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Frozen apsidal line orbits around tiaxial Moon with coupling quadrupole nonlinearity

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ABSTRACT

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In this research paper, new families of frozen orbits of a satellite orbiting the oblate as well as triaxial Moon are investigated. The Hamiltonian of the problem is constructed including the zonal harmonic coefficients of the Moon's gravity field up to J_4 and its triaxiality term $J_{2,2}$. Using two successive canonical Lie transforms, the short and long periodic terms are eliminated from the Hamiltonian. The secular terms are retained up to first order plus the coupling quadrupole nonlinearity. New families of the critical roots of inclination are revealed, one of them is very close the polar orbits and the other is near to the usual critical inclination. The variations in the critical inclination due to the change in the eccentricity, in the semi-major axis and in the argument of periaxis are studied. A family of frozen apsidal line orbits is obtained and then is represented graphically. To guarantee these orbits, the solution for the periaxis argument is solved. This actually set out some restrictions on choosing the inclination satisfying the frozen argument of periaxis orbits. The perturbations in the critical inclination become significant for the high lunar orbits.

Introduction

The orbit that has no secular change in eccentricity e and argument of periaxis ω is called frozen orbit. In more precise phrase: These drift rates have been minimized by choosing carefully the orbital elements. It characterized by constant values of a and e and the inclination I .

Yang computed frozen orbits due to Earth's dynamical parameters J_n , $n = 2, 3$ [1]. He used Brouwer's results [2]. Although the constraints on frozen orbits are not strict, it requires a very small eccentricity. Considering the second zonal harmonics only, the frozen orbits have usual critical inclinations (i.e., 63.4° or 116.6°). Considering the temporal variations of the elements I and ω keeping terms up to $\mathcal{O}(J_2)$, one can verify that $d\omega/dt \rightarrow 0$ as $I_c \cong 63.4$ so that I_c is the critical inclination. Hence, near to I_c the long period behaviour of ω represents a libration with minimum period $2\pi/k \simeq 102$ years, or generally a period of order $J_2^{-3/2}$ and approaches ∞ as $e \rightarrow 0$. The corresponding motion in I has an amplitude of order $J_2^{1/2}$ (provided e is apart from zero). Similar reasoning holds for e . Away from I_c the argument of periaxis ω circulates with a period of order J_2^{-1} so that the amplitudes of the corresponding motion in I and e are of order J_2 . Revealing that the perturbations in I and e near to I_c are larger than elsewhere by a factor

$J_2^{-1/2} \cong 30$. Including J_4 then the coefficient J_2^3 will be $J_2(J_4 + J_2^2)$, and since $(J_4 + J_2^2) < 0$, then the equilibrium position becomes stable at $\pm \pi/2$.

There are many works dealing with the critical inclination, and it seems worth to sketch some of these works. Hori and Garfinkel utilized the von Zeipel method and the Bohlin technique. They obtained solutions including J_2 and J_4 in terms of elliptic integrals and up to $J_2^{1/2}$ [3,4]. Izsak investigated the qualitative behaviour in the phase plane including J_2 and J_4 [5]. Aoki investigated the behaviour in the phase plane for small and moderate eccentricities but using unsatisfactory assumption that $J_n \equiv \mathcal{O}(n)$, see [6,7], Hoots and Fitzpatrick [8], Delhase and Henrard [9,10], Henrard [11] and Delhase and Morbidelli [12].

As an applications of these developed ideas on the lunar frozen orbits, Park and Junkins [13]. For low-altitude orbiters about planetary satellites, see Scheeres et al. [14]. San-Juan et al. [15]. Paskowitz and Scheeres accounts for the perturbation arising from first zonal harmonics [16]. For more details on the problem and related issues refer to Lara et al. [17–20], Tzirtzi et al. [21,22], Enceladus [23], Liu et al. [24,25], Carvalho et al. [26], Carlo et al. [27], Pardal et al. [28] and Rahoma et al. [29,30].

Finally the concept of the frozen orbits can be used in designing

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orbits for certain missions in the three body problem see [31]. It also can be extended to orbits that have Resonant capture [32,33].

After this brief introduction, the article is displayed as follows: In Section “The Hamiltonian of the problem”, we constructed the Hamiltonian of a orbiter retaining the terms up to J_4 as well as the triaxiality of Moon. In Section “Brief note on Lie transformation”, we expressed the Hamiltonian in the Delaunay canonical-set. In Section “Short period transformation”, we normalized the considered Hamiltonian via removing short period terms, namely the mean anomaly. In Section “Elimination of node”, we removed the longitude of the ascending node Ω . In Section “The apsidal frozen line”, we constructed the dynamical equation for the frozen argument of pericentre. In Section “Solution for the inclination”, we solved dynamical equation for the critical inclination and analysed it in the subsequent subsections. Finally in Section “Conclusion” we gave a conclusion.

The Hamiltonian of the problem

Consider a satellite of mass m moves with an angular velocity ω_s around an oblate as well as tiaxial Moon with a gravitational parameter μ , then its Hamiltonian function is given

$$\mathcal{H} = \frac{m^2}{2}(\dot{\mathbf{r}} \cdot \dot{\mathbf{r}}) - \omega_s \cdot (\mathbf{r} \times \dot{\mathbf{r}}) \frac{\mu}{r} - \frac{\mu}{r} - \mathcal{R}(\mathbf{r}) \quad (1)$$

where \mathbf{r} is the radius vector of the satellite with respect to the Moon center, its magnitude is r and its orbital velocity is $\dot{\mathbf{r}}$. The function $\mathcal{R}(\mathbf{r})$ represents any considered perturbations. Here in our model we will consider $\mathcal{R}(\mathbf{r})$ so as to include the Moon' oblateness up to fourth zonal harmonic coefficients J_4 as well as its triaxiality term, namely terms factored by $J_{2,2}$. In this light $\mathcal{R}(\mathbf{r})$ becomes,

$$\begin{aligned} \mathcal{R}(\mathbf{r}) = & \frac{1}{4} \frac{\mu}{r^3} J_2 R_M^2 [(3S^2 - 2) - 3S^2 \cos F_{2,2,0}] + \frac{1}{8} \frac{\mu}{r^4} J_3 R_M^3 [(15S^3 - 12S) \sin F_{1,1,0} \\ & - 5S^3 \sin F_{3,3,0}] + \frac{1}{64} \frac{\mu}{r^5} J_4 R_M^4 [(24 - 120S^2 + 105S^4) \\ & + (120S^2 - 140S^4) \cos F_{2,2,0} + 35S^4 \cos F_{4,4,0}] \\ & - \frac{\mu J_{2,2}}{2a} \left(\frac{R_M}{a} \right)^2 \left(\frac{a}{r} \right)^3 \left[\frac{10}{3} (2 - 3S^2 + 3S^2 \cos F_{2,2,0}) + 3(2S^2 \cos F_{0,0,2} \right. \\ & \left. + (1-C)^2 \cos F_{2,2,-2}) \right] - \frac{\mu}{4a} \left(\frac{\omega_s}{n} \right)^2 \left(\frac{r}{a} \right)^3 \left[\frac{3}{2} (2S^2 \cos F_{0,0,2} \right. \\ & \left. + (1-C)^2 \cos F_{2,2,-2}) \right] \end{aligned}$$

where J_2 , J_3 , J_4 are the considered zonal harmonic coefficients of the Moon's gravity field. They are assumed as small parameters. (a , I , ω , f) are some of usual Keplerian elements, the first three are defined earlier and the fourth is the true anomaly, $n = \sqrt{\mu/a^3}$ is the instantaneous satellite mean motion and R_M is the equatorial raduis of the Moon. $C = \cos I$, $S = \sin I$, also adopting the notation $F_{i,j,k} = if + j\omega + k\Omega$, where Ω is the longitude of the ascending node (Tables 1–3).

Transformation to Delaunay canonical-variables

Introducing the Delaunay canonical-set (l , g , h , L , G , H) defined as;

$$\begin{aligned} l &= M, \quad g = \omega, \quad h = \Omega, \\ L &= (\mu a)^{\frac{1}{2}}, \quad G = (\mu a)^{\frac{1}{2}}(1-e^2)^{\frac{1}{2}}, \quad H = (\mu a)^{\frac{1}{2}}(1-e^2)^{\frac{1}{2}} \cos I. \end{aligned}$$

Then Eq. (1) can now written as

Table 1

The effects of the some selected eccentricities and the semimajor axes on the critical inclinations I_{ci} , $i = 1, 2, 3, 4$ for all range of argument of periapsis.

a	e			
		I_{c1}	0.1	0.2
2000 km	I_{c1}	(64.3397°, 64.3426°)	(64.3386°, 64.3437°)	(64.3382°, 64.3441°)
	I_{c2}	(89.9976°, 89.7206°)	(89.9849°, 89.6294°)	(89.9814°, 89.5939°)
	I_{c3}	(115.66°, 115.657°)	(115.661°, 115.656°)	(115.662°, 115.656°)
	I_{c4}	(90.0024°, 90.2794°)	(90.0151°, 90.3706°)	(90.0186°, 90.406°)
4000 km	I_{c1}	(64.2546°, 64.4409°)	(64.1864°, 64.5094°)	(64.1567°, 64.5389°)
	I_{c2}	(89.8709°, 87.7528°)	(89.8277°, 87.0135°)	(89.8109°, 86.7243°)
	I_{c3}	(115.745°, 115.559°)	(115.814°, 115.491°)	(115.843°, 115.461°)
	I_{c4}	(90.1291°, 92.2472°)	(90.1723°, 92.9865°)	(90.1891°, 93.2757°)
6000 km	I_{c1}	(63.442°, 65.6177°)	(62.8224°, 66.7724°)	(62.5741°, 67.4164°)
	I_{c2}	(89.557°, 82.0498°)	(89.4122°, 78.9372°)	(89.3559°, 77.5326°)
	I_{c3}	(116.558°, 114.382°)	(117.178°, 113.228°)	(117.426°, 112.584°)
	I_{c4}	(90.443°, 97.9502°)	(90.5878°, 101.063°)	(90.6441°, 102.467°)

Table 2

The effects of the some selected eccentricities and the argument of periapsis on the critical inclinations I_{ci} , $i = 1, 2, 3, 4$ for a range of semi-major axes.

