



# Cattaneo-Christov double-diffusion theory for three-dimensional flow of viscoelastic nanofluid with the effect of heat generation/absorption

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## ABSTRACT

The present research article focuses on three-dimensional flow of viscoelastic(second grade) nanofluid in the presence of Cattaneo-Christov double-diffusion theory. Flow caused is due to stretching sheet. Characteristics of heat transfer are interpreted by considering the heat generation/absorption. Nanofluid theory comprises of Brownian motion and thermophoresis. Cattaneo-Christov double-diffusion theory is introduced in the energy and solutal relaxation times framework. Suitable variables are implemented for the conversion of partial differential systems into a sets of ordinary differential equations. The transformed expressions have been explored through homotopic algorithm. Behavior of sundry variables on the velocities, temperature and concentration are scrutinized graphically. Numerical values of skin friction coefficients are also calculated and examined. Here thermal field enhances for heat generation parameter while reverse situation is noticed for heat absorption parameter.

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## Introduction

The dilute suspension of nano-sized particles and dispersion of fibers in a fluid is termed as nanoliquid. The mixture of nanoparticles changed the physical nature of liquid in comparison to ordinary fluids e.g. density, thermal conductivity, viscosity etc. In all such characteristics, thermal conductivity has role in various industrial and technological applications. The nanoparticles are widely implemented in the applications of medicine, electronics, optics, solar cells, catalysis, materials, manufacturing, smart computers, renewable energy and many others. At present the concept of energy transfer in nanoliquids can be categorized in two classes. In one category, the researchers assumed that the nanoliquids are composite, developed by nanoparticles and surrounded by nanolayers like shell. Some investigations on this concept can be found in the studies [1–10]. The other theory states that the thermal conductivity of nanoliquid based on part of Brownian motion and particle convention static due to which micro-mixing occurs. The dynamics of particles is considered in such models. The interaction of particle mechanism in nanoliquids can be visualized through this theory. Buongiorno [11] developed a model to explore the mechanism of thermal conductivity of nanoliquids by

considering the Brownian motion and thermophoretic. Further researches on this topic can be seen in the studies [12–18].

In the past, the investigators made the analysis of heat and mass transport problems by employing classical Fourier and Fick's theories of heat and mass diffusion. In these theories, the anomalous of heat and mass diffusion is ignored. Cattaneo [19] firstly proposed the concept of thermal relaxation time in Fourier's theory of heat transport to denote the "thermal inertia". This idea is known as Maxwell-Cattaneo theory of heat flux. Christov [20] used the upper-convective Oldroyd differentiation in place of partial time derivative and he also employed the frame indifferent generalization of Fourier's law in energy expression [21]. Haddad [22] explored the thermal instability Cattaneo-Christov formula of heat flux in a non-Darcy porous space. Li et al. [23] extended the concept of Cattaneo-Christov for hydromagnetic flow of Maxwell liquid induced by a vertical moving surface. The aspects of Cattaneo-Christov double-diffusion model for flow of Jeffrey fluid over a stretched are reported by Hayat et al. [24]. Waqas et al. [25] explored the impact of thermal relaxation time for variable conductivity flow of non-Newtonian fluid. They employed the homotopic theory to evaluate the results of governing model. Shehzad et al. [26] addressed the Oldroyd-B liquid flow in a Darcy-Forchheimer porous media through Cattaneo-Christov heat diffusion. Sui et al. [27] examined the double-diffusive model of Cattaneo-Christov for Maxwell liquid flow with Brownian motion

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and slip conditions. Hayat et al. [28] discussed the squeezed flow of Jeffrey fluid in the frame of Cattaneo–Christov heat flux.

The main idea here is to evaluate impact of Cattaneo–Christov heat and mass diffusions model for flow of second grade liquid. Second grade model is an important sub-category of non-Newtonian liquids. Such liquids have vital roles in the applications like movement of biological liquids, lubricants performance, plastic manufacturing, food processing etc. Aspects of Brownian motion, thermophoretic and heat absorption/generation are further considered in this work. The theory of boundary layer is employed to govern the mathematical expressions of considered flow model. Computations of solutions are made through homotopic theory [29–46]. The results of presented analysis are displayed and discussed.

**Formulation**

We investigate three-dimensional flow of an incompressible viscoelastic nanofluid over a impermeable stretching surface at  $z = 0$ . The flow is confined in the domain  $z > 0$ . Here we choose the Cartesian coordinate in such away that  $x$ -axis is along the stretching sheet and  $y$ -axis perpendicular to sheet (see Fig. 1). Let  $(u, v, w)$  be the velocity components along the  $(x, y, z)$  directions, respectively. Here  $u_w(x) = ax$  and  $v_w(y) = by$  are stretching velocity components (where  $a$  and  $b$  being stretching rate constants having dimension  $T^{-1}$ ). The heat and nanoparticle mass transfer phenomena have been analyzed in view of Cattaneo–Christov double-diffusion expressions. The behavior of thermophoresis and Brownian motion is taken into account. The equations are

