	285.5	883.9	1468.1	\$E wl Rm934
93017	24	ropp	988.75	993.75	290.5	410	883.9	1468.1	\$E wl Rm936
93018	24	ropp	988.75	993.75	415	534.5	883.9	1468.1	\$E wl Rm938
93019	24	ropp	1116.5	1121.5	-80.5	-49.5	883.9	1468.1	\$E wl Rm941

93020 24 rpp 1116.5 1121.5 -13.5 119.5 883.9 1468.1 \$E wl Rm941-943  
 93021 24 rpp 1116.5 1121.5 155.5 171.5 883.9 1468.1 \$E wl Rm943  
 93022 24 rpp 1116.5 1121.5 207.5 368.5 883.9 1468.1 \$E wl Rm945  
 93023 24 rpp 1116.5 1121.5 404.5 420.5 883.9 1468.1 \$E wl Rm947  
 93024 24 rpp 1116.5 1121.5 456.5 539.5 883.9 1468.1 \$E wl Rm949  
 93025 24 rpp 1099.5 1116.5 -9.25 37.75 883.9 1468.1 \$NE block Rm949  
 93026 24 rpp 1099.5 1116.5 239.5 285.5 883.9 1468.1 \$NE block Rm945  
 93027 24 rpp 1097.5 1116.5 521.5 534.5 883.9 1468.1 \$NE block Rm941  
 93028 24 rpp 866 988.75 -80.5 37.75 883.9 1468.1 \$Roomspace 930  
 93029 24 rpp 866 988.75 42.75 161 883.9 1468.1 \$Roomspace 932  
 93030 24 rpp 866 988.75 166 285.5 883.9 1468.1 \$Roomspace 934  
 93031 24 rpp 866 988.75 290.5 410 883.9 1468.1 \$Roomspace 936  
 93032 24 rpp 866 988.75 415 534.5 883.9 1468.1 \$Roomspace 938  
 93033 24 rpp 993.75 1116.5 -80.5 37.75 883.9 1468.1 \$Roomspace 941  
 93034 24 rpp 993.75 1116.5 42.75 161 883.9 1468.1 \$Roomspace 943  
 93035 24 rpp 993.75 1116.5 166 285.5 883.9 1468.1 \$Roomspace 945  
 93036 24 rpp 993.75 1116.5 290.5 410 883.9 1468.1 \$Roomspace 947  
 93037 24 rpp 993.75 1116.5 415 534.5 883.9 1468.1 \$Roomspace 949

c

c

c Floor2 Room 940/942/944/946/948/954/955/956/957/958

94001 24 rpp 1181.5 1341.5 -85.5 -80.5 883.9 1468.1 \$S wl Rm940  
 94002 24 rpp 1377.5 1510 -85.5 -80.5 883.9 1468.1 \$S wl Rm954  
 94003 24 rpp 1205.5 1210.5 -80.5 -49.5 883.9 1468.1 \$W wl Rm940  
 94004 24 rpp 1205.5 1210.5 -13.5 119.5 883.9 1468.1 \$W wl Rm942  
 94005 24 rpp 1205.5 1210.5 155.5 171.5 883.9 1468.1 \$W wl Rm942  
 94006 24 rpp 1205.5 1210.5 207.5 368.5 883.9 1468.1 \$W wl Rm944  
 94007 24 rpp 1205.5 1210.5 404.5 420.5 883.9 1468.1 \$W wl Rm946  
 94008 24 rpp 1205.5 1210.5 456.5 539.5 883.9 1468.1 \$W wl Rm948  
 94009 24 rpp 1331.5 1336.5 -80.5 539.5 883.9 1468.1 \$E wl Rm954-958  
 94010 24 rpp 1210.5 1331.5 37.75 42.75 883.9 1468.1 \$N wl Rm940  
 94011 24 rpp 1210.5 1331.5 161 166 883.9 1468.1 \$N wl Rm942  
 94012 24 rpp 1210.5 1331.5 285.5 290.5 883.9 1468.1 \$N wl Rm944  
 94013 24 rpp 1210.5 1331.5 410 415 883.9 1468.1 \$N wl Rm946  
 94014 24 rpp 1210.5 1331.5 534.5 539.5 883.9 1468.1 \$N wl Rm948  
 94015 24 rpp 1210.5 1229 -9.25 37.75 883.9 1468.1 \$NW block Rm940  
 94016 24 rpp 1210.5 1229 239.5 285.5 883.9 1468.1 \$NW block Rm944  
 94017 24 rpp 1210.5 1229.5 521.5 534.5 883.9 1468.1 \$NW block Rm948  
 94018 24 rpp 1384.5 1389.5 -80.5 -5 883.9 1468.1 \$W wl Rm954  
 94019 24 rpp 1384.5 1389.5 31 119.5 883.9 1468.1 \$W wl Rm955  
 94020 24 rpp 1384.5 1389.5 155.5 171.5 883.9 1468.1 \$W wl Rm956  
 94021 24 rpp 1384.5 1389.5 207.5 368.5 883.9 1468.1 \$W wl Rm957  
 94022 24 rpp 1384.5 1389.5 404.5 420.5 883.9 1468.1 \$W wl Rm957  
 94023 24 rpp 1384.5 1389.5 456.5 539.5 883.9 1468.1 \$W wl Rm958  
 94024 24 rpp 1389.5 1510 37.75 42.75 883.9 1468.1 \$N wl Rm954  
 94025 24 rpp 1389.5 1510 161 166 883.9 1468.1 \$N wl Rm955  
 94026 24 rpp 1389.5 1510 285.5 290.5 883.9 1468.1 \$N wl Rm956  
 94027 24 rpp 1389.5 1510 410 415 883.9 1468.1 \$N wl Rm957  
 94028 24 rpp 1389.5 1510 534.5 539.5 883.9 1468.1 \$N wl Rm958  
 94029 24 rpp 1510 1515 -85.5 539.5 883.9 1468.1 \$E wl Rm954-958  
 94030 24 rpp 1210.5 1331.5 -80.5 37.75 883.9 1468.1 \$Roomspace 940  
 94031 24 rpp 1210.5 1331.5 42.75 161 883.9 1468.1 \$Roomspace 942  
 94032 24 rpp 1210.5 1331.5 166 285.5 883.9 1468.1 \$Roomspace 944  
 94033 24 rpp 1210.5 1331.5 290.5 410 883.9 1468.1 \$Roomspace 946  
 94034 24 rpp 1210.5 1331.5 415 534.5 883.9 1468.1 \$Roomspace 948  
 94035 24 rpp 1389.5 1510 -80.5 37.75 883.9 1468.1 \$Roomspace 954  
 94036 24 rpp 1389.5 1510 42.75 161 883.9 1468.1 \$Roomspace 955  
 94037 24 rpp 1389.5 1510 166 285.5 883.9 1468.1 \$Roomspace 956  
 94038 24 rpp 1389.5 1510 290.5 410 883.9 1468.1 \$Roomspace 957  
 94039 24 rpp 1389.5 1510 415 534.5 883.9 1468.1 \$Roomspace 958

c

c

c Floor2 Room 961/960/951/952/950 with the Elevator

c In the NW section where the lunchroom meets the bathrooms some walls were omitted  
 c for the sake of saving time. Removing these few walls decreases reflection and is  
 c therefore conservative.