ω	e			
		I_{c1}	0.1	0.2
0.0°	I_{c1}	(46.3397°, 63.442°)	(64.3386°, 62.8224°)	(64.3382°, 62.5741°)
	I_{c2}	Φ	Φ	Φ
	I_{c3}	(115.66°, 116.558°)	(115.661°, 117.178°)	(115.662°, 117.426°)
	I_{c4}	Φ	Φ	Φ
45°	I_{c1}	(64.3412°, 64.4063°)	(64.3412°, 64.3871°)	(64.3411°, 64.3726°)
	I_{c2}	Φ	Φ	Φ
	I_{c3}	(115.659°, 115.594°)	(115.659°, 115.613°)	(115.659°, 115.627°)
	I_{c4}	Φ	Φ	Φ
90°	I_{c1}	(64.3426°, 65.6177°)	(64.3437°, 66.7724°)	(64.3441°, 67.4164°)
	I_{c2}	(89.7206°, 82.0498°)	(89.6294°, 78.9372°)	(89.5939°, 77.5326°)
	I_{c3}	(115.657°, 114.382°)	(115.656°, 113.228°)	(115.656°, 112.584°)
	I_{c4}	(89.7206°, 82.0498°)	(89.6294°, 78.9372°)	(89.5939°, 77.5326°)

Table 3

The effects of the some selected eccentricities and the semi-major axes on the critical inclinations I_{ci} , $i = 1, 2, 3, 4$ for all range of argument of periapsis.

a	ω			
		I_{c1}	0.0°	45°
2000 km	I_{c1}	(64.3397°, 64.3382°)	(64.3412°, 64.3411°)	(64.3426°, 64.3441°)
	I_{c2}	Φ	Φ	(89.7206°, 89.5939°)
	I_{c3}	(115.66°, 115.662°)	(115.659°, 115.659°)	(115.657°, 115.656°)
	I_{c4}	Φ	Φ	(90.2794°, 90.4061°)
4000 km	I_{c1}	(64.2546°, 64.1567°)	64.3468°, 64.3439°	(64.4409°, 64.5389°)
	I_{c2}	Φ	Φ	(87.7528°, 86.7243°)
	I_{c3}	(115.745°, 115.843°)	(115.653°, 115.656°)	(115.559°, 115.461°)
	I_{c4}	Φ	Φ	(92.2472°, 93.2757°)
6000 km	I_{c1}	(63.442°, 62.5741°)	(64.3397°, 64.3382°)	(65.6177°, 67.4164°)
	I_{c2}	Φ	Φ	(82.0498°, 77.5326°)
	I_{c3}	64.3397°, 64.3382°	(64.3412°, 64.3411°)	(64.3426°, 64.3441°)
	I_{c4}	Φ	Φ	(89.7206°, 89.5939°)

$$\begin{aligned} \mathcal{H} = & -\frac{\mu^2}{2L^2} \left(\frac{\omega_s}{n} \right)^2 \sqrt{1-e^2} C + \frac{\mu^4 R_M^2}{4L^6} J_2 \left(\frac{a}{r} \right)^3 [(3S^2-2)-3S^2 \cos F_{2,2,0}] \\ & + J_3 \frac{\mu^5 R_M^3}{8L^8} \left(\frac{a}{r} \right)^4 [(15S^3-12S) \sin F_{1,1,0}-5S^3 \sin F_{3,3,0}] \\ & + J_4 \frac{\mu^6 R_M^4}{64L^{10}} \left(\frac{a}{r} \right)^5 [(24-120S^2+105S^4)+(120S^2-140S^4) \cos F_{2,2,0} \\ & + 35S^4 \cos F_{4,4,0}] - \frac{J_{2,2} R_M^2 \mu^3}{2a} \left(\frac{a}{r} \right)^3 \left[\frac{10}{3}(2-3S^2+3S^2 \cos F_{2,2,0}) \right. \\ & \left. + 3(2S^2 \cos F_{0,0,2}+(1-C)^2 \cos F_{2,2,-2}) \right] \\ & - \frac{\mu}{4a} \left(\frac{\omega_s}{n} \right)^2 \left(\frac{r}{a} \right)^3 \left[\frac{3}{2}(2S^2 \cos F_{0,0,2}+(1-C)^2 \cos F_{2,2,-2}) \right. \\ & \left. + (2-3S^2+3S^2 \cos F_{2,2,0})+2(1+C)^2 \cos F_{2,2,2} \right] \end{aligned} \quad (2)$$

Now, the Hamiltonian (2) can be written as

$$\mathcal{H} = \mathcal{H}_0 + \mathcal{H}_1 \quad (3)$$

where \mathcal{H}_0 is the integrable part of the problem

$$\mathcal{H}_0 = -\frac{\mu^2}{2L^2} \quad (4)$$

and

$$\begin{aligned} \mathcal{H}_1 = & \frac{1}{4} \frac{A_{1,2}}{L^6} \Psi^3 [(3S^2-2)-3S^2 \cos F_{2,2,0}] + \frac{1}{8} \frac{A_{2,3}}{L^8} \Psi^4 [(15S^3-12S) \sin F_{1,1,0} \\ & -5S^3 \sin F_{3,3,0}] + \frac{1}{64} \frac{A_{2,4}}{L^{10}} \Psi^5 [(105S^4-102S^2+24) \\ & + (-140S^4+120S^2) \cos F_{2,2,0}+35S^4 \cos F_{4,4,0}] \\ & - \frac{J_{2,2} R_M^2 \mu^3}{2a} \frac{1}{L^4} \Psi^3 \left[\frac{10}{3}(2-3S^2+3S^2 \cos F_{2,2,0})+3(2S^2 \cos F_{0,0,2} \right. \\ & \left. +(1-C)^2 \cos F_{2,2,-2}) \right] - \frac{\mu^2}{L^2} \left(\frac{\omega_s}{n} \right) \sqrt{1-e^2} C \\ & - \frac{\mu}{4a} \left(\frac{\omega_s}{n} \right)^2 \Psi^3 \left[\frac{3}{2}(2S^2 \cos F_{0,0,2}+(1-C)^2 \cos F_{2,2,-2}) \right. \\ & \left. + (2-3S^2+3S^2 \cos F_{2,2,0})+2(1+C)^2 \cos F_{2,2,2} \right] \end{aligned} \quad (5)$$

where $\Psi = \frac{a}{r}$ and

$$A_{1,2} = \mu^4 R_M^2 J_2, \quad A_{1,2,2} = \mu^3 R_M^2 J_{2,2}, \quad A_{2,3} = 2\mu^5 R_M^3 J_3, \quad A_{2,4} = 2\mu^6 R_M^4 J_4 \quad (6)$$

are zero-order parameters.

Brief note on Lie transformation

The canonical transformations, namely here Lie transforms are usually performed so as to normalize the Hamiltonian of the problem and left the problem mathematically tractable. It consists of removing all or some of the angular variables from the Hamiltonian. We will perform two transformations. The first is to eliminate the true anomaly, and the second transformation is to remove Ω . We leave ω without averaging because we aim to study the frozen apsidal line orbits, i.e. we will compute $\frac{\partial \mathcal{H}^{**}}{\partial G}$ and set to zero which is the criteria of the frozen orbits, namely $\dot{g} = -\frac{\partial \mathcal{H}^{**}}{\partial G} = 0$

$$\mathcal{H}_0^* = \mathcal{H}_0$$

$$\mathcal{H}_n^* = \widetilde{\mathcal{H}}_n + (\mathcal{H}_0; W_n)$$

where W_n are the generating functions of the transformation

$$\widetilde{\mathcal{H}}_n = \mathcal{H}_n + \sum_{j=1}^{n-1} \{C_{j-1}^{n-1} (\mathcal{H}_{n-j}; W_j) + C_j^{n-1} G_j \mathcal{H}_{n-j}\}$$

where C_{j-1}^{n-1} are the binomial coefficients, and $G_j = L_j - \sum_{m=0}^{j-2} C_{j-1}^{j-1} L_{m+1} G_{j-m-1}$. It is clear that G_j is a recursive formula

of Lie derivative given by Poisson bracket as $L_W \mathcal{H} = (\mathcal{H}, W)$.

Let l be the fast variable in \mathcal{H} . We choose \mathcal{H}_n^* to be the average of $\widetilde{\mathcal{H}}_n$ over l , i.e.

$$\mathcal{H}_n^* = \langle \widetilde{\mathcal{H}}_n \rangle_\sigma, \quad \sigma \equiv M, \quad \Omega$$

So that the average $\langle \cdot \rangle_\sigma$ of any general function $F(\sigma)$ is defined as;

$$\langle F(\sigma) \rangle_\sigma = \frac{1}{2\pi} \int_0^{2\pi} F(\sigma) d\sigma$$

The short periodic part will be;

$$W_n = \left(\frac{\partial \mathcal{H}_0}{\partial L} \right)^{-1} \int (W_n; \mathcal{H}_0) d\sigma$$

The details at order one

$$\widetilde{\mathcal{H}}_1 = \mathcal{H}_1$$

$$\mathcal{H}_1^* = \widetilde{\mathcal{H}}_1 + (\mathcal{H}_0; W_1)$$

Choosing $\mathcal{H}_1^* = \langle \widetilde{\mathcal{H}}_1 \rangle_\sigma$, then W_1 is therefore obtained by the quadrature

$$W_1 = \left(\frac{\partial \mathcal{H}_0}{\partial L} \right)^{-1} \int (W_1; \mathcal{H}_0) d\sigma$$

The averaging over the true anomaly is evaluated in the following section.