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \tag{1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = v \frac{\partial^2 u}{\partial z^2} + \beta \left[ u \frac{\partial^3 u}{\partial x \partial z^2} + w \frac{\partial^3 u}{\partial z^3} - \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial z} \frac{\partial^2 w}{\partial z^2} - 2 \frac{\partial u}{\partial z} \frac{\partial^2 u}{\partial x \partial z} - 2 \frac{\partial w}{\partial z} \frac{\partial^2 u}{\partial z^2} \right], \tag{2}$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = v \frac{\partial^2 v}{\partial z^2} + \beta \left[ v \frac{\partial^3 v}{\partial x \partial z^2} + w \frac{\partial^3 v}{\partial z^3} - \frac{\partial v}{\partial y} \frac{\partial^2 v}{\partial z^2} - \frac{\partial v}{\partial z} \frac{\partial^2 w}{\partial z^2} - 2 \frac{\partial v}{\partial z} \frac{\partial^2 v}{\partial y \partial z} - 2 \frac{\partial w}{\partial z} \frac{\partial^2 v}{\partial z^2} \right], \tag{3}$$

with the boundary conditions

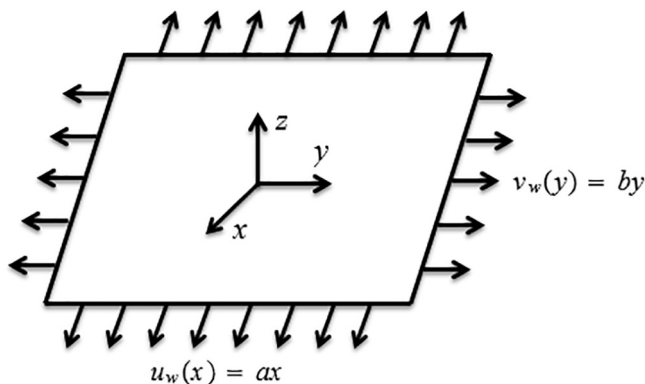


Fig. 1. Physical sketch.

$$u = u_w(x) = ax, \quad v = v_w(y) = by, \quad w = 0 \text{ at } z = 0, \\ u \rightarrow 0, \quad v \rightarrow 0 \text{ as } y \rightarrow \infty, \tag{4}$$

where  $\nu = (\mu/\rho)_f$  denotes the kinematic viscosity,  $\beta$  for normal stress moduli and  $\rho_f$  for viscoelastic fluid density. The Cattaneo–Christov diffusion theory describing the thermal and concentration diffusion with relaxation of heat and mass fluxes are

$$\mathbf{q} + \Lambda_e \left[ \frac{\partial \mathbf{q}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{q} - \mathbf{q} \cdot \nabla \mathbf{V} + (\nabla \cdot \mathbf{V}) \mathbf{q} \right] = -k_f \nabla T, \tag{5}$$

$$\mathbf{J} + \Lambda_c \left[ \frac{\partial \mathbf{J}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{J} - \mathbf{J} \cdot \nabla \mathbf{V} + (\nabla \cdot \mathbf{V}) \mathbf{J} \right] = -D_B \nabla C, \tag{6}$$

where  $\mathbf{q}$  is for heat flux and  $\mathbf{J}$  for mass flux,  $\mathbf{V}$  for velocity,  $k_f$  for fluid thermal conductivity and  $D_B$  for Brownian diffusion coefficient. Here  $\Lambda_e$  and  $\Lambda_c$  are the thermal and solutal relaxation time factors. For  $\Lambda_e = 0$  and  $\Lambda_c = 0$ , the Eqs. (5) and (6) recovers laws due to Fourier and Fick. For incompressible fluid situation one has

$$\mathbf{q} + \Lambda_e [\mathbf{V} \cdot \nabla \mathbf{q} - \mathbf{q} \cdot \nabla \mathbf{V}] = -k_f \nabla T, \tag{7}$$

$$\mathbf{J} + \Lambda_c [\mathbf{V} \cdot \nabla \mathbf{J} - \mathbf{J} \cdot \nabla \mathbf{V}] = -D_B \nabla C. \tag{8}$$

The energy and concentration expressions are

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} + \Omega_e \Lambda_e = \frac{k_f}{(\rho c_p)_f} \frac{\partial^2 T}{\partial z^2} + \tau D_B \left( \frac{\partial T}{\partial z} \frac{\partial C}{\partial z} \right) + \frac{\tau D_T}{T_\infty} \left( \frac{\partial T}{\partial z} \right)^2 + \frac{Q^*}{(\rho c_p)_f} (T - T_\infty), \tag{9}$$

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} + w \frac{\partial C}{\partial z} + \Omega_c \Lambda_c = D_B \frac{\partial^2 C}{\partial z^2} + \frac{D_T}{T_\infty} \left( \frac{\partial^2 T}{\partial z^2} \right), \tag{10}$$

with

$$T = T_w, \quad C = C_w \text{ at } z = 0 \text{ and } T \rightarrow T_\infty, \quad C \rightarrow C_\infty \text{ as } z \rightarrow \infty, \tag{11}$$

$$\Omega_e = u^2 \frac{\partial^2 T}{\partial x^2} + v^2 \frac{\partial^2 T}{\partial y^2} + w^2 \frac{\partial^2 T}{\partial z^2} + \left( u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) \frac{\partial T}{\partial x} + \left( u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) \frac{\partial T}{\partial y} + \left( u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right) \frac{\partial T}{\partial z} + 2uv \frac{\partial^2 T}{\partial x \partial y} + 2vw \frac{\partial^2 T}{\partial y \partial z} + 2uw \frac{\partial^2 T}{\partial x \partial z}, \tag{12}$$

$$\Omega_c = u^2 \frac{\partial^2 C}{\partial x^2} + v^2 \frac{\partial^2 C}{\partial y^2} + w^2 \frac{\partial^2 C}{\partial z^2} + \left( u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) \frac{\partial C}{\partial x} + \left( u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) \frac{\partial C}{\partial y} + \left( u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right) \frac{\partial C}{\partial z} + 2uv \frac{\partial^2 C}{\partial x \partial y} + 2vw \frac{\partial^2 C}{\partial y \partial z} + 2uw \frac{\partial^2 C}{\partial x \partial z}. \tag{13}$$