96101 24 rpp 964 969 613.5 697 883.9 1468.1 \$W wl Rm961  
 96102 24 rpp 964 969 733 749 883.9 1468.1 \$W wl Rm961  
 96103 24 rpp 964 969 785 865 883.9 1468.1 \$W wl Rm960  
 96104 24 rpp 950 1121.5 865 870 883.9 1468.1 \$N wl Rm960

96105 24 rpp 969 1116.5 738.5 743.5 883.9 1468.1 \$N wl Rm961  
 96106 24 rpp 969 1116.5 613.5 618.5 883.9 1468.1 \$S wl Rm961  
 96107 24 rpp 1116.5 1121.5 613.5 823 883.9 1468.1 \$E wl Rm960-961  
 96108 24 rpp 1102.5 1116.5 810 815 883.9 1468.1 \$NE wl Rm960  
 96109 24 rpp 1097.5 1102.5 810 865 883.9 1468.1 \$NE wl Rm960  
 96110 24 rpp 1097 1102 870 872.5 883.9 1468.1 \$NE wl Rm960  
 96111 24 rpp 1116.5 1120.5 859 865 883.9 1468.1 \$NE wl Rm960  
 96112 24 rpp 1205.5 1308 613.5 618.5 883.9 1468.1 \$S wl Rm951  
 96113 24 rpp 1344 1354.5 613.5 618.5 883.9 1468.1 \$S stub wl Rm951  
 96114 24 rpp 1385 1469 613.5 618.5 883.9 1468.1 \$S wl Rm952  
 96115 24 rpp 1505 1510 613.5 618.5 883.9 1468.1 \$SE wl Rm952  
 96116 24 rpp 1510 1514 612.5 1079.75 883.9 1468.1 \$E wl Rm952-LR  
 96117 24 rpp 1514 1519 612.5 1079.5 883.9 1468.1 \$E o wl Rm952-LR  
 96118 24 rpp 1437.5 1510 665.5 670.5 883.9 1468.1 \$SE wl Rm952  
 96119 24 rpp 1437.5 1442.5 660 665.5 883.9 1468.1 \$SE wl Rm952  
 96120 24 rpp 1437.5 1442.5 618.5 624 883.9 1468.1 \$SE wl Rm952  
 96121 24 rpp 1474 1510 776.5 781.5 883.9 1468.1 \$E partitioning wall wl Rm952  
 96122 24 rpp 1474 1510 843 848 883.9 1468.1 \$E partitioning wall wl Rm952  
 96123 24 rpp 1474 1510 891.5 896.5 883.9 1468.1 \$E partitioning wall wl Rm952  
 96124 24 rpp 1275 1510 896.5 901.5 883.9 1468.1 \$N wl Rm952-950  
 96125 24 rpp 1365.5 1370.5 630 896.5 883.9 1468.1 \$Central wl Rm952/951  
 96126 24 rpp 1329.5 1365.5 890 896.5 883.9 1468.1 \$Central wl Rm952/951  
 96127 24 rpp 1349.5 1365.5 630 846.5 883.9 1468.1 \$Central wl Rm952/952  
 96128 24 rpp 1279.5 1349.5 814 819 883.9 1468.1 \$Dividing wl Rm951  
 96129 24 rpp 1329.5 1349.5 819 846.5 883.9 1468.1 \$Dividing wl Rm951 <-----Omitted Block in NE Corner-----  
 ---Find it and put it in  
 96130 24 rpp 1275 1349.5 674 679 883.9 1468.1 \$Dividing wl Rm951  
 96131 24 rpp 1275 1280 660 674 883.9 1468.1 \$Dividing wl Rm951  
 96132 24 rpp 1275 1280 618.5 623 883.9 1468.1 \$Dividing wl Rm951  
 96133 24 rpp 1349.5 1390 625 630 883.9 1468.1 \$Central wl Rm952/951  
 96134 24 rpp 1349.5 1354.5 618.5 625 883.9 1468.1 \$Central wl Rm952/951  
 96135 24 rpp 1385 1390 618.5 625 883.9 1468.1 \$Central wl Rm952/951  
 96136 24 rpp 1205.5 1210.5 922 1064 883.9 1468.1 \$W wl LR  
 96137 24 rpp 1102 1510 1064 1069.5 883.9 1468.1 \$N wl LR  
 96138 24 rpp 1097.5 1102 1060.5 1079.75 883.9 1468.1 \$NW wl LR  
 96139 24 rpp 1001.5 1009.5 911 1027.2 883.9 1468.1 \$W wl Elev  
 96140 24 rpp 1009.5 1097.5 1019.25 1027.25 883.9 1468.1 \$N wl Elev  
 96141 24 rpp 1089.5 1097.5 1006 1019.25 883.9 1468.1 \$NE wl Elev  
 96142 24 rpp 1089.5 1097.5 911 938.5 883.9 1468.1 \$SE wl Elev  
 96143 24 rpp 1009.5 1089.5 911 919 883.9 1468.1 \$S wl Elev  
 96144 24 rpp 1205.5 1210.5 618.5 834 883.9 1468.1 \$W wl Rm951  
 96145 24 rpp 969 1116.5 618.5 738.5 883.9 1468.1 \$Roomspace 961  
 96146 24 rpp 969 1097.5 743.5 865 883.9 1468.1 \$Roomspace 960 Room Partial Fill  
 96147 24 rpp 1210.5 1510 922 1064 883.9 1468.1 \$Roomspace LR<-----Did not fill all rooms here-----

-

c

c

c

C

C

8

C /// Begin Northeast Section of FloorZ  
C \*\*\*\*\*Notes for this section of Surfaces\*\*\*\*\*

c. The origin was placed on the west boundary wall. The origin was placed on the south east corner of the house.

c The origin was place on the west boundary wall. The origin was placed on the south east corner of the boundary wall.

c The origin was only moved in the x direction not the y. To accurately relocate the origin I had to delete the overlying yellow line. Small well stubs were ignored on the exterior walls.

c overlying yellow line. Small wall stubs were ignored on the exterior walls.

3

3

6

c This room contains all of the surfaces fo

90001 21 rpp 0 148 906.25 911.25 883.9 14

90001 21 rpp 3 148 906.25 911.25 883.9 1468.1 \$S w1 Rm90  
90002 21 rpp 143 148 911.25 958.25 883.9 1468.1 \$E w1 Rm90

90002 21 rpp 143 148 911.25 938.25 883.9 1468.1 \$E w/ Rm900  
90003 21 rpp 143 148 994.25 1039.25 883.9 1468.1 \$E w/ Rm900

90003 21 rpp 145 148 794.25 1039.25 883.9 1468.1 \$E w/ Rm 900

90005 21 spp 474.25 479.25 844.75 974.75 883.9 1468.1 \$W w/CE

90005 21 spp 474.25 479.25 844.75 974.75 883.9 1468.1 \$W w/CR  
90006 21 spp 479.25 659.75 969.75 974.75 883.9 1468.1 \$N w/CR

90006 21 1pp 479.25 659.75 969.75 974.75 883.9 1468.1 \$N w/CR  
90007 21 rpp 654.75 659.75 841.75 969.75 883.9 1468.1 \$E w/CR

