

Non-Darcy flow of water-based carbon nanotubes with nonlinear radiation and heat generation/absorption

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ABSTRACT

Here modeling and computations are presented to introduce the novel concept of Darcy-Forchheimer three-dimensional flow of water-based carbon nanotubes with nonlinear thermal radiation and heat generation/absorption. Bidirectional stretching surface induces the flow. Darcy's law is commonly replaced by Forchheimer relation. Xue model is implemented for nonliquid transport mechanism. Nonlinear formulation based upon conservation laws of mass, momentum and energy is first modeled and then solved by optimal homotopy analysis technique. Optimal estimations of auxiliary variables are obtained. Importance of influential variables on the velocity and thermal fields is interpreted graphically. Moreover velocity and temperature gradients are discussed and analyzed. Physical interpretation of influential variables is examined.

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Introduction

A carbon nanotube (CNTs) is a tube shaped material, allotropes of carbon with a cylindrical nanostructure. These carbon molecules in cylindrical shape have exceptional characteristics, which are beneficial for nanotechnology, optics, electronics and other fields of materials science and engineering. Owing to the material's excellent strength and stiffness the cylindrical nanotubes are established with length-to-diameter ratio up to 132,000,000 remarkably higher when compared with other material. Carbon nanotubes have extensive applications in different fields for example in tissue engineering, prostheses, genomics, pharmacogenomics, drug delivery, surgery and general medicine etc. Carbon nanotubes can be categorized into two subclasses. These depend on structure of material, namely single wall carbon nanotubes (SWCNTs) and multi wall carbon nanotubes (MWCNTs). Thermal conductivity enhancement through nanotube suspension is examined by Choi et al. [1]. They considered oil based nanoliquids comprising carbon nanotubes and found that nanotubes yield remarkable thermal conductivity enhancement. A model based on Maxwell theory valid for carbon nanotubes (CNTs) characteristics transport is presented by Xue [2]. Non-Fourier heat flux and

unsteady chemically reactive flow through SWCNTs and MWCNTs is investigated by Hayat et al. [3]. They considered Xue model for the effective thermal conductivity of nanoliquid. They found that Nusselt number is enhanced for large thermal relaxation and curvature parameters. MHD flow of carbon water nanomaterial by a stretchable disk with Marangoni convection and Rosseland approximation is explored by Mahanthesh et al. [4]. They used Runge-Kutta method via shooting technique to find out the computational results of nonlinear expressions. Their results illustrated that heat transfer rate increases for higher Marangoni number and nanoparticles volume fraction. However it declines for magnetic variable. MHD slip flow with convective heat transport in presence of SWCNTs and MWCNTs is analyzed by Haq et al. [5]. Recently few meaningful attempts for flows with SWCNTs and MWCNTs have been presented these studies [6–10].

Flow through porous space have extensive applications in various fields like petroleum engineering, industries and geothermal operations. Flow regime in porous space is commonly characterized by a dimensionless number (Reynolds number). Darcy's law is valid to describe flow in porous space at low flow rates i.e., ($Re < 1$) (when flow rate and pressure gradient have linear relationship). This law predicts that viscous forces dominate over inertial forces in porous space. Mostly flow in porous space is described by Darcy's law, this law is not adequate for high flow rates. For higher flow rates the Forchheimer relation is used. Infact

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Nomenclature

u, v, w	velocity components	T_w	surface temperature
C_p	specific heat	T_∞	ambient temperature
F_l	Forchheimer parameter	κ_{fh}	Forchheimer permeability
ν_{nf}	kinematic viscosity	μ_{nf}	dynamic viscosity
σ^*	Stefan Boltzman constant	ρ_{nf}	density of nanofluid
$(\rho c_p)_{nf}$	heat capacity	k_{nf}	Effective thermal conductivity
q_w	heat flux	Nr	radiation parameter
λ	heat generation/absorption parameter	k^*	mean absorption coefficient
μ_f	dynamic viscosity	ρ_f	density of fluid
Pr	Prandtl number	Re_x	Reynold number
ω	porosity parameter	θ_w	temperature ratio variable
ϕ	volume fraction of nanomaterial	Nu_x	Nusselt number
C_{fx}	skin friction coefficient	q_r	radiative flux
τ_w	shear stress	k	thermal conductivity parameter
nf	nanofluid		

Forchheimer [11] introduced a new nonlinear contribution of velocity which is called Forchheimer term. Hayat et al. [12] investigated Darcy Forchheimer flow of ferromagnetic second grade fluid over a stretchable sheet. Some recent investigations about Darcy-Forchheimer flow can be seen in the studies [13–20].

In view of fast development of human society, numerous energy problems emerge for example environmental pollution and storage of global energy. Engineers and scientists are engaged in modeling new resources for sustainable energy. Solar energy is best source of renewable energy which offers a solution to this issue. Heat transport subject to Rosseland approximation has many applications in engineering, physics, nuclear plants and space technology, aerodynamic rockets, solar power technology, gas cooled nuclear reactors, counting combustion, furnace design, nuclear reactor protection and photo chemical reactors etc. Cortell [21] initially examined radiative flow over a stretchable surface. Sheikholeslami et al. [22] explored MHD flow of nanomaterial in subject to thermal radiation. Reddy et al. [23] studied impact of nonlinear radiation MHD flow of ferroliquids with temperature dependent viscosity. Few modern investigations on this topic can be mentioned in Refs. [24–30].