In the above expressions  $\rho_f$  for fluid density,  $(c_p)_f$  for fluid heat capacity,  $\rho_p$  for particle density,  $(c_p)_p$  for particle heat capacity,  $k_f$  for thermal conductivity,  $\tau = (\rho c_p)_p / (\rho c_p)_f$  for heat capacity ratio,  $D_B$  for Brownian diffusion coefficient,  $D_T$  for thermophoretic diffusion coefficient,  $Q^*$  for coefficient of heat generation/absorption,  $T$  and  $C$  for temperature and nanoparticle concentration of fluid respectively,  $T_w$  and  $C_w$  for temperature and nanoparticle concentration of surface respectively,  $T_\infty$  for ambient fluid temperature and  $C_\infty$  for ambient fluid concentration. The suitable transformations are

$$\eta = z \sqrt{\frac{a}{\nu}}, \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty}, \quad \phi(\eta) = \frac{C - C_\infty}{C_w - C_\infty}, \\ u = ax f'(\eta), \quad v = ay g'(\eta), \quad w = -\sqrt{a\nu} (f(\eta) + g(\eta)). \tag{14}$$

Eq. (1) is trivially satisfied by variables defined in previous equation and other equations yield

$$f''' + (f+g)f'' - (f')^2 + \alpha((f+g)f^{iv} + (f'' - g'')f'' - 2(f' + g')f''') = 0, \tag{15}$$

$$g''' + (f+g)g'' - (g')^2 + \alpha((f+g)g^{iv} + (f'' - g'')g'' - 2(f' + g')g''') = 0, \tag{16}$$

$$\theta'' + \text{Pr}(f+g)\theta' - \text{Pr}\delta_e((f+g)^2\theta'' + (f+g)(f'+g')\theta') + \text{Pr}N_b\theta'\phi' + \text{Pr}N_t(\theta')^2 + \text{Pr}\gamma\theta = 0, \tag{17}$$

$$\phi'' + \text{Sc}(f+g)\phi' - \text{Sc}\delta_c((f+g)^2\phi'' + (f+g)(f'+g')\phi') + \frac{N_t}{N_b}\theta'' = 0, \tag{18}$$

$$f(\eta)=0, f'(\eta)=1, g(\eta)=0, g'(\eta)=\delta, \theta(\eta)=1, \phi(\eta)=1 \text{ at } \eta=0, \\ f'(\eta)\rightarrow 0, g(\eta)\rightarrow 0, \theta(\eta)\rightarrow 0, \phi(\eta)\rightarrow 0 \text{ as } \eta\rightarrow \infty, \tag{19}$$

where  $\alpha$  for dimensionless viscoelastic parameter,  $\text{Pr}$  for Prandtl number,  $N_b$  for Brownian motion parameter,  $N_t$  for thermophoresis parameter,  $\gamma$  for heat generation/absorption parameter,  $\delta_e$  for non-dimensional thermal relaxation time,  $\text{Sc}$  for Schmidt number,  $\delta_c$  for non-dimensional solutal relaxation time and  $\delta$  for ratio parameter. The involved variables are defined as:

$$\alpha = \frac{\beta a}{\nu}, \text{Pr} = \frac{\mu c_p}{k_f}, N_b = \frac{(\rho c_p)_p D_B (C_w - C_\infty)}{(\rho c_p)_f \nu}, N_t = \frac{(\rho c_p)_p D_T (T_w - T_\infty)}{(\rho c_p)_f \nu T_\infty}, \\ \gamma = \frac{Q^*}{(\rho c_p)_f a}, \delta_e = \Lambda_e a, \text{Sc} = \frac{\nu}{D_B}, \delta_c = \Lambda_c a, \delta = \frac{b}{a}. \tag{20}$$

It should be noted that  $g(\eta) = \delta = 0$  in Eqs. (15)–(19) yields two-dimensional situation.

The skin friction coefficient along the  $x$  and  $y$  directions are defined for the given problem in the forms

$$C_{f_x} = \frac{\tau_{wx}}{\frac{1}{2}\rho u_w^2}, C_{f_y} = \frac{\tau_{wy}}{\frac{1}{2}\rho u_w^2}, \tag{21}$$

where  $\tau_{wx}$  and  $\tau_{wy}$  denote the surface shear stresses along the  $x$  and  $y$  directions which can be expressed as

$$\tau_{wx} = \left[ \mu \frac{\partial u}{\partial z} + \beta \left( u \frac{\partial^2 u}{\partial x \partial z} + v \frac{\partial^2 u}{\partial y \partial z} + w \frac{\partial^2 u}{\partial z^2} + \frac{\partial u \partial u}{\partial x \partial z} + \frac{\partial v \partial v}{\partial x \partial z} - \frac{\partial w \partial u}{\partial z \partial z} \right) \right]_{z=0}, \\ \tau_{wy} = \left[ \mu \frac{\partial v}{\partial z} + \beta \left( u \frac{\partial^2 v}{\partial x \partial z} + v \frac{\partial^2 v}{\partial y \partial z} + w \frac{\partial^2 v}{\partial z^2} + \frac{\partial u \partial u}{\partial y \partial z} + \frac{\partial v \partial v}{\partial y \partial z} - \frac{\partial w \partial v}{\partial z \partial z} \right) \right]_{z=0} \tag{22}$$

In dimensionless form the skin friction coefficients  $C_{f_x}$  and  $C_{f_y}$  along  $x$  and  $y$  directions are given by

$$\frac{1}{2} \text{Re}_x^{0.5} C_{f_x} = [f'' + \alpha(-(f+g)f'' + 2f'f'' + (f'+g')f'')]_{\eta=0}, \\ \frac{1}{2} \text{Re}_y^{0.5} C_{f_y} = [g'' + \alpha(-(f+g)g'' + 2g'g'' + (f'+g')g'')]_{\eta=0}, \tag{23}$$

in which  $\text{Re}_x = \frac{u_w x}{\nu}$  and  $\text{Re}_y = \frac{u_w y}{\nu}$  denote the local Reynolds number.