90007 21 rpp 654.75 659.75 841.75 909.75 883.9 1468.1 \$E w/CR  
90008 21 rpp 654.75 659.75 795.75 805.75 883.9 1468.1 \$SE w/CR

90008 21 Ipp 654.75 659.75 795.75 805.75 885.9 1468.1 \$SE w/ CR  
90009 21 rpp 253 820.25 1165.25 1168.25 883.9 1468.1 \$N exterior w/ Rm900



c \*\*\*\*\*Notes for this section of Surfaces\*\*\*\*\*

c The origin was place on the Southwest corner of Room 609 on the inside corner of the wall

c

c The intersection of the wall 60941 with the wall 60936 differs slightly from reality in that there is  
c small sections of the wall omitted at the junction. This omission decreases reflectivity and is therefore  
c conservative.

c

c

c Floor2 Room 609/608/607/Topp of hot cells

c Room 609 is used as the designation of both the small room 609 and as the  
c rest of the walls for the area

60901	23	ropp	-7	-3	-4	981.25	883.9	1071.9	\$W o wl Rm609
60902	23	ropp	-3	0	0	153	883.9	1071.9	\$W i wl
60903	23	ropp	0	243	150	153	883.9	1071.9	\$N wl Rm
60905	23	ropp	199	241	48.5	53.5	883.9	1071.9	\$SE wl Rm609
60906	23	ropp	199	202	46.25	48.25	883.9	1071.9	\$SE wl Rm609
60907	23	ropp	199	202	0	13.25	883.9	1071.9	\$SE wl Rm609
60908	23	ropp	-3	574	-4	0	883.9	1071.9	\$S wl Rm609-607
60909	23	ropp	279.75	537.25	199	202	883.9	1071.9	\$N wl Rm608
60910	23	ropp	534.25	537.25	0	199	883.9	1071.9	\$E wl Rm607
60911	23	ropp	481.25	534.25	70	73.25	883.9	1071.9	\$N wl Rm607
60912	23	ropp	434.75	437.75	0	15.25	883.9	1071.9	\$SW wl Rm607
60913	23	ropp	434.75	437.75	45.25	53	883.9	1071.9	\$W wl Rm607
60914	23	ropp	432.5	434.75	48.5	199	883.9	1071.9	\$W wl Rm607
60915	23	ropp	332.5	402.5	48.5	53	883.9	1071.9	\$S wl Rm608
60916	23	ropp	332.5	335.5	53	199	883.9	1071.9	\$W wl Rm608
60917	23	ropp	279.75	282	53	199	883.9	1071.9	\$Staircase wall <-----Check vs reality -----Started here after being sick-----
60918	23	ropp	356	364	2	12	883.9	1071.9	\$Block S of Rm608<-----Check vs reality
60919	23	ropp	241	243	48.5	150	883.9	1071.9	\$E wl Rm609
60920	23	ropp	570	574	0	288	883.9	1071.9	\$E wl Rm609< Strange block here-----
60921	23	ropp	555.5	570	266.5	273.5	883.9	1071.9	\$Block in E wl in SE Rm609
60922	23	ropp	574	1073	259.5	264.5	883.9	1071.9	\$S wl in SE Rm609
60923	23	ropp	1068	1073	264.5	288	883.9	1071.9	\$SE wl in SE Rm609
60924	23	ropp	1068	1073	324	342	883.9	1071.9	\$E wl in SE Rm609
60925	23	ropp	1068	1073	486	527	883.9	1071.9	\$NE wl in SE Rm609
60926	23	ropp	1057.5	1067.5	506	514	883.9	1071.9	\$NE block in N wl in SE Rm609, ignored very small wall here
60927	23	ropp	574	1057.5	509	511	883.9	1071.9	\$N wl in SE Rm609
60928	23	ropp	816.5	828.5	511	515	883.9	1071.9	\$Block on N wl in SE Rm609
60929	23	ropp	816.5	828.5	505	509	883.9	1071.9	\$Block on N wl in SE Rm609
60930	23	ropp	555.25	573.5	506.5	513.5	883.9	1071.9	\$NW Block in N wl in SE Rm609
60931	23	ropp	570	574	462	506.5	883.9	1071.9	\$NW wl in SE Rm609
60932	23	ropp	578.5	586.5	266	274	883.9	1071.9	\$SW Column in SE Rm609
60933	23	ropp	818.5	826.5	266	274	883.9	1071.9	\$S Column in SE Rm609
60934	23	ropp	1058.5	1066.5	266	274	883.9	1071.9	\$SE Column in SE Rm609
60935	23	ropp	196.5	364.5	324	822	883.9	1071.9	\$Top of hot cells <-----No details put in, fix this later-----
60936	23	ropp	574	1073	742.5	747.5	883.9	1071.9	\$N wl in E Rm609
60937	23	ropp	1068	1073	562	742.5	883.9	1071.9	\$E wl in E Rm609
60938	23	ropp	578.5	586.5	733	741	883.9	1071.9	\$NW column in E Rm609
60939	23	ropp	818.5	826.5	733	741	883.9	1071.9	\$N column in E Rm609<-----Ignored mezzanine and columns within it-----
60940	23	ropp	555.5	573.5	746.5	753.5	883.9	1071.9	\$NW Block in E Rm609
60941	23	ropp	570	574	753.5	1548.5	883.9	1071.9	\$E wl Rm609
60942	23	ropp	187.25	570	1544.5	1548.5	883.9	1071.9	\$N wl Rm609
60943	23	ropp	187.25	191.25	994.5	1544.5	883.9	1071.9	\$W wl of Mezzanine Rm609
60944	23	ropp	348.25	352.25	994.5	1544.5	883.9	1071.9	\$E wl of Mezzanine Rm609
60945	23	ropp	-4	353.75	990.5	994.5	883.9	1071.9	\$S wl of Mezzanine Rm609
60946	23	ropp	332	335	288	324	883.9	1071.9	\$Dividing wl S of Hot cell Rm609
60947	23	ropp	25.5	35.5	266	274	883.9	1071.9	\$SW Column Rm609
60948	23	ropp	25.5	35.5	506	514	883.9	1071.9	\$W Column Rm609
60949	23	ropp	25.5	35.5	746	754	883.9	1071.9	\$NW Column Rm609
60950	23	ropp	551	569	986	994	883.9	1071.9	\$E Column Rm609
60951	23	ropp	548	569	1048.5	1057.5	883.9	1071.9	\$E Column next column N of (60950)Rm609
60952	23	ropp	548	569	1285.5	1294.5	883.9	1071.9	\$E Column next column N of (60951)Rm609
60953	23	ropp	548	569	1534.5	1543.5	883.9	1071.9	\$E Column next column N of (60952) Rm609
60954	23	ropp	354.5	362.5	985	995	883.9	1071.9	\$Column at SE Corner of Mezzanine Rm609
c 60955	23	ropp	-4	187.25	994.5	1548.5	800.1	830.6	\$Roof Next to Mezzanine Rm609 Assumed 50 cm thick
60956	23	ropp	-7	-4	981.25	1548.5	883.9	1071.9	\$W wl Roof Rm609
60957	23	ropp	0	199	0	150	883.9	1071.9	\$Roomspace 609 Room Partial Fill
60958	23	ropp	335.5	432.5	53	199	883.9	1071.9	\$Roomspace 608



```

c
c
c
c
c
c -----BLANK LINE FOLLOWS THIS LINE-----
c =====
c #####
c # Data definition cards #
c #####
c
c Start of Data Card =====
c =====
c #####
c # Material definition cards#
c #####
c
c
c TAG=TAGmaterials
c Start of Materials =====
c
c Wherever possible natural isotopic distribution were used. .66c was used preferentially
c but if that library was not available then .60c, .55c, .50c was the hierarchy. These libraries
c were all evaluated at or near room temperature. Except for Argon the current library is .59c.
c same evaluation temp as the others.
c
c Standard material definitions were taken from PNNL - 15870 Materials List
c
c Calculated Density -0.001205
m1 6000.66c      0.000151  $ C Air
    7014.66c      0.784437  $ N
    8016.66c      0.210750  $ O
    18000.59c     0.004671  $ Ar
c
c Calculated Density -1.53 g/cc
m2 14000.60c      1      $ Si Dirt (Sand)
    8016.66c      2      $ O
c
c Calculated Density -2.3
m3 1001.66c      -0.022100  $ H Concrete (Ordinary)
    6000.66c      -0.002484  $ C
    8016.66c      -0.574930  $ O
    11023.66c     -0.015208  $ Na
    12000.66c     -0.001266  $ Mg
    13027.66c     -0.019953  $ Al
    14000.60c     -0.304627  $ Si
    19000.66c     -0.010045  $ K
    20000.66c     -0.042951  $ Ca
    26000.55c     -0.006435  $ Fe
c
c Calculated Density -0.29 g/cc
m4 20000.66c      1      $ Ca Drywall (Sheet Rock Brand)
    16000.66c     1      $ S
    8016.66c      6      $ O
    1001.66c      4      $ H
c
c Calculated Density 0.00359833
m5 26000.55c     0.00263792  $ Fe Metal walls
    24000.50c     0.000689167 $ Cr
    28000.50c     0.00027125  $ Ni
c