The purpose of present attempt is to model three-dimensional flow subject to SWCNTs and MWCNTs, Darcy-Forchheimer relation for porous space is considered. Heat transfer process is explored subject to nonlinear thermal radiation and heat generation/absorption. Outcomes of SWCNT and MWCNT with water as base fluid are achieved and compared. Xue model [2] of nanomaterial is employed. The resulting nonlinear expressions are solved by Optimal homotopy analysis method (OHAM) [31]. Heat transfer rate and surface drag forces are computed and discussed.

Problem statement

Three-dimensional Darcy-Forchheimer flow of water and carbon nanotubes are considered. Both single (SWCNTs) and multiple (MWCNTs) walls carbon nanotubes are studied. Flow is due to bidirectional stretchable surface. Heat transport process is examined through nonlinear thermal radiation and heat absorption/generation. Xue [2] model for nanoliquid transport is implemented. In cartesian coordinates system, the flow equations are governed by

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \tag{1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = \nu_{nf} \frac{\partial^2 u}{\partial z^2} - \frac{\nu_{nf}}{\kappa_{fh}} u - F_0 u^2, \tag{2}$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = \nu_{nf} \frac{\partial^2 v}{\partial z^2} - \frac{\nu_{nf}}{\kappa_{fh}} v - F_0 v^2, \tag{3}$$

$$(\rho c_p)_{nf} \left(u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} \right) = k_{nf} \frac{\partial^2 T}{\partial z^2} - \frac{\partial q_r}{\partial z} + Q_0(T - T_\infty), \tag{4}$$

with

$$\begin{aligned} u = U_w(x) = ax, \quad v = V_w(y) = by, \quad w = 0, \quad T = T_w, \quad \text{at } z = 0 \\ u = 0, \quad v = 0, \quad T \rightarrow T_\infty, \quad \text{at } z \rightarrow \infty. \end{aligned} \tag{5}$$

The theoretical model for nanoliquid transport proposed by Xue [2] gives:

$$\left. \begin{aligned} \mu_{nf} = \frac{\mu_f}{(1-\phi)^{2.5}}, \quad \nu_{nf} = \frac{\mu_{nf}}{\rho_{nf}}, \quad \rho_{nf} = \rho_f(1-\phi) + \rho_s\phi, \\ (\rho c_p)_{nf} = (\rho c_p)_f(1-\phi) + (\rho c_p)_s\phi, \quad \frac{k_{nf}}{k_f} = \frac{k_s + 2k_f - 2\phi(k_f - k_s)}{k_s + 2k_f + 2\phi(k_f - k_s)}. \end{aligned} \right\} \tag{6}$$

The radiative heat flux in terms of Rosseland approximation is [26]:

$$q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial T^4}{\partial r} = -\frac{16\sigma^*}{3k^*} T^3 \frac{\partial T}{\partial r}. \tag{7}$$

In above expression k^* represents the mean absorption coefficient and σ^* the Stefan-Boltzman constant.

Considering

$$\left. \begin{aligned} u = axf'(\eta), \quad v = ayg'(\eta), \quad w = -\sqrt{a}\bar{v}_r(f(\eta) + g(\eta)) \\ \theta = \frac{T - T_\infty}{T_w - T_\infty}, \quad \eta = \sqrt{\frac{a}{\nu_f}} z \end{aligned} \right\} \tag{8}$$

Eq. (1) is verified and Eqs. (2)–(5) take the form

$$\frac{1}{(1-\phi)^{2.5} \left(1 - \phi + \frac{\rho_{CNT}}{\rho_f} \phi \right)} (f''' - \omega f') + f''(f + g) - (1 + F_l)f'^2 = 0, \tag{9}$$

$$\frac{1}{(1-\phi)^{2.5} \left(1 - \phi + \frac{\rho_{CNT}}{\rho_f} \phi \right)} (g''' - \omega g') + g''(f + g) - (1 + F_l)g'^2 = 0, \tag{10}$$

$$\left[\frac{1}{\left(1 - \phi + \frac{(\rho c_p)_{CNT}}{(\rho c_p)_f} \phi \right)} \left[\frac{k_{nf}}{k_f} \theta'' + \lambda Pr \theta + Nr(\theta_w - 1) + 1 \right]^2 \right. \\ \left. \times \left\{ \begin{aligned} &3\theta^2(\theta_w - 1) \\ &+ \theta'(\theta(\theta_w - 1) + 1) \end{aligned} \right\} + Pr \theta'(f + g) = 0, \right] \tag{11}$$

$$\left\{ \begin{aligned} f(0) = 0, f'(0) = 1, f'(\infty) = 0, g(0) = 0, g'(\infty) = \alpha, \\ g'(\infty) = 0, \theta(0) = 0, \theta(\infty) = 1. \end{aligned} \right\} \quad (12)$$

Here $\omega (= \frac{v_f}{ak})$ represents the porosity variable, $Pr (= \frac{(\mu c_p)_f}{k_f})$ the Prandtl number, $\lambda (= \frac{Q_0}{a(\rho c_p)_f})$ the heat generation/absorption variable, $F_l (= \frac{C_b}{\sqrt{k_{fb}}})$ the Forchheimer parameter, $Nr (= \frac{16\sigma^* T_\infty^3}{3k^* k_f})$ the radiation variable and $\theta_w (= \frac{T_w}{T_\infty})$ the dimensionless temperature ratio variable.