**Solutions expressions**

The initial approximations  $(f_0, g_0, \theta_0, \phi_0)$  and auxiliary linear operators  $(\mathcal{L}_f, \mathcal{L}_g, \mathcal{L}_\theta, \mathcal{L}_\phi)$  for homotopic expressions are

$$f_0(\eta) = (1 - \exp(-\eta)), g_0(\eta) = \delta(1 - \exp(-\eta)), \\ \theta_0(\eta) = \exp(-\eta), \phi_0(\eta) = \exp(-\eta), \tag{24}$$

$$f(f) = \frac{d^3 f}{d\eta^3} - \frac{df}{d\eta}, \mathcal{L}_g(g) = \frac{d^3 g}{d\eta^3} - \frac{dg}{d\eta}, \\ \mathcal{L}_\theta(\theta) = \frac{d^2 \theta}{d\eta^2} - \theta, \mathcal{L}_\phi(\phi) = \frac{d^2 \phi}{d\eta^2} - \phi, \tag{25}$$

with the associated properties

$$\mathcal{L}_f[\Gamma_1 + \Gamma_2 \exp(-\eta) + \Gamma_3 \exp(\eta)] = 0, \\ \mathcal{L}_g[\Gamma_4 + \Gamma_5 \exp(-\eta) + \Gamma_6 \exp(\eta)] = 0, \\ \mathcal{L}_\theta[\Gamma_7 \exp(-\eta) + \Gamma_8 \exp(\eta)] = 0, \\ \mathcal{L}_\phi[\Gamma_9 \exp(-\eta) + \Gamma_{10} \exp(\eta)] = 0. \tag{26}$$

Employing procedure in Refs. [43–46] we have the general solutions

$$f_m(\eta) = f_m^*(\eta) + \Gamma_1 + \Gamma_2 \exp(-\eta) + \Gamma_3 \exp(\eta), \\ g_m(\eta) = g_m^*(\eta) + \Gamma_4 + \Gamma_5 \exp(-\eta) + \Gamma_6 \exp(\eta), \\ \theta_m(\eta) = \theta_m^*(\eta) + \Gamma_7 \exp(-\eta) + \Gamma_8 \exp(\eta), \\ \phi_m(\eta) = \phi_m^*(\eta) + \Gamma_9 \exp(-\eta) + \Gamma_{10} \exp(\eta), \tag{27}$$

where  $f_m^*(\eta), g_m^*(\eta), \theta_m^*(\eta)$  and  $\phi_m^*(\eta)$  are the special solutions and  $\Gamma_i$  ( $i = 1 - 10$ ) are the arbitrary constants given by

$$\Gamma_1 = - \left. \frac{\partial f_m^*(\eta)}{\partial \eta} \right|_{\eta=0} - f_m^*(0), \Gamma_2 = \left. \frac{\partial f_m^*(\eta)}{\partial \eta} \right|_{\eta=0}, \Gamma_3 = 0, \\ \Gamma_4 = - \left. \frac{\partial g_m^*(\eta)}{\partial \eta} \right|_{\eta=0} - g_m^*(0), \Gamma_5 = \left. \frac{\partial g_m^*(\eta)}{\partial \eta} \right|_{\eta=0}, \Gamma_6 = 0, \\ \Gamma_7 = - \theta_m^*(\eta)|_{\eta=0}, \Gamma_8 = 0, \Gamma_9 = - \phi_m^*(\eta)|_{\eta=0}, \Gamma_{10} = 0. \tag{28}$$

**Convergence analysis**

Construction of the series solutions by homotopy analysis technique involve convergence control variables  $h_f, h_g, h_\theta$  and  $h_\phi$ . These convergence control variables plays vital role to adjust and control the convergence region of the series solutions. Hence Figs. 2 and 3 displayed the  $h$ -curves. It is seen that acceptable values of  $h_f, h_g, h_\theta$  and  $h_\phi$  are  $-2.1 \leq h_f \leq -0.15, -2.1 \leq h_g \leq -0.25, -1.3 \leq h_\theta \leq -0.2$  and  $-1.2 \leq h_\phi \leq -0.25$ .

**Results and discussion**

The effect of various physical variables on the velocities, thermal and concentration fields are interpreted in this section. Figs. 4 and 5 ensure the impact of dimensionless viscoelastic parameter  $\alpha$  and ratio parameter  $\delta$  on velocities  $f'(\eta)$  and  $g'(\eta)$ . Variation of velocities of  $f'(\eta)$  and  $g'(\eta)$  within the frame of viscoelastic param-

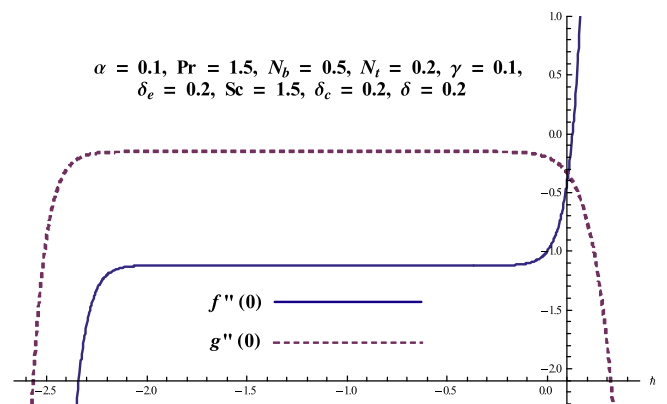


Fig. 2.  $h$ -curves for  $f''(0)$  and  $g''(0)$ .