```

c Calculated Density

c A full office has the density of -0.04855

c A half full office has the density of -0.02427

m6 6000.66c -0.0215754 \$ C Office filler  
   1001.66c -0.00301979 \$ H  
   8016.66c -0.0239544 \$ O

c

c

c Calculated Density -0.05514 .020240g/cc

m7 13027.66c -0.0009904701 \$ Al Lab room sparsley filled  
   5010.66c -0.0036647 \$ B  
   11023.66c -0.0040609 \$ Na  
   8016.66c -0.31452 \$ O  
   14000.60c -0.037341 \$ Si  
   26000.55c -0.26313 \$ Fe  
   24000.50c -0.064005 \$ Cr  
   28000.50c -0.028447 \$ Ni  
   82000.50c -0.0032121 \$ Pb  
   6000.66c -0.23157 \$ C  
   1001.66c -0.032412 \$ H  
   7014.66c -0.016642 \$ N

c

c

c The density for a full lab is -0.10907 .03928g/cc

m8 13027.66c -0.0010014 \$ Al Lab room fully filled  
   5010.66c -0.0037051 \$ B  
   11023.66c -0.0041057 \$ Na  
   8016.66c -0.31567 \$ O  
   14000.60c -0.037752 \$ Si  
   26000.55c -0.26603 \$ Fe  
   24000.50c -0.06471 \$ Cr  
   28000.50c -0.02876 \$ Ni  
   82000.50c -0.0032475 \$ Pb  
   6000.66c -0.23413 \$ C  
   1001.66c -0.032769 \$ H  
   7014.66c -0.0081198 \$ N

c

c

c Calculated Density -0.06

m9 6000.66c -0.026664 \$ C 8" inch wood walls  
   1001.66c -0.003732 \$ H  
   8016.66c -0.029604 \$ O

c

c

c Calculated Density -0.12

m10 6000.66c -0.053328 \$ C 4" inch wood walls  
   1001.66c -0.007464 \$ H  
   8016.66c -0.059208 \$ O

c

c

c Calculated Density -2.6467 g/cc

m12 13027.66c -0.03177 \$ Al 1st Floor Deck/Basement1 Ceiling  
   20000.66c -0.04112 \$ Ca  
   26000.55c -0.0616 \$ Fe  
   1001.66c -0.00934 \$ H  
   8016.66c -0.49712 \$ O  
   14000.60c -0.31491 \$ Si  
   11023.66c -0.0271 \$ Na  
   24000.50c -0.0118 \$ Cr  
   28000.50c -0.00524 \$ Ni

c

c

c Calculated Density -7.92 g/cc

m13 24000.50c 0.202087 \$ Cr SS-304  
   25055.66c 0.020133 \$ Mn  
   26000.55c 0.688268 \$ Fe  
   28000.50c 0.089514 \$ Ni