Short period transformation

Using the canonical Lie transformation procedure, one can perform a number of normalization so as to eliminate all the cyclic coordinates from the Hamiltonian. The first step is eliminating the short periodic terms keeping only the first order secular terms. The transformed Hamiltonian \mathcal{H}_n^* , $n = 0, 1$ plus the averaged quadrupole coupling term \mathcal{H}_{qc}^* reads

$$\mathcal{H}^* = \mathcal{H}_0^* + \mathcal{H}_1^* + \mathcal{H}_{qc}^* \quad (7)$$

with

$$\mathcal{H}_0^* = \mathcal{H}_0|_{L=L'} = -\frac{\mu^2}{2L^2}$$

$$\begin{aligned} \mathcal{H}_1^* = & \frac{1}{4} A_{1,2} \frac{1}{G^3} (3S^2-2) + \frac{3}{8} A_{2,3} (5S^3-4S) e \frac{1}{L^3 G^5} \sin G \\ & + \frac{3}{128} A_{2,4} \left\{ (175S^4-200S^2+40) \frac{1}{L^3 G^7} + (-105S^4+120S^2 \right. \\ & \left. -24) \frac{1}{L^5 G^5} \right\} + \frac{15}{64} A_{2,4} (7S^4-6S^2) \left(\frac{1}{L^5 G^5} - \frac{1}{L^3 G^7} \right) \cos 2G \\ & - \frac{A_{1,2,2}}{3} \frac{1}{G^3 L^3} [5(2-3S^2)+9S^2 \cos F_{0,0,2}] - \frac{\mu^2}{L^2} \left(\frac{\omega_s}{n} \right) \sqrt{1-e^2} C \\ & - \frac{\mu^2}{8L^2} \left(\frac{\omega_s}{n} \right)^2 (2+3e^2) [(2-3S^2)+3(S^2 \cos F_{0,0,2})] \\ & - \frac{\mu^2}{16L^2} \left(\frac{\omega_s}{n} \right)^2 \{15e^2 [2S^2 \cos F_{0,2,0}+(1-C)^2 \cos F_{0,2,-2}] \\ & + (1+C)^2 \cos F_{0,2,2}\} \end{aligned}$$

$$\begin{aligned} \mathcal{H}_{qc}^* = & \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ (-35S^4+80S^2-40) \frac{1}{L^3 G^7} + (-36S^4+48S^2-16) \frac{1}{L^6 G^4} \right. \\ & \left. + (-5S^4-8S^2+8) \frac{1}{L^5 G^5} \right\} + \frac{3}{32} \frac{A_{1,2}^2}{\mu^2} (15S^4 \\ & -14S^2) \left(\frac{1}{L^5 G^5} - \frac{1}{L^3 G^7} \right) \cos 2G \end{aligned}$$

Using $S = (1-C^2)^{1/2} = \left(1-\frac{1}{2}C^2-\frac{1}{8}C^4+\dots\right)$, then \mathcal{H}_1^* and \mathcal{H}_{qc}^* can be rewritten as

$$\begin{aligned} \mathcal{H}_1^* = & \frac{1}{4} A_{1,2}(1-3C^2) \frac{1}{G^3} + \frac{3}{8} A_{2,3} \left\{ 11e \left(-\frac{1}{2} C^4 + 1 \right) \frac{1}{L^3 G^6} \right. \\ & + \left(-\frac{19}{8} C^4 + \frac{1}{2} C^2 + 4 \right) \left[\frac{5e}{L^3 G^6} + \frac{1}{L^5 G^4 e} \right] \left. \right\} \sin F_{0,1,0} \\ & + \frac{3}{128} A_{2,4} \left\{ (175C^4 - 150C^2 + 15) \frac{1}{L^3 G^7} - (105C^4 - 90C^2 + 9) \frac{1}{L^5 G^5} \right\} \\ & - \frac{15}{64} A_{2,4} \left\{ (1-8C^2 + 7C^4) \left[\frac{1}{L^5 G^5} - \frac{1}{L^3 G^7} \right] \right\} \cos F_{0,2,0} \\ & - \frac{A_{1,2,2}}{3L^2} \frac{1}{G^3 L} [5(3C^2 - 1) + 9(1-C^2) \cos F_{0,0,2}] - \frac{\mu^2}{L^2} \left(\frac{\omega_s}{n} \right) \sqrt{1-e^2} C \\ & - \frac{\mu^2}{8L^2} \left(\frac{\omega_s}{n} \right)^2 (2 + 3e^2) [(3C^2 - 1) + 3(1-C^2) \cos F_{0,0,2}] \\ & - \frac{\mu^2}{16L^2} \left(\frac{\omega_s}{n} \right)^2 \{ 15e^2 [2S^2 \cos F_{0,2,0} + (1-C^2) \cos F_{0,2,-2}] \\ & + (1 + C)^2 \cos F_{0,2,2} \} \end{aligned} \quad (8)$$

$$\begin{aligned} \mathcal{H}_{qc}^* = & \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ (-35C^4 - 5C^2 + 5) \frac{1}{L^3 G^7} - (36C^4 - 24C^2 + 4) \frac{1}{L^4 G^6} \right. \\ & - (5C^4 - 18C^2 + 5) \frac{1}{L^5 G^5} \left. \right\} + \frac{3}{32} \frac{A_{1,2}^2}{\mu^2 G} (1-16C^2) \\ & + 15C^4 \left[\frac{1}{L^5 G^5} - \frac{1}{L^3 G^7} \right] \cos F_{0,2,0} \end{aligned} \quad (9)$$

In the subsequent Sections “Elimination of node”, “The apsidal frozen line”, and “Solution for the inclination”, we shall use Hamilton canonical equations using the transformed Hamiltonian (8) and (9) to compute some special families of frozen orbits around the triaxial Moon after normalizing the right ascension of the ascending node.

Elimination of node

Elimination $h = \Omega$ from the components \mathcal{H}_1^* and \mathcal{H}_{qc}^* yields

$$\begin{aligned} \mathcal{H}_1^{**} = & \frac{1}{4} A_{1,2}(1-3C^2) \frac{1}{L^3 G^3} + \frac{3}{8} A_{2,3} \left\{ 11e \left(-\frac{1}{2} C^4 + 1 \right) \frac{1}{L^3 G^6} \right. \\ & + \left(-\frac{19}{8} C^4 + \frac{1}{2} C^2 + 4 \right) \left[\frac{5e}{L^3 G^6} + \frac{1}{L^5 G^4 e} \right] \left. \right\} \sin g \\ & + \frac{3}{128} A_{2,4} \left\{ (175C^4 - 150C^2 + 15) \frac{1}{L^3 G^7} - (105C^4 - 90C^2 + 9) \frac{1}{L^5 G^5} \right\} \\ & - \frac{15}{64} A_{2,4} (1-8C^2 + 7C^4) \left[\frac{1}{L^5 G^5} - \frac{1}{L^3 G^7} \right] \cos 2g \\ & - \frac{5A_{1,2,2}}{3} \frac{1}{G^3 L^3} (3C^2 - 1) - \frac{\mu^2}{L^2} \left(\frac{\omega_s}{n} \right) \frac{G}{L} C - \frac{\mu^2}{8L^2} \left(\frac{\omega_s}{n} \right)^2 [(2 + 3e^2)(3C^2 - 1) \\ & + 15e^2(1-C^2) \cos 2g] \end{aligned} \quad (9.1)$$

$$\begin{aligned} \mathcal{H}_{qc}^{**} = & \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ (-35C^4 - 5C^2 + 5) \frac{1}{L^3 G^7} - (36C^4 - 24C^2 + 4) \frac{1}{L^4 G^6} \right. \\ & - (5C^4 - 18C^2 + 5) \frac{1}{L^5 G^5} \left. \right\} + \frac{3}{32} \frac{A_{1,2}^2}{\mu^2 G} (1-16C^2) \\ & + 15C^4 \left[\frac{1}{L^5 G^5} - \frac{1}{L^3 G^7} \right] \cos 2g \end{aligned} \quad (9.2)$$

The apsidal frozen line

The periapsis argument becomes frozen if $\frac{\partial \mathcal{H}^{**}}{\partial G} = 0$

$$\begin{aligned} \frac{\partial \mathcal{H}^{**}}{\partial G} = & \frac{3}{4} A_{1,2}(5C^2 - 1) \frac{1}{G^4} + \frac{3}{8} A_{2,3} \left\{ \left(\frac{436}{4} C^4 - 308C + 30 \right) \frac{e}{L^3 G^7} \right. \\ & + \left(\frac{55}{8} C^4 - 374C^2 + 44 \right) \frac{1}{e L^5 G^5} \left. \right\} \sin g \\ & + \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ (245C^4 + 45C^2 - 35) \frac{1}{L^3 G^8} + (260C^4 - 192C^2) \frac{1}{L^4 G^7} \right. \\ & + (45C^4 - 126C^2 + 25) \frac{1}{L^5 G^6} \left. \right\} \\ & + \frac{3}{128} A_{2,4} \left\{ (525C^4 - 750C^2 + 15) \frac{1}{L^3 G^8} - (125C^4 - 270C^2 \right. \\ & \left. + 9) \frac{1}{L^5 G^6} \right\} + \frac{15}{64} A_{2,4} \left\{ [(315C^4 - 376C^2 + 49) \frac{1}{L^3 G^8} \right. \\ & - (7C^4 - 26C^2 + 5) \frac{1}{L^5 G^6}] + \frac{3}{32} \frac{A_{1,2}^2}{\mu^2} \left\{ [165C^4 - 144C^2 + 7] \frac{1}{L^3 G^8} \right. \\ & + (112C^2 - 135C^4 - 5) \frac{1}{L^5 G^6} \left. \right\} \cos 2g + \frac{5A_{1,2,2}}{G^4 L^3} (5C^2 - 1) \\ & + \frac{3\mu^2}{4L^2} \left(\frac{\omega_s}{n} \right)^2 \left[\frac{C^2}{G} (2 + 3e^2) + \frac{2eG}{L^2} (3C^2 - 1) \right. \\ & \left. + 30e \left(\frac{e}{G} C^2 - \frac{2G}{L^2} (1-C^2) \right) \cos 2g \right] = 0 \end{aligned} \quad (10)$$