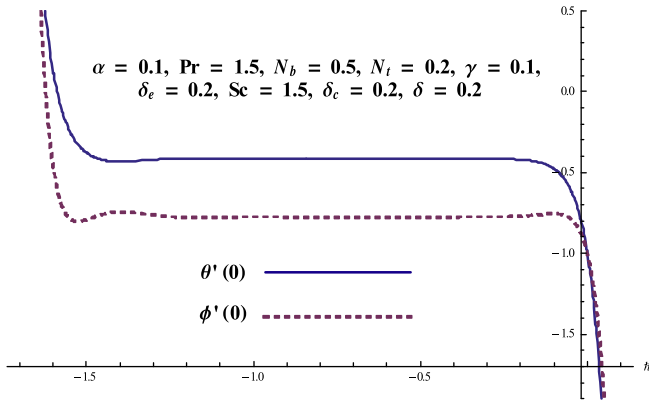


Fig. 3.  $h$ -curves for  $\theta'(0)$  and  $\phi'(0)$ .

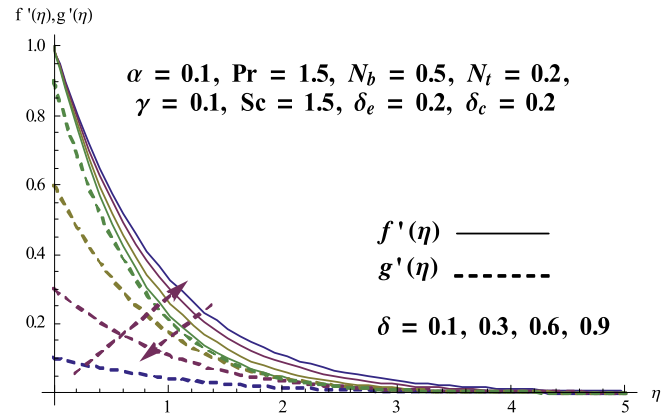


Fig. 5. Behavior of  $\delta$  on  $f'(\eta)$ .

eter  $\alpha$  are captured in Fig. 4. One can see that velocities and layer thickness are reduced via larger  $\alpha$ . Physically it can be observed that for higher values of  $\alpha$ , the viscoelasticity enhances which resists the fluid flow due to which the fluid velocities are diminished. Fig. 5 illustrates the behavior of  $\delta$  on  $x$ - and  $y$ -components of velocity. Large  $\delta$  implies to an increase in rate of stretching along  $y$ -direction due to which velocity field  $g'(\eta)$  is increasing whereas  $f'(\eta)$  shows the decreasing behavior.

Variations in temperature for different values of viscoelastic parameter  $\alpha$ , Prandtl number  $Pr$ , Brownian motion parameter  $N_b$ , thermophoresis parameter  $N_t$ , heat generation/absorption parameter  $\gamma$  and non-dimensional thermal relaxation time  $\delta_e$  are studied in the Figs. 6–11. Fig. 6 disclosed the behavior of  $\alpha$  on the temperature. Both temperature and thermal layer thickness are enhanced via  $\alpha$ . Physically larger viscoelastic parameter result in more temperature inside the boundary layer region. It is seen from Fig. 7 that both temperature and thickness layer diminish for higher Prandtl number  $Pr$ . Physically, higher  $Pr$  lead to lower thermal diffusivity which ensures decrease in temperature. Fig. 8 demonstrates the features of Brownian motion parameter  $N_b$  on temperature field. There is an enhancement in temperature and thermal layer thickness in view of  $N_b$ . In fact more heat is produced through the random motion of the fluid particles within the frame of larger Brownian motion parameter  $N_b$ . Therefore temperature increases. Fig. 9 clearly indicates that the temperature and associated layer thickness are increased for larger thermophoresis parameter  $N_t$ . In thermophoresis phenomenon the heated particles are pulled away from hot surface to the cold region and fluid temperature rises. Behavior of heat generation/absorption parameter  $\gamma$  on tem-

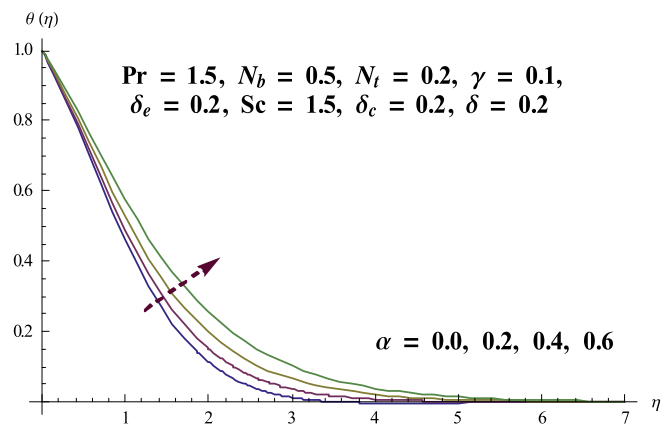


Fig. 6. Behavior of  $\alpha$  on  $\theta(\eta)$ .