c

c

c Calculated Density -0.539

m14 13027.66c -0.034 \$ Al Cinder Block  
 20000.66c -0.044 \$ Ca  
 26000.55c -0.014 \$ Fe  
 1001.66c -0.01 \$ H  
 8016.66c -0.532 \$ O  
 14000.60c -0.337 \$ Si  
 11023.66c -0.029 \$ Na  
 c  
 c  
 c Calculated Density -0.4751  
 m15 13027.66c -0.00454 \$ Al Exterior walls  
 5010.66c -0.0168 \$ B  
 8016.66c -0.2429 \$ O  
 14000.60c -0.1712 \$ N  
 11023.66c -0.01861 \$ Na  
 26000.55c -0.404 \$ Fe  
 24000.50c -0.09828 \$ Cr  
 28000.50c -0.04368 \$ Ni  
 c  
 c  
 c Optimally moderated Pu and H2O Solution Ref: NCS99  
 c Calculated Density 32 g/l 239Pu in H2O  
 m16 94239.66c 8.0614E-05 \$ Pu 239  
 8016.66c 3.3374E-02 \$ O  
 1001.66c 6.6748E-02 \$ H  
 c  
 c  
 c Water Calculated Density of 1 g/cc  
 m17 8016.66c 1 \$ O  
 1001.66c 2 \$ H  
 c  
 c  
 c Fe Representing a cask containing a criticality accident  
 c Calculated Density -7.874 g/cc  
 m18 26000.55c 1 \$ Fe  
 c  
 c  
 c Calculated Density .9300 g/cc  
 m19 1001.66c -0.143716 \$ H Polyethylene (Standard)  
 6000.66c -0.856284 \$ C  
 c  
 c  
 c  
 c  
 c  
 c  
 c Translation Cards Begin Below Here  
 c  
 c Sections are grouped by floor and the first numerical digit is the floor number with the exception  
 c of the Basement floor being numbered as 4. For the translations in the y direction I used the elevational  
 c drawing H-4-50013. It is very hard to read precisely. The decision was made to align the first floor inset  
 c of the exterior walls of the first Basement floor. If the afore mentioned drawing is closely examined this  
 c can be verified. Floors 1 and 2 were aligned with their exterior walls flush.  
 c  
 c  
 c  
 BBBB  
 BBBB  
 c  
 BBBB  
 BBBB  
 c  
 BBBB  
 BBBB  
 c  
 BBBB  
 BBBB  
 c  
 BBBB  
 BBBB  
 c  
 BBBB  
 BBBB





```

c
c SE Section
c sdef pos 1753.5 680.5 50 ERG=D1 RAD=D2 WGT=3.94E15 $ Pu Sphere in Rm34 B1
c sdef pos 2882 40 50 ERG=D1 RAD=D2 WGT=3.94E15 $ Rm40c
c
c
c W Section
c sdef pos -202 171 50 ERG=D1 RAD=D2 WGT=3.94E15 $ Pu Sphere in SW corner of Rm23B in cell 425 2321
c
c sdef pos -202 474 50 ERG=D1 RAD=D2 WGT=3.94E15 $ Pu Sphere in W of Rm23 in cell 425 2322
c
c sdef pos -92 921 50 ERG=D1 RAD=D2 WGT=3.94E15 $ Pu Sphere in E of Rm32 (Under SAL) in cell 426
c
c sdef pos -382 1141 50 ERG=D1 RAD=D2 WGT=3.94E15 $ Pu Sphere in NW of Rm32 (Under SAL)
c
c
c NW Section
c sdef pos 44.5 2577 50 ERG=D1 RAD=D2 WGT=3.94E15 $ NW corner of NW section B1 Rm45
c
c sdef pos 1144.5 1028.5 50 ERG=D1 RAD=D2 WGT=3.94E15 $ SE corner of NW section B1 -Center of B1
c
c sdef pos 44.5 2338.5 50 ERG=D1 RAD=D2 WGT=3.94E15 $ NW corner B1
c
c
c N Central Section
c Source in N of B1
c sdef pos 1314.5 2300.5 50 ERG=D1 RAD=D2 WGT=3.94E15 $ N B1 center of Rm90
c
c
c NE Section
c Source in E Central B1 in Rm 48
c sdef pos 2303.5 1228.5 50 ERG=D1 RAD=D2 WGT=3.94E15 $ E Edge central B1 Rm48
c
c Source in NE B1 N of Rm52
c sdef pos 2178.5 2288.5 50 ERG=D1 RAD=D2 WGT=3.94E15 $ NE Corner B1
c
c -----
c
c First Floor Accident Locations Rm203, LR, Rm327A, Rm528, Truck Lock, Rm119, Rm410
c
c sdef pos -634.5 1132.5 492 ERG=D1 RAD=D2 WGT=3.94E15 $ Rm203
c
c
c sdef pos 541.5 -847.5 492 ERG=D1 RAD=D2 WGT=3.94E15 $ LR
c
c
c sdef pos 40 2332.5 492 ERG=D1 RAD=D2 WGT=3.94E15 $ Rm327A
c
c
c sdef pos 2277.5 2340.5 492 ERG=D1 RAD=D2 WGT=3.94E15 $ Rm528
c
c
c sdef pos 3355.5 402 492 ERG=D1 RAD=D2 WGT=3.94E15 $ Truck Lock
c
c
c sdef pos 2261.5 27.5 492 ERG=D1 RAD=D2 WGT=3.94E15 $ Rm119
c
c
c sdef pos 1367.5 960.5 492 ERG=D1 RAD=D2 WGT=3.94E15 $ Rm410
c
c
c Second Floor Accident Locations
c
c sdef pos 2875 1520 1072 ERG=D1 RAD=D2 WGT=3.94E15 $ Above Rm 603
c
c
c sdef pos 44.5 2350 884 ERG=D1 RAD=D2 WGT=3.94E15 $ Above Rm 327 in Rm903 cell202
c
c

```



FC4 461=B1 Rm22, 462=B1 N of Rm34, 463=W of Rm35, 464=F1 W of Rm516,  
 465=F1 N of Rm115, 466=F1 W of Rm316, 467=F1 N of Rm605, 468=F1 E of 604  
 c  
 c  
 c  
 E4 4E-6 20

MCNP Input Modeled by Bryce Greenfield

c Listing for NIST 3" dry sphere; detailed src, sphere & detectors, Table 24  
 c  
 c 34567890123456789112345678921234567893123456789412345678951234567896123456789712345678  
 c  
 c  
 c  
 c Cell Records  
 c Fission Chamber Except Spaces, +Z  
 1 6 -21.45 -1 2 -3 imp:n=1 \$1,Pt  
 2 5 -2.581 1 -4 6 -5 imp:n=1 \$2,Al reduced for smearing  
 3 5 -2.7 7 -1 6 -2 imp:n=1 \$3,Al  
 4 8 -2.2 8 -9 10 -6 imp:n=1 \$4,KEL-F  
 5 5 -2.7 11 -12 13 -10 imp:n=1 \$5,Al  
 6 5 -2.7 14 -15 17 -16 imp:n=1 \$6,Al  
 7 5 -2.7 -18 19 -13 imp:n=1 \$7,Al  
 8 8 -2.2 20 -21 22 -19 imp:n=1 \$8,KEL-F  
 9 8 -2.2 23 -21 19 -24 imp:n=1 \$9,KEL-F  
 10 8 -2.2 25 -4 3 -26 imp:n=1 \$10,KEL-F  
 11 8 -2.2 27 -4 26 -28 imp:n=1 \$11,KEL-F  
 12 5 -2.7 36 -27 26 -29 imp:n=1 \$12,Al  
 13 5 -2.7 30 -36 31 -32 imp:n=1 \$13,Al  
 14 8 -2.2 33 -27 34 -35 imp:n=1 \$14,KEL-F  
 15 8 -2.046 27 -4 37 -35 imp:n=1 \$15,KEL-F reduced for smearing  
 16 5 -2.7 -27 29 -34 imp:n=1 \$16,Al  
 17 5 -2.7 38 -39 40 -41 imp:n=1 \$21,Al  
 18 5 -2.7 -39 42 -43 imp:n=1 \$22,Al  
 19 5 -2.7 4 -38 46 -42 imp:n=1 \$24,Al  
 20 5 -2.7 -4 46 -47 imp:n=1 \$25,Al  
 c Fission Chamber Except Spaces, -Z  
 21 6 -21.45 -51 53 -52 imp:n=1 \$1,Pt  
 22 5 -2.581 51 -54 55 -56 imp:n=1 \$2,Al reduced for smearing  
 23 5 -2.7 57 -51 52 -56 imp:n=1 \$3,Al  
 24 8 -2.2 58 -59 56 -60 imp:n=1 \$4,KEL-F  
 25 5 -2.7 61 -62 60 -63 imp:n=1 \$5,Al  
 26 5 -2.7 64 -65 66 -67 imp:n=1 \$6,Al  
 27 5 -2.7 -68 63 -69 imp:n=1 \$7,Al  
 28 8 -2.2 70 -71 69 -72 imp:n=1 \$8,KEL-F  
 29 8 -2.2 73 -71 74 -69 imp:n=1 \$9,KEL-F  
 30 8 -2.2 75 -54 76 -53 imp:n=1 \$10,KEL-F  
 31 8 -2.2 77 -54 78 -76 imp:n=1 \$11,KEL-F  
 32 5 -2.7 86 -77 79 -76 imp:n=1 \$12,Al  
 33 5 -2.7 80 -86 82 -81 imp:n=1 \$13,Al  
 34 8 -2.2 83 -77 85 -84 imp:n=1 \$14,KEL-F  
 35 8 -2.046 77 -54 85 -87 imp:n=1 \$15,KEL-F reduced for smearing  
 36 5 -2.7 -77 84 -79 imp:n=1 \$16,Al  
 37 5 -2.7 88 -89 91 -90 imp:n=1 \$21,Al  
 38 5 -2.7 -89 93 -92 imp:n=1 \$22,Al  
 39 5 -2.7 54 -88 92 -96 imp:n=1 \$24,Al