Solution for the inclination

Eq. (10) can be solved for the inclination as follows; It can be written as

$$\mathcal{A}_2 C^4 + \mathcal{A}_1 C^2 + \mathcal{A}_0 = 0 \quad (11)$$

Eq. (11) admits the critical inclination ($C = \cos I$) as follows

$$I_{1,2,3,4} = \cos^{-1} \left(\pm \sqrt{\frac{-\mathcal{A}_1 \pm \sqrt{\mathcal{A}_1^2 - 4\mathcal{A}_2 \mathcal{A}_0}}{2\mathcal{A}_2}} \right) \quad (12)$$

where

$$\begin{aligned} \mathcal{A}_2 = & \frac{3}{8} A_{2,3} \left\{ \frac{436e}{4L^3 G^7} - \frac{22}{e L^5 G^5} \right\} \sin g + \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ \frac{245}{L^3 G^8} + \frac{260}{L^4 G^7} + \frac{45}{L^5 G^6} \right\} \\ & + \frac{3}{128} A_{2,4} \left\{ \frac{525}{L^3 G^8} - \frac{125}{L^5 G^6} \right\} - \frac{15}{64} A_{2,4} \left\{ \left[\frac{7}{L^5 G^6} - \frac{315}{L^3 G^8} \right] \right. \\ & \left. + \frac{3}{32} \frac{A_{1,2}^2}{\mu^2} \left\{ \frac{165}{L^3 G^8} + \frac{112}{L^5 G^6} \right\} \right\} \cos 2g \end{aligned}$$

$$\begin{aligned} \mathcal{A}_1 = & \frac{15}{4} A_{1,2} \frac{1}{L^3 G^4} + \frac{3}{8} A_{2,3} \left\{ \frac{132e}{L^3 G^7} - \frac{44}{e L^5 G^5} \right\} \sin g \\ & + \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ \frac{45}{L^3 G^8} - \frac{192}{L^4 G^7} - \frac{126}{L^5 G^6} \right\} + \frac{3}{128} A_{2,4} \left\{ \frac{750}{L^3 G^8} - \frac{270}{L^5 G^6} \right\} \\ & - \frac{15}{64} A_{2,4} \left\{ \left[\frac{376}{L^3 G^8} - \frac{26}{L^5 G^6} \right] - \frac{3}{32} \frac{A_{1,2}^2}{\mu^2} \left\{ \frac{144}{L^3 G^8} + \frac{135}{L^5 G^6} \right\} \right\} \cos 2g \\ & + \frac{25A_{1,2,2}}{G^4 L^3} + \frac{3\mu^2}{4L^2} \left(\frac{\omega_s}{n} \right)^2 \left[\frac{1}{G} (2 + 3e^2) + 6e \frac{G}{L^2} \right. \\ & \left. + 30e \left(\frac{e}{G} + \frac{2G}{L^2} \right) \cos 2g \right] \end{aligned}$$

$$\begin{aligned} \mathcal{A}_0 = & -\frac{3}{4}A_{1,2}\frac{1}{L^3G^4} + \frac{3}{8}A_{2,3}\left\{\frac{30e}{L^3G^7} + \frac{4}{eL^5G^5}\right\}\sin g \\ & + \frac{3}{64}\frac{A_{1,2}^2}{\mu^2}\left\{-\frac{35}{L^3G^8} + \frac{25}{L^5G^6}\right\} + \frac{3}{128}A_{2,4}\left\{\frac{15}{L^3G^8} - \frac{9}{L^5G^6}\right\} \\ & + \frac{15}{64}A_{2,4}\left\{\left[\frac{49}{L^3G^8} - \frac{5}{L^5G^6}\right] + \frac{3}{32}\frac{A_{1,2}^2}{\mu^2}\left\{\frac{7}{L^3G^8} - \frac{5}{L^5G^6}\right\}\right\}\cos 2g - \frac{5A_{1,2,2}}{G^4L^3} \\ & - \frac{3\mu^2eG}{2L^4}\left(\frac{\omega_s}{n}\right)^2[1 + 30\cos 2g] \end{aligned}$$

When ignoring second order zonal harmonics we get

$$\frac{\partial \mathcal{H}^*}{\partial G} = \frac{15A_{1,2}}{4L^3G^4}C^2 - \frac{3A_{1,2}}{4L^3G^4} = 0$$

the critical inclination arise from this equation are

$$C_{1,2} = \pm\sqrt{1/5} \Rightarrow I_{1,2} = \cos^{-1}(\pm\sqrt{1/5}) \Rightarrow I_{1,2} = 63.435^\circ, 116.57^\circ \quad (13)$$

Nonlinear partial differential equations expound the fundamental structure in nature and science such as plasma containment in stellarators for energy generation and tokamaks, chaotic behavior in biological systems, population ecology, neural networks and solitonic fibre optical communication devices [34–60].

Graphical representation of Eq. (12)

In what follows, we plotted the critical I versus ω , a , and e respectively. We will plot three different sets of figures.

In the following set of figures we will plot the critical I versus ω , we are taking into account the variation in $a \in [2000, 6000]$ km with stepsize 2000 km and eccentricity as $e \in [0.1, 0.3]$ with stepsize 0.1 so we have three bundles of curves.

The curves keys are as follows: Red curve $e = 0.1$, blue curve $e = 0.2$, green curve $e = 0.3$. Solid, dashed, dotted curves for $a = 2000$ km, $a = 4000$ km, $a = 6000$ km respectively.

Analysis of Figs. 1–6

There exists a family of critical roots of inclination very close the polar orbits, namely $I_c \in (89.6^\circ, 90.4^\circ)$, see the first three curve near to $I_c = 90^\circ$ in Fig. 2. The other two bundles on the Fig. 2 corresponds to different hights of the satellite as well as different eccentricities. There exists another two families of critical roots of inclination near to the very well known critical inclination in the theory of artificial satellite and its complementary respectively, namely $I_c \in (62^\circ, 64^\circ)$ and $I_c \in (115^\circ, 116^\circ)$. See Fig. 1. It is very clear that the size of perturbations in I_c in the first family given in 1 is much bigger then the other two

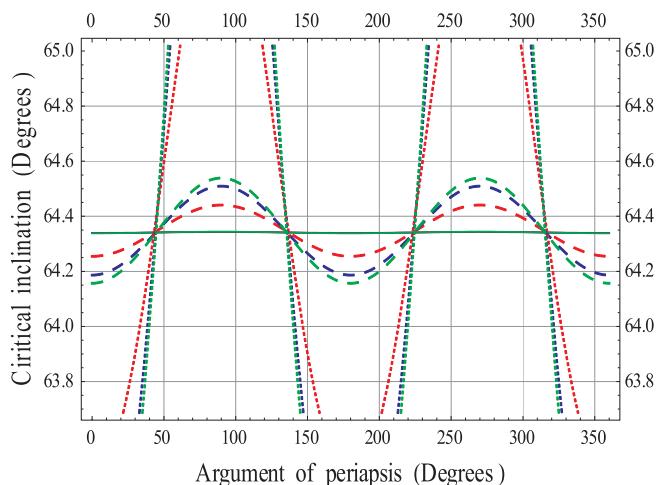


Fig. 1. The first root of the critical I versus ω .

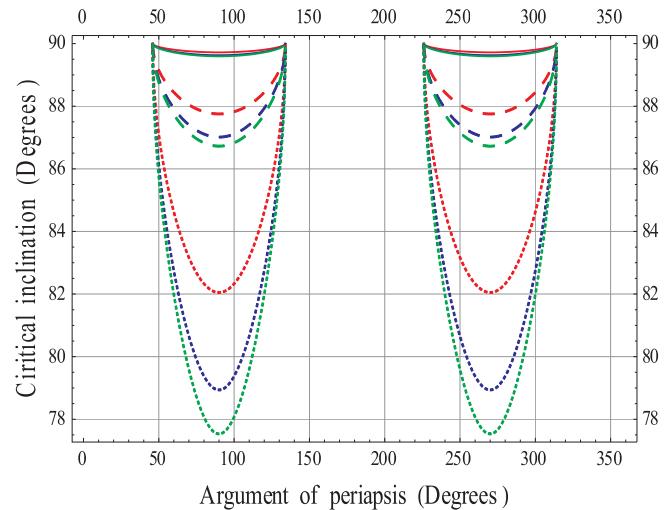


Fig. 2. The second root of the critical I versus ω .

families given by 2. This is approximately 100 times bigger. The variation in the critical inclination due to the change in the root of the critical a and e for the first and third roots can be represented by a harmonic function. While for the second and the fourth roots the variation in I_c can be represented by some squared harmonic function except there is forbidden values for I_c that corresponds to some values of the argument of periapsis $g \in ([0^\circ, 45.7^\circ] \cap [134.3^\circ, 225.7^\circ])$. There is no critical roots available for the first and the third roots for the whole range of the argument of the periapsis in the following intervals $I_c \in (0^\circ, 64.337^\circ) \cap (64.345^\circ, 115.655^\circ) \cap (115.662^\circ, 180^\circ)$. There is no perturbation due to a and e for the polar frozen orbits, i.e. at the $I_c = 90^\circ$, as well as at $I_c \in (64.34^\circ, 115.7^\circ)$. Apart from these values of inclination the perturbations become visible. Fig. 5 is an assembly of Fig. 1 and Fig. 3 while Fig. 6 is an assembly of Figs. 2 and 4.