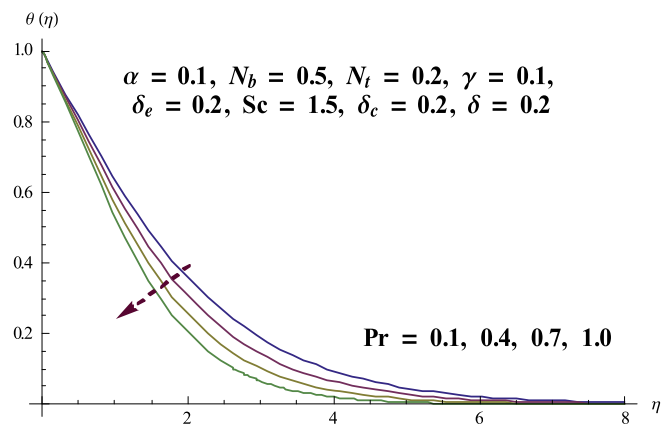


Fig. 7. Behavior of  $Pr$  on  $\theta(\eta)$ .

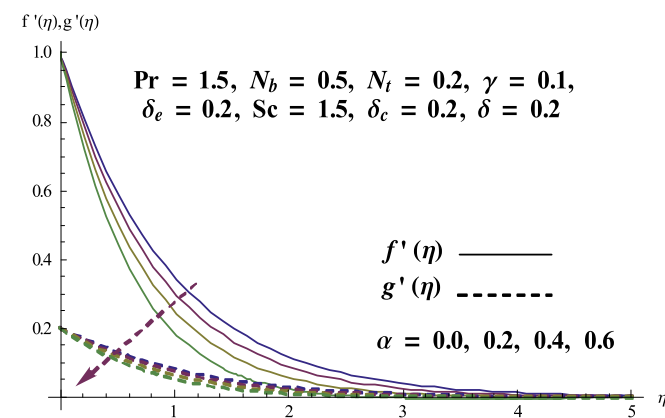


Fig. 4. Behavior of  $\alpha$  on  $f'(\eta)$ .

perature field is elucidated in Fig. 10. It is concluded that temperature and thickness of thermal layer are enhanced when heat generation parameter ( $\gamma > 0$ ) increases while reverse situation is observed for heat absorption situation ( $\gamma < 0$ ). Obviously in heat generation parameter  $\gamma > 0$  process more heat is produced which results in the enhancement of temperature field. Variation of temperature field within the frame of non-dimensional thermal relaxation time  $\delta_e$  is shown in Fig. 11. One can see that temperature and thermal layer thickness are reduced via larger  $\delta_e$ . Physically it

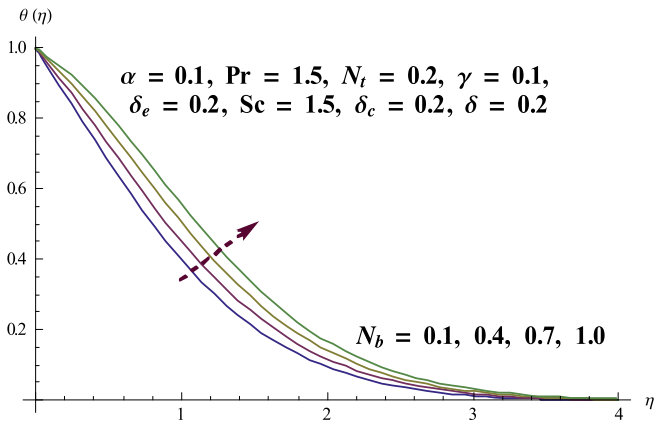


Fig. 8. Behavior of  $N_b$  on  $\theta(\eta)$ .

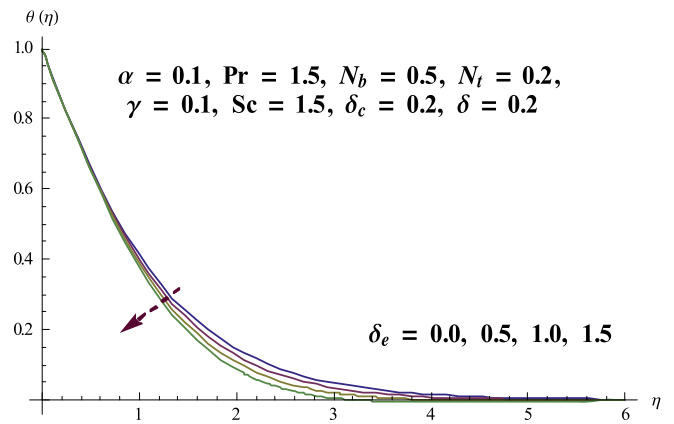


Fig. 11. Behavior of  $\delta_e$  on  $\theta(\eta)$ .

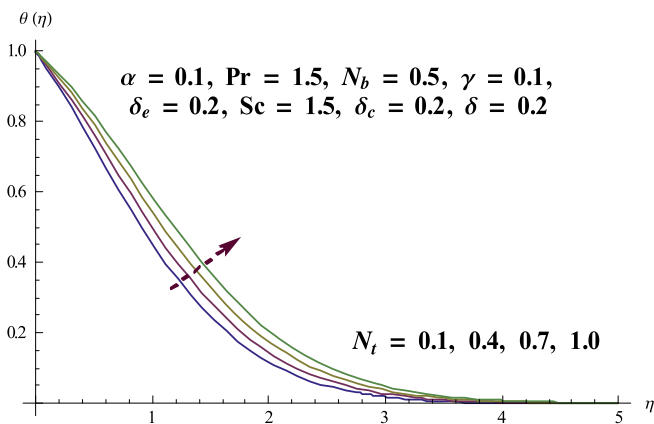


Fig. 9. Behavior of  $N_t$  on  $\theta(\eta)$ .