40 5 -2.7 -54 97 -96 imp:n=1 \$25,Al  
 c Source, sphere, supports  
 51 7 -1.85 -101 102 -103 imp:n=1 \$Cf  
 52 11 -2.0 -104 103 -105 imp:n=1 \$A  
 53 5 -2.7 104 -106 102 -105 imp:n=1 \$B  
 54 5 -2.7 -106 107 -102 imp:n=1 \$C  
 55 2 -7.92 108 -109 107 -105 imp:n=1 \$D  
 56 2 -7.92 -109 110 -107 imp:n=1 \$E  
 57 2 -7.92 111 -109 105 -112 imp:n=1 \$F  
 58 2 -7.92 -109 112 -113 imp:n=1 \$G  
 59 2 -7.92 -114 113 -115 imp:n=1 \$H  
 60 2 -7.92 116 -109 113 -117 imp:n=1 \$I  
 61 2 -7.92 114 -118 120 -119 imp:n=1 \$J  
 62 2 -7.92 121 -106 119 -122 imp:n=1 \$K  
 63 2 -7.92 123 -106 122 -124 imp:n=1 \$L  
 64 2 -7.92 123 -125 124 -126 imp:n=1 \$M  
 65 2 -7.92 123 -127 126 -128 imp:n=1 \$N  
 66 2 -7.92 -127 128 -129 imp:n=1 \$O  
 67 2 -7.92 -104 129 -130 imp:n=1 \$P  
 68 2 -2.1 -131 -146 130 imp:n=1 \$Q Chain  
 69 1 -0.001185 114 -121 119 -115 imp:n=1 \$R, water or air  
 70 1 -0.001185 -121 115 -122 imp:n=1 \$S, water or air  
 71 1 -0.001185 -123 122 -124 imp:n=1 \$T, water or air  
 72 5 -2.7 141 -142 145 -146 imp:n=1 \$U stem support ring  
 75 5 -2.7 38 -152 154 -146 imp:n=1 \$stem,+Z  
 76 5 -2.7 38 -151 154 -146 imp:n=1 \$stem,-Z  
 79 2 -7.92 158 -159 -124 imp:n=1 \$SS shell  
 c Spaces  
 c air cells above water line  
 105 1 -0.001185 -141 129 -146 (131:-130) 104 151 152 imp:n=1 \$ around src shaft above O  
 106 1 -0.001185 -141 124 -129 (125:126) 127 151 152 imp:n=1 \$ around src shaft below P  
 107 1 -0.001185 -123 124 -128 imp:n=1 \$ just above T in central tube  
 108 1 -0.001185 -149 141 124 -146 (-141:142:-145) imp:n=1 \$ away from src shaft  
 c  
 c air cells below water line  
 109 1 -0.001185 148 -124 96 -46 -149 159  
     imp:n=1 \$ outside SS sphere, inside detector Zs  
 110 1 -0.001185 148 -124 46 -149 (38:43) (-40:39:43)  
     (152:-38:-154) imp:n=1 \$ beyond +Z detector  
 c inner face  
 111 1 -0.001185 148 -124 -149 -96 (38:-93) (90:39:-93)  
     (151:-38:-154) imp:n=1 \$ beyond -Z detector  
 c inner face  
 c water or air cells inside sphere but outside source+holder  
 112 1 -0.001185 -116 114 113 -117 imp:n=1 \$ annular recess at top of src capsule  
 113 1 -0.001185 -158 -120 (109:-110:117) (114:-113) imp:n=1 \$ below src holder  
 114 1 -0.001185 -158 120 -124 (118:119) 106 imp:n=1 \$ at src holder elevations  
 c air in source capsule  
 115 1 -0.001185 -104 101 102 -103 imp:n=1 \$ gap immediately around Cf  
 116 1 -0.001185 -108 106 107 -105 imp:n=1 \$ gap immediately inside src capsule wall D  
 117 1 -0.001185 -111 105 -112 imp:n=1 \$ gap inside of F in source capsule  
 c P-10 gas in +Z detector  
 121 0 -4 47 -19 (-20:-22) imp:n=1 \$ before collector B  
 122 0 -4 12 24 -10 imp:n=1 \$ gap outboard of Item 5  
 123 0 -11 8 13 -10 (-14:-17:16) imp:n=1 \$ around Item 6  
 124 0 -8 13 -2 (-7:-6) imp:n=1 \$ between collector B and Pt plate  
 125 0 -4 27 28 -37 imp:n=1 \$ gap outboard of Item 12  
 126 0 -36 25 26 -29 (-30:-31:32) imp:n=1 \$ around Item 13  
 127 0 -25 3 -29 imp:n=1 \$ before collector B  
 128 0 -4 34 -41 (-33:35) imp:n=1 \$ between collector B and Pt plate  
 c P-10 gas in -Z detector  
 131 0 -4 69 -97 (-20:72) imp:n=1 \$ before collector B  
 132 0 -4 12 60 -74 imp:n=1 \$ gap outboard of Item 5  
 133 0 -11 8 60 -63 (-14:-66:67) imp:n=1 \$ around Item 6  
 134 0 -8 52 -63 (-7:56) imp:n=1 \$ between collector B and Pt plate  
 135 0 -4 27 87 -78 imp:n=1 \$ gap outboard of Item 12  
 136 0 -36 25 79 -76 (-30:-82:81) imp:n=1 \$ around Item 13  
 137 0 -25 79 -53 imp:n=1 \$ before collector B  
 138 0 -4 91 -84 (-33:-85) imp:n=1 \$ between collector B and Pt plate  
 c

199 0 149:-148:146 imp:n=0 \$ external to model

c  
c Surface Records  
c Fission Chamber +Z  
1 cz 0.953  
2 pz 7.606  
3 pz 7.634  
4 cz 1.194  
5 pz 7.634  
6 pz 7.558  
7 cz 0.921  
8 cz 1.021  
9 cz 1.194  
10 pz 7.507  
11 cz 1.119  
12 cz 1.157  
13 pz 7.126  
14 cz 1.081  
15 cz 1.119  
16 pz 7.471  
17 pz 7.253  
18 cz 1.157  
19 pz 7.113  
20 cz 0.882  
21 cz 1.194  
22 pz 7.075  
23 cz 1.157  
24 pz 7.329  
25 cz 0.858  
26 pz 7.710  
27 cz 1.150  
28 pz 7.837  
29 pz 8.091  
30 cz 1.074  
31 pz 7.746  
32 pz 7.964  
33 cz 0.874  
34 pz 8.104  
35 pz 8.142  
36 cz 1.112  
37 pz 7.888  
38 cz 1.245  
39 cz 1.786  
40 pz 8.435  
41 pz 8.529  
42 pz 8.529  
43 pz 8.583  
46 pz 7.005  
47 pz 7.056  
c Fission Chamber -Z  
51 cz 0.953  
52 pz -7.606  
53 pz -7.634  
54 cz 1.194  
55 pz -7.634  
56 pz -7.558  
57 cz 0.921  
58 cz 1.021  
59 cz 1.194  
60 pz -7.507  
61 cz 1.119  
62 cz 1.157  
63 pz -7.126  
64 cz 1.081  
65 cz 1.119  
66 pz -7.471  
67 pz -7.253  
68 cz 1.157  
69 pz -7.113