We can also construct a table from the Figs. 1 to 6 as follows.

In the following set of figures we will plot the critical I versus a , we are taking into account the variation of the argument of periapsis the $g \in [0.0^\circ, 90.0^\circ]$ with stepsize $g = 45.0^\circ$ and eccentricity as $e \in [0.1, 0.3]$ with stepsize 0.1 so we have three bundles of curves. The curves key are as follows: Red, Blue, Green curves for $e = 0.1$, $e = 0.2$, $e = 0.3$ respectively. Solid, dashed, dotted curves for $g = 0.0^\circ$, $g = 45^\circ$, $g = 90^\circ$ respectively.

Analysis of Figs. 7–12

We have two families of critical inclinations $I_c \in (63.8^\circ, 64.9^\circ)$ and its complementary $I_c \in (115.1^\circ, 116.2^\circ)$. See Figs. 7 and 9. At the centers of the above two sets, namely at $I_c = 64.38^\circ$, $g = 45^\circ$ and at $I_c = 115.62^\circ$,

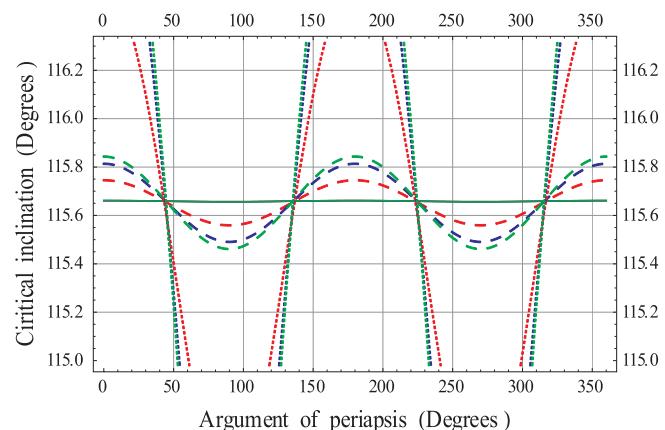


Fig. 3. The third root of the critical I versus ω .

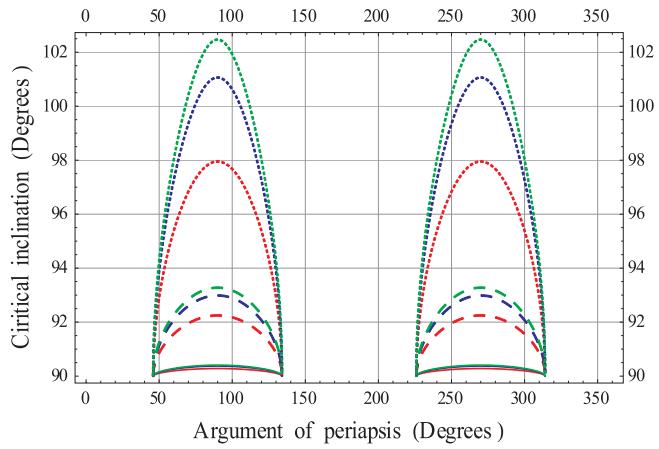
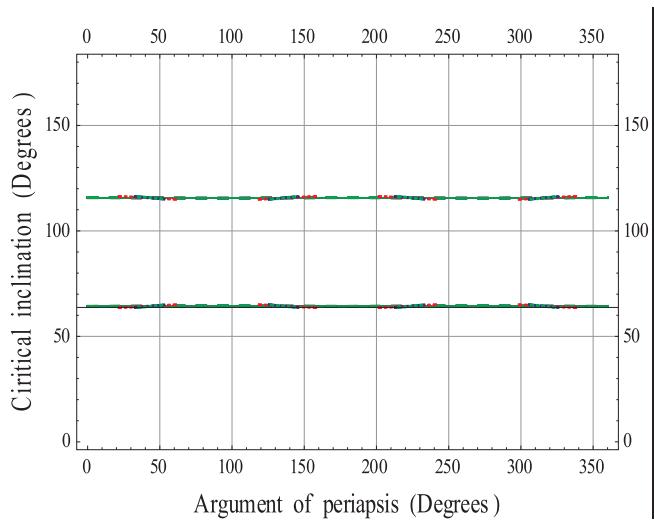
Fig. 4. The fourth root of the critical I versus ω .

Fig. 5. Assembly of Figs. 1 and 3.

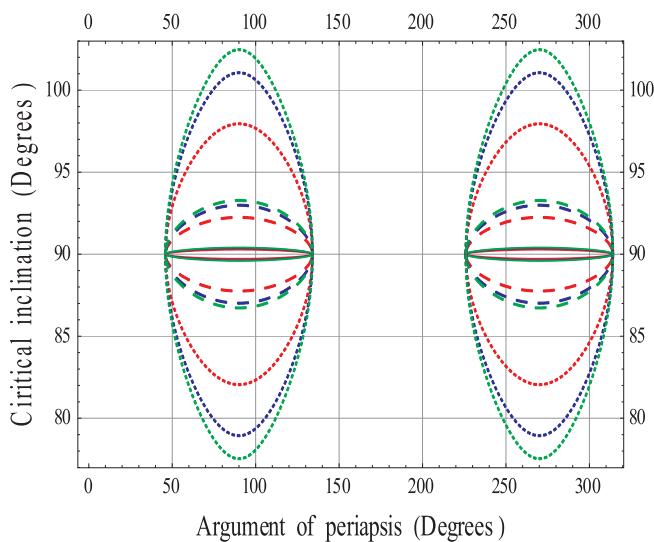
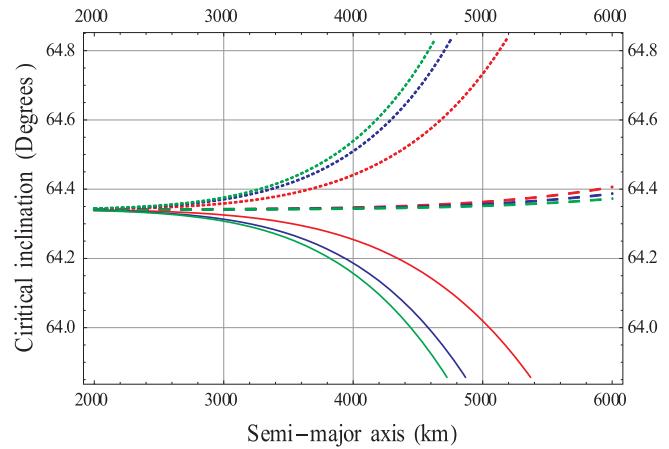
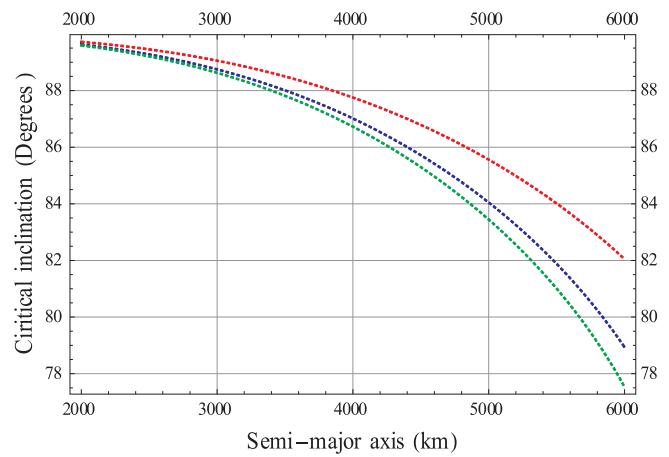
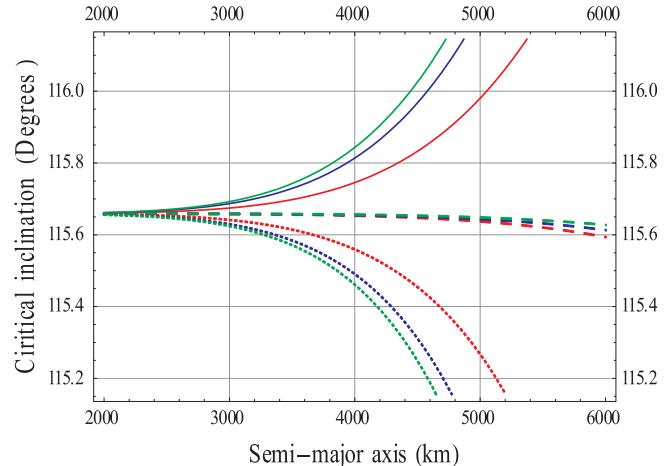


Fig. 6. Assembly of Figs. 2 and 4.

respectively, the perturbations are very small due to the variations in $a \in [2000 \text{ km}, 5000 \text{ km}]$ and $e \in [0.1, 0.3]$. For $I_c > 64.38^\circ$, $g = 90^\circ$, the increasing in the eccentricity yields increasing in critical inclination. While for $I_c < 64.38^\circ$, $g = 0^\circ$ the increasing in the eccentricity yields

Fig. 7. The first root of the critical I versus a .Fig. 8. The second root of the critical I versus a .Fig. 9. The third root of the critical I versus a .

decreasing in critical inclination. The perturbation in I_c becomes significant for the high lunar orbits. See Figs. 7–10. The second and fourth roots for the whole range of semi-major axis between 2000, 6000 kms is disappeared completely for $g = 0^\circ, 45^\circ$ while it appears for $g = 90^\circ$. Fig. 11 is an assembly of Figs. 7 and 9 while Fig. 12 is an assembly of Figs. 8 and 10.