Quantities of physical interest

Skin friction coefficients

Mathematically we have

$$C_{fx} = \frac{2\tau_{wx}}{\rho_f U_w^2}, \quad C_{fy} = \frac{2\tau_{wy}}{\rho_f U_w^2}, \quad (13)$$

where

$$\tau_{wx} = \mu_{nf} \left(\frac{\partial u}{\partial z} \right) \Big|_{z=0}, \quad \tau_{wy} = \mu_{nf} \left(\frac{\partial v}{\partial z} \right) \Big|_{z=0}. \quad (14)$$

Inserting Eq. (14) in Eq. (13) one has

$$\left\{ \begin{aligned} C_{fx} Re_x^{0.5} &= \frac{2f''(0)}{(1-\phi)^{2.5}}, \\ C_{fy} Re_y^{0.5} &= \frac{2g''(0)}{\alpha^2 (1-\phi)^{2.5}}. \end{aligned} \right\} \quad (15)$$

Nusselt number

It is defined as

$$Nu_x = \frac{xq_w}{k_f(T_w - T_\infty)}, \quad (16)$$

where

$$q_w = -k_{nf} \left(\frac{\partial T}{\partial z} \right) \Big|_{z=R} + (q_r)_w. \quad (17)$$

Putting Eq. (17) in Eq. (16) we have

$$Nu_x Re_x^{-0.5} = - \left(\frac{k_{nf}}{k_f} + Nr(\theta(0)(\theta_w - 1) + 1)^3 \right) \theta'(0). \quad (18)$$

In above expressions τ_{wx} and τ_{wy} represent shear stresses in x- and y-directions, q_w the heat flux and Re_x and Re_y the local Reynolds numbers.

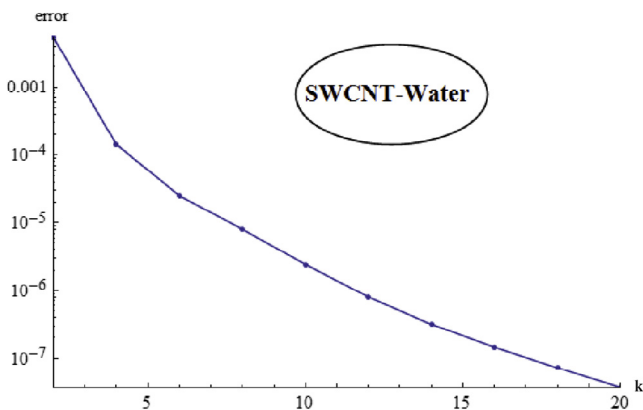


Fig. 1. SWCNTs residual error plots.

OHAM solutions

Initial guesses and operators for the desired solutions are

$$f_0 = 1 - e^{-\eta}, \quad g_0 = \alpha(1 - e^{-\eta}), \quad \theta_0 = e^{-\eta}, \quad (19)$$

$$L_f = \frac{d^3 f}{d\eta^3} - \frac{df}{d\eta}, \quad L_g = \frac{d^3 g}{d\eta^3} - \frac{dg}{d\eta}, \quad L_\theta = \frac{d^2 \theta}{d\eta^2} - \theta. \quad (20)$$

The non-zero auxiliary variables h_f, h_g and h_θ in homotopy solutions indicate the convergence region. To get the optimal estimations of h_f, h_g and h_θ we have utilized the concept given by Liao [31]. The average squared residual errors of the k th order approximation is as follow:

$$\hat{E}_k = \frac{1}{N+1} \sum_{i=0}^N \left[N_f \left(\sum_{j=0}^k (f_j), \sum_{j=0}^k (g_j) \right) \Big|_{\eta=i\delta\eta} \right]^2, \quad (21)$$

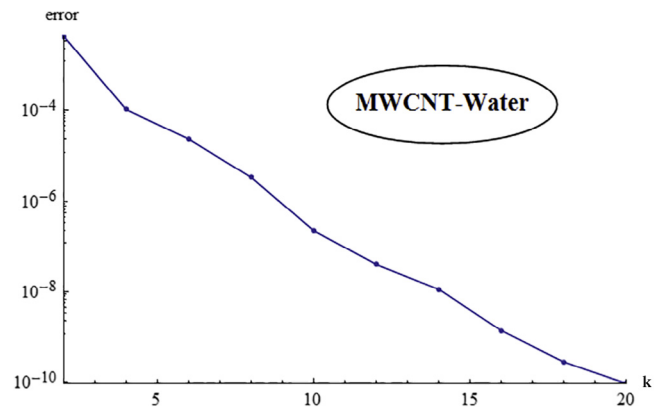


Fig. 2. MWCNTs residual error plots.