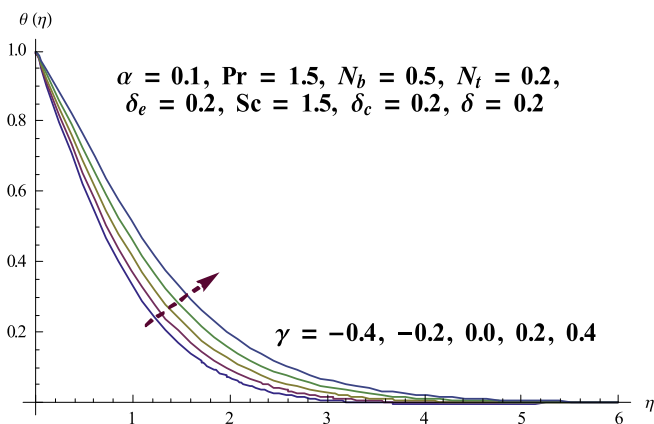


Fig. 10. Behavior of  $\gamma$  on  $\theta(\eta)$ .

can be observed that material particle requires more time for heat transfer to its neighboring particles due to thermal relaxation enhancement.

Influences of dimensionless viscoelastic parameter  $\alpha$ , Brownian motion parameter  $N_b$ , thermophoresis parameter  $N_t$ , Schmidt number  $Sc$  and non-dimensional solutal relaxation time  $\delta_c$  on the nanoparticle concentration are analyzed in the Figs. 12–16. Fig. 12 is prepared to see the behavior of viscoelastic parameter  $\alpha$  on concentration field. We see that both concentration and

boundary layer thickness are increasing via  $\alpha$ . Fig. 13 exhibits impact of Brownian motion parameter  $N_b$  on the concentration distribution. For higher values of  $N_b$  the concentration and layer thickness have dominant behavior. It is interpreted that for larger Brownian motion parameter  $N_b$ , the collision of the fluid particles enhances and the concentration field diminishes. Fig. 14 shows that both concentration profile and boundary layer thickness are enhanced for larger thermophoresis parameter  $N_t$ . The thermal conductivity of the fluid enhances in presence of nanoparticles. Higher  $N_t$  give rise to thermal conductivity of the fluid. Such higher thermal conductivity indicates rise in concentration. It is revealed that concentration and related layer thickness are reduced for larger Schmidt number  $Sc$  (see Fig. 15). Physically Schmidt number  $Sc$  is the momentum to mass diffusivities ratio. Thus for larger Schmidt number  $Sc$  the mass diffusivity decreases which is responsible in reduction of concentration field. Fig. 16 presents impact of non-dimensional solutal relaxation time  $\delta_c$  on concentration distribution. Through  $\delta_c$  the concentration and layer thickness are diminished. In fact that material particle requires more time for mass transfer to its neighboring particles due to solutal relaxation enhancement.

Table 1 explores the convergence of velocities  $f'(\eta)$  and  $g'(\eta)$ , temperature and concentration. Presented values scrutinized that 16th order of approximations are enough for  $f''(0)$  and  $g''(0)$  and 8th and 20th orders of approximations are sufficient for  $\theta'(0)$  and  $\phi'(0)$ . Table 2 computed skin friction coefficients for various values

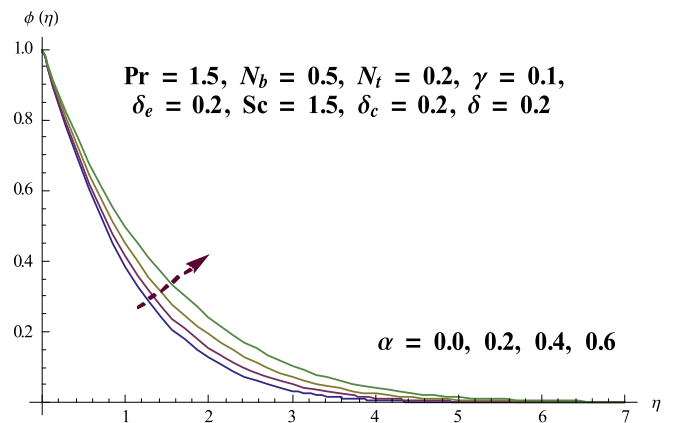


Fig. 12. Behavior of  $\alpha$  on  $\phi(\eta)$ .

**Table 1**  
Convergence solutions when  $\alpha = 0.1, Pr = 1.5, N_b = 0.5, N_t = 0.2, \gamma = 0.1, \delta_e = 0.2, Sc = 1.5, \delta_c = 0.2$  and  $\delta = 0.2$ .

Order of approximation	$-f''(0)$	$-g''(0)$	$-h'(0)$	$-\phi'(0)$
1	1.05333	0.18400	0.62500	0.92000
5	1.11434	0.15784	0.42485	0.82930
8	1.12069	0.15253	0.42323	0.80628
10	1.12103	0.15198	0.42323	0.79707
16	1.12106	0.15192	0.42323	0.78475
20	1.12106	0.15192	0.42323	0.78336
25	1.12106	0.15192	0.42323	0.78336
30	1.12106	0.15192	0.42323	0.78336
35	1.12106	0.15192	0.42323	0.78336

**Table 2**  
Skin friction coefficient  $\frac{1}{2}Re_x^{0.5}C_{f_x}$  and  $\frac{1}{2}Re_x^{0.5}C_{f_y}$  when  $Pr = 1.2, N_b = 0.5, N_t = 0.2, \gamma = 0.1, \delta_e = 0.2, Sc = 1.2$  and  $\delta_c = 0.2$ .