We can also construct a table from the Figs. 7 to 12 as follows.

In the following set of figures we will plot the critical inclination versus the eccentricity, we are taking into account the variation of the

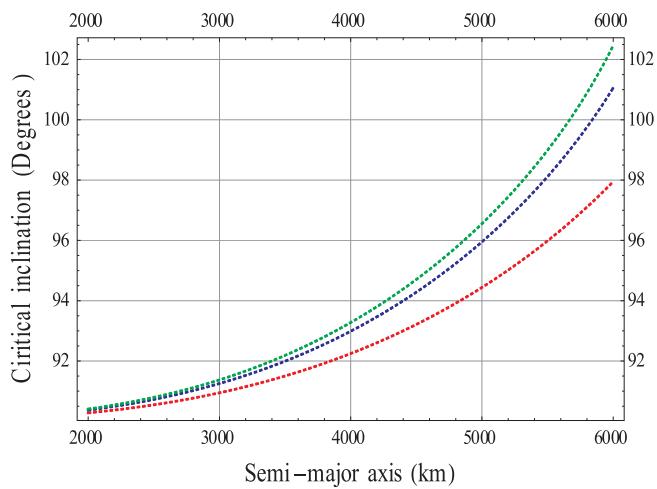
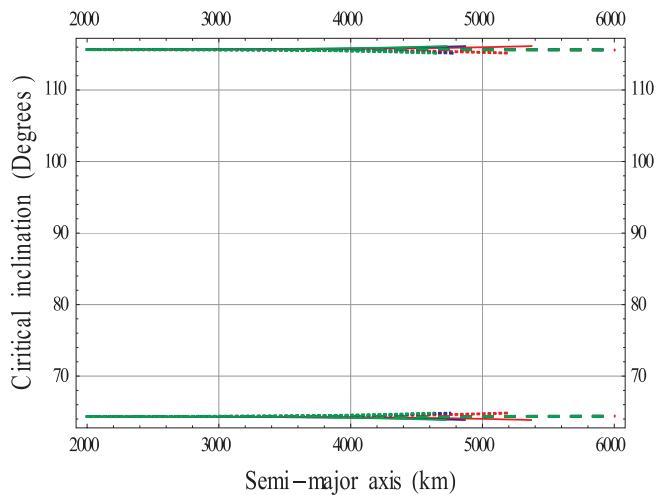
Fig. 10. The fourth root of the critical I versus a .

Fig. 11. Assembly of Figs. 7 and 9.

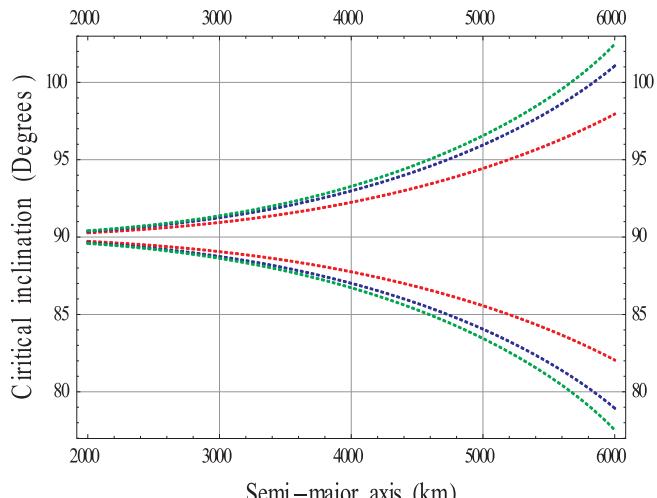
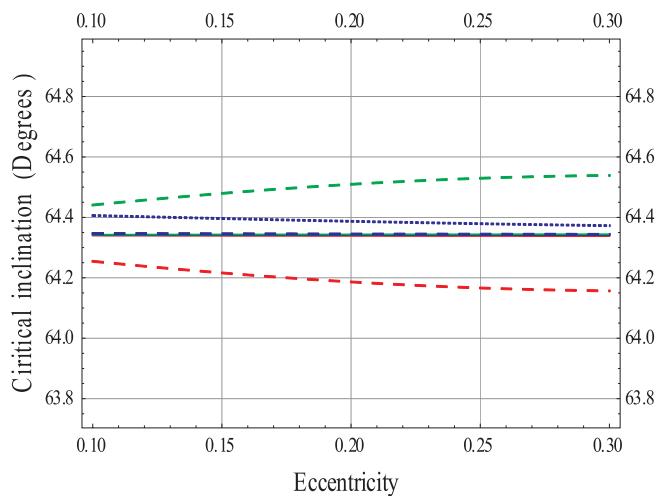


Fig. 12. Assembly of Figs. 8 and 10.

argument of periapsis $g \in [0.0^\circ, 90.0^\circ]$ with stepsize $g = 45.0^\circ$ and semi-major axis as $a \in [2000, 6000]$ with stepsize 2000 km, so we have three bundles of curves. The curves key are as follows: Red, blue, green curves for $g = 0.0^\circ$, $g = 45^\circ$, $g = 90^\circ$ respectively. Solid, dashed, dotted curves for $a = 2000$ km, $a = 4000$ km, $a = 6000$ km respectively. Finally

Fig. 13. The first root of the critical I versus e .

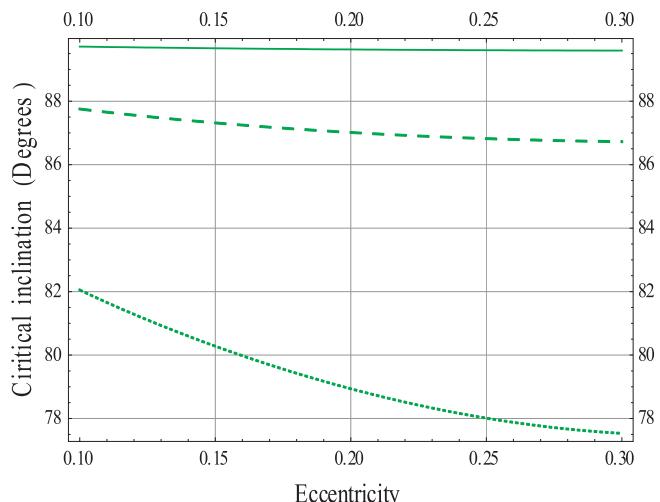
Φ is the empty set.

Analysis of Figs. 13–18

We have plotted Figs. 13–18 to visualize the effects on I_c due to selected initial conditions of argument of perigee $g = 0.0^\circ, 45^\circ, 90^\circ$, and semi-major axis $a = 2000$ km, 4000 km, 6000 km respectively and eccentricity $e \in [0.1, 0.3]$. The four roots yield four families of critical inclinations $I_c \in (64.15^\circ, 64.55^\circ)$, $I_c \in (77.5^\circ, 90^\circ)$ and their complementaries $I_c \in (115.45^\circ, 115.85^\circ)$, $I_c \in (90^\circ, 102.5^\circ)$. In the second and third families, we have critical inclinations only at $g = 90^\circ$. The perturbation in I_c becomes significant for orbits having $g = 90^\circ$. See Figs. 10 and 11. The remarkable feature is the absence of some curves that represent some values of g at $g = 0.0^\circ, g = 45^\circ$ versus the whole range of the semi-major axis, see Figs. 14 and 16 due to the appearance of imaginary values.

We also can also construct a table from the Figs. 13 to 18.

In the following solve Eq. (10) for the argument of pericentre. To do this Eq. (10) can be re-written as;

Fig. 14. The second root of the critical I versus e .

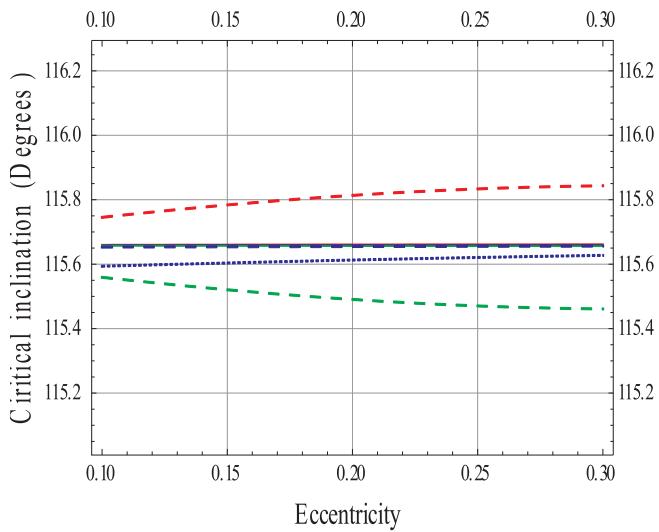
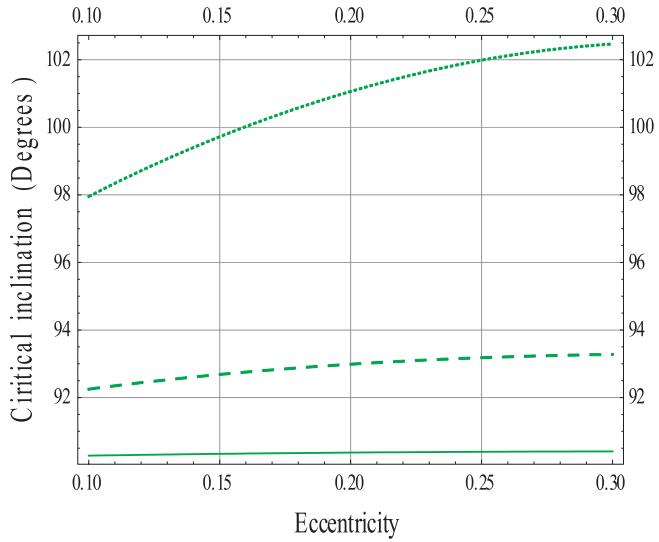
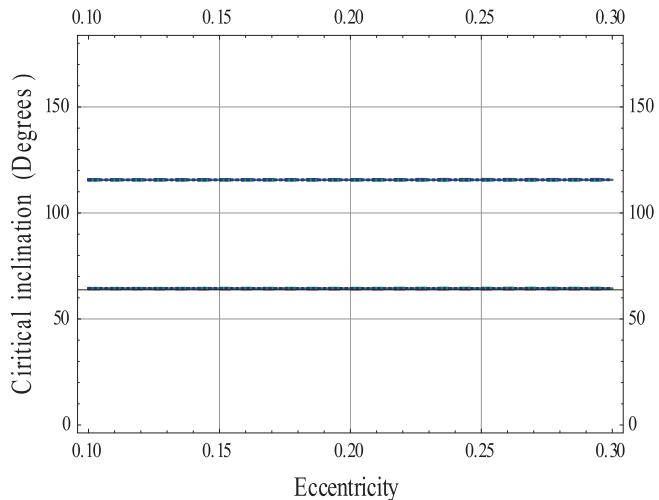
Fig. 15. The third root of the critical I versus e .Fig. 16. The fourth root of the critical I versus e .