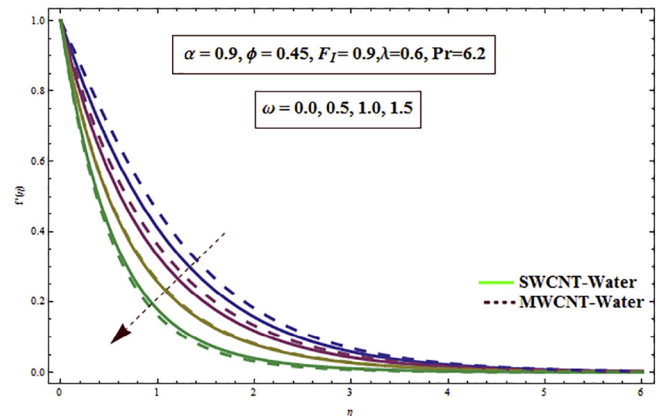


Fig. 3. $f''(\eta)$ via ω .

Table 1
Thermophysical properties for water and SWCNTs and MWCNTs.

Physical properties	Base fluid	Nanoparticles	
	Water	SWCNT	MWCNT
ρ (kg/m ³)	997	2600	1600
c_p (j/kg K)	4179	425	796
k (w/mK)	0.613	6600	3000

Table 2
Estimations of average square residual errors for SWCNTs when $\omega = 0.4$, $\phi = 0.1$ and $\lambda = 0.1$.

k	ϵ_k^f	ϵ_k^g	ϵ_k^θ
2	3.32008×10^{-4}	2.76555×10^{-7}	5.16469×10^{-3}
6	8.95163×10^{-6}	2.08492×10^{-9}	1.6136×10^{-5}
10	9.94229×10^{-7}	2.06756×10^{-10}	1.43437×10^{-6}
16	8.31798×10^{-8}	1.72592×10^{-11}	6.22315×10^{-8}
24	5.72362×10^{-9}	1.18649×10^{-12}	4.76692×10^{-9}
30	9.72581×10^{-10}	2.01331×10^{-13}	8.03829×10^{-10}

Table 3
Estimations of average square residual errors for MWCNTs when $\omega = 0.4$, $\phi = 0.1$ and $\lambda = 0.1$.

k	ϵ_k^f	ϵ_k^g	ϵ_k^θ
2	8.10583×10^5	8.97036×10^{-9}	4.22733×10^{-3}
6	2.80161×10^{-7}	6.45576×10^{-11}	2.38942×10^{-5}
10	3.81951×10^{-9}	8.11443×10^{-13}	2.20259×10^{-7}
16	1.3476×10^{-11}	2.82062×10^{-15}	1.39151×10^{-9}
24	1.34658×10^{-14}	2.81155×10^{-18}	1.87558×10^{-12}
30	9.54607×10^{-17}	1.98982×10^{-20}	2.21502×10^{-14}

$$\epsilon_k^g = \frac{1}{N+1} \sum_{i=0}^N \left[N_g \left(\sum_{j=0}^k (f_j), \sum_{j=0}^k (g_j) \right)_{\eta=i\delta\eta} \right]^2, \tag{22}$$

$$\epsilon_k^\theta = \frac{1}{N+1} \sum_{i=0}^N \left[N_\theta \left(\sum_{j=0}^k (f_j), \sum_{j=0}^k (g_j), \sum_{j=0}^k (\theta_j) \right)_{\eta=i\delta\eta} \right]^2. \tag{23}$$

Total residual error is [31]:

$$\epsilon_k^t = \epsilon_k^f + \epsilon_k^g + \epsilon_k^\theta. \tag{24}$$

Here ϵ_k^t signifies total residual error. The values of convergence control variables for momentum and energy expressions are $h_f = -0.861563$, $h_g = -0.679111$ and $h_\theta = -0.19295$ and $h_f = -0.751529$, $h_g = -0.687246$ and $h_\theta = -0.19914$ for both the cases i.e., (SWCNTs and MWCNTs). The total averaged squared residual error for both SWCNTs and MWCNTs are $\epsilon_k^t = 5.49697 \times 10^{-3}$ and $\epsilon_k^t = 4.30848 \times 10^{-3}$ respectively. Figs. 1 and 2 represent average square residual errors for SWCNTs and MWCNTs.

Table 4
Numerical values of $(Cf_x Re_x^{0.5})$ for various parameters.

ϕ	ω	F_l	α	$-Cf_x Re_x^{0.5}$		$-Cf_y Re_y^{0.5}$			
				SWCNTs	MWCNTs	SWCNTs	MWCNTs		
0.1	0.3	0.5	0.4	2.90211	2.86991	1.1399	1.16566		
0.2				3.81395	3.71753	1.59567	1.67281		
0.3				5.14122	4.90268	2.37541	2.56624		
				2.80485	2.76345	1.21771	1.25083		
				2.90211	2.86991	1.1399	1.16566		
				2.99937	2.97637	1.062099	1.08049		
		0.1	0.3	0.2	2.77197	2.73978	1.20237	1.22812	
					2.83704	2.80484	1.17113	1.19689	
					2.93464	2.90245	1.12428	1.15004	
					2.88042	2.84822	0.624173	0.637052	
					0.4	2.90211	2.86991	1.1399	1.16566
					0.6	2.9238	2.8916	1.54718	1.58582

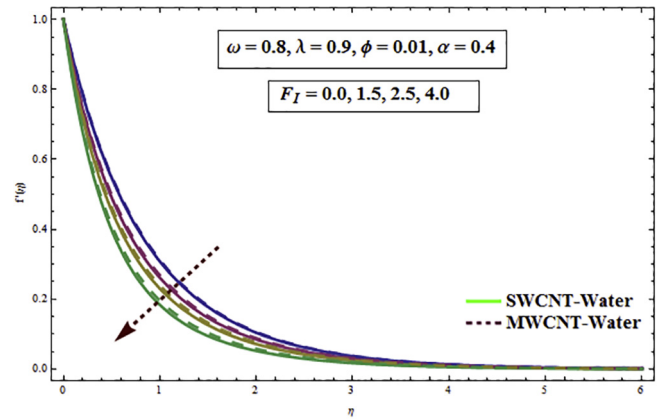


Fig. 4. $f'(\eta)$ via F_l .