70 cz 0.882  
71 cz 1.194  
72 pz -7.075  
73 cz 1.157  
74 pz -7.329  
75 cz 0.858  
76 pz -7.710  
77 cz 1.150  
78 pz -7.837  
79 pz -8.091  
80 cz 1.074  
81 pz -7.746  
82 pz -7.964  
83 cz 0.874  
84 pz -8.104  
85 pz -8.142  
86 cz 1.112  
87 pz -7.888  
88 cz 1.245  
89 cz 1.786  
90 pz -8.435  
91 pz -8.529  
92 pz -8.529  
93 pz -8.583  
96 pz -7.005  
97 pz -7.056  
c  
c source, holder  
101 cy 0.1  
102 py -0.04  
103 py 0.04  
104 cy 0.127  
105 py 0.506  
106 cy 0.318  
107 py -0.154  
108 cy 0.330  
109 cy 0.381  
110 py -0.205  
111 cy 0.152  
112 py 0.563  
113 py 0.608  
114 cy 0.114  
115 py 2.289  
116 cy 0.277  
117 py 0.659  
c Holder  
118 cy 0.366  
119 py 2.108  
120 py 1.613  
121 cy 0.254  
122 py 2.616  
123 cy 0.3  
124 py 3.753  
125 cy 1.27  
126 py 3.879  
127 cy 0.445  
128 py 4.133  
129 py 4.260  
130 py 4.895  
131 cy 0.159  
132 py 79.0  
c  
141 cy 7.858  
142 cy 8.493  
143 cy 14.446  
144 cy 20.010  
145 py 11.43  
146 py 11.667  
148 py -11.667  
149 cy 11.667

151 c/y 0 -7.62 0.21  
 152 c/y 0 7.62 0.21  
 154 py 0.0  
 c  
 157 cz 0.635  
 158 so 3.810  
 159 so 3.851  
 c  
 c Data Records  
 c Source  
 sdef erg=d1 pos=0 0 0 cel=51 rad=d2 ext=d3 axs=0 1 0  
 sp1 -3 1.175 1.04  
 si2 0 0.099  
 sp2 -21 1  
 si3 0.0399  
 c Materials  
 c  
 c Air 0.001185 g/cc  
 m1 7014.50c 3.8466e-5  
     8016.50c 1.0348e-5  
     18000 2.3223e-7  
 c  
 c SS304, 7.92 g/cc  
 m2 6012.50c 1.5884e-4  
     25055.50c 8.6816e-4  
     15031.50c 3.4647e-5  
     16032.50c 2.2309e-5  
     14000.50c 6.3683e-4  
     24000.50c 1.7428e-2  
     28000.50c 7.5171e-3  
     7014.50c 1.7026e-4  
     26000.55c 5.9994e-2  
 c  
 c water, 0.9972 g/cc  
 m4 1001.50c 6.6669e-1  
     8016.50c 3.3334e-1  
 mt4 lwtr.01t  
 c  
 c Al 6061, 2.70 g/cc  
 m5 14000.50c 3.4736e-4  
     26000.55c 1.0190e-4  
     29000.50c 7.0365e-5  
     25055.50c 2.2197e-5  
     12000.50c 6.6899e-4  
     24000.50c 6.0978e-5  
     29000.50c 3.1082e-5  
     22000.50c 2.5469e-5  
     13027.50c 5.8639e-2  
 c  
 c Pt, 21.45 g/cc  
 m6 78000.35c 6.6217e-2  
 c  
 c Cf<sub>2</sub>O<sub>2</sub>SO<sub>4</sub>, 1.85 g/cc  
 m7 98252 3.5243e-3  
     8016.50c 1.0573e-2  
     16032 1.7622e-3  
 c  
 c KEL-F, 2.2 g/cc  
 m8 6012.50c 2.2750e-2  
     9019.50c 3.4125e-2  
     17000.50c 1.1375e-2  
 c  
 c Al powder, 2.0 g/cc  
 m11 13027.50c 6.0552e-2  
 c  
 c fissionable deposits  
 m21 92235.50c 1.0  
 m22 94239.55c 1.0  
 m23 92238.50c 1.0

```

m24 93237.55c 1.0
c
c Tallies
fc2 Fission Rate Tallies. The deposit is inside Surface 157
f2:n (3 53) (2 52)
sd2 2.53354 6.42400 2.53354 3.17291
fs2 -157
fm2 (1 21 -6) (1 22 -6) (1 23 -6) (1 24 -6)
c
c
mode n
nps 82222222
ctme 1260.0
print

```

Plutonium Containing Optimally moderated H2O Sollution Minimum Accidents of Concern for RPL

c 3 Scenarios included in this deck. 1) Bare Sphere 2) Water Reflected Sphere

c 3) Iron Reflected Sphere.

c

c Modeled by Bryce Greenfield 12-10-2008

c

c

c Scenario 1: A Bare Sphere

c Cell cards

```

c 1   1     .10020   (-1)      imp:n,p=1
c 2   0     (1 -2)    imp:n,p=1
c 3   2     -0.001205 (2 -3)    imp:n,p=1
c 4   0     (3)       imp:n,p=0
c
c
c

```

c Scenario 2: A Water Reflected Sphere

c Cell cards

```

c 1   1     .10020   (-1)      imp:n,p=1
c 2   3     -1       (1 -4)    imp:n,p=1
c 3   2     -0.001205 (2 -3)    imp:n,p=1
c 4   0     (4 -2)    imp:n,p=1
c 5   0     (3)       imp:n,p=0
c
c
c

```

c Scenario 3: Fe Shielded Sphere

c Cell cards

```

c
c 1   1     .10020   (-1)      imp:n,p=1
c 2   4     -7.874   (1 -4)    imp:n,p=1
c 3   2     -0.001205 (2 -3)    imp:n,p=1
c 4   0     (4 -2)    imp:n,p=1
c 5   0     (3)       imp:n,p=0
c
c
c