Fig. 17. Assembly of Figs. 13 and 15.

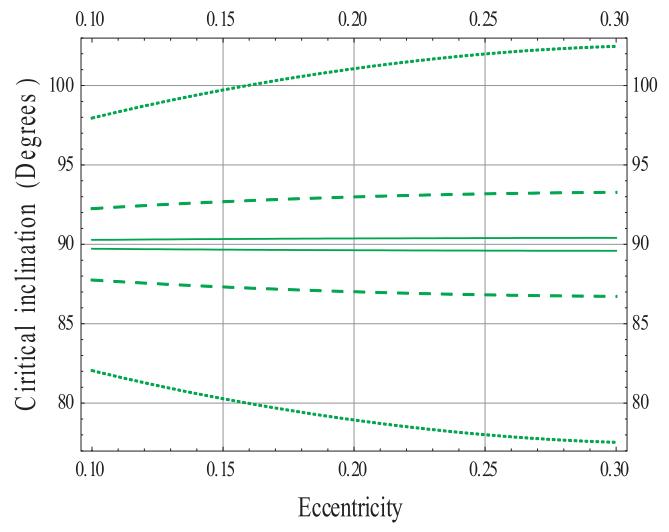


Fig. 18. Assembly of Figs. 14 and 16.

$$\begin{aligned} \frac{\partial \mathcal{H}^{**}}{\partial G} = & -\frac{6}{32} \frac{A_{1,2}^2}{\mu^2} \left\{ [165C^4 - 144C^2 + 7] \frac{1}{L^3 G^8} + (112C^2 - 135C^4 \right. \\ & \left. - 5) \frac{1}{L^5 G^6} \right\} \sin^2 g + \frac{3}{8} A_{2,3} \left\{ \left(\frac{436}{4} C^4 - 308C + 30 \right) \frac{e}{L^3 G^7} \right. \\ & + \left(\frac{55}{8} C^4 - 374C^2 + 44 \right) \frac{1}{e L^5 G^5} \left. \right\} \sin g + \frac{3}{4} A_{1,2} (5C^2 - 1) \frac{1}{L^3 G^4} \\ & + \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ (245C^4 + 45C^2 - 35) \frac{1}{L^3 G^8} + (260C^4 - 192C^2) \frac{1}{L^4 G^7} \right. \\ & + (45C^4 - 126C^2 + 25) \frac{1}{L^5 G^6} \left. \right\} \\ & + \frac{3}{128} A_{2,4} \left\{ (525C^4 - 750C^2 + 15) \frac{1}{L^3 G^8} - (125C^4 - 270C^2 \right. \\ & + 9) \frac{1}{L^5 G^6} \left. \right\} + \frac{15}{64} A_{2,4} \left\{ (315C^4 - 376C^2 + 49) \frac{1}{L^3 G^8} \right. \\ & - (7C^4 - 26C^2 + 5) \frac{1}{L^5 G^6} \left. \right\} + \frac{3}{32} \frac{A_{1,2}^2}{\mu^2} \left\{ [165C^4 - 144C^2 + 7] \frac{1}{L^3 G^8} \right. \\ & + (112C^2 - 135C^4 - 5) \frac{1}{L^5 G^6} \left. \right\} + \frac{5A_{1,2,2}}{G^4 L^3} (5C^2 - 1) \\ & + \frac{3\mu^2}{4L^2} \left(\frac{\omega_s}{n} \right)^2 \left[\frac{2C^2}{G} (9e^2 + 1) + \frac{4eG}{L^2} (9C^2 - 8) \right. \\ & \left. - 15e \left(\frac{e}{G} C^2 - \frac{2G}{L^2} (1 - C^2) \right) \sin^2 g \right] \end{aligned} \quad (14)$$

which can be reformulated as

$$\mathcal{P}_2 \sin^2 g + \mathcal{P}_1 \sin g + \mathcal{P}_0 = 0 \quad (15)$$

which has been solved for g as

$$g_{1,2} = \sin^{-1} \left(\frac{-\mathcal{P}_1 \pm \sqrt{\mathcal{P}_1^2 - 4\mathcal{P}_2\mathcal{P}_0}}{2\mathcal{P}_2} \right) \quad (16)$$

where the coefficients are

$$\mathcal{P}_2 = -\frac{6}{32} \frac{A_{1,2}^2}{\mu^2} \left\{ [165C^4 - 144C^2 + 7] \frac{1}{L^3 G^8} + (112C^2 - 135C^4 - 5) \frac{1}{L^5 G^6} \right\}$$

$$\frac{3\mu^2}{4L^2} \left(\frac{\omega_s}{n} \right)^2 \left[-15e \left(\frac{e}{G} C^2 - \frac{2G}{L^2} (1 - C^2) \right) \right]$$

$$\mathcal{P}_1 = \frac{3}{8} A_{2,3} \left\{ \left(\frac{436}{4} C^4 - 308C + 30 \right) \frac{e}{L^3 G^7} + \left(\frac{55}{8} C^4 - 374C^2 + 44 \right) \frac{1}{e L^5 G^5} \right\}$$

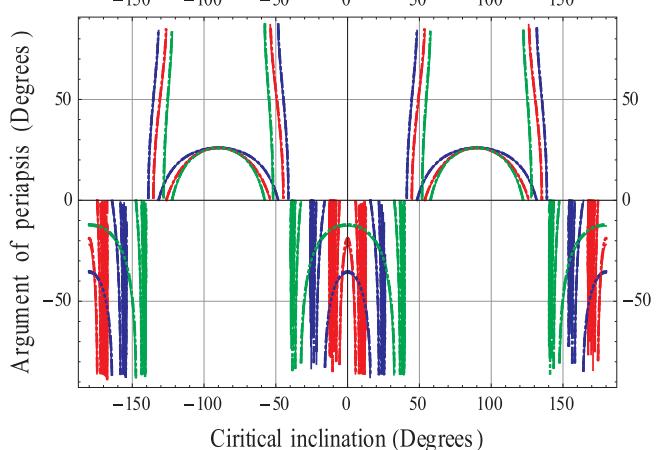
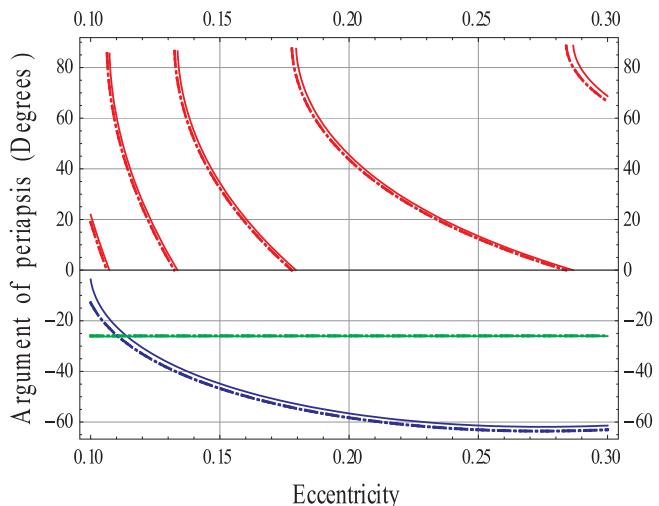
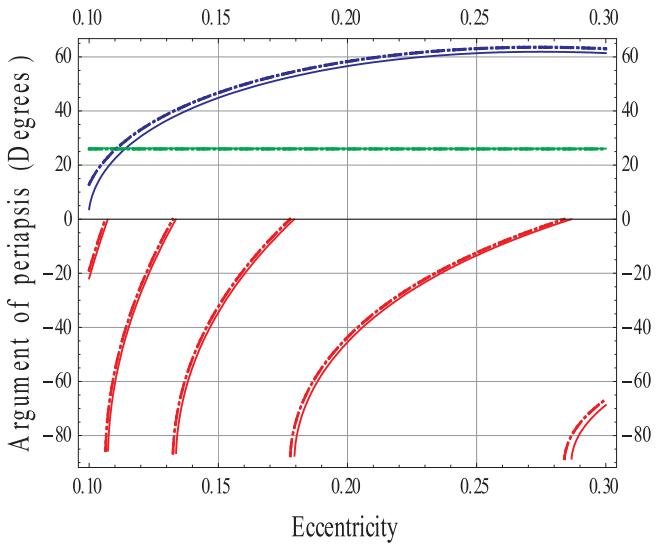
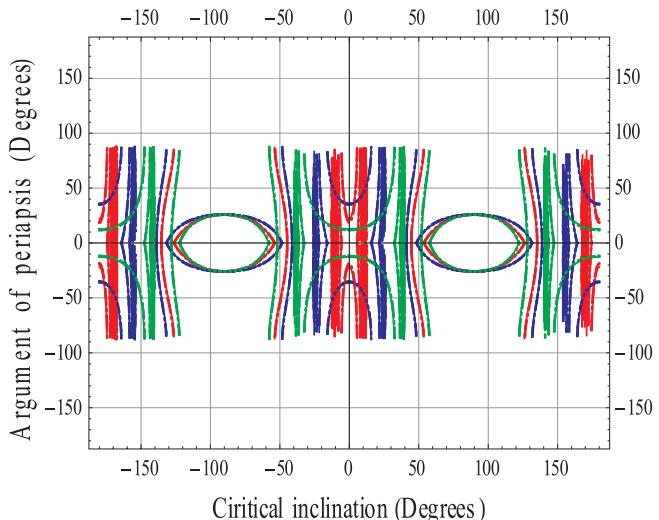
Fig. 19. The first root of ω versus I .Fig. 22. The second root of ω versus I .Fig. 20. The first root of ω versus I .