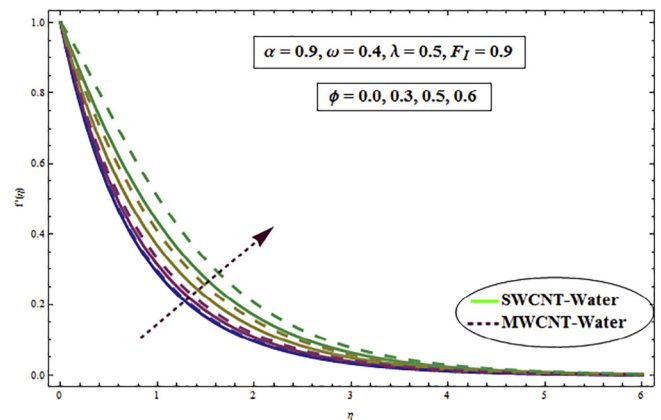


Fig. 5. $f'(\eta)$ via ϕ .

Discussion

This section highlights influences of various physical variables like heat generation/absorption parameter (λ), volume fraction (ϕ), porosity parameter (ω), non-uniform inertia coefficient (F_l), temperature ratio parameter (θ_w) and radiation parameter (Nr) on velocities ($f'(\eta), g'(\eta)$) and temperature ($\theta(\eta)$) for both SWCNTs and MWCNTs. Table 1 characterizes the thermophysical properties of continuous phase base fluid and SWCNTs and MWCNTs. Tables 2 and 3 provide total square residual error for both (SWCNTs) and (MWCNTs) respectively for distinct order of approximations. Here error decays for higher order of approximations. Table 4 shows

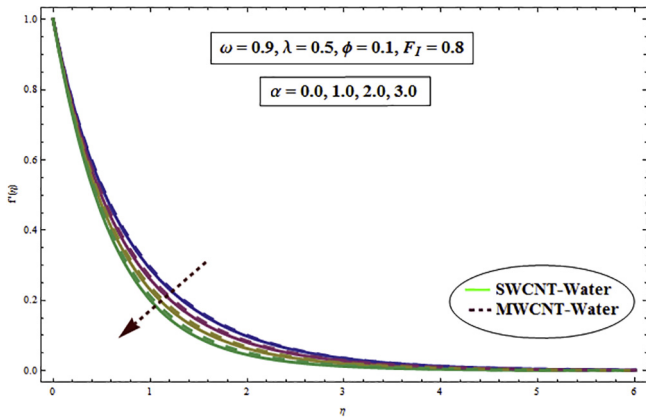


Fig. 6. $f'(\eta)$ via α .

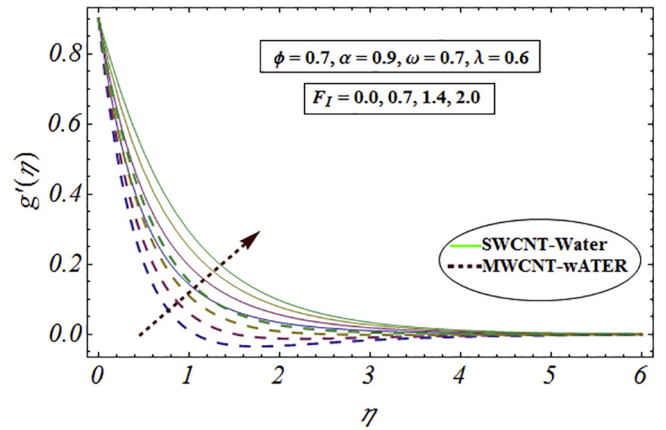


Fig. 9. $g'(\eta)$ via F_I .

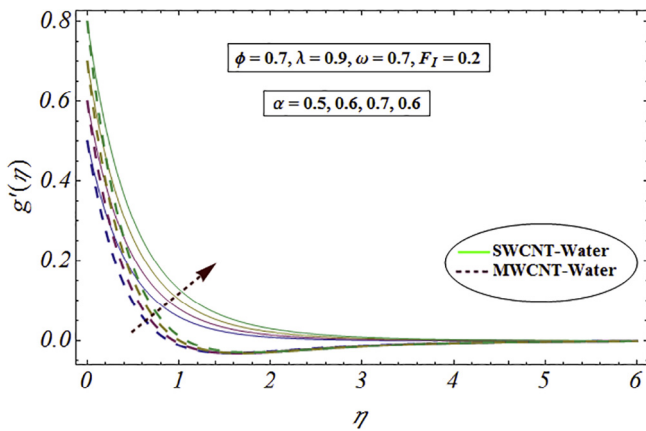


Fig. 7. $g'(\eta)$ via α .