Parameters (fixed values)	Parameters		$-\frac{1}{2}Re_x^{0.5}C_{f_x}$	$-\frac{1}{2}Re_x^{0.5}C_{f_y}$
$\delta = 0.2$	$\alpha$	0.1	1.47980	0.17619
		0.2	2.01272	0.19923
		0.3	2.68852	0.20252
$\alpha = 0.1$	$\delta$	0.1	1.42483	0.07529
		0.2	1.47980	0.17619
		0.5	1.65094	0.63171

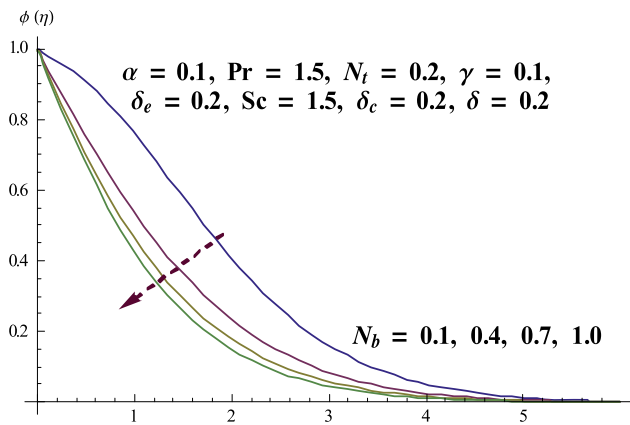


Fig. 13. Behavior of  $N_b$  on  $\phi(\eta)$ .

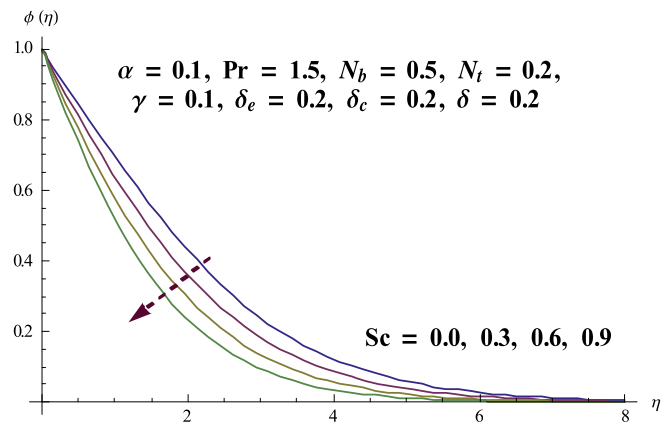


Fig. 15. Behavior of  $Sc$  on  $\phi(\eta)$ .

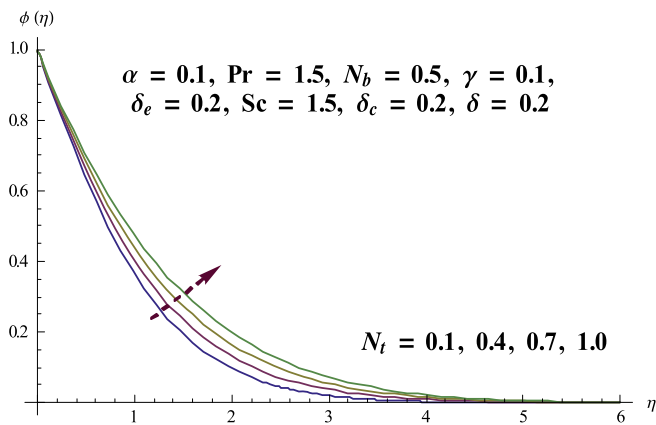


Fig. 14. Behavior of  $N_t$  on  $\phi(\eta)$ .

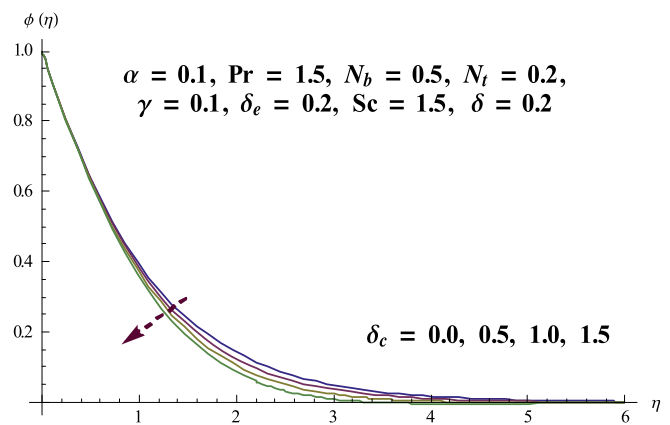


Fig. 16. Behavior of  $\delta_c$  on  $\phi(\eta)$ .



of physical variables. Skin friction coefficients are enhanced for  $\alpha$  and  $\delta$ .

### Concluding remarks

Three-dimensional flow of viscoelastic nanofluid in view of Cattaneo-Christov double-diffusion theory has been considered. Key points are listed below:

- Velocities  $f'(\eta)$  and  $g'(\eta)$  are similar in a qualitative sense within the frame of viscoelastic parameter  $\alpha$ .
- Temperature via  $N_b$  and  $N_t$  has similar qualitative effect.
- Reduction in concentration is observed for  $\delta_c$ .
- The velocities  $f'(\eta)$  and  $g'(\eta)$  have opposite behavior for larger  $\delta$  while skin friction coefficient along  $x$ - and  $y$ -directions are enhanced.
- An increase in  $N_b$  gives a reduction in the concentration while it enhances due to  $N_t$ .
- Both components of skin friction coefficient are increased via ratio parameter  $\delta$ .

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