Fig. 23. Assembly of Figs. 19 and 21.

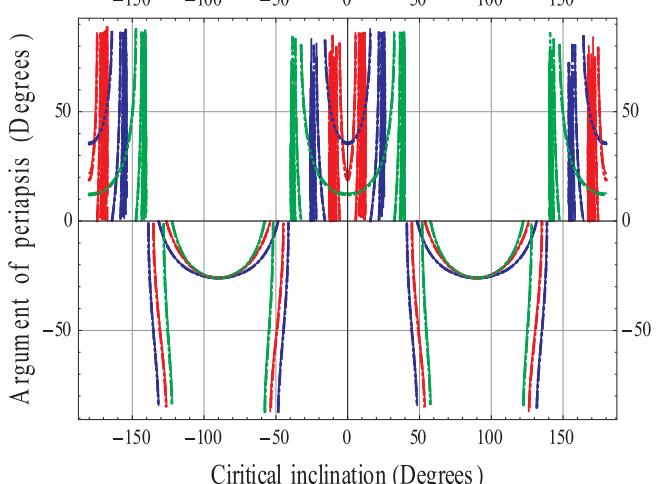
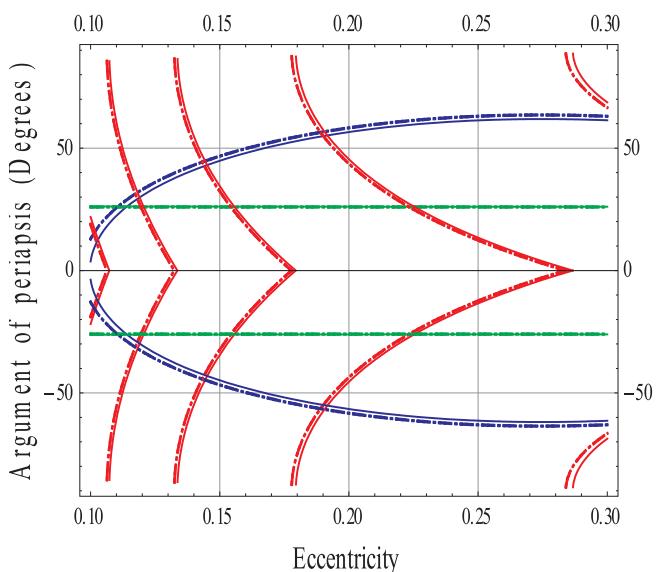
Fig. 21. The second root of ω versus I .

Fig. 24. Assembly of Figs. 20 and 22.

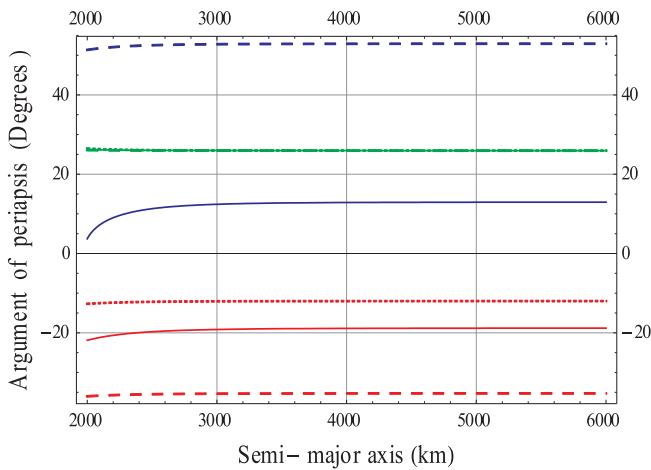
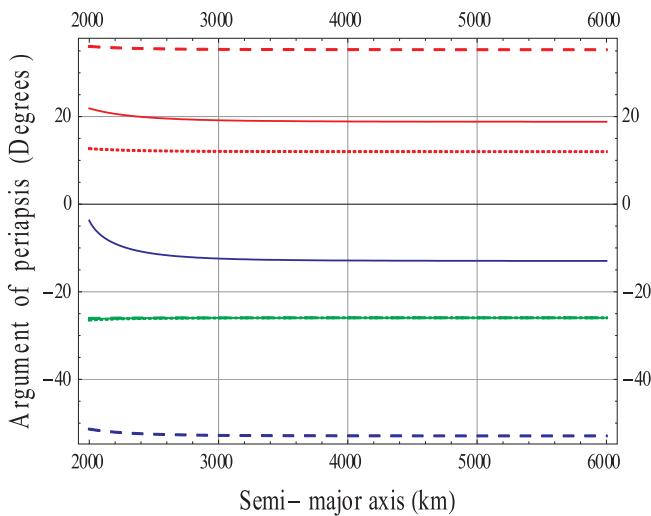
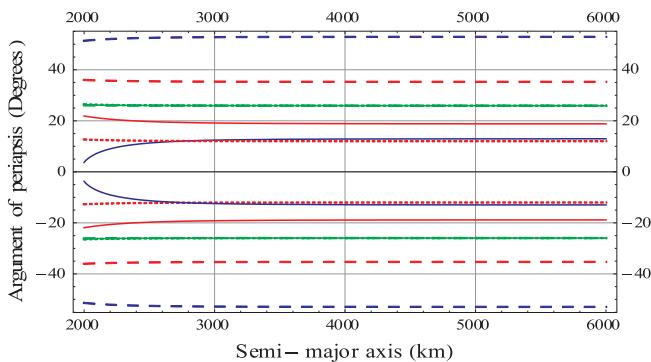
Fig. 25. The first root of ω versus a .Fig. 26. The second root of ω versus a .

Fig. 27. Assembly of Figs. 25 and 26.

$$\begin{aligned} \mathcal{P}_0 = & \frac{3}{4} A_{1,2}(5C^2-1) \frac{1}{L^3 G^4} + \frac{3}{64} \frac{A_{1,2}^2}{\mu^2} \left\{ (245C^4 + 45C^2 - 35) \frac{1}{L^3 G^8} \right. \\ & + (260C^4 - 192C^2) \frac{1}{L^4 G^7} + (45C^4 - 126C^2 + 25) \frac{1}{L^5 G^6} \Big\} \\ & + \frac{3}{128} A_{2,4} \left\{ (525C^4 - 750C^2 + 15) \frac{1}{L^3 G^8} - (125C^4 + 270C^2 - 9) \frac{1}{L^5 G^6} \right\} \\ & + \frac{15}{64} A_{2,4} \left\{ (315C^4 - 376C^2 + 49) \frac{1}{L^3 G^8} - (7C^4 - 26C^2 + 5) \frac{1}{L^5 G^6} \right\} \\ & + \frac{3}{32} \frac{A_{1,2}^2}{\mu^2} \left\{ [165C^4 - 144C^2 + 7] \frac{1}{L^3 G^8} + (112C^2 - 135C^4 - 5) \frac{1}{L^5 G^6} \right\} \\ & + \frac{5A_{1,2,2}}{G^4 L^3} (5C^2 - 1) + \frac{3\mu^2}{4L^2} \left(\frac{\omega_s}{n} \right)^2 \left[\frac{2C^2}{G} (9e^2 + 1) + \frac{4eG}{L^2} (9C^2 - 8) \right] \end{aligned}$$

To visualize solution (16), we plot in the following Subsection “Graphical representation of Eq. (16)”.

Graphical representation of Eq. (16)

On the Figs. 19–27, we plotted ω against the $I_c \in (0^\circ, 180^\circ)$, the red, blue and green curves represent respectively increasing in the concerned independent variables. The figures reveal that the solution splits the regions into four parts for the first root and for the second root for the argument of periapsis. This actually set out restrictions on choosing the inclination satisfying the argument of periapsis frozen orbits. We have only two roots, since Eq. (16) is quadratic.

Analysis of Figs. 19–27

Figs. 19, 21, 23 represent the graphs of the inverse function represented on Figs. 1–6. Figs. 20, 22, 24, 25, 26, 27 reveal that we still have frozen orbits for the chosen domains of the eccentricity and semi-major axis.

Conclusion

Analytical theories and their graphical representations help a lot in designing some specific missions. From this prospective, we presented a doubly averaged problem of a satellite moves in lunar orbits using Delaunay canonical-variables. The Moon is considered as an oblate as well as triaxial body. We constructed the dynamical equation for the frozen argument of periapsis. We solved the obtained equation for I_c . We plotted and analysed the solutions under changing a , e , and ω . We have obtained new families of critical roots of inclination, one of them is very close the polar orbits and the other is near to the usual I_c . The perturbation in the critical inclination becomes significant for the high lunar orbits.

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