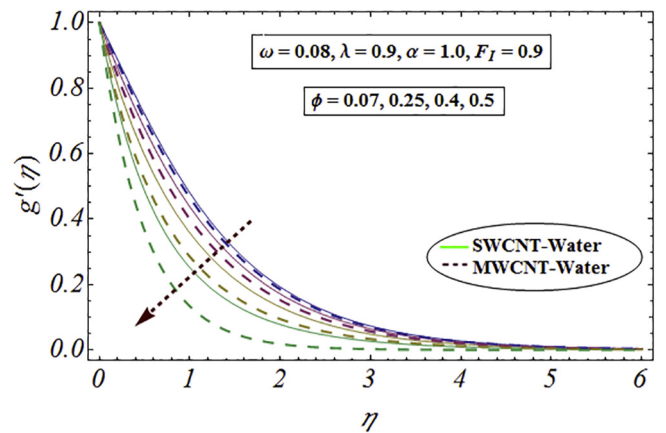


Fig. 10. $g'(\eta)$ via ϕ .

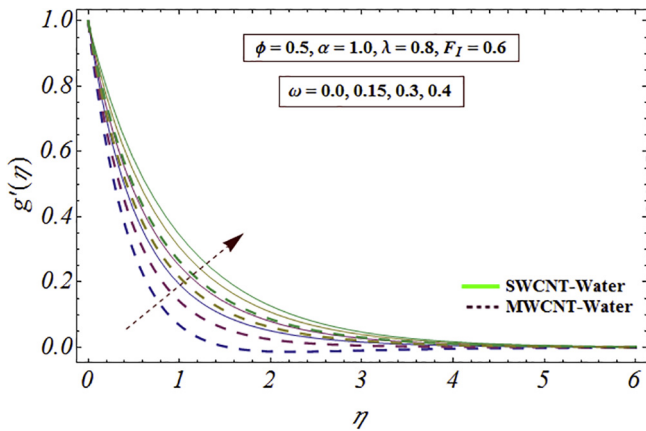


Fig. 8. $g'(\eta)$ via ω .

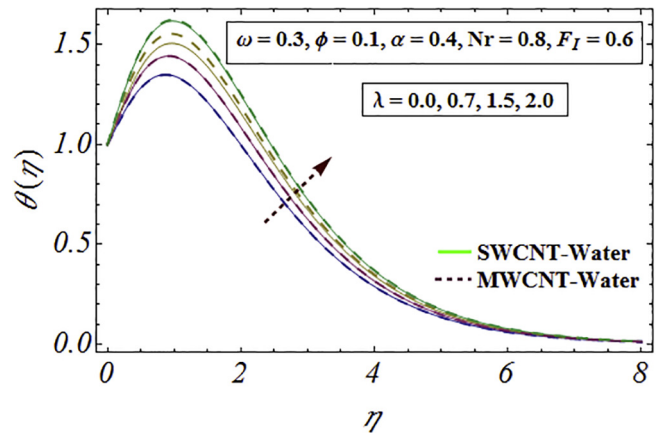


Fig. 11. $\theta(\eta)$ via λ (heat source case).

numerical results of surface drag force (skin friction coefficient) for different physical variables. From Table 4 it is found that surface drag force decreases for larger nanoparticle volume fraction and porosity parameter. However opposite behavior is noticed for larger Forchhiemer number. Impact of (ω) on ($f'(\eta)$) is shown in Fig. 3. It is noted that with the enhancement of (ω) the velocity declines for both SWCNTs and MWCNTs. Fig. 4 is sketched to investigate velocity profile for values of Forchhiemer parameter. Here velocity field decays for larger Forchhiemer parameter. Physically

for larger Forchhiemer parameter the inertial force enhances and therefore velocity of fluid decays. Nanoparticle volume fraction (ϕ) impact on velocity ($f'(\eta)$) is depicted in Fig. 5. It is examined that velocity and associated layer thickness are enhanced for both SWCNTs and MWCNTs. Further velocity of fluid particle dominant in case of MWCNTs when compared with SWCNTs. Figs. 6 and 7 demonstrate that how the velocity distribution varies by (α).

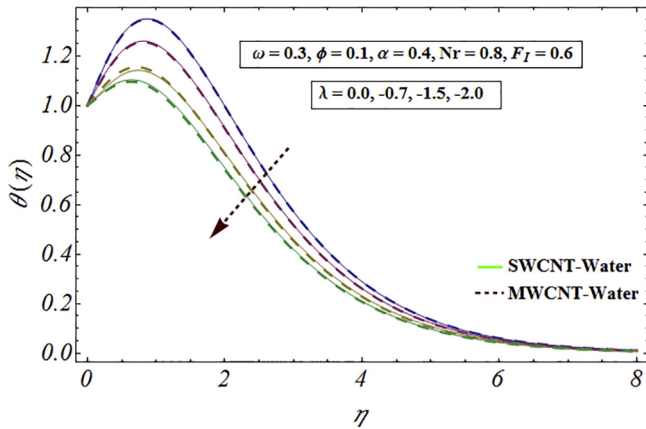


Fig. 12. $\theta(\eta)$ via λ (heat sink case).