```

c Blank line Follows

c Scenario 1: A Bare Sphere

c Surface cards

c 1 so 19.54 \$ H2O and Pu Sphere

c 2 so 219.04 \$ .50 cm less than 2m

c 3 so 220.04 \$ .50 cm greater than 2m

c

c

c Scenario 2: A Water Reflected Sphere

c c

c c Surface cards

c 1 so 19.54 \$ H2O and Pu Sphere

c 2 so 219.04 \$ .50 cm less than 2m

c 3 so 220.04 \$ .50 cm greater than 2m

c 4 so 25.54 \$ Water Reflector

c

```

c
c c Scenario 3: A Metal Shielded Sphere
c c
c c Surface cards
c 1 so 19.54 $ H20 and Pu Sphere
c 2 so 219.04 $.50 cm less than 2m
c 3 so 220.04 $.50 cm greater than 2m
c 4 so 31.54 $ Fe Reflector
c
c
c
c
c
c Blank line Follows

c Data cards
c
c
c Materials Cards
c
c
c Optimally moderated Pu and H20 Solution Ref: NCS99
c Calculated Density 32 g/l 239Pu in H2O
m1 plib=04p nlib=50m pnlib=24u
    94239.60c     8.0614E-05 $ Pu 239
    1001.50m      .0666657   $ H
    8016          .0333343   $ O
c
c
mpn1
    82208
    1001.50m
    8016
c
c
c
c Air 0.001205 g/cc
m2 6012      -0.000124 $ C
    7014      -0.755268 $ N
    8016      -0.231781 $ O
    18000     -0.012827 $ Ar
c
c
mpn2 6012
    8016
    8016
    8016
c
c
c Water Calculated Density of 1 g/cc
m3 1001      .666657 $ H
    8016      .333343 $ O
mt3 lwtr.01t
mpn3
    1002
    8016
c
c
c Fe Representing a cask containing a criticality accident
c Calculated Density 7.874 g/cc
m4 26056      1      $ Fe
c
mpn4
    26056
c
c
phys:p 3j 1
c
c
MODE N P

```

```

c
c Criticality Control Cards
c kcode 2000 1.0 50 250
c ksrc 0 0 0
c
sdef pos 0 0 0 ERG=D1 RAD=D2
c
sp1 -3 0.966 2.842
c
si2 0 19.539
c
c
c This is an Average Energy Deposited over a cell Tally
F6:N 3
SD6 7.28905E+02
c
F16:P 3
SD16 7.28905E+02

Calibration Analyses of the low field (80mrem/hr) NCD for building 325
c Detectors are calibrated in a neutron tank using a Cf-252 source. This source
c was born on 9-27-95 with an initial activity of .688Ci. Decay correct it is
c .0208Ci as of 1-19-2008.
c
c Modeled by Bryce Greenfield 1-19-2008
c
c Cell cards
c
2 2 -0.001205 (-2 8 9 10) imp:n=1
3 3 -.93 (-6 5) imp:n=1
4 4 -7.84 (-3 2 4) imp:n=1
5 5 1.7487e-5 (-5) imp:n=1
6 6 -3.35 (-7 3 4) imp:n=1
7 2 -0.001205 (7 -999 6 5 11) imp:n=1
8 2 -0.001205 (-4) imp:n=1
9 4 -7.84 (-8) imp:n=1
10 3 -.93 (-9 8) imp:n=1
11 4 -7.84 (-10) imp:n=1
c 12 3 -.93 (-12) imp:n=1
13 33 -1.17 (-11) imp:n=1
c 14 3 -.93 (-13) imp:n=1
c 15 3 -.93 (-14) imp:n=1
c 16 3 -.93 (-15) imp:n=1
c 17 3 -.93 (-16) imp:n=1
c
c
999 0 (999) imp:n=0
c
c
c Blank line Follows-----
c
c Surface cards
c
2 RCC 0 0 0 0 998 15.24 $ Counting well 10m deep
3 RCC 0 0 -.5 0 0 1000.5 17.24 $ Counting well wall assumed .5cm thick
4 RCC 0 0 998 0 0 2 15.24 $ Opening at the top of the well
5 RCC 0 -11.16 1013 0 22.32 0 .635 $ BF3 tube .5"X8" .635X20.32cm
6 RCC 0 -10.15 1013 0 20.32 0 5.715 $ Polyethylene Moderating collar around BF3 tube 2.25"X8" 5.715X20.32cm
7 RCC 0 0 -100 0 0 1100 100 $ Structural concrete
8 RCC 0 0 844.5 0 0 5.715 1.27 $ 0.5"X2.25" Metal Source Holder
9 RCC 0 0 824.18 0 0 26.035 10.16 $ 4"X2.75" Poly Colimator
10 RCC 0 0 820.18 0 0 4 15 $ Metal Support Plate
11 RPP -13 13 -13 13 1002.285 1007.28 $ Lucite Slab
c 11 RCC 0 0 1002.285 0 0 2.54 13 $ Poly thermalizer slab
c 12 RPP -20 20 -20 20 1020 1026 $ Reflector Box top

```

```

c 13 RPP -20 20 14 20 1002 1020 $ Reflector Box
c 14 RPP -20 -14 -14 14 1002 1020 $ Reflector Box
c 15 RPP 14 20 -14 14 1002 1020 $ Reflector Box
c 16 RPP -20 20 -20 -14 1002 1020 $ Reflector Box
c
c
c
999 RPP -500 500 -500 500 -400 2000 $ Void Box surrounding model
c
c Blank line Follows-----
c Data cards
c
c
c Materials Cards
c
c
c Air 0.001205 g/cc
m2 6012 -0.000124 $C
    7014 -0.755268 $N
    8016 -0.231781 $O
    18000 -0.012827 $Ar
c
c
c Polyethylene .93 g/cc
m3 1001 -0.143716 $H
    6012 -0.856284 $C
MT3 POLY.60t
c
c Lucite 1.19g/cc
m33 1001 -0.080538
    6012 -0.599848
    8016 -0.319614
c
c
c
c Fe Representing a cask containing a criticality accident
c Calculated Density -7.874 g/cc
m4 26056 1 $Fe
c
c
c
c Boron-10 Trifluoride Fill Gas Assumed Pressure of .70atm~70kPa, .001963g/cc
m5 5010.60c .250 $B-10
    9019.60c .750 $F
c
c
c
c
c High Density Barritic Concrete rho=3.35g/cc
m6 1001 -0.003585 $H
    8016 -0.311622 $O
    12000 -0.001195 $C
    13027 -0.004183 $Al
    14000 -0.010457 $Si
    16000 -0.107858 $S
    20000 -0.050194 $Ca
    26000 -0.047505 $Fe
    56138.60c -0.463400 $Ba
c
c
c MODE N
c
sdef pos 0 0 847 ERG=D1
c
c Watt fission spectrum with spontaneous fission coefficients for Cf-252 from MCNP5 manual
sp1 -3 1.025 2.926
c
c

```

```

nps 5000000
c
c
c This is a current tally over the surface of the poly collar
c F2:N (6.1)
c 6.2 6.3)
c .4eV is the Cd cutoff
c 4eV is a rough thermal cutoff where the Cd threshold becomes negligible
c
c E2 4E-6 20
c
c F12:N (5.1)
c E12 4E-6 20
c 5.2 5.3)
c Surface area of BF3 tube
c SD2 162.14 5.067 5.067
c
c Surface area of the Poly collar 934.875
c SD2 935
c
c Cell Flux Tally over poly collar
c 729.7 102.6 102.6
F4:N 3
SD4 2059.26
E4 1.00E-07 1.00E-06 1.00E-05 1.00E-04 1.00E-03 1.00E-02
    1.00E-01 5.00E-01 1.00E+00 2.00E+00 3.00E+00 4.00E+00
    5.00E+00 6.00E+00
c Cell Flux Tally over poly collar
F14:N 3
SD14 2059.26
E14 4E-6 20
F1:N 11.5
C1 0 1
E1 4E-6 20

```

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