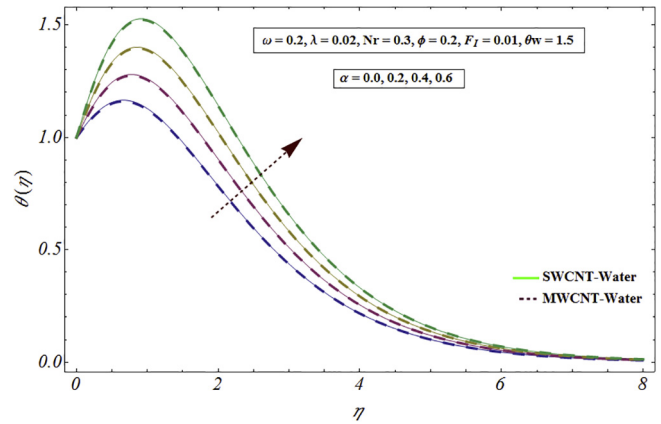


Fig. 15. $\theta(\eta)$ via α .

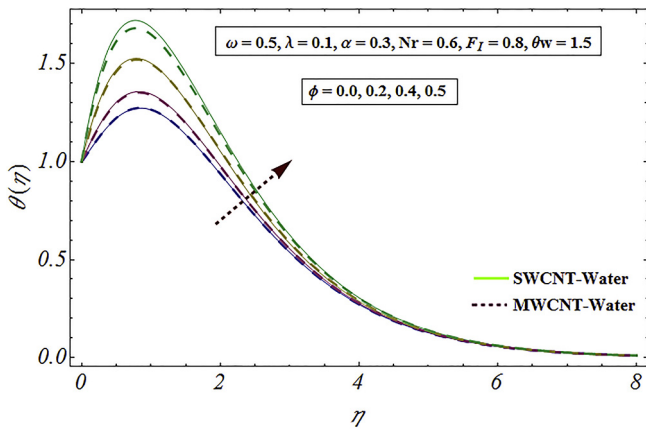


Fig. 13. $\theta(\eta)$ via ϕ .

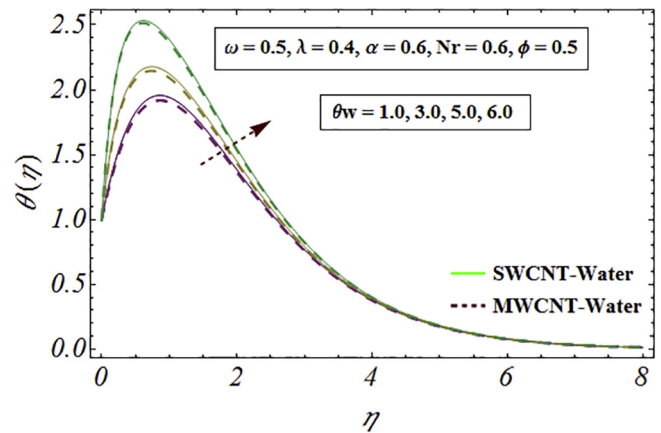


Fig. 16. $\theta(\eta)$ via θ_w .

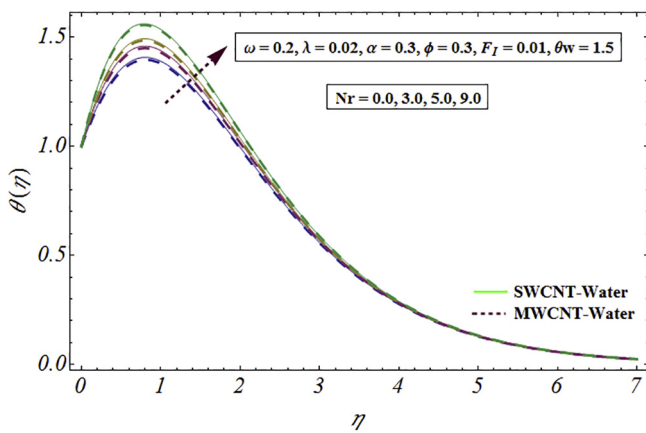


Fig. 14. $\theta(\eta)$ via Nr .

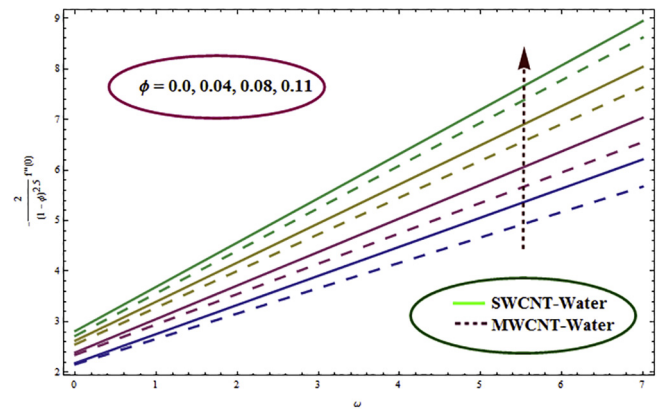


Fig. 17. $Cf_x Re_x^{0.5}$ via ϕ and ω .

Velocity and associated layer thickness in x -direction decayed via (α) for both SWCNTs and MWCNTs. Reverse behavior is noticed in y -direction for both SWCNTs and MWCNTs (see Fig. 7). Fig. 8 declares porosity variable effects on velocity field $g'(\eta)$. Here velocity field increases for higher estimation of porosity variable for both SWCNTs and MWCNTs. Fig. 9 is drawn to interpret impact

of (F_I) on velocity $(g'(\eta))$. Here $(g'(\eta))$ is increasing function of (F_I) . Physically higher estimation of (F_I) constitutes larger inertial forces which oppose the flow motion and therefore velocity field decays. Influence of nanoparticle volume fraction (ϕ) on $(g'(\eta))$ is shown in Fig. 10. Through Fig. 10 the velocity decays when nanoparticle volume fraction (ϕ) increases for both SWCNTs and MWCNTs. It is also observed that velocity dominates in case of MWCNTs when compared with SWCNTs. Consequences of heat

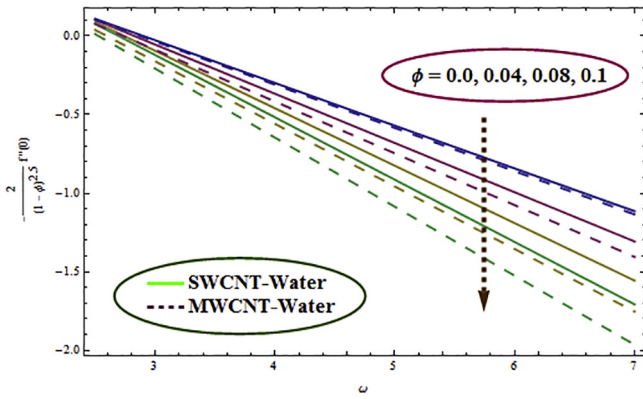


Fig. 18. $C_f, Re_y^{0.5}$ via ϕ and ω .

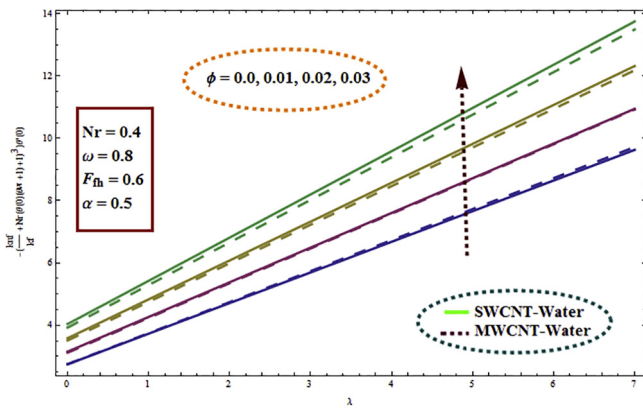


Fig. 19. $Nu Re_x^{-0.5}$ via ϕ and λ .

source ($\lambda > 0$) and heat sink ($\lambda < 0$) variables on temperature ($\theta(\eta)$) are captured in Figs. 11 and 12. Here temperature of liquid rises for larger heat source ($\lambda > 0$) while it decays with heat sink. Fig. 13 presents the impact of nanoparticle volume fraction (ϕ) on ($\theta(\eta)$). An increasing behavior of thermal diffusivity is observed for an increment in nanoparticle volume fraction. Such enhancement in thermal diffusivity provides stronger thermal field. Also stronger thermal layer is noticed for both MWCNTs and SWCNTs. Moreover thermal field is stronger in case of MWCNTs when compared with SWCNTs. From Fig. 14 it is clearly scrutinized that a stronger thermal field is generated by larger estimation of (Nr). Physically more kinetic energy occurs in this process. That is why thermal field increases for both single wall carbon nanotubes and multi wall carbon nanotubes. Fig. 15 displays effect of (α) on ($\theta(\eta)$). Here temperature is increased function of (α) for both SWCNTs and MWCNTs. Fig. 16 demonstrates that for larger estimation of (θ_w), thermal field and thickness of layer are enhanced for both SWCNTs and MWCNTs. Moreover thermal field is more in case of MWCNTs than SWCNTs. Figs. 17–19 explains the influence of different physical variables like nanoparticle volume fraction, porosity variable and heat generation absorption variable on surface drag forces (skin friction coefficients) and heat transfer rate (Nusselt number). We observed that surface drag force decays for higher (ϕ) along x -direction while it increases in y -direction (see Figs. 17 and 18). We also noticed that heat transfer rate has larger for nanoparticle volume fraction and porosity. Physically for larger porosity variable the motion of liquid particles faced more resistance. Also internal energy of particle enhances for higher thermal diffusivity which is directly proportional to the nanoparticle volume fraction. Therefore heat transfer rate enhances (see Fig. 19).

Final conclusions

The main points of present flow are:

- Velocity field decays for larger estimations of porosity and ratio of stretching variables.
- Estimations of F_l on velocity and temperature are opposite.
- Velocity components along x and y axes have reverse behavior for nanoparticles volume fraction.
- Temperature increases for an enhancement in volume fraction (ϕ).
- Increasing values of temperature ratio and radiation variables lead to stronger temperature distribution.
- $(C_f_x Re_x^{-\frac{1}{2}})$ increases for estimations of (ϕ) and (ω).
- Heat transfer rate is enhanced for larger nanoparticle volume fraction